Tabba Tabba Lithium Mine Project

Groundwater Modelling Technical Report

Wildcat Resources

Suite 3 Ground Floor
16 Ord Street
West Perth, WA

Prepared by:

SLR Consulting Australia Pty Ltd

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Making Sustainability Happen

Revision Record

Revision	Date	Prepared By	Checked By	Authorised By
02	02 June 2026	Louis Bouchet	S Weeks	S Weeks
01	19 May 2026	Banafsheh Sheikhipoor & Louis Bouchet	S Weeks	I Epari

Basis of Report

This report has been prepared by SLR Consulting Australia Pty Ltd (SLR) with all reasonable skill, care and diligence, and taking account of the timescale and resources allocated to it by agreement with Wildcat Resources (the Client). Information reported herein is based on the interpretation of data collected, which has been accepted in good faith as being accurate and valid. SLR may have used AI in the preparation of this document.

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Executive Summary

This report presents a regional groundwater modelling assessment for the proposed Tabba Tabba Project, located southeast of Port Hedland, to support the environmental approval submissions and evaluate potential hydrogeological impacts associated with mining.

The model was developed using MODFLOW-USG based on a conceptual understanding of a fractured rock aquifer system influenced by structural features such as the Tabba Tabba shear zone and dolerite dyke, with recharge primarily driven by episodic rainfall and discharge dominated by evapotranspiration.

Model calibration was undertaken using an automated ensemble-based approach (PESTPP-IES) against groundwater level data from 17 monitoring bores, resulting in a good overall fit to observed conditions, with a root mean square error of approximately 2.8 m and a scaled RMS of 15.6%. The model reproduces regional groundwater trends and seasonal variability reasonably well, particularly within the main aquifer (upper fractured rock), although some local discrepancies remain due to data limitations and system complexity.

Predictions suggest that mining and associated dewatering will result in significant but localised drawdown, with maximum impacts extending along key geological structures, and total groundwater extraction peaking at approximately 6 GL/year.

Post-mining, pit lakes are predicted to form and act as long-term groundwater sinks, remaining below regional water levels due to high evaporation rates.

Uncertainty and sensitivity analyses highlight that while the model is robust at a regional scale, key predictions—particularly drawdown and inflows—are influenced by poorly constrained parameters in deeper fractured zones. Overall, the model provides a suitable tool for impact assessment and decision-making, although results should be interpreted within the context of data limitations and inherent predictive uncertainty.

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Appendix A Parameters Distributions

Appendix B Drawdown Maps

1.0 Introduction

1.1 Project Background

The Tabba Tabba Project (the Project) is located about 57 km south-east of Port Hedland, within the Wallareenya pastoral lease which is primarily used for cattle grazing. Wildcat (Tabba) Pty Ltd (Wildcat, the Proponent) proposes to develop the Project to mine spodumene, tantalum and petalite.

Wildcat plan to mine the resource via three open pits and an underground mine over a 14-year period. It is anticipated that the project will require approximately 6 GL of water per year.

Key mining infrastructures relevant to groundwater includes (**Figure 1-1**):

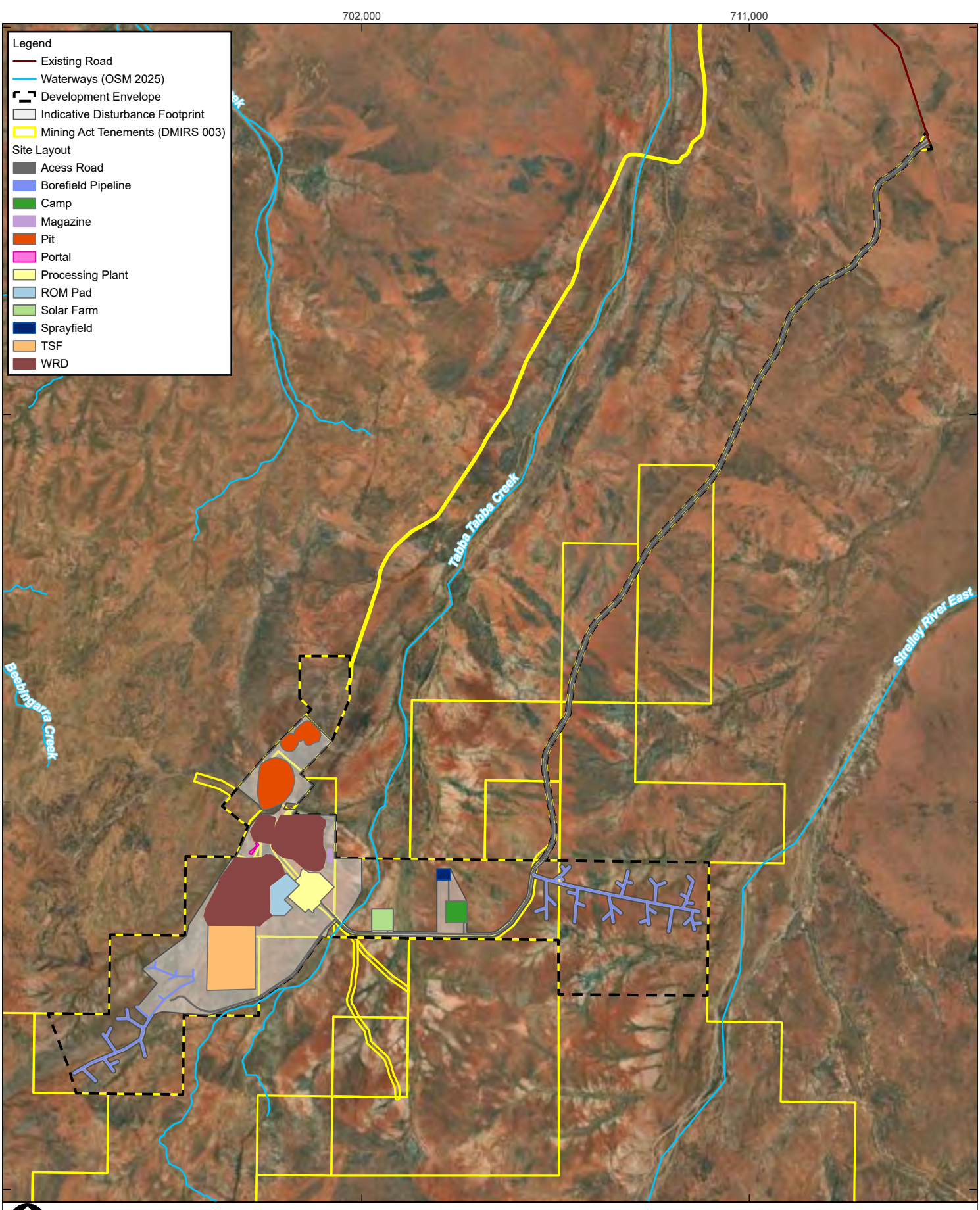
- One large open pit (Main pit)
- Two smaller open pits (Hann and Hutt pits)
- One underground mine connected to the Main pit
- Dewatering bores (location to be confirmed)
- A Tailing Storage Facility (TSF)
- Two Waste Rock Dumps (WRD).

1.2 Groundwater Modelling Objectives

The groundwater modelling presented in this report supports Wildcat environmental approval submissions for the Project development.

The aim of the modelling is to estimate potential impacts to groundwater related to the project as well groundwater abstraction volumes. The Quantity of Interest (QoI) to be simulated are:

- Mine induced drawdown;
- Mine inflows (open pits and underground; during active mining and post mining);
- Mine dewatering bores abstraction volumes; and
- Final void lake level equilibrium.



0 1 2 km

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TABBA TABBA LITHIUM MINE PROJECT, GROUNDWATER MODELLING TECHNICAL REPORT

PROPOSED DEVELOPMENT ENVELOPE AND INDICATIVE SITE LAYOUT

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FIGURE 1-1

Path: H:\Local Resources\Mining Advisory\ADVGIS\03-Projects\Australia-WA\TabbaTabbaLithium\ADVAU00796\01-ESRI\ADVAU00796.aprx\GW - Figure 1-1_Proposed Development Envelope and Indicative Site Layout

1.3 Conceptual Hydrogeological Model

1.3.1 Summary

Conceptual hydrogeological models for the site are provided in Rockwater (2024) and Wildcat (2025). Additional data was also compiled by SLR (2026). The key information relevant to the numerical model development and calibration is summarised in **Table 1-1.**

Table 1-1 Conceptual Model Summary

Item	Description
Drainage	Ephemeral, structurally controlled
Recharge	0 - 15 mm/yr. Episodic, Jan–Mar dominant. Evaporation >> rainfall.
Surface Geology	• Limited alluvium (up to 2m deep in some drainages. Not mapped) • Regolith thickness is approximately 10 m (low permeability)
Solid Geology	Metamorphic rocks. Pegmatite thicknesses up to 300 m. dip 35–40° NE Fracture zones: • 0–40 m: high fracture density • 40–80 m: moderate • >80 m: decreasing, local deep zones
Structural Geology	Two major features conceptualised as highly permeable: • Tabba Tabba Shear Zone (includes multiple faulting in a large zone SE - NW oriented) • A large dolerite dyke trending E – W (target for water supply bores)
Aquifer Systems	• Regolith: dry/unsaturated • Shallow fractured rock: 0 - 45 mbgl (primary aquifer) • Deeper fractured rock: up to 80 mbgl (secondary aquifer)
Groundwater Flow	Follows topography and structural geology (SW → NE).
Hydraulic conductivity (Kx)	• Fractured rock: 0.01 – 10 m/day (Slug testing) • Structures: 1–10 m/day (Slug testing)
Water Levels	Available in 2014/2015 and 2025/2026 • Depth to water table approximately 14 mbgl • Limited variation in Water Level (WL) over time. Delayed response to intense rainfall period at some bores. • Response to pumping indicate compartmentalised system (strong response to low volumes at FMG bore and no response to greater pumping at TABH002)
Discharge	• Evapotranspiration • Baseflow to creeks (limited to areas and periods where the water table elevation is greater than riverbed elevation)
Water quality	Reflective of highly heterogenous residence times pH: 7.4 – 8.8; EC: 1,830 – 10,100 µS/cm
GDE	Terrestrial Groundwater Dependant Ecosystem (GDE) mapped along some creeks based on vegetation types

2.0 Model Construction and Development

2.1 Model Code

MODFLOW-USG Transport was used as the model code (Panday, 2021). MODFLOW-USG is a version of industry standard MODFLOW code and is suitable for accomplishing the Model objectives. MODFLOW-USG optimises the model grid and increases numerical stability by using unstructured, variably sized cells. Cells take any polygonal shape, with variable size allowing for refinement in areas of interest (e.g. geological or mining features).

Where previous MODFLOW versions restricted interlayer flow to vertical connectivity, MODFLOW-USG offers lateral connectivity between model layers. Lateral connectivity enables more accurate representations of hydrostratigraphic units, particularly those that pinch out, outcrop, or cross geological faults.

MODFLOW-USG is also able to simulate unsaturated conditions, allowing progressive mine dewatering and post mining rewetting to be represented by the model. For the current model, vadose zone properties have been excluded, and the unsaturated zone was simulated using the upstream-weighting method.

Python\Fortran code and a MODFLOW-USG edition of the Groundwater Data Utilities (Watermark Numerical Computing, 2021) were used to construct the MODFLOW-USG input files.

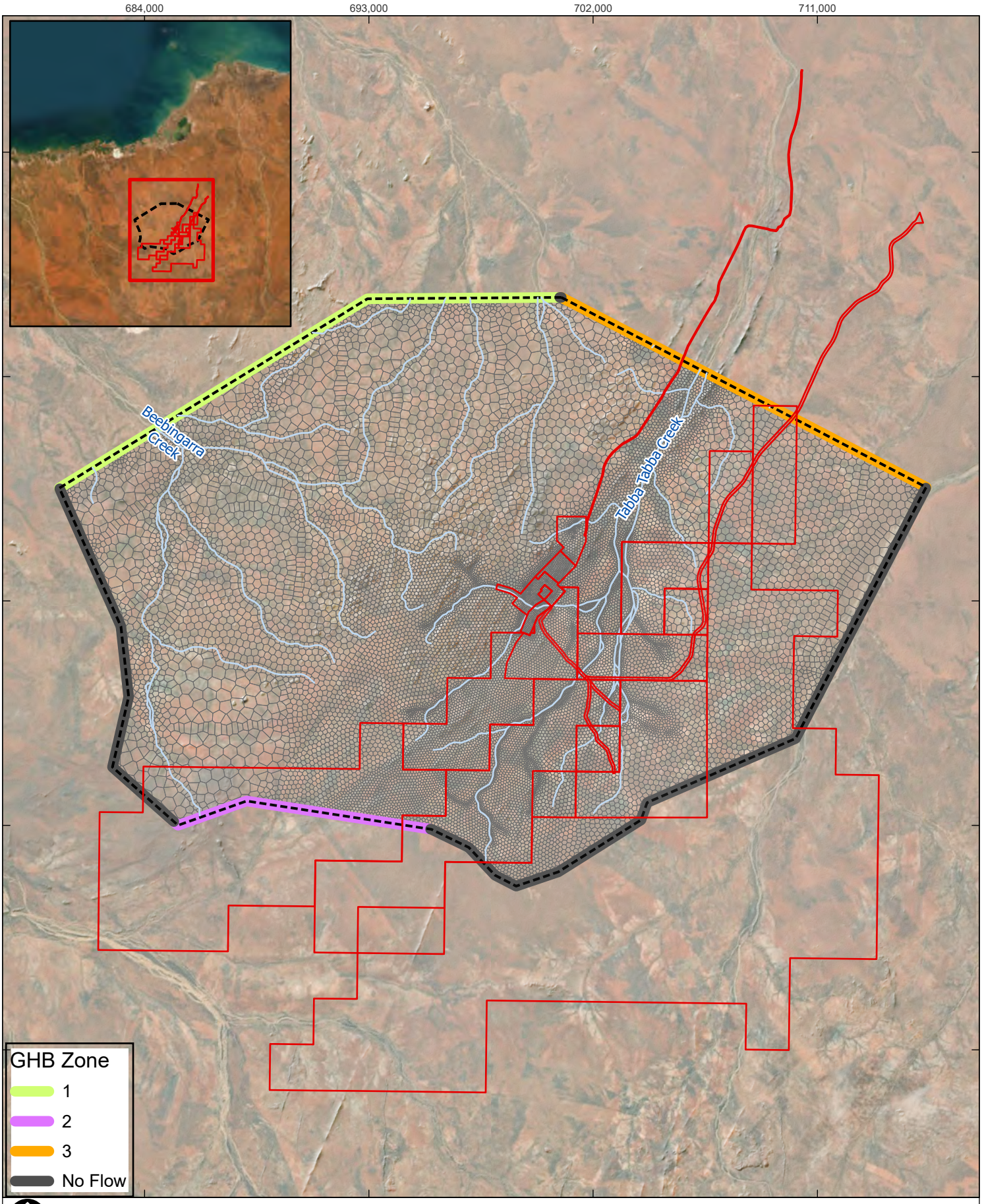
2.2 Model Extent and Mesh Design

The model domain was designed to place boundary conditions sufficiently distant from the mines to allow the extent of potential impacts from mining activities on the groundwater system to be assessed. At its widest extents, the model is approximately 33 km west-east by 23 km north-south. To allow stable numerical modelling of the large spatial area of the model domain, an unstructured grid with varying Voronoi cell sizes was designed using Algomesh (HydroAlgorithmics, 2014). Varying Voronoi cell sizes allowed refinement around areas of interest, while a coarser resolution elsewhere reduces the total cell count to a manageable size (**Figure 2-1).**

The model domain was vertically discretised into nine layers, each layer comprising a cell count up to 20,422. The total number of cells in the Model is 175,608. This is after pinching out areas in layer 2 which were not present based on the mapped geology.

The following features have been included in the grid design:

- Drainage systems are represented with 200 metre (m) cell edges length.
- Mining areas are represented with a 100 metre (m) cell edge length.
- The Tabba Tabba shear zone is represented as an approximately 1.5km wide zone with a 200 metre (m) cell edge length.
- The dolerite dyke is represented as with a 200 metre (m) cell edge length.
- The GDE and potential GDE areas are represented with a 100 metre (m) cell edge length.



0 1 2 km

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LEGEND

- Creeks
- Model Boundary
- Mining Tenements

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MODEL DOMAIN, MESH AND BOUNDARY CONDITIONS ON MODEL EDGES

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FIGURE 2-1

Path: H:\Local Resources\Mining Advisory\ADVGIS\03-Projects\Australia-WA\TabbaTabbaLithium\ADVAU00796\01-ESRI\ADVAU00796.aprx\GW - Figure 2-1 Model Domain, Mesh and Boundary Conditions on Model Edges

2.3 Model Layers

Topography within the model domain has been defined using numerous sources of varying accuracy ranging from high resolution LiDAR within the project area to publicly available Digital Elevation Models (DEMs).

The model domain is discretised into nine layers of varying thicknesses (**Table 2-1**).

Layer 1 is fully extensive across the model with an average thickness of 0.8 m it represents the base of unconsolidated sediments from the site geological model, and the first 1 m of the depth to regolith from CISRO (2014) outside of the site model domain. A minimum thickness of 0.5m was imposed.

Layer 2 is represented only in areas where regolith is present and is therefore not extended across the entire model domain. It represents the base of weathering from the site geological model, and the remaining depth to regolith from CISRO (2014) outside of the site model domain.

Layers 3 to 5 are fully extensive across the model and represent the fractured rock units. The upper fractured rock layer is relatively shallow and more transmissive, allowing greater groundwater flow. The fourth layer is interpreted to have higher transmissivity compared to the other fractured rock layers, while the deeper fractured rock units are generally less transmissive, reflecting reduced permeability with depth.

Layers 6 to 9 are fully extensive across the model and represent the basement granite. The basement granite was divided into 4 layers to better represent the underground mine.

Table 2-1 Model Layers and Thicknesses

Model Layer	Geologic Formation	Data Source	Average Thickness (m)
1	Unconsolidated sediments	1. Geological model; 2. CSIRO	0.8
2	Weathered rock	1. Geological model; 2. CSIRO	6.6
3	Fractured rock	Conceptual	45.3
4	Fractured rock	Conceptual	30
5	Fractured rock	Conceptual	70
6	Granite	Conceptual	150
7	Granite	Conceptual	180
8	Granite	Conceptual	200
9	Granite	Conceptual	200

2.4 Hydrogeological Parameterisation

2.4.1 Hydrogeological Zones

Hydrogeological zones were defined for each layer to represent the main hydrogeological units and their spatial extent (**Table 2-2**). The unconsolidated units were represented as separate zones (as per the layering), to reflect the distinction made in the geological model (zones 1 and 2).

The fractured rock was divided into two zones, each then divided into three subzones:

- The Tabba Tabba shear zone, defined as an approximately 1.5 km wide zone to represent the damage zone associated with several mapped long faults and which include the pegmatite zones (up to 150 m deep). This zone is assumed to be more permeable and conductive than the rest of the fractured rock. The zone is divided into 3 zones based on depth (zone 3, 4, and 5)
- The fractured rock outside of the Tabba Tabba shear zone, assumed to be less permeable. The zone is divided into 3 zones based on depth (zone 6, 7, and 8)

The basement granite was divided into 3 zones, based on depth (zone9, 10 and 11). The Dolerite dyke was represented as a single zone spanning over layer 3 to 7 (zone 12).

Table 2-2 Hydrogeological Zones

Geological Unit	Hydrogeological Unit	Parameter Zone	Layer
Unconsolidated sediments	Unconsolidated Sediment	1	1
Weathered rock	Regolith	2	2
Fractured rock	Tabba Tabba Shear zone upper	3	3
Fractured rock	Tabba Tabba Shear zone middle	4	4
Fractured rock	Tabba Tabba Shear zone lower	5	5
Fractured rock	Fractured rock upper	6	3
Fractured rock	Fractured rock middle	7	4
Fractured rock	Fractured rock lower	8	5
Granite	Granite Upper	9	6
Granite	Granite Middle	10	7
Granite	Granite Lower	11	8
Granite	Granite Lower (Basement)	11	9
Dolerite Dyke	Dolerite Dyke	12	3, 4, 5, 6, 7

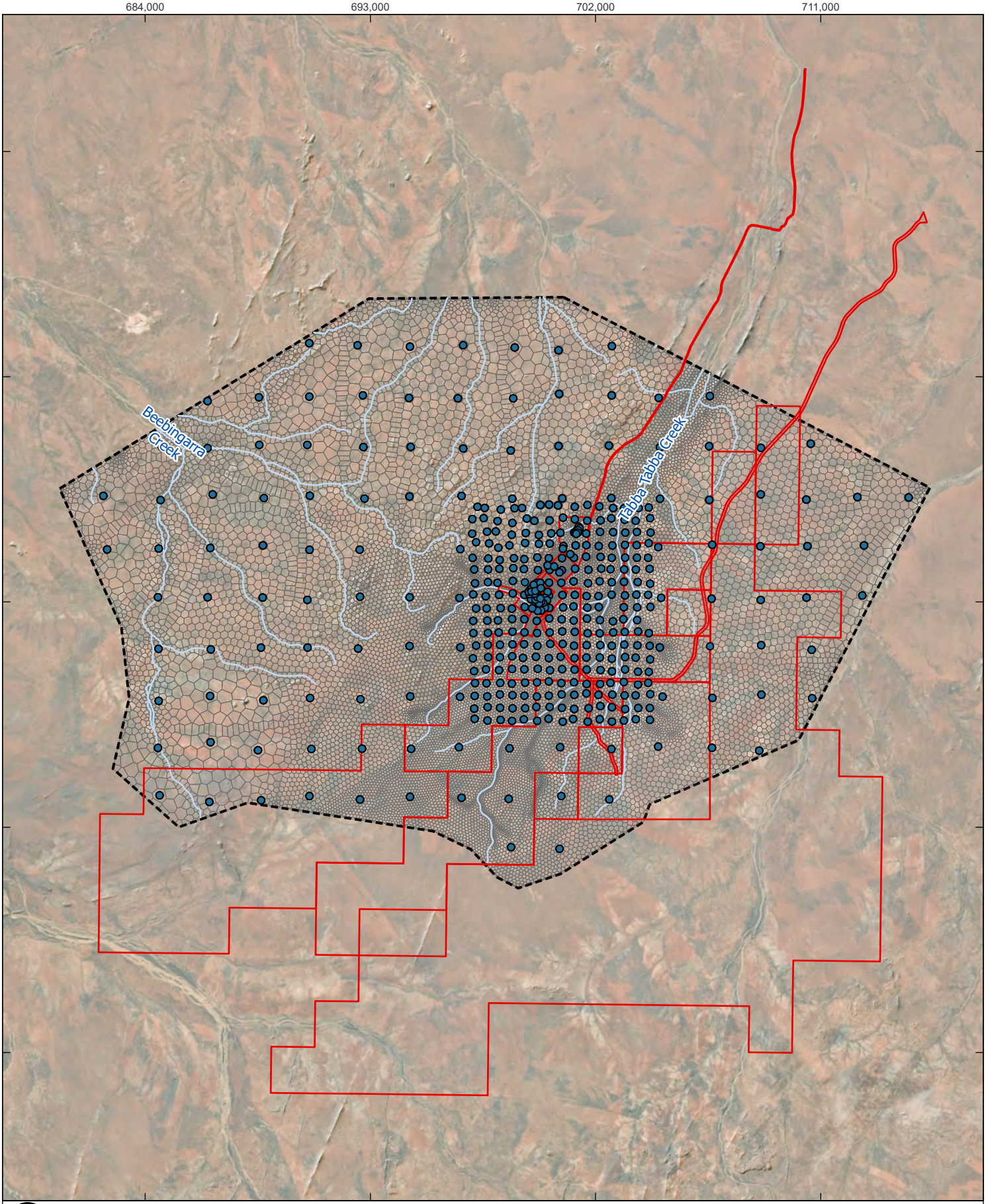
2.4.1.1 Structural Geology

2.4.2 Pilot Points

Pilot points were used to model the spatial variability of hydraulic conductivity (horizontal and vertical) and specific yield in most of the hydrogeological units intercepted by the project. These are zones 2, 3, 4, 5, 6, 7, 8, 9, and 10.

Pilot locations (**Figure 2-2**) were defined as:

- Regular 500 m grid covering the project area and potential receptors (Groundwater Dependant Vegetation (GDV) and potential GDV)
- Regular 2000 m grid for the rest of the model
- Additional triangulation around the observation bores



0 1 2 km

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LEGEND

- Mining Tenements
- Creeks
- Model Boundary
- Grid
- pilot_points_location

TABBA TABBA LITHIUM MINE PROJECT, GROUNDWATER MODELLING TECHNICAL REPORT

PILOT POINTS

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FIGURE 2-2

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Pilot points enable interpolating between the pilot point values to create a surface across the model domain for a targeted model parameter. This surface of model parameter values is then interrogated for values at the model cell centres to provide a value at each model cell.

Pilot point covariance matrices were generated independently for each geologic zone in the groundwater model. Pilot point covariance matrices are used to impose spatial correlation between pilot points, ensuring parameter fields vary smoothly and realistically during calibration rather than changing independently at each point.

Pilot points are placed in all zones from layer 2 to 7, except for the Dolerite dyke, which is assumed as a single parameter value zone (**Table 2-3**).

Table 2-3 Summary of Pilot Points Assigned to Geological Units by Model Layer

Parameter Zone	Hydrogeological Unit	Layer Number	Pilot Point Count
2	Regolith	2	249
3 & 6	Tabba Tabba Shear zone upper and Fractured rock upper	3	458
4 & 7	Tabba Tabba Shear zone middle and Fractured rock middle	4	458
5 & 8	Tabba Tabba Shear zone lower and Fractured rock lower	5	458
9	Granite upper	6	421
10	Granite middle	7	421

2.5 Model Stresses and Boundary Conditions

2.5.1 Regional Groundwater Flow

General Head Boundary (GHB) conditions have been specified along the northern and part of the southern boundaries (**Figure 2-1**). The GHB boundary condition is used to represent the regional flow into and out of the model area and was assigned using GHB cells from layer 1 to 7 (groundwater fluxes within the deep lower granite and basement is assumed to be negligible).

Fluxes at the model boundary are calculated at each cell using a conductance factor based on Darcy's law:

$Q = \frac{K*A}{L} * (H_{GHB} - H_{cell})$

With:

K= Horizontal hydraulic conductivity in the cell; **A=** Area of the cell face through which the flux occurs; **L=** Distance from the cell to the GHB head; **H_{GHB}=** GHB Head; **H_{cell}=** Head simulated in the cell.

Groundwater will enter the model where the head in the GHB is higher than the simulated head in the adjacent cell and will leave the model when the water level is lower in the GHB.

Three zones have been defined based on the boundary orientation and distance to an assumed discharge point (i.e. assumed fixed groundwater elevation at this point), as presented in **Table 2-4**.

Table 2-4 GHB Setup

Zone	Discharge Point	GHB Head (m AHD)	Distance (Km)
1	Indian Ocean	0	30
2	Oakover River	100	8
3	Indian Ocean	0	45

2.5.2 Watercourses

Surface water features (i.e. Rivers and Creeks) were built into the model using the MODFLOW-USG RIV package. River cells in the model are shown in **Figure 2-3**. Topography data was used to define the riverbed elevation. River stage was set to zero for all surface water feature, based on their highly ephemeral nature. As such, the surface water features in the model can only act as “drains”: If the groundwater level in a River cell is greater than the riverbed elevation, water will be removed (i.e. flow out of) from the model.

Fluxes at the model boundary are calculated at each cell using a conductance factor based on Darcy’s law:

$Q = \frac{K*A}{L} * (H_{RIVbed} - H_{cell})$

With:

K= Vertical hydraulic conductivity of the riverbed; **A=** Area of the cell base through which the flux occurs; **L=** Thickness of the riverbed; **H_{RIVbed}=** Stage elevation; **H_{cell}=** Head simulated in the cell.

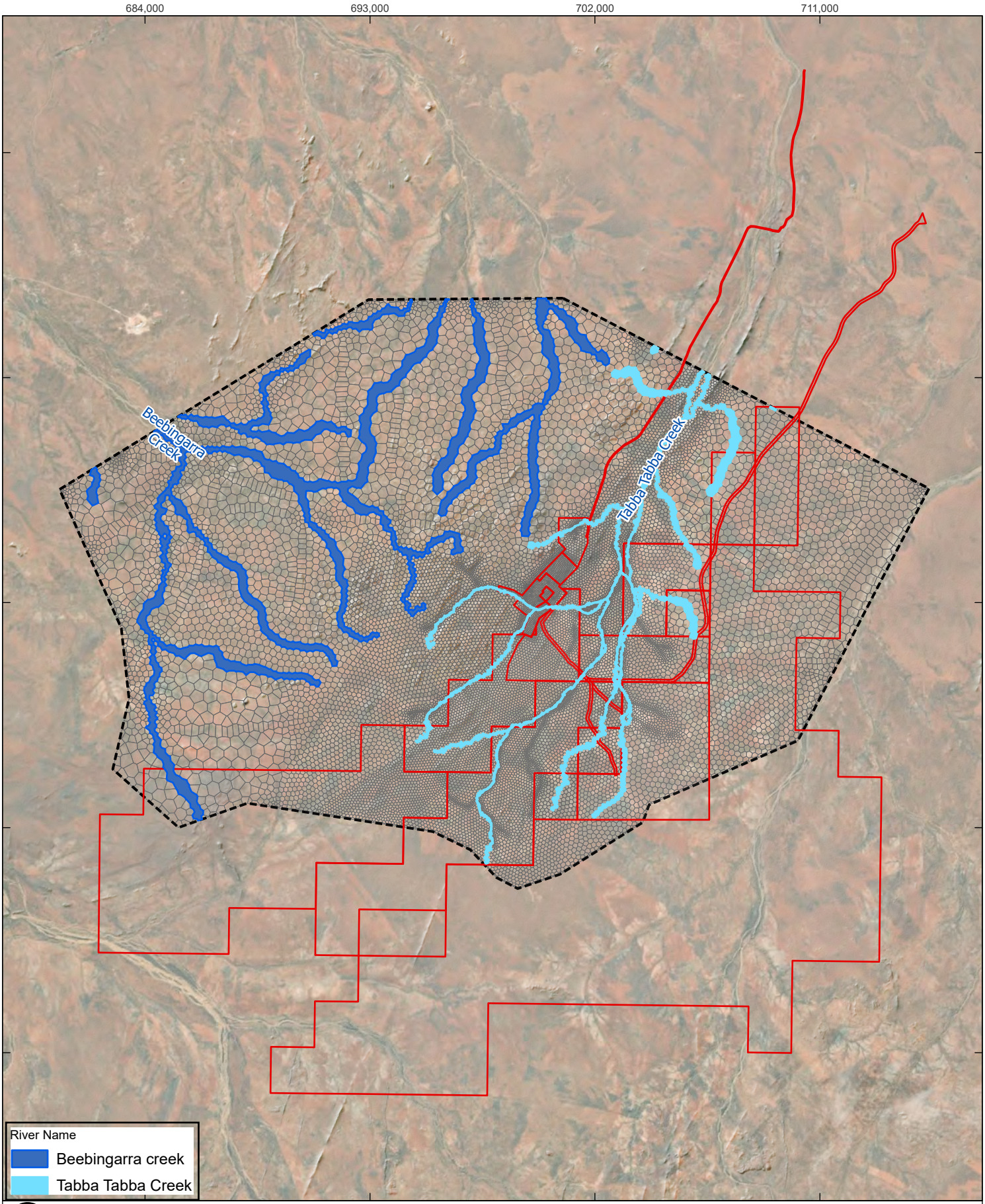
2.5.3 Rainfall Recharge

Recharge to the groundwater system mainly occurs through rainfall infiltrating the soil and draining down to the aquifer. This process was simulated in the model using the MODFLOW-USG Recharge (RCH) package. As recharge is conceptualised to occurs primarily via structures and drainage lines, the following zones were defined:

- Tabba Tabba shear zone
- Creeks
- Rest of the model

Recharge was based on deep drainage data from the Bureau of Meteorology (BoM) AWRA-L model. For the steady-state model, long-term average values (1988–2026) were used. For the transient model, time-varying deep drainage data from 2008 to 2026 were applied.

The original dataset included about 30 grid-based zones. The gridded data was combined with the three recharge zones, resulting in a total of 64 recharge zones (**Figure 2-4**). Recharge in each zone was adjusted during calibration.



0 1 2 km

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LEGEND

- Mining Tenements
- Creeks
- Model Boundary
- Grid
- Beebingarra creek
- Tabba Tabba Creek

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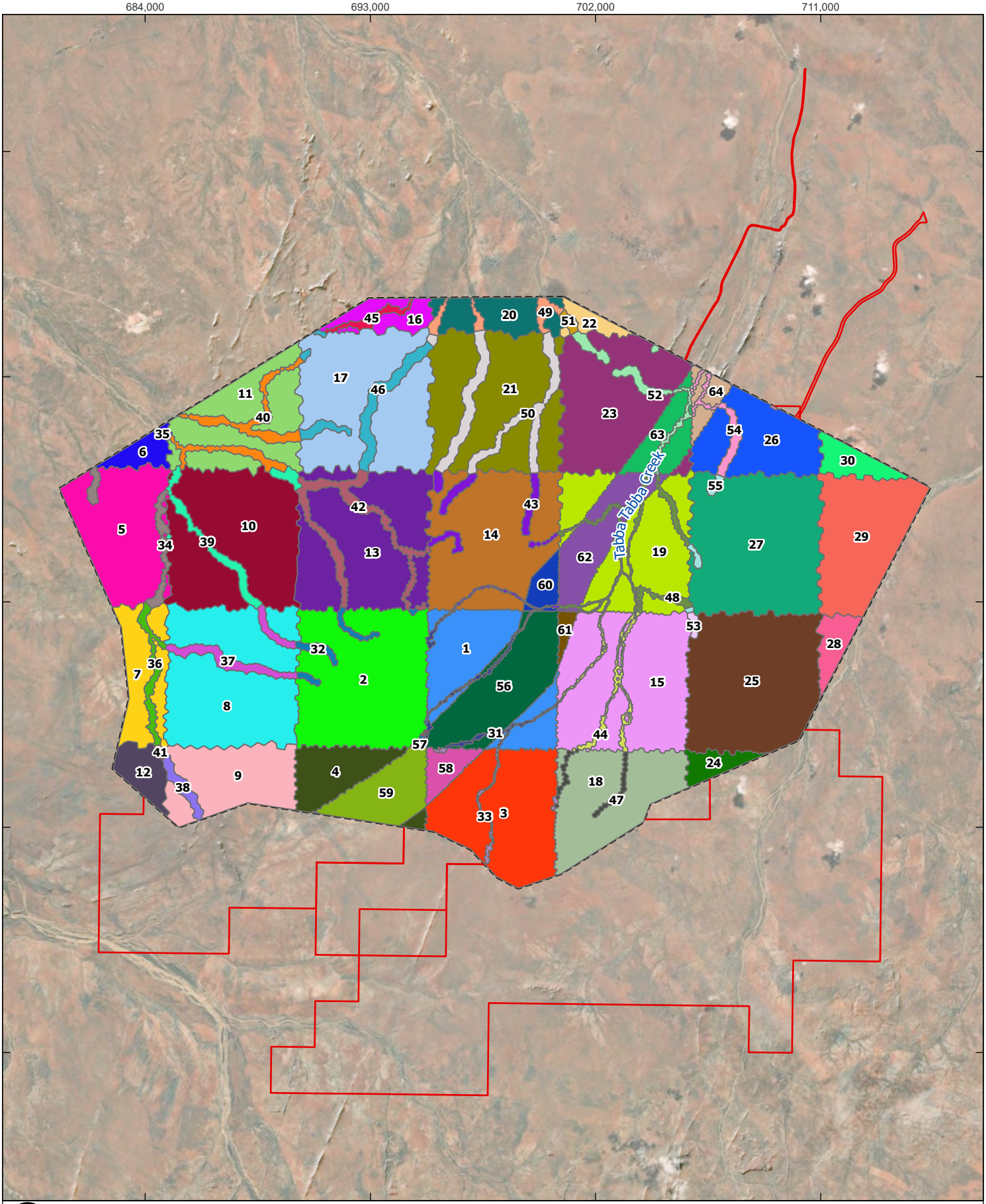
STREAM AND RIVER CELLS

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FIGURE 2-3

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0 1 2 km

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Drawn by:	JP

LEGEND

- Creeks
- Model Boundary
- Mining Tenements

TABBA TABBA LITHIUM MINE PROJECT, GROUNDWATER MODELLING TECHNICAL REPORT

MODEL RECHARGE ZONES

SLR

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FIGURE 2-4

Path: H:\Local Resources\Mining Advisory\ADVGIS\03-Projects\Australia-WA\TabbaTabbaLithium\ADVAU00796\01-ESRI\ADVAU00796.aprx\GW - Figure 2-4 Model Recharge Zones

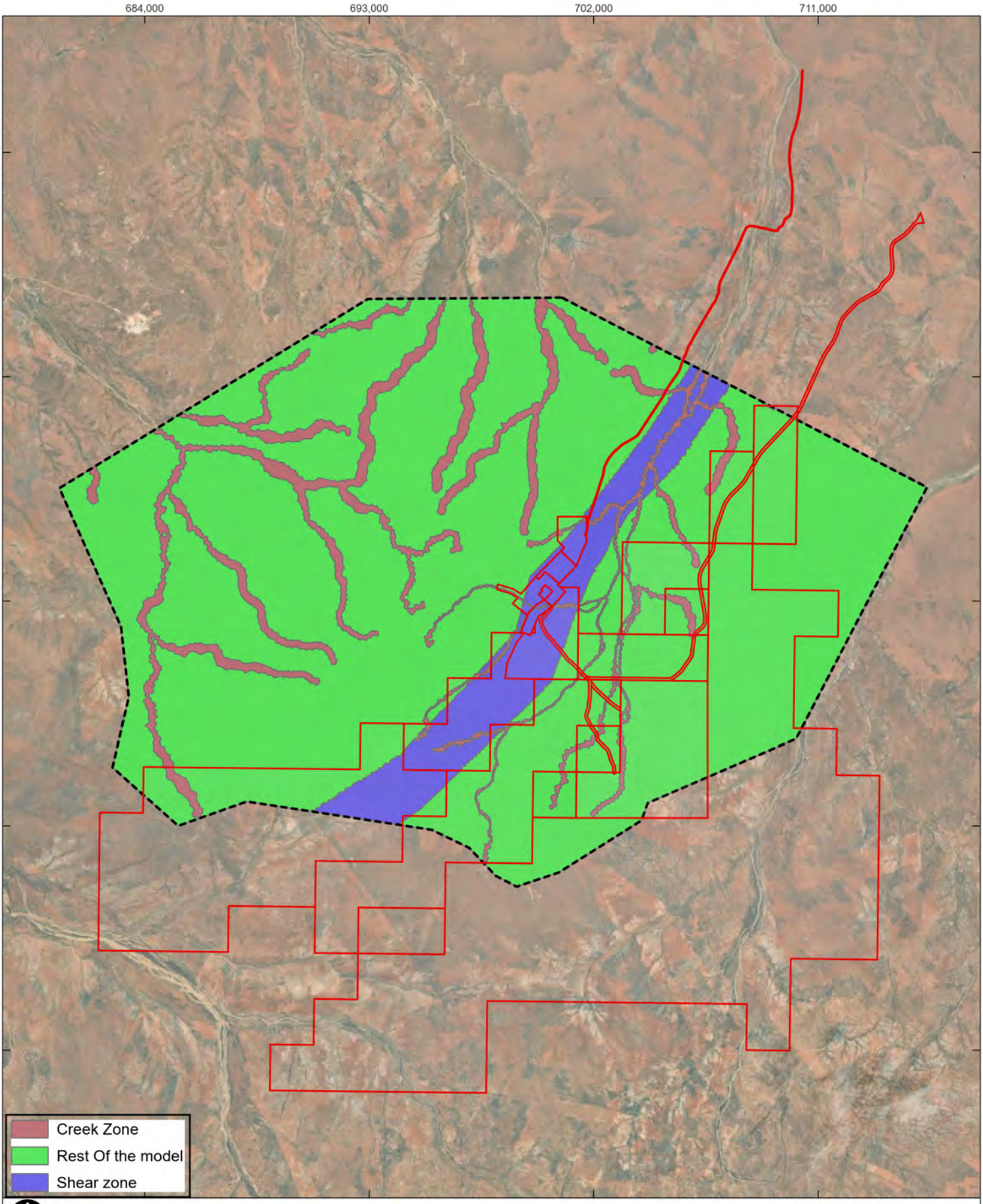
2.5.4 Evapotranspiration

Evapotranspiration (EVT) has been applied using MODFLOW's linear function in the EVT package. Topographic elevation is used as the 'evaporation surface' at which MODFLOW simulates EVT at the specific rate. The EVT extinction depth parameter defines the maximum depth from which water can be extracted by vegetation through transpiration. Any water that is available below this depth is assumed to be unavailable to plants.

The model included three EVT zones as per the recharge zones (**Figure 2-5)**

- Tabba Tabba shear zone
- Creeks
- Rest of the model

EVT rates and extinction depths were included as calibration parameters for each zone. Extinction depths are included as absolute value while the rate is a multiplier of potential EVT: The maximum potential rate was set using potential evapotranspiration values (from the Bureau of Meteorology), with the average value (3100 mm/year).



0 1 2 km

Coordinate System:	GDA 1994 MGA Zone 50
Scale:	1:200,000 at A4
Project Number:	620.042733
Date Drawn:	5/19/2026
Drawn by:	JP

LEGEND

- Model Boundary
- Mining Tenements

TABBA TABBA LITHIUM MINE PROJECT, GROUNDWATER MODELLING TECHNICAL REPORT

EVAPOTRANSPIRATION ZONES

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FIGURE 2-5

Path: H:\Local Resources\Mining Advisory\ADVGIS\03-Projects\Australia-WA\TabbaTabbaLithium\ADVAU00796\01-ESRI\ADVAU00796.aprx\GW - Figure 2-5 Evapotranspiration Zones

2.5.5 Groundwater Use

2.5.5.1 Pumping Wells

Two pumping bores (FMG and TABH002) were active during the calibration period. TABH002 operated from January 2024 to December 2025, while FMG operated from February 2024 to December 2025 (**Figure 2-6**).

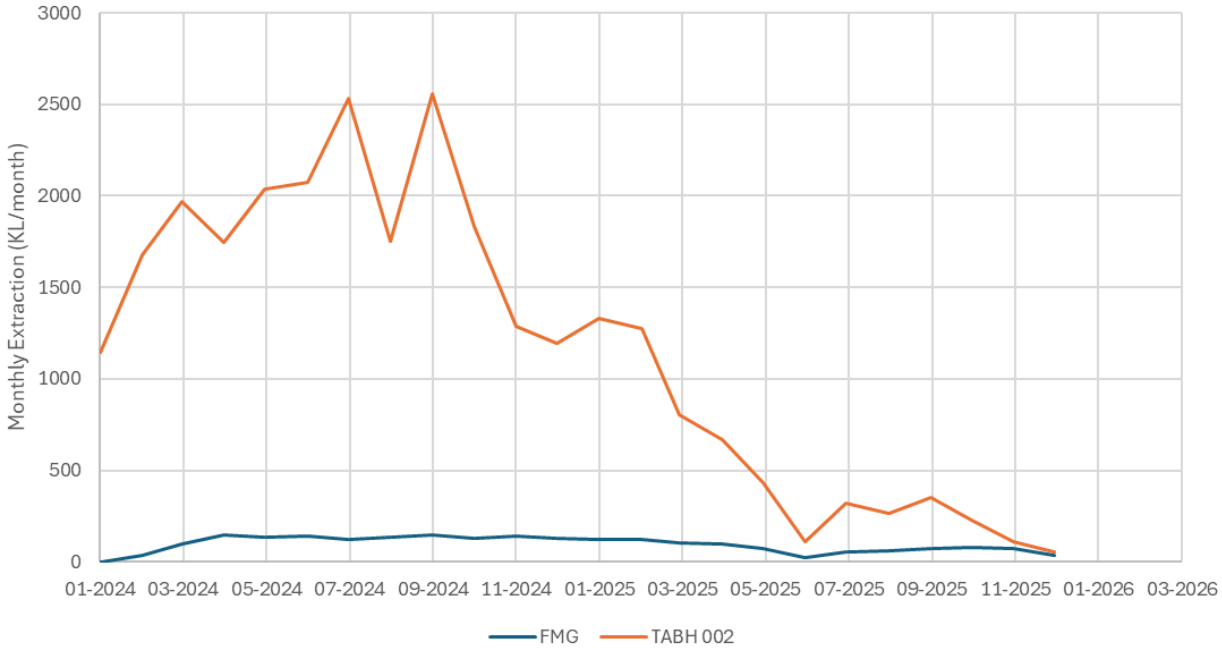


Figure 2-6 Pumping Bores Volumes

Pumping Well are applied using the WEL package. Inputs include the location and depth of the well (model node) as well as pumping rate for each location. Pumping rates were applied as per **Figure 2-6**.

2.6 Timing

A combined steady-state, transient warm-up, and transient calibration model was developed with the following stress periods (**Table 2-1**):

- A warmup transient period with one 365-day stress period from January 2000 to December 2000.
- A steady-state stress period representing pre-mining groundwater conditions.
- A transient calibration period with 120 stress periods from January 2021 to February 2026.

The warmup and steady-state periods do not include any mining activities. The calibration period includes a mix of stress periods, with 36 six-monthly (wet and dry season) periods, 83 monthly periods, and one quarterly period. Stress period length for the transient calibration period (SP3 to SP122) was determined based on the following:

- Minimum of 6-monthly periods to capture key seasonal trends; and
- Monthly stress periods one year prior to and during periods of available monthly monitoring data (to best reproduce measured water levels).

Together, the warmup transient, steady state, and transient calibration periods make up a total of 122 stress periods.

To assist the model in overcoming the numerical difficulties, MODFLOW-USG Adaptive Time-Stepping (ATS) option was used. The ATS option of MODFLOW automatically decreases time-step size when the simulation becomes numerically difficult and increases it when the difficulty passes.

Table 2-5 Model Timing

Stress Periods	Predictive Period	Date Start	Date End	Stress Period Length (day)	Max Time Step length (day)
1	Warm up	01 - 2000	12 - 2000	365	365
2	Steady State	01 -2001	01 -2001	1	1
3 - 122	Calibration	01 -2001	02 -2026	28 - 183	183

2.7 Solver Settings

The solver settings were defined in the Sparse Matrix Solver (SMS) package. The PCGU method was selected with inner and outer convergence set at 0.001 and 0.01 respectively during calibration.

3.0 Model Calibration

3.1 Calibration Method

Automated calibration was undertaken using PESTPP-IES (White et al., 2020) to match simulated groundwater levels to observations. This method uses an iterative ensemble smoother, which starts by generating a range of plausible parameter sets based on prior assumptions. These parameter sets are then progressively adjusted in batches through successive iterations to improve the match between model outputs and observed data. This process allows the model to efficiently explore uncertainty and converge toward parameter combinations that best reproduce the measured groundwater behaviour.

3.2 Calibration Dataset

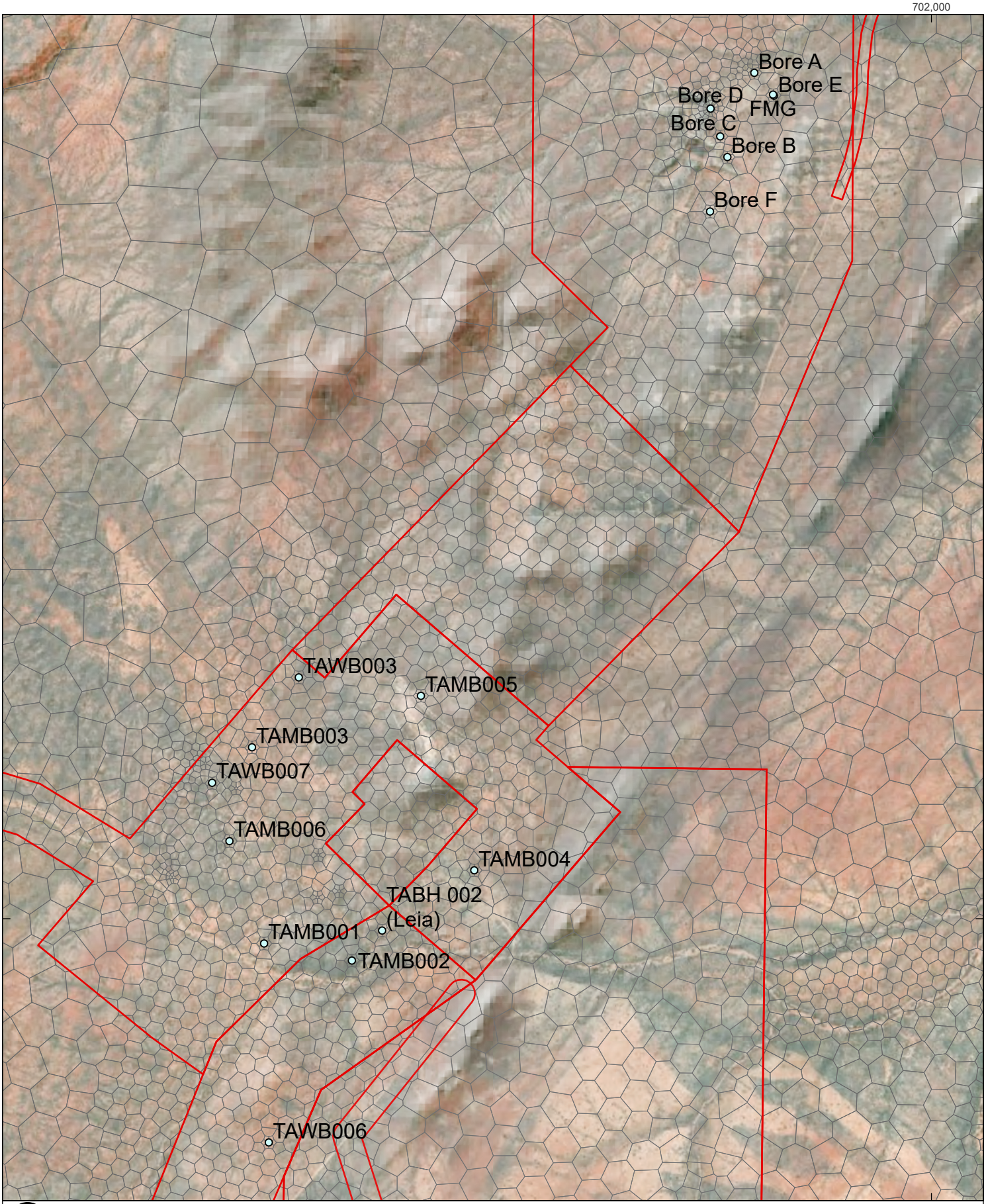
3.2.1 Groundwater Levels

Groundwater levels range from May 2014 to February 2026, with most of the data available for the 2025-2026 period. In all, 120 target heads have been established for 17 bores.

Most bores screen the upper fractured rock formation (layer 3). Bores TAWB006, TAWB007 and TAWB003 are deep open bore holes. Assuming that the depth is reflective of water bearing zones at depth, the bores were assigned to deeper layers based on maximum bore depth (**Table 3-1**). Locations are show on **Figure 3-1.**

Table 3-1 Observation Targets and Bores Details

Bore Name	Maximum Depth (m)	Layer
Bore F	20.2	Layer 1
Bore C	50	Layer 3
Bore B	35.2	Layer 3
TAMB001	26.3	Layer 3
TAMB002	60.1	Layer 3
TAMB003	55.2	Layer 3
TAMB006	55.2	Layer 3
TAMB004	54	Layer 3
TAMB005	36	Layer 3
Bore A	36	Layer 3
TABH 002 (Leia)	36	Layer 3
Bore E	42	Layer 3
FMG	44	Layer 3
Bore D	36	Layer 3
TAWB006	102	Layer 4
TAWB007	102	Layer 4
TAWB003	204	Layer 5



0 0.1 0.3 Kilometers

Coordinate System:	GDA 1994 MGA Zone 50
Scale:	1:18,190 at A4
Project Number:	620.042733
Date Drawn:	18-May-2026
Drawn by:	JP

LEGEND

- Mining Tenements
- Model Boundary
- Grid
- Bore Locations

TABBA TABBA LITHIUM MINE PROJECT, GROUNDWATER MODELLING TECHNICAL REPORT

BORE LOCATIONS

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FIGURE 3-1

Path: H:\Local Resources\Mining Advisory\ADVGIS\03-Projects\Australia-WA\TabbaTabbaLithium\ADVAU00796\01-ESRI\ADVAU00796.aprx\GW - Figure 3-1 Bore Locations

3.2.2 Calibration Weighting

In PEST calibration, observation weighting is used to control the relative influence of different data groups on the objective function and ensure a balanced fit across datasets, so that each type contributes appropriately to calibration despite differences in magnitude and count. In this model, observations are divided into two primary groups: Water levels (i.e. the first available water level at a location) and drawdowns (subsequent variations from the first water level).

Within each group, individual observation weights are scaled by dividing by the square root of the number of observations in that group, which normalises their collective contribution and prevents groups with more data points from dominating the calibration.

Although groups and weight are used to assist the calibration process, results are provided simply as one group (i.e. absolute water level) with no weighting applied (see **Section 3.4**).

3.3 Calibration Variables

The following parameters are able to vary during calibration to provide the best match between the measurements and the model simulated levels:

- **Hydraulic Properties:** Horizontal and vertical hydraulic conductivity, as well as storage parameters (specific storage and specific yield), were calibrated within predefined ranges consistent with available data and the conceptual model.
- **Pilot Points Hydraulic Properties:** Hydraulic properties at pilot points (horizontal and vertical conductivity and specific yield) were calibrated to better capture aquifer variability.
- **Evapotranspiration and Evapotranspiration Extinction Depths:** Both evapotranspiration rates and extinction depths were varied for each designated evapotranspiration zone in the model.
- **Recharge:** Transient recharge was based on deep drainage data from the AWRA-L model, obtained from the Bureau of Meteorology (BoM). These data were used to define recharge across the model area, with additional zones assigned for river and mining areas to better represent local conditions. Recharge in each zone was adjusted during calibration using multipliers.
- **River Conductance:** River conductance values were adjusted during calibration for each drainage feature.

Initial parameter ranges (i.e. min and max prior model calibration) are provided on **Table 3-2**.

Table 3-2 Parameter Ranges for PEST Automated Calibration

Hydraulic Property	Description	Unit	Min PEST Input	Max PEST Input
kx_z01	Unconsolidated Sediment	m/d	0.25	1
kx_z02	Regolith	m/d	0.05	1
kx_z03	Tabba Tabba Shear zone upper	m/d	0.25	4
kx_z04	Tabba Tabba Shear zone middle	m/d	0.05	0.4
kx_z05	Tabba Tabba Shear zone lower	m/d	0.01	0.1
kx_z06	Fractured rock upper	m/d	0.005	0.2

Hydraulic Property	Description	Unit	Min PEST Input	Max PEST Input
kx_z07	Fractured rock middle	m/d	0.001	0.1
kx_z08	Fractured rock lower	m/d	0.001	0.05
kx_z09	Granite Upper	m/d	0.0005	0.01
kx_z10	Granite Middle	m/d	0.0005	0.005
kx_z11	Granite Lower	m/d	0.000005	0.001
kx_z12	Dolerite Dyke	m/d	0.01	1
Kz/Kx_z01	Unconsolidated Sediment	m/d	0.05	0.05
Kz/Kx_z02	Regolith	m/d	0.05	0.05
Kz/Kx_z03	Tabba Tabba Shear zone upper	m/d	0.05	0.2
Kz/Kx_z04	Tabba Tabba Shear zone middle	m/d	0.05	0.1
Kz/Kx_z05	Tabba Tabba Shear zone lower	m/d	0.05	0.1
Kz/Kx_z06	Fractured rock upper	m/d	0.05	0.1
Kz/Kx_z07	Fractured rock middle	m/d	0.001	0.1
Kz/Kx_z08	Fractured rock lower	m/d	0.001	0.1
Kz/Kx_z09	Granite Upper	m/d	0.001	0.02
Kz/Kx_z10	Granite Middle	m/d	0.001	0.02
Kz/Kx_z11	Granite Lower	m/d	0.001	0.02
Kz/Kx_z12	Dolerite Dyke	m/d	0.05	0.5
sy_z01	Unconsolidated Sediment	m-1	0.05	0.06
sy_z02	Regolith	m-1	0.02	0.03
sy_z03	Tabba Tabba Shear zone upper	m-1	0.0005	0.01
sy_z04	Tabba Tabba Shear zone middle	m-1	0.0005	0.01
sy_z05	Tabba Tabba Shear zone lower	m-1	0.0005	0.01
sy_z06	Fractured rock upper	m-1	0.0005	0.01
sy_z07	Fractured rock middle	m-1	0.0005	0.01
sy_z08	Fractured rock lower	m-1	0.0005	0.004
sy_z09	Granite Upper	m-1	0.0005	0.004
sy_z10	Granite Middle	m-1	0.0005	0.004
sy_z11	Granite Lower	m-1	0.0005	0.004
sy_z12	Dolerite Dyke	m-1	0.0005	0.01
ss_z01	Unconsolidated Sediment	_	1.00E-06	1.00E-05
ss_z02	Regolith	_	1.00E-06	1.00E-05
ss_z03	Tabba Tabba Shear zone upper	_	1.50E-07	2.00E-07
ss_z04	Tabba Tabba Shear zone middle	_	1.50E-07	2.00E-07



Hydraulic Property	Description	Unit	Min PEST Input	Max PEST Input
ss_z05	Tabba Tabba Shear zone lower	_	1.50E-07	2.00E-07
ss_z06	Fractured rock upper	_	1.50E-07	2.00E-07
ss_z07	Fractured rock middle	_	1.50E-07	2.00E-07
ss_z08	Fractured rock lower	_	1.50E-07	2.00E-07
ss_z09	Granite Upper	_	1.50E-07	2.00E-07
ss_z10	Granite Middle	_	1.50E-07	2.00E-07
ss_z11	Granite Lower	_	1.50E-07	2.00E-07
ss_z12	Dolerite Dyke	_	1.50E-07	2.00E-07

3.4 Calibration Performance

3.4.1 Calibration Statistics

An industry-standard approach for assessing the calibration of a model is to analyse statistics related to the calibration. One way of doing this is by comparing the simulated differential (i.e. error) between the simulated and observed (measured) water levels, which is often expressed as the root mean square (RMS). The RMS value is calculated by taking the square root of the mean of the squared differences between the simulated and observed water levels. In accordance with Barnett et al. (2012), the root mean square (RMS) is considered one of the available options for calculating goodness of fit.

Another option for measuring the goodness of fit is the Scaled Root Mean Squared error (SRMS). SRMS is computed by dividing the RMS by the range of measured heads and expressing it as a percentage. When the goal is to fit historical measurements of water levels, SRMS provides a valuable indicator of the goodness of fit (Barnett et al., 2012). This is primarily due to its ability to compare errors in the simulated values against the total head changes in the system. If the errors are small relative to the total head change, they can be considered negligible.

The PESTPP-IES ensemble calibration process was initiated with 200 randomly generated realisations and resulted in 127 calibrated realisations. A summary of statistical analyses of the error residual between simulated and observed water level elevation for all calibrated realisations is provided in **Table 3-3**. It is noted that the best calibrated realisation was selected during the calibration process, based on the sum of squares for the weighted data set (as described in **Section 3.2.2**). The data presented in **Table 3-3** is for all measured water level, without weight applied.

In this study, RMS error calculated for the best calibrated model within the ensemble is 2.8 m, leading to a SRMS value of 15.6 %. The maximum RMS error the ensemble is 2.9 m.

Table 3-3 Transient Calibration Statistics for All Realisations – Water Levels

Statistic	Minimum	Median	Maximum	Best Calibrated Realisation
Mean Residual (m)	-3.16	0.19	4.69	0.32
Mean Absolute Residual (m)	1.82	2.51	4.69	1.94
Standard Deviation (m)	2.61	2.76	2.88	2.81
Sum of Squares (m2)	851.86	1158.16	3498.77	949.52
Root Mean Square Error (RMS) (m)	2.66	3.11	5.4	2.81
Minimum Residual (m)	-7.68	-4.15	0.29	-4.2
Maximum Residual (m)	4.2	7.63	12.13	7.65
Number of Observations	120	120	120	120
Range in Observations (m)	18.06	18.06	18.06	18.06
Scaled Standard Deviation (%)	14.45	15.29	15.95	15.54
Scaled Absolute Mean (%)	10.1	13.9	25.97	10.73
Scaled RMS (SRMS) (%)	14.75	17.2	29.9	15.58

Figure 3-2 presents the observed and simulated groundwater levels graphically as a scattergram for water level elevations dataset for the Tabba Tabba bores included in the calibration. As can be seen in the figure, most data points fall near the line of equality and within the expected confidence interval, indicating that the model generally reproduces observed groundwater levels well.

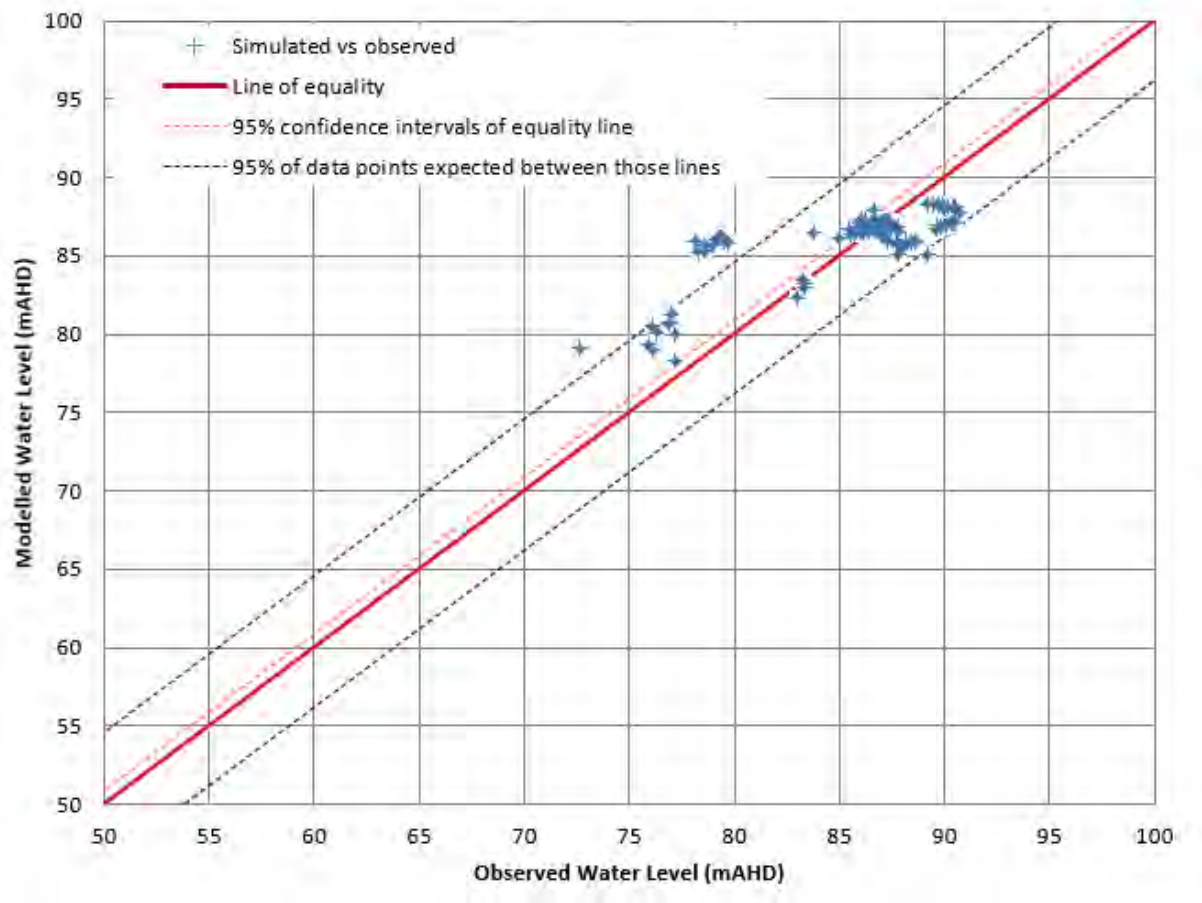


Figure 3-2 Observed Vs Modelled Groundwater Levels

The mean residuals are shown for each layer on **Table 3-4**. The highest residual is observed in layer 1, whilst the main aquifer (layer 3) shows the best fit overall with a mean residual less than 1 m.

Table 3-4 Layers Calibration Statistics

Model Layer	Mean Residual (m)	Mean Absolute Residual (m)	Number of Observation Targets	Number of Boreholes
1	4.27	4.27	1	1
3	0.92	1.79	96	13
4	-2.31	2.42	22	2
5	-2.82	2.82	1	1

Figure 3-3 shows a histogram of calibration residuals with counts separated by layer. The histogram shows that the residuals are generally well centred around zero, showing a balanced model performance with no strong bias toward either overprediction or underprediction of groundwater levels. Most residuals fall within the -2.5 to +2.5 range, suggesting a good overall fit to the measured data.

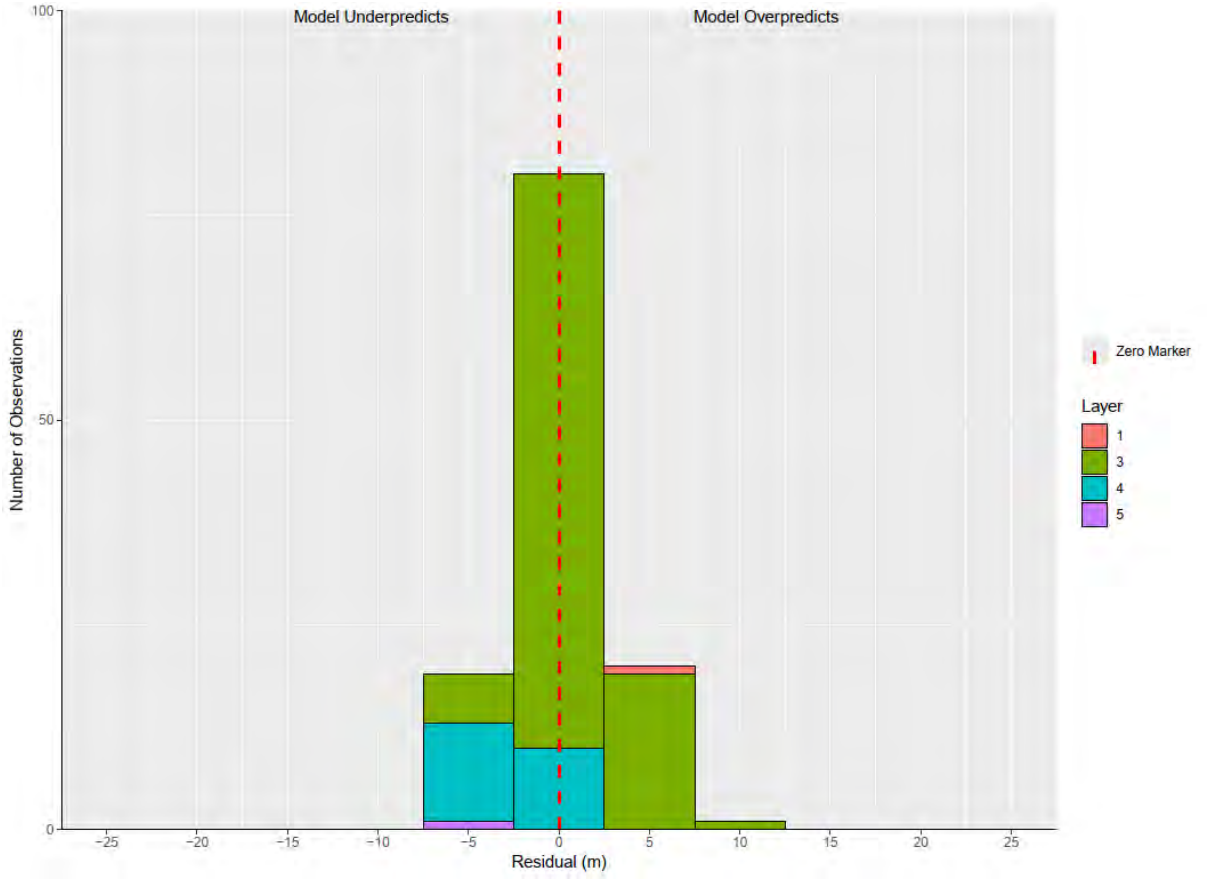
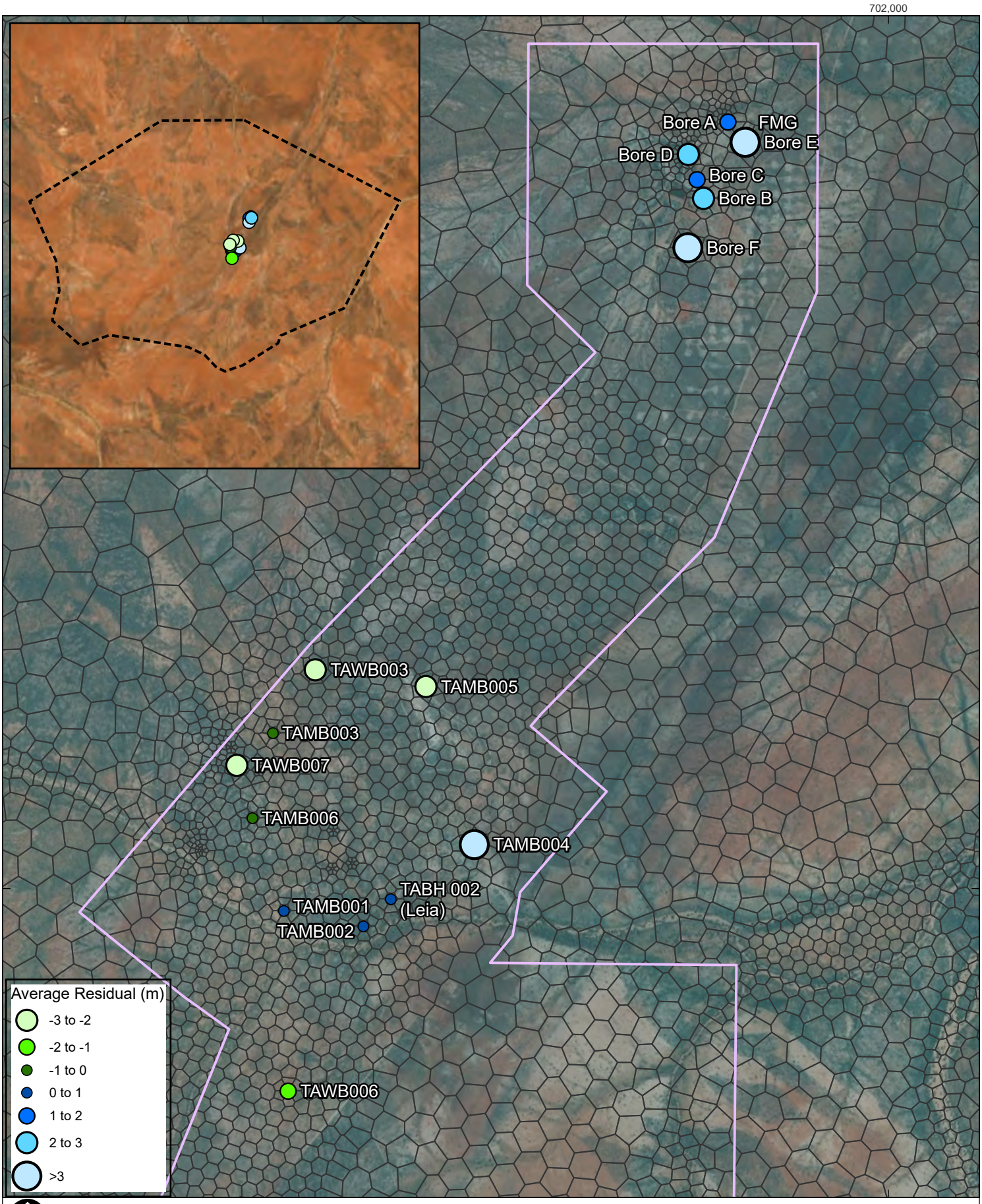


Figure 3-3 Calibration Residual Histogram

The spatial distribution of average residuals for each borehole from the transient calibration is shown in Figure 3-4 (where the size of the borehole symbol is proportional to the residual (i.e. a larger residual has a larger symbol size). Figure 3-4 shows that there is a good match between observed and simulated groundwater levels. The figure shows that bores located near the mining area (southern group of bores) are generally well calibrated.



0 0.1 0.3 Kilometers

Coordinate System:	GDA2020 MGA Zone 50
Scale:	1:20,000 at A4
Project Number:	620.042733
Date Drawn:	19-May-2026
Drawn by:	JP

LEGEND

- Model Boundary
- Development Envelope
- Model Boundary
- Model Mesh

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BORE AVERAGE RESIDUAL

SLR

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FIGURE 3-4

Path: H:\Local Resources\Mining Advisory\ADVGIS\03-Projects\Australia-WA\TabbaTabbaLithium\ADVAU00796\01-ESRI\ADVAU00796.aprx\GW - Figure 3-4 Bore Average Residual1

3.4.2 Calibration Hydrographs

3.4.2.1 Water Level

Calibration hydrographs for all the bores in the calibration dataset are show from **Figure 3-5** to **Figure 3-13.** The model is able to reproduce seasonal trends overall at most bores. The absolute magnitude of water level change however is not always captured, as shown for Bore D (**Figure 3-6**) and Bore A (**Figure 3-8**).

At bore FMG (**Figure 3-6**), the drawdown, which is likely due to pumping is not well reproduced (pumping volumes are small and this is likely reflective of a small productive water bearing zone that cannot be well reproduced at the model scale). Water levels at TABH 002 (**Figure 3-7**), which extract much greater volumes than FMG (refer to **Section 2.5.5.1**) does not appear to affect by pumping over time. The model reproduces this well (i.e. it does not simulate lowering at TABH 002 due to pumping over time).

At TAMB 004, water levels are consistently lower than at all other bores screening the same aquifer (**Figure 3-8**). The reason for this is not obvious and the model was not able to reproduce this difference spatially.

Overall, the ensemble envelope includes most of the data points, illustrating that the ensemble provides a reasonable representation of variability in the observed system.

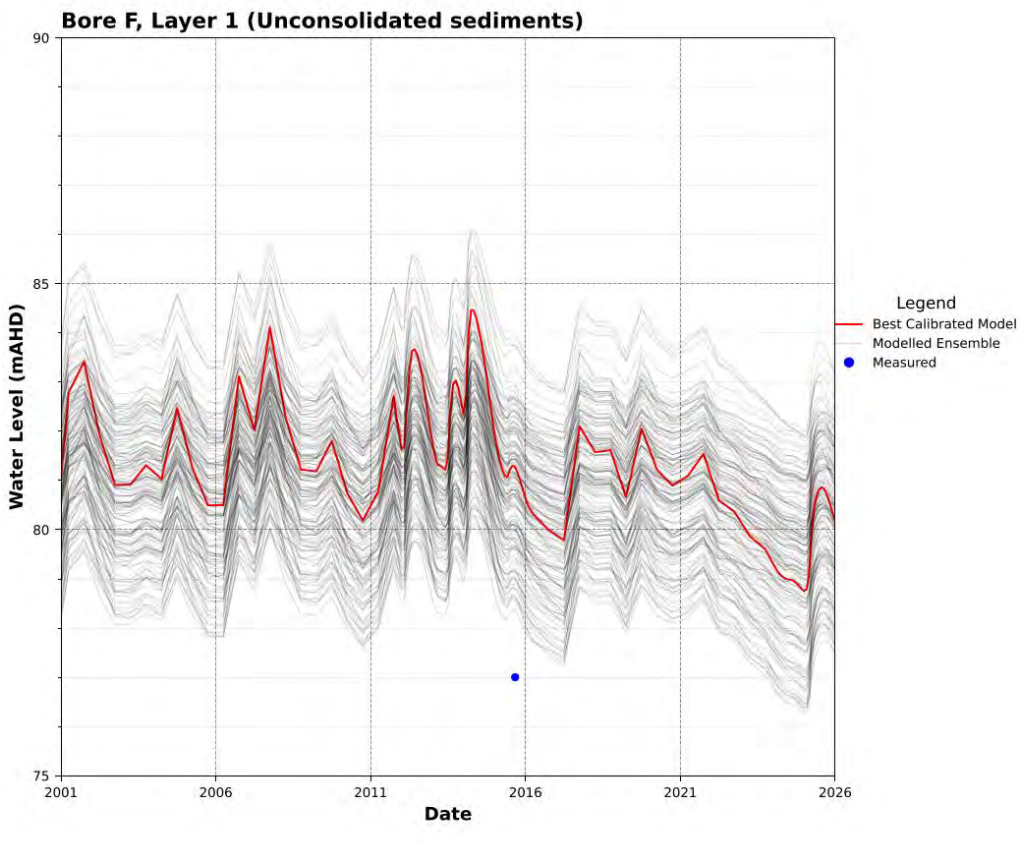


Figure 3-5 Calibration Hydrographs Bore F

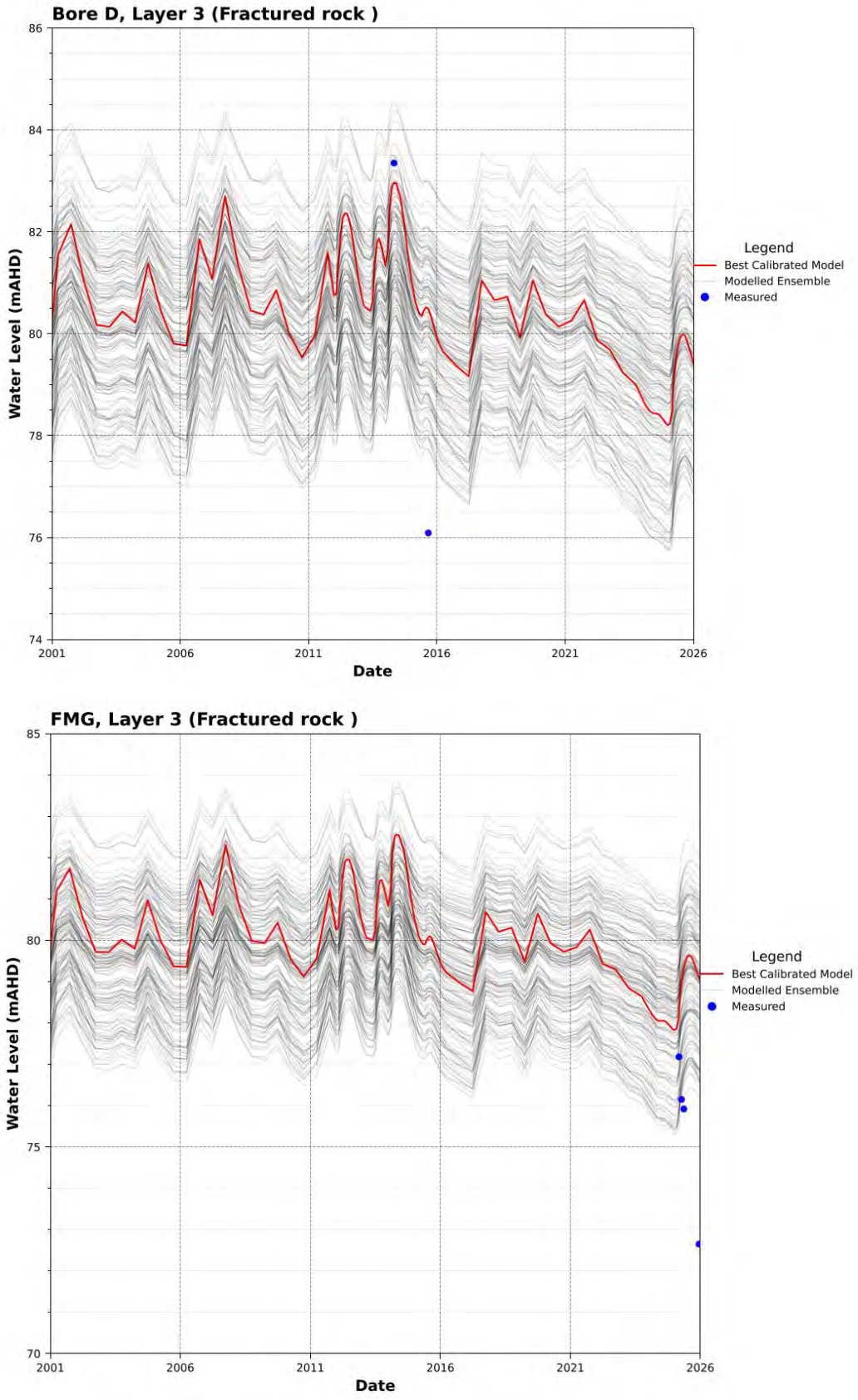


Figure 3-6 Calibration Hydrographs Bore D and FMG

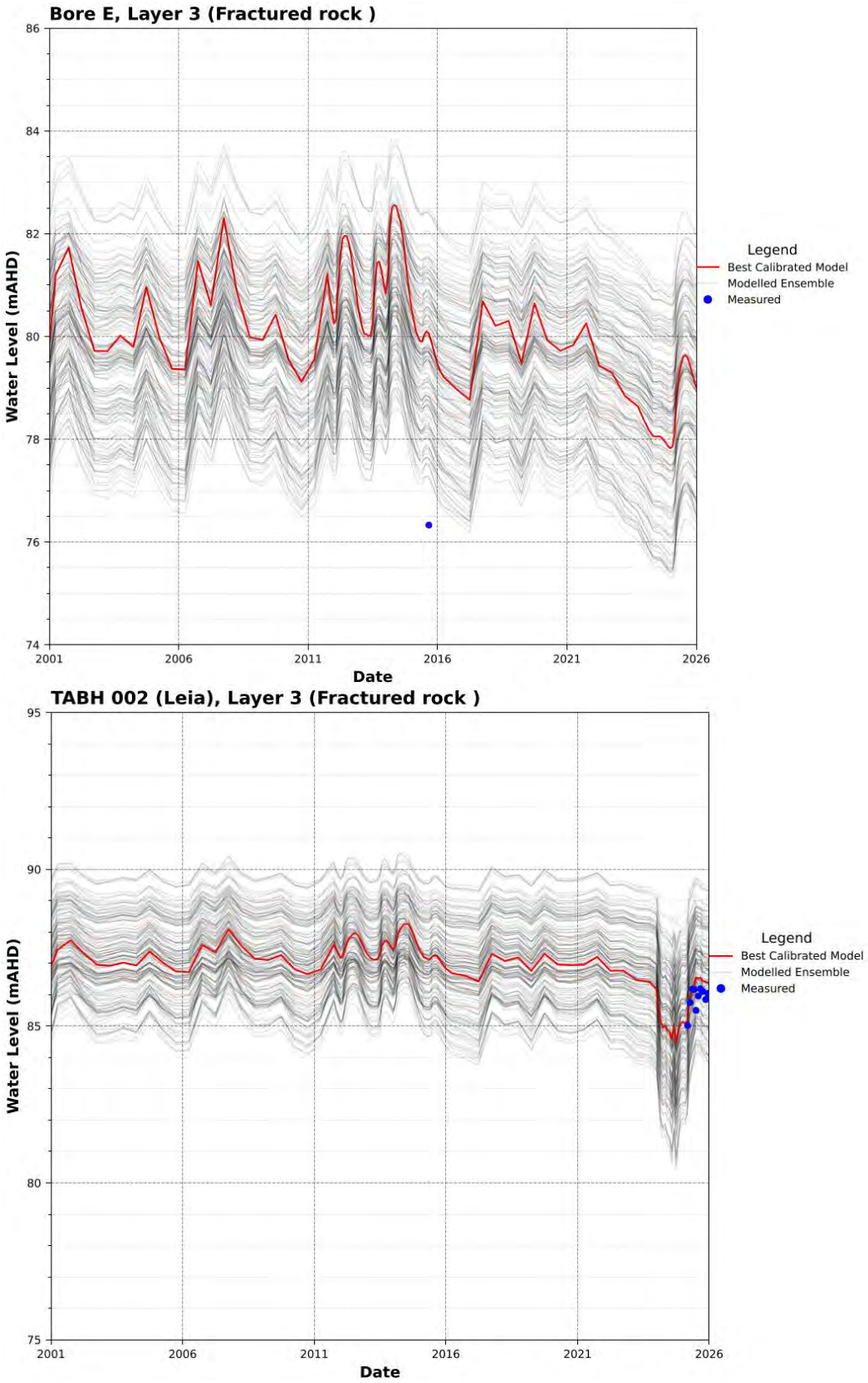


Figure 3-7 Calibration Hydrographs Bore E and TABH 002

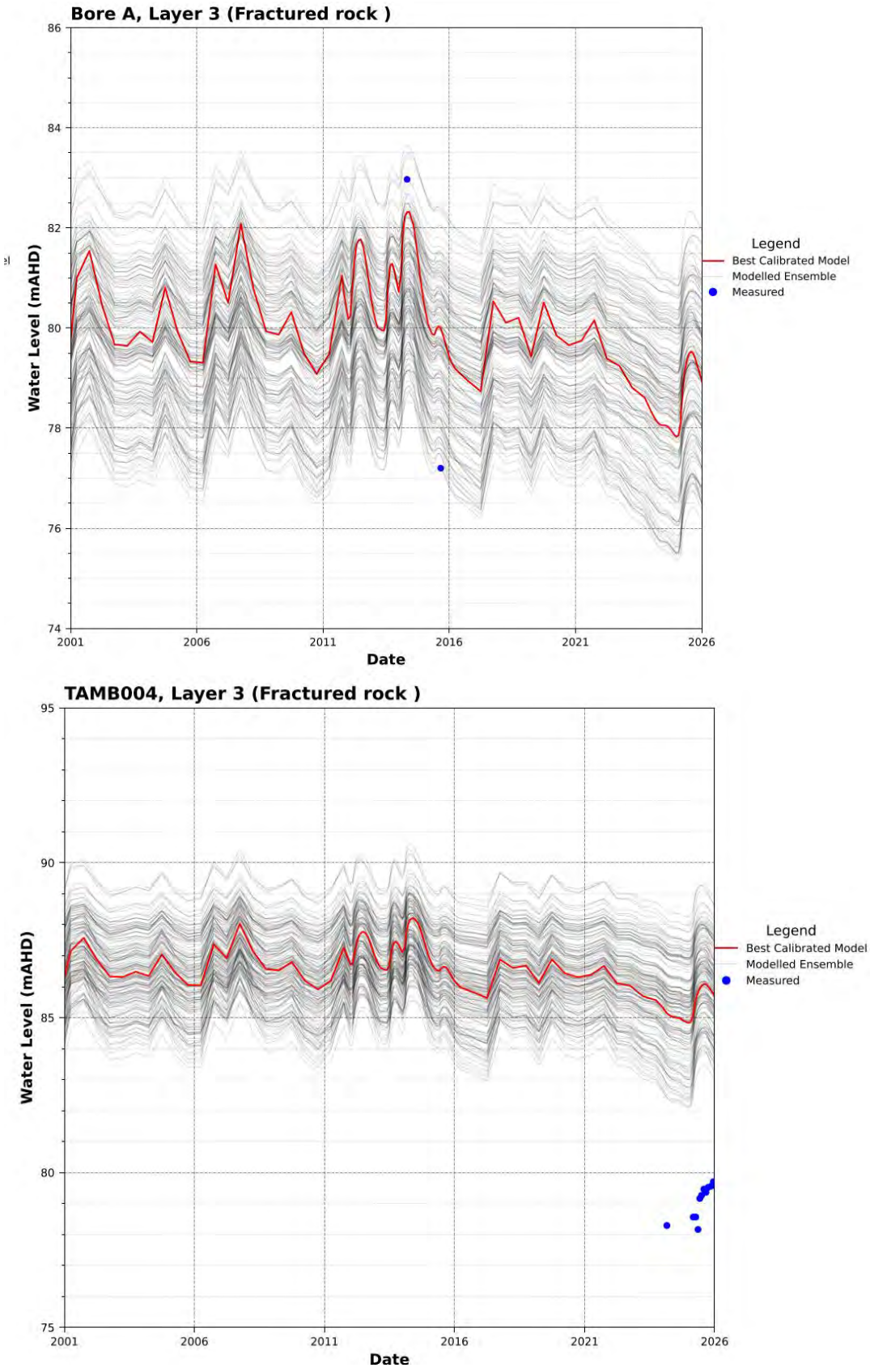


Figure 3-8 Calibration Hydrographs Bore A and TAMB 004

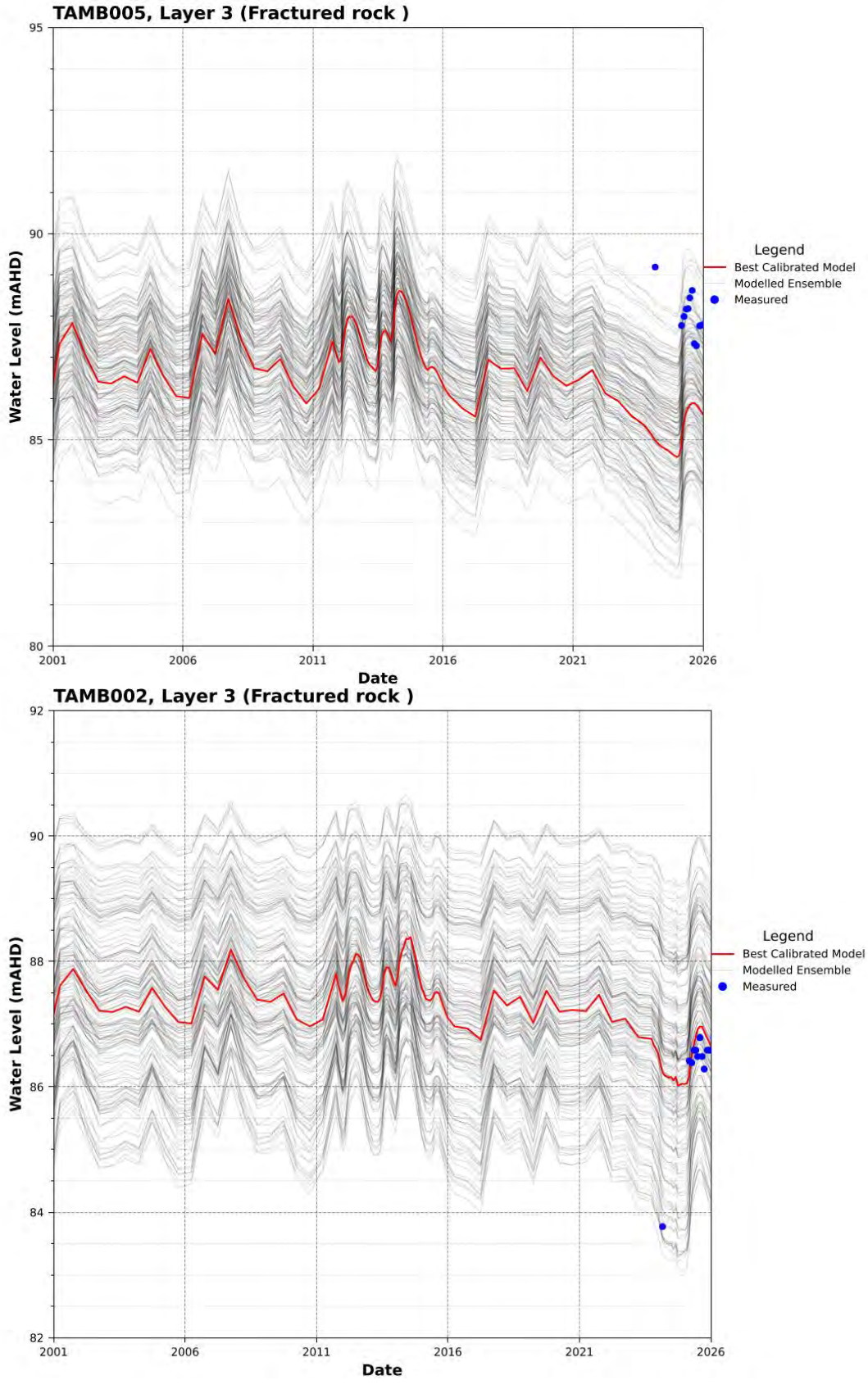


Figure 3-9 Calibration Hydrographs TAMB 005 and TAMB 002

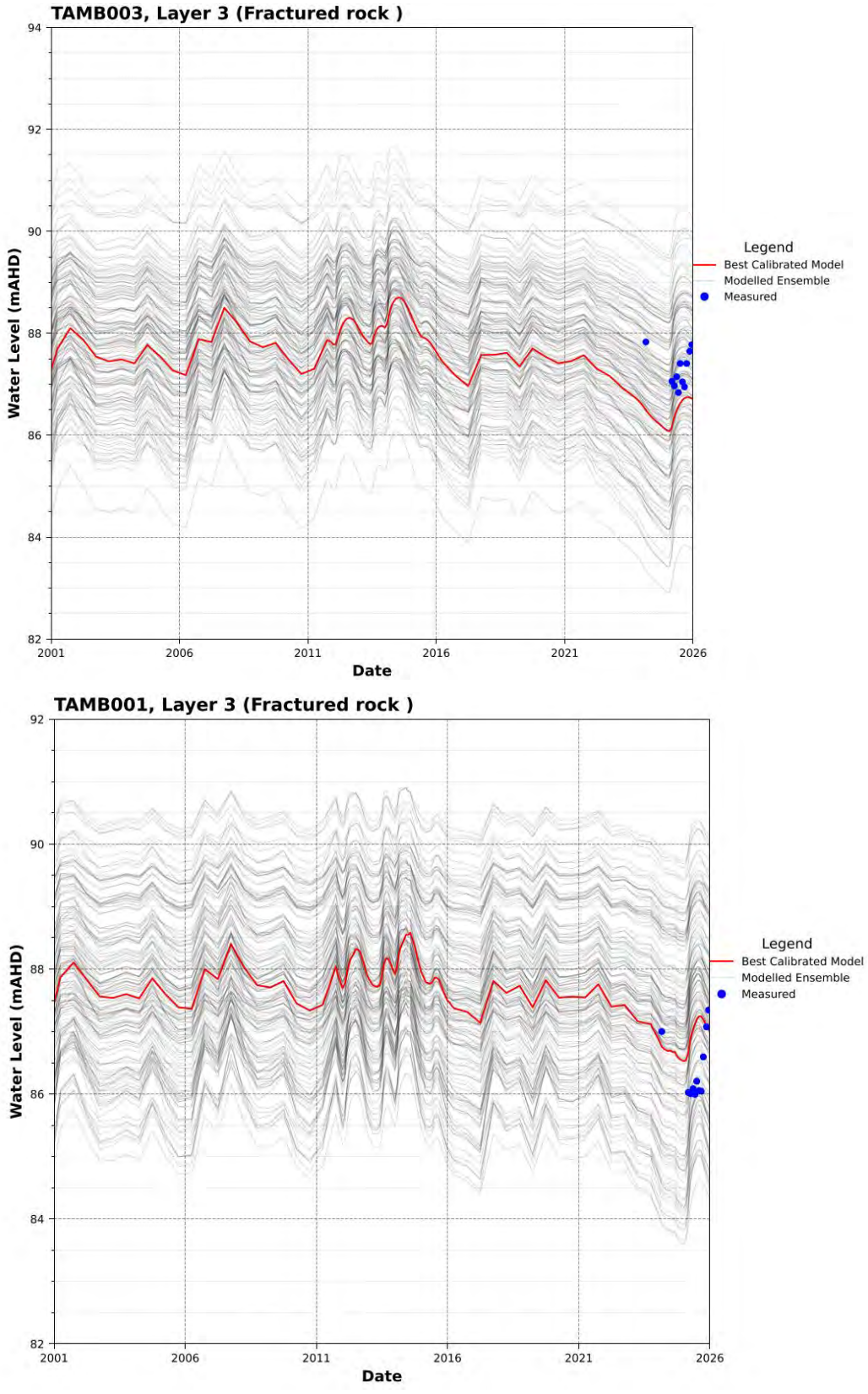


Figure 3-10 Calibration Hydrographs TAMB 003 and TAMB 001

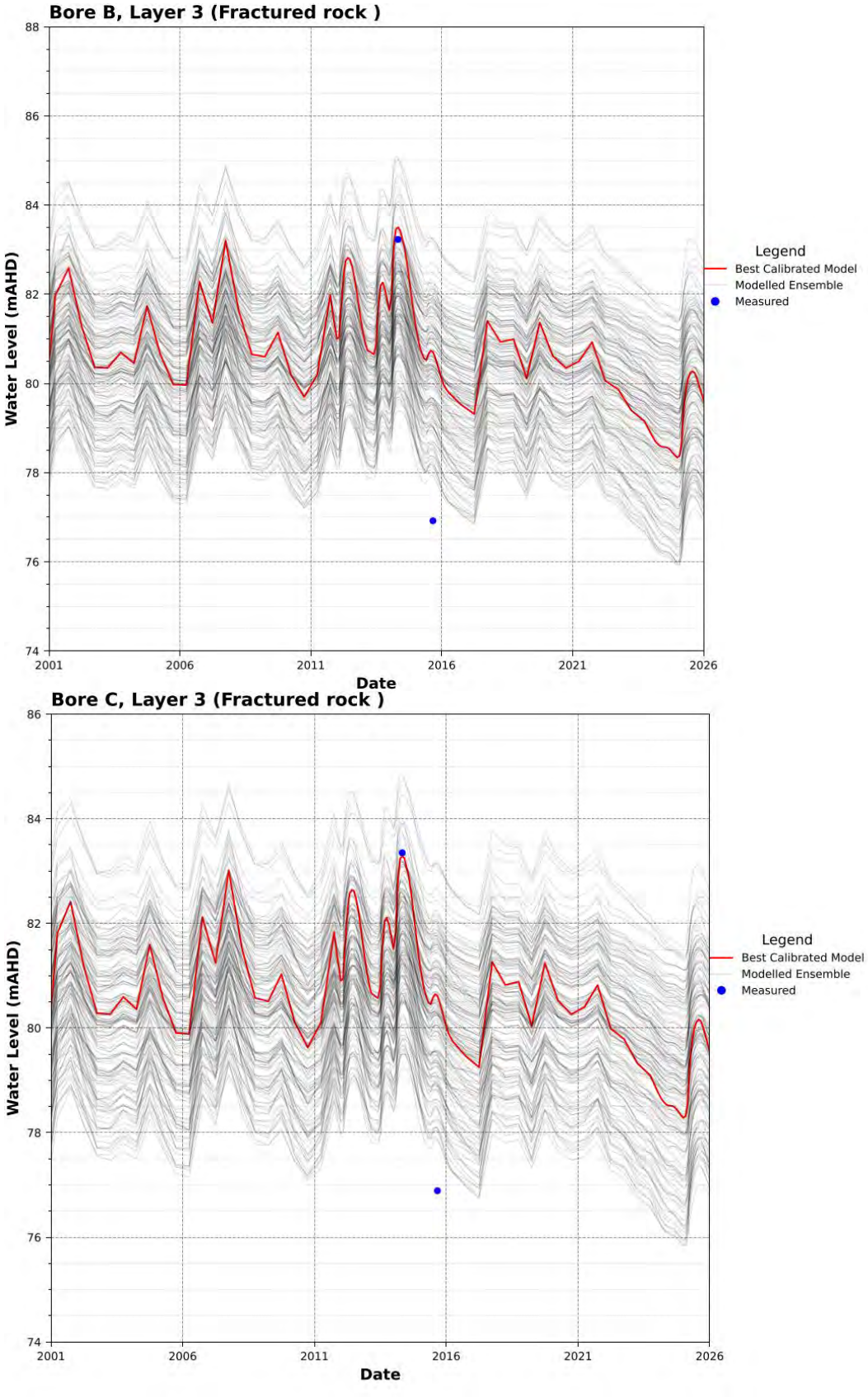


Figure 3-11 Calibration Hydrographs Bore B and Bore C

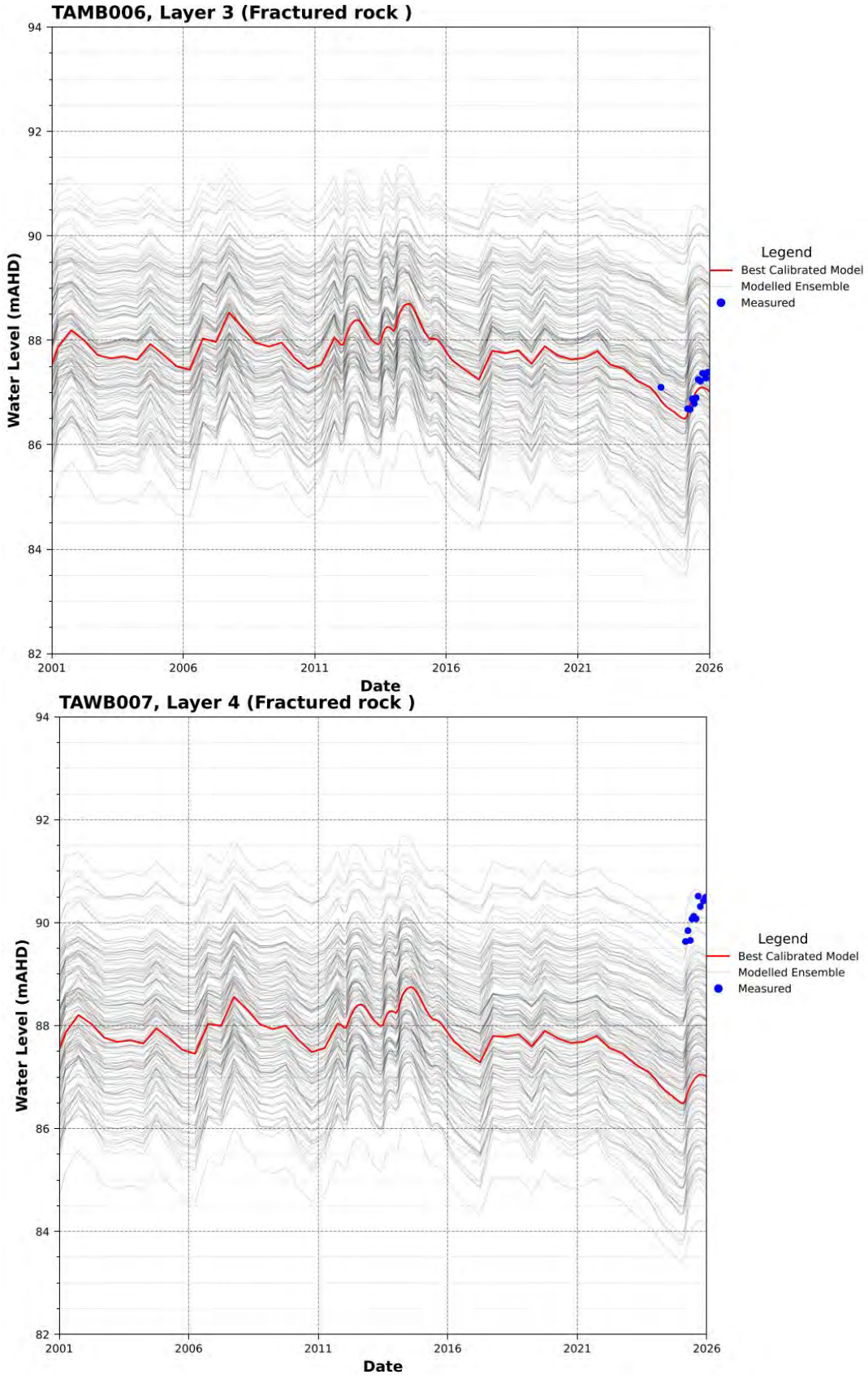


Figure 3-12 Calibration Hydrographs TAMB 006 and TAWB 007

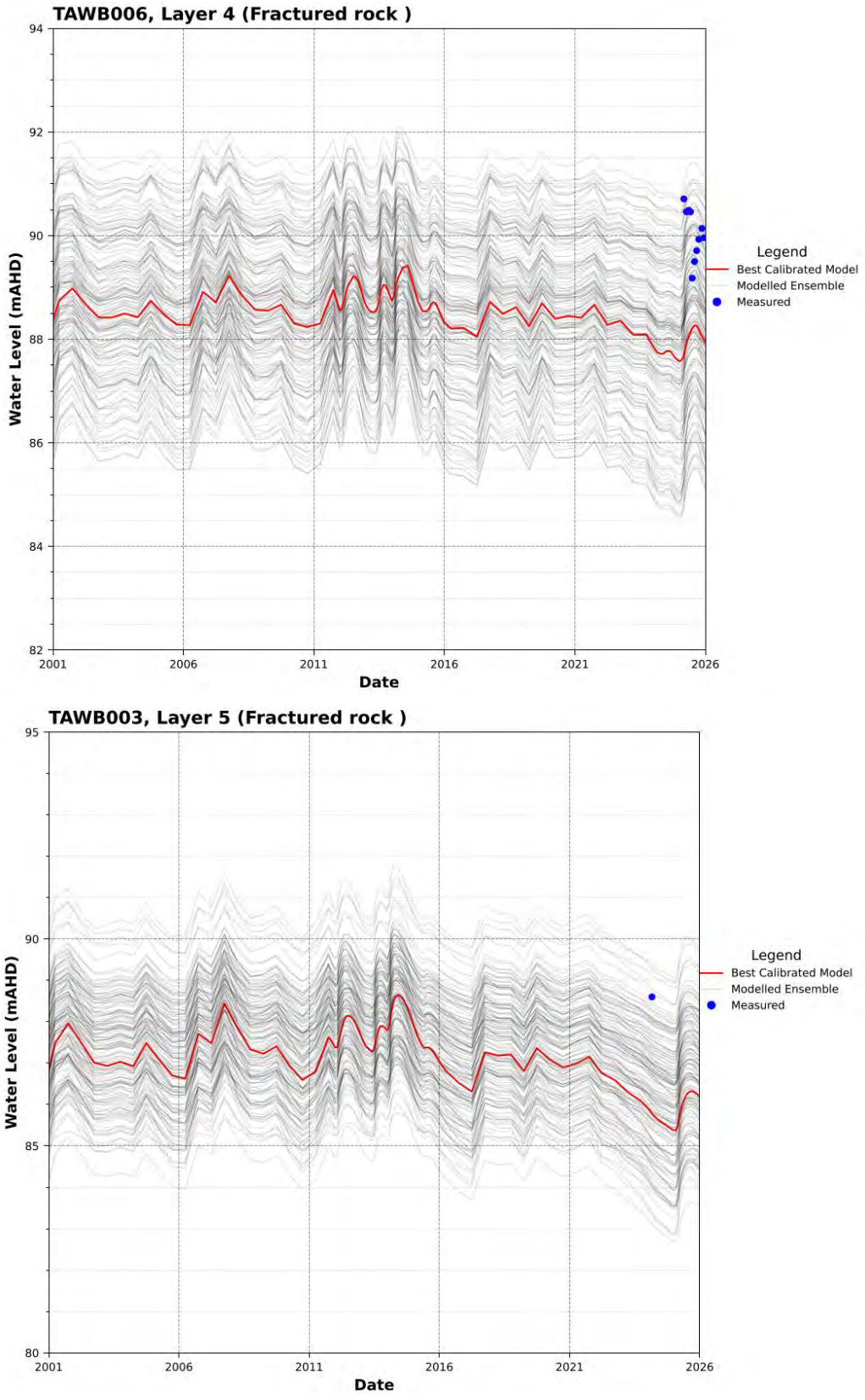


Figure 3-13 Calibration Hydrograph TAWB 006 and TAWB 003

3.5 Calibration Results

3.5.1 Calibrated Fluxes

3.5.1.1 Steady State Water Balance

The water balance for the steady state model indicates that recharge is the largest net inflow contributor to the steady state model accounting for 99.9 % of inflow, while evapotranspiration is the largest net outflow contributor with 84 % of outflow. Regional groundwater inflow and outflow are 0.01 ML/d and 1.55 ML/d, respectively, indicating that groundwater leaves the model domain through this boundary. No groundwater discharge to the drainages lines is observed, indicating that the water table is too deep to discharge to riverbed and that areas of shallow groundwater table discharge via evapotranspiration (**Table 3-5**).

The mass balance error for the steady state calibration is less than 0.01 %, within the error threshold recommended by the Australian Groundwater Modelling Guidelines (Barnett et al., 2012).

Table 3-5 Water Balance – Steady State Calibration Period (Best Calibrated Model)

Component	Inflow (ML/day)	Percent of Total Inflow (%)	Outflow (ML/d)	Percent of Total outflow (%)
Recharge	9.66	99.85	-	
Evapotranspiration (ET)	-		8.12	83.95
SW/GW Interaction Minor Rivers (RIV)	0.00	0.00	0.00	0.00
Regional GW flow (GHB)	0.01	0.15	1.55	16.05
Mines (DRN)	-	-	0.00	0.00
Well	0.00	0.00	0.00	0.00
Storage	0.00	0.00	0.00	0.00
Total	9.67	100.00	9.67	100.00

3.5.1.2 Transient Water Balance

During the transient calibration period, the recharge contribution to inflow reduces to 81% with the remaining 19 % now accountable to storage (The transient nature of the simulation allows for water to be stored to and released from storage according to the transient stresses). The mass balance error, that is the difference between calculated model inflows and outflows at the completion of the transient calibration, is less than 0.01 % (**Table 3-6**).

The water balance timeseries show the evolution of fluxes with time for each component of the water balance. The relationship between rainfall, evapotranspiration and storage - out is apparent, with period of large rainfall leading to an increase in storage out (water being stored into the aquifer matrix) and evapotranspiration (as the water table rises). Conversely, period of lower rainfall led to increase in storage in (water being released from the aquifer matrix) (**Figure 3-14**).

Table 3-6 Water Balance – Transient Calibration Period Average (Best Calibrated Model)

Component	Inflow (ML/day)	Percent of Total Inflow (%)	Outflow (ML/d)	Percent of Total outflow (%)
Recharge	9.86	80.88	-	
Evapotranspiration (ET)	-	-	8.66	71.06
SW/GW Interaction Minor Rivers (RIV)	0.00	0.00	0.00	0.00
Regional GW flow (GHB)	0.01	0.12	1.55	12.75
Mines (DRN)	-	-	0.00	0.00
Well	0.00	0.00	0.003	0.03
Storage	2.32	19.00	1.97	16.17
Total	12.19	100.00	12.19	100.00
Recharge (direct rainfall)	12.19	100.00	12.19	100.00



Figure 3-14 Transient Water Balance Timeseries – Calibration Period

3.5.2 Calibrated Hydraulic Parameters

Calibrated hydraulic parameters are presented in **Table 3-7**. The calibrated hydraulic properties are shown for the calibrated ensemble and best calibrated model on **Table 3-7**. It includes calibrated values for horizontal hydraulic conductivity (Kx) and vertical to horizontal hydraulic conductivity ratio (Kzf = Kz/Kx), Ss, and Sy. Calibrated distribution for the ensemble is presented in **Appendix A.**

Table 3-7 Calibrated Hydraulic Parameters

Hydraulic Property	Description	Unit	Max Ensemble[1]	Min Ensemble[1]	Mean Ensemble[1]	Mean Best Calibrated[1]
kx_1	Unconsolidated Sediment	m/d	0.67	0.31	0.45	0.48
kx_2	Regolith	m/d	0.84	0.28	0.69	0.77
kx_3	Tabba Tabba Shear zone upper	m/d	2.51	0.53	1.34	1.41
kx_4	Tabba Tabba Shear zone middle	m/d	0.31	0.09	0.21	0.11
kx_5	Tabba Tabba Shear zone lower	m/d	0.08	0.03	0.06	0.05
kx_6	Fractured rock upper	m/d	0.13	0.02	0.08	0.04
kx_7	Fractured rock middle	m/d	0.07	0.01	0.04	0.03
kx_8	Fractured rock lower	m/d	0.03	0.0025	0.01	0.003
kx_9	Granite Upper	m/d	0.002	0.0006	0.001	0.001
kx_10	Granite Middle	m/d	0.003	0.0007	0.001	0.001
kx_11	Granite Lower	m/d	0.001	0.0002	0.001	0.001
kx_12	Dolerite Dyke	m/d	0.66	0.06	0.41	0.10
kzf_1	Unconsolidated Sediment	_	0.05	0.05	0.05	0.05
kzf_2	Regolith	_	0.05	0.05	0.05	0.05
kzf_3	Tabba Tabba Shear zone upper	_	0.11	0.06	0.07	0.06
kzf_4	Tabba Tabba Shear zone middle	_	0.09	0.06	0.07	0.07
kzf_5	Tabba Tabba Shear zone lower	_	0.07	0.05	0.05	0.05
kzf_6	Fractured rock upper	_	0.09	0.06	0.07	0.07
kzf_7	Fractured rock middle	_	0.07	0.01	0.05	0.05
kzf_8	Fractured rock lower	_	0.06	0.004	0.03	0.04
kzf_9	Granite Upper	_	0.05	0.05	0.05	0.05
kzf_10	Granite Middle	_	0.01	0.002	0.01	0.01
kzf_11	Granite Lower	_	0.01	0.002	0.01	0.01
kzf_12	Dolerite Dyke	_	0.22	0.07	0.10	0.10
sy_1	Unconsolidated Sediment	_	0.06	0.05	0.06	0.06
sy_2	Regolith	_	0.03	0.02	0.03	0.03
sy_3	Tabba Tabba Shear zone upper	_	0.01	0.002	0.01	0.004

Hydraulic Property	Description	Unit	Max Ensemble[1]	Min Ensemble[1]	Mean Ensemble[1]	Mean Best Calibrated[1]
sy_4	Tabba Tabba Shear zone middle	_	0.01	0.002	0.01	0.01
sy_5	Tabba Tabba Shear zone lower	_	0.01	0.001	0.004	0.01
sy_6	Fractured rock upper	_	0.01	0.002	0.01	0.01
sy_7	Fractured rock middle	_	0.01	0.003	0.01	0.01
sy_8	Fractured rock lower	_	0.003	0.001	0.002	0.002
sy_9	Granite Upper	_	0.003	0.001	0.002	0.003
sy_10	Granite Middle	_	0.003	0.001	0.003	0.002
sy_11	Granite Lower	_	0.003	0.001	0.002	0.002
sy_12	Dolerite Dyke	_	0.01	0.001	0.01	0.005
ss_1	Unconsolidated Sediment	m-1	6.4E-06	1.6E-06	3.3E-06	2.6E-06
ss_2	Regolith	m-1	8.0E-06	2.0E-06	5.9E-06	5.3E-06
ss_3	Tabba Tabba Shear zone upper	m-1	1.9E-07	1.6E-07	1.7E-07	1.7E-07
ss_4	Tabba Tabba Shear zone middle	m-1	1.8E-07	1.5E-07	1.6E-07	1.6E-07
ss_5	Tabba Tabba Shear zone lower	m-1	1.9E-07	1.6E-07	1.8E-07	1.9E-07
ss_6	Fractured rock upper	m-1	1.9E-07	1.6E-07	1.8E-07	1.8E-07
ss_7	Fractured rock middle	m-1	1.8E-07	1.6E-07	1.7E-07	1.7E-07
ss_8	Fractured rock lower	m-1	1.9E-07	1.6E-07	1.8E-07	1.8E-07
ss_9	Granite Upper	m-1	1.9E-07	1.6E-07	1.7E-07	1.8E-07
ss_10	Granite Middle	m-1	1.9E-07	1.6E-07	1.8E-07	1.8E-07
ss_11	Granite Lower	m-1	1.9E-07	1.6E-07	1.7E-07	1.7E-07
ss_12	Dolerite Dyke	m-1	1.9E-07	1.6E-07	1.8E-07	1.8E-07

[1] Values provided are for each zone, prior pilot point multiplier. They provide a good approximation of the ensemble range but are not the true min, mean or max value at any cell within that zone.

3.5.3 Calibrated Boundary Conditions

Table 3-8 provides the long-term average rainfall recharge rate in mm/yr for each zone and for reference the equivalent recharge percentage of long-term average rainfall is also provided (**Table 3-9**). The overall recharge rate was calibrated at 1.7 % of rainfall over the entire model, with larger infiltration calibrated for the Tabba Tabba shear zone (6.1 %) and the creeks (7.1 %), and lower infiltration for the rest of the model (1.3 %). This is in line with the conceptual model (refer to **Section 1.3**).

Table 3-8 Calibrated Recharge Rates (mm/year)

Outcropping Unit	Min (Ensemble)	Max (Ensemble)	Mean (Ensemble)	Best Calibrated Model
Shear zone	65.6	3.3	15.6	19.2
Creek Zone	65.6	5.6	22.4	22.5
Rest Of the model	11.6	1	4.4	4

Table 3-9 Calibrated Recharge Rates (% Rainfall)

Outcropping Unit	Min (Ensemble)	Max (Ensemble)	Mean (Ensemble)	Best Calibrated Model
Shear zone	20.8%	1.1%	5.0%	6.1%
Creek Zone	20.8%	1.8%	7.1%	7.1%
Rest Of the model	3.7%	0.3%	1.4%	1.3%

3.5.3.1 Evapotranspiration

Table 3-10 and **Table 3-11** shows the calibrated ET rates and extinction depth respectively, for different zones in the model. It is noted that the calibrated EVT rates are applied at the model surface. The actual EVT outflow from each cell is computed using a linear interpolation between the surface rate and extinction depth, based on the simulated water table position within the cell.

Table 3-10 Calibrated Evapotranspiration Rates (mm/year)

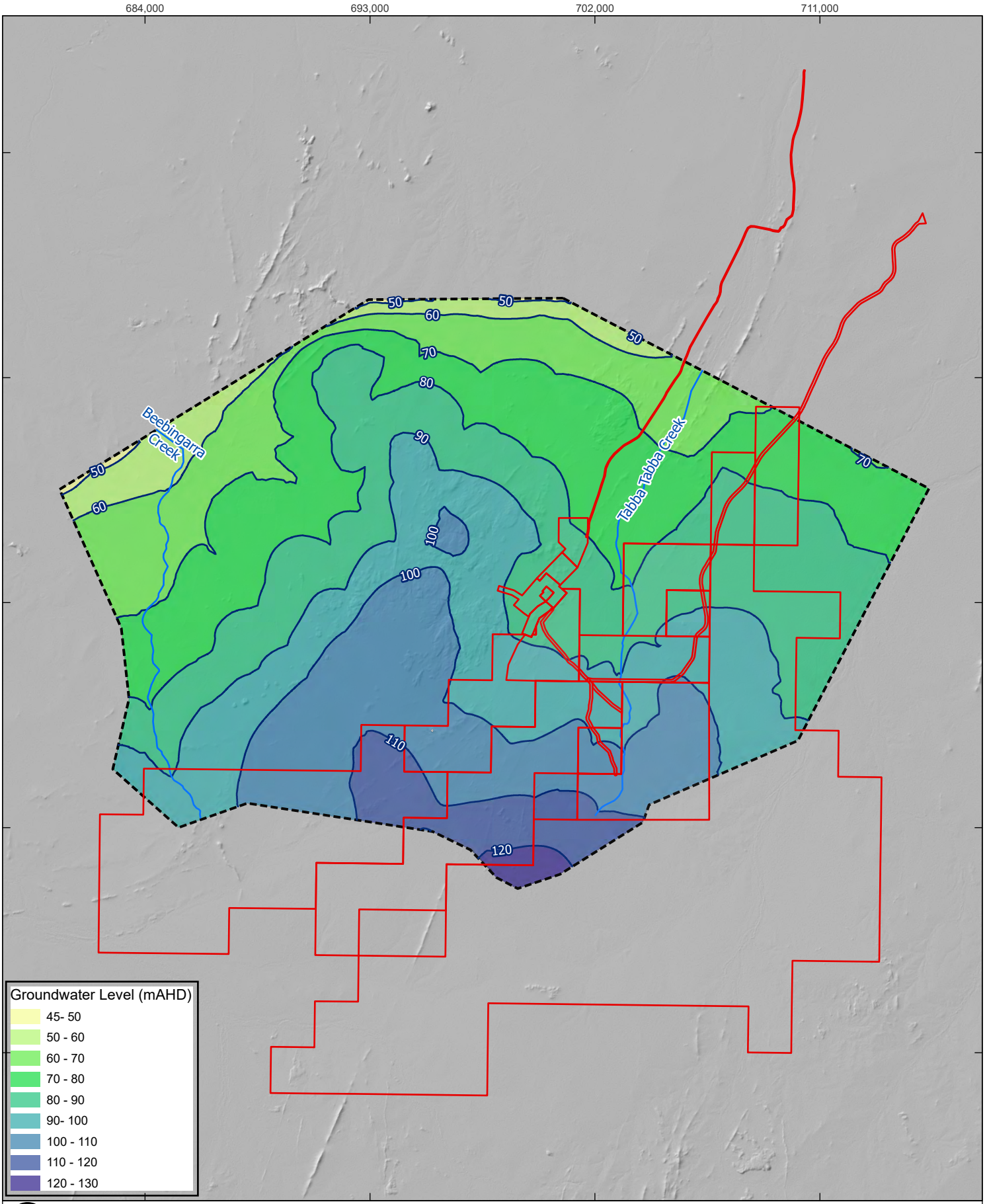
Zone	Min (Ensemble)	Max (Ensemble)	Mean (Ensemble)	Best Calibrated Model
1	2760.2	2005.4	2463.3	2331.0
2	2698.3	1835.9	2316.8	2392.9
3	2462.1	1701.1	1911.7	1954.2

Table 3-11 Calibrated Evapotranspiration Extinction Depth (m)

Zone	Min (Ensemble)	Max (Ensemble)	Mean (Ensemble)	Best Calibrated Model
1	11.24	2.45	7.67	8.35
2	8.35	2.77	6.68	2.91
3	3.92	0.98	2.81	1.38

3.5.4 Calibrated Water Table Elevation

The calibrated water table elevation (which is defined here as the upper surface of groundwater, marking the level below which the soil or rock is fully saturated with water) is presented for the steady state period (**Figure 3-15**) and at the end of the calibration period (**Figure 3-16**).



0 1 2 km

Coordinate System:	GDA 1994 MGA Zone 50
Scale:	1:200,000 at A4
Project Number:	620.042733
Date Drawn:	18-May-2026
Drawn by:	DC

LEGEND

- Major Drainage System
- Groundwater Level Contour (mAHD)
- Model Boundary
- Mining Tenements

TABBA TABBA LITHIUM MINE PROJECT, GROUNDWATER MODELLING TECHNICAL REPORT

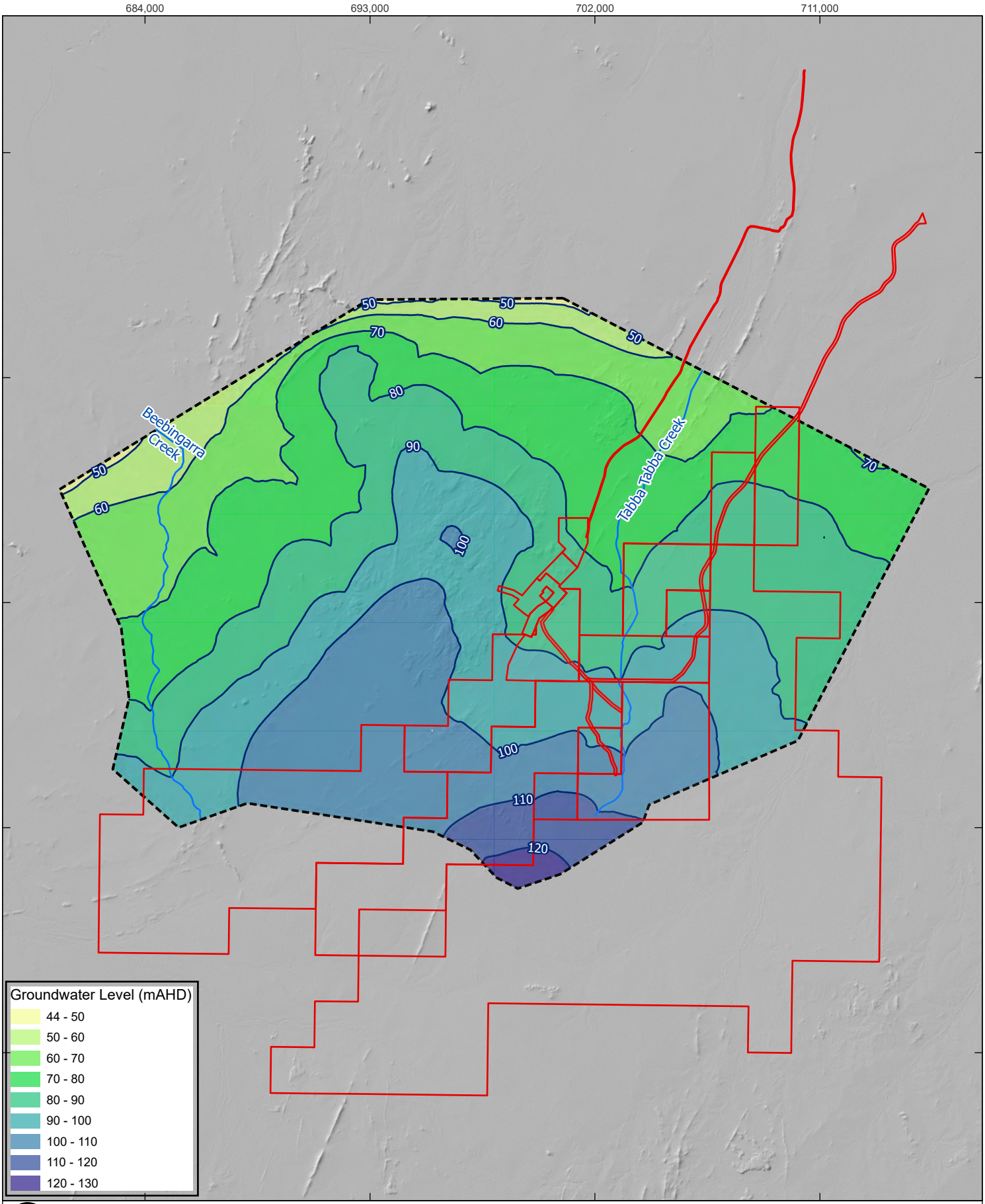
CALIBRATED WATER TABLE ELEVATION, STEADY STATE PERIOD

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FIGURE 3-15

Path: H:\Local Resources\Mining Advisory\ADVGIS\03-Projects\Australia-WA\TabbaTabbaLithium\ADVAU00796\01-ESRI\ADVAU00796.aprx\GW - Figure 3-15 Calibrated Water Table Elevation, Steady State Period



0 1 2 km

Coordinate System:	GDA 1994 MGA Zone 50
Scale:	1:200,000 at A4
Project Number:	620.042733
Date Drawn:	18-May-2026
Drawn by:	DC

LEGEND

- Major Drainage System
- Groundwater Level Contour (mAHD)
- Mining Tenements
- Model Boundary

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CALIBRATED WATER TABLE ELEVATION - END OF CALIBRATION

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FIGURE 3-16

Path: H:\Local Resources\Mining Advisory\ADVGIS\03-Projects\Australia-WA\TabbaTabbaLithium\ADVAU00796\01-ESRI\ADVAU00796.aprx\GW - Figure 3-16 Calibrated Water Table Elevation - End of Calibration

4.0 Model Predictions

4.1 Predictive Model Setup

The calibration model presented in **Section 2.0** was used to develop a predictive model (i.e. an extension of the calibration model). This section details the development of the predictive model.

4.1.1 Timing

The model timing was extended from the calibration model to include both mining (2026 – 2040) and post-mining (2041 – 2500) periods (**Table 4-1**).

Table 4-1 Predictive Model Timing

Stress Periods	Predictive Period	Date Start	Date End	Stress Period Length (day)	Max Time Step length (day)
123 - 137	Mining	03 - 2026	12 - 2040	306 to 365.25	365.25
138 - 186	Post Mining	01 - 2041	12 - 2500	365.25 to 36,525	365.25

4.1.2 Rainfall and Evapotranspiration

Long term rates of rainfall and evapotranspiration have been applied to the predictive stress periods (as per stress period 2 of the calibration model).

4.1.3 Predictive Scenarios

Two predictive scenarios are developed to assess the impact of the project:

1. No mining scenario: In this scenario, there is no groundwater abstraction or mining activity.
2. Project: This scenario includes the mines, water abstraction and waste rock dump.

The following **Sections 4.1.4** to **4.1.7** detail the development of the “Project” model.

4.1.4 Mine Dewatering

4.1.4.1 Mining

The MODFLOW Drain (DRN) package is used to simulate mine dewatering in the model for all mines. Boundary conditions for drain cells allow one-way flow of water out of the model. When the computed head drops below the stage elevation of the drain, the drain cells become inactive. This is an effective way of theoretically representing removal of water seeping into a mine over time, with the actual removal of water being via pumping and evaporation.

To simulate the open cut mine, drain cells are applied to all active layers from the surface to the base of the mine target elevation, with the drain elevation equal to the base of the layer (if the mine extends below that layer) or to the base of the mine (if the mine does not extend below that layer).

To simulate the underground mine, drain cells are applied to the layer(s) intersected by the mine, with the drain elevation equal to the base of the layer (if the mine extends below that layer) or to the base of the mine (if the mine does not extend below that layer).

4.1.4.2 Post Mining

Drain cells are deactivated following mining cessation, allowing water level to progressively recover in the previously drained cells.

4.1.5 Water Supply Bores

4.1.5.1 Mining

Water supply bores are required to provide additional water supply to reach the mine requirements of 6GL per year. Water supply bores are simulated using the WEL package, as described in **Section 2.5.5.1**.

Bore locations and depths have been selected as part of scenario testing. A total of 47 bores, screened from layer 1 to 7 have been simulated.

4.1.5.2 Post Mining

Water supply bores are assumed to be only required during active mining and are deactivated during the post mining period.

4.1.6 Variation in Hydraulic Properties due to Mining

4.1.6.1 Mining

During mining, the hydraulic conductivity of the mined cells is changed to “air properties” using the Time-variant materials (TVM) package of MODFLOW-USG Transport.

4.1.6.2 Post Mining

Post mining, the changed hydraulic conductivity for the mined cells is conserved and storage is also changed to “air properties”.

Table 4-2 Changed Hydraulic Properties (TVM)

Property	Open Pit	Underground
Kx (m/d)	1000	100
Ky (m/d)	1000	100
Sy (-)	1	0.3
Ss (m^{-1})	$5x10^{-6}$	$1x10^{-5}$

4.1.7 Variation in Recharge and EVT due to Mining

4.1.7.1 Post Mining

After cessation of mining, recharge and EVT are changed to simulate:

- **Final void**: Recharge is increased to 100% of rainfall while EVT is set at 75% of potential evapotranspiration. This changed allow simulating the post mining lake formation in the final void, due to rainfall, evaporation and groundwater fluxes.
- **Waste Rock Dump (WRD)**: The effect of the WRD on the groundwater system is simulated using an increase recharge over the WRD area. The recharge over the

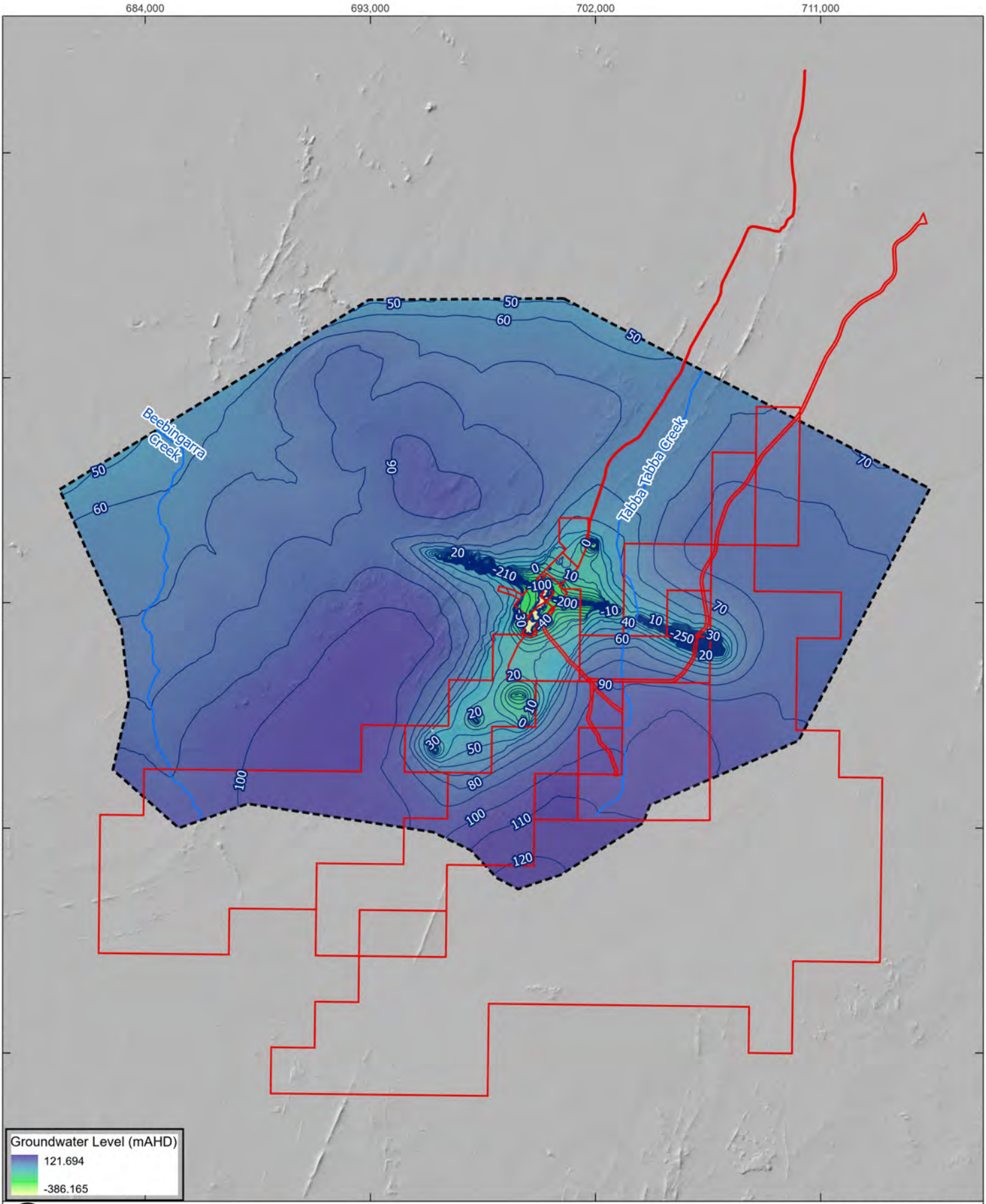
WRD was set at 5% rainfall. The evapotranspiration surface (i.e. elevation at which the EVT is active) was also changed to reflect the elevation of the WRD.

4.2 Predictive Model Results

4.2.1 Water Levels

At the end of mining, the water table elevation is depressed in the areas associated with the open pits, underground mine and bore extraction. The lowering of the water table is also visible along the dyke (**Figure 4-1**).

Post mining, lakes progressively form in the three open pits. The lake level is a function of inflows and outflows to the lake (see **Section 4.2.4**). Due to evaporation being much greater than rainfall, the lake elevation in the main pit remains significantly lower than the regional water table. Thus, main pit act as a “sink” feature, with groundwater flow toward main pit (**Figure 4-2**).



Coordinate System:	GDA 1994 MGA Zone 50
Scale:	1:200,000 at A4
Project Number:	620.042733
Date Drawn:	5/19/2026
Drawn by:	DC

LEGEND

- Major Drainage System
- Groundwater Level Contour (mAHD)
- Mining Tenements
- Model Boundary

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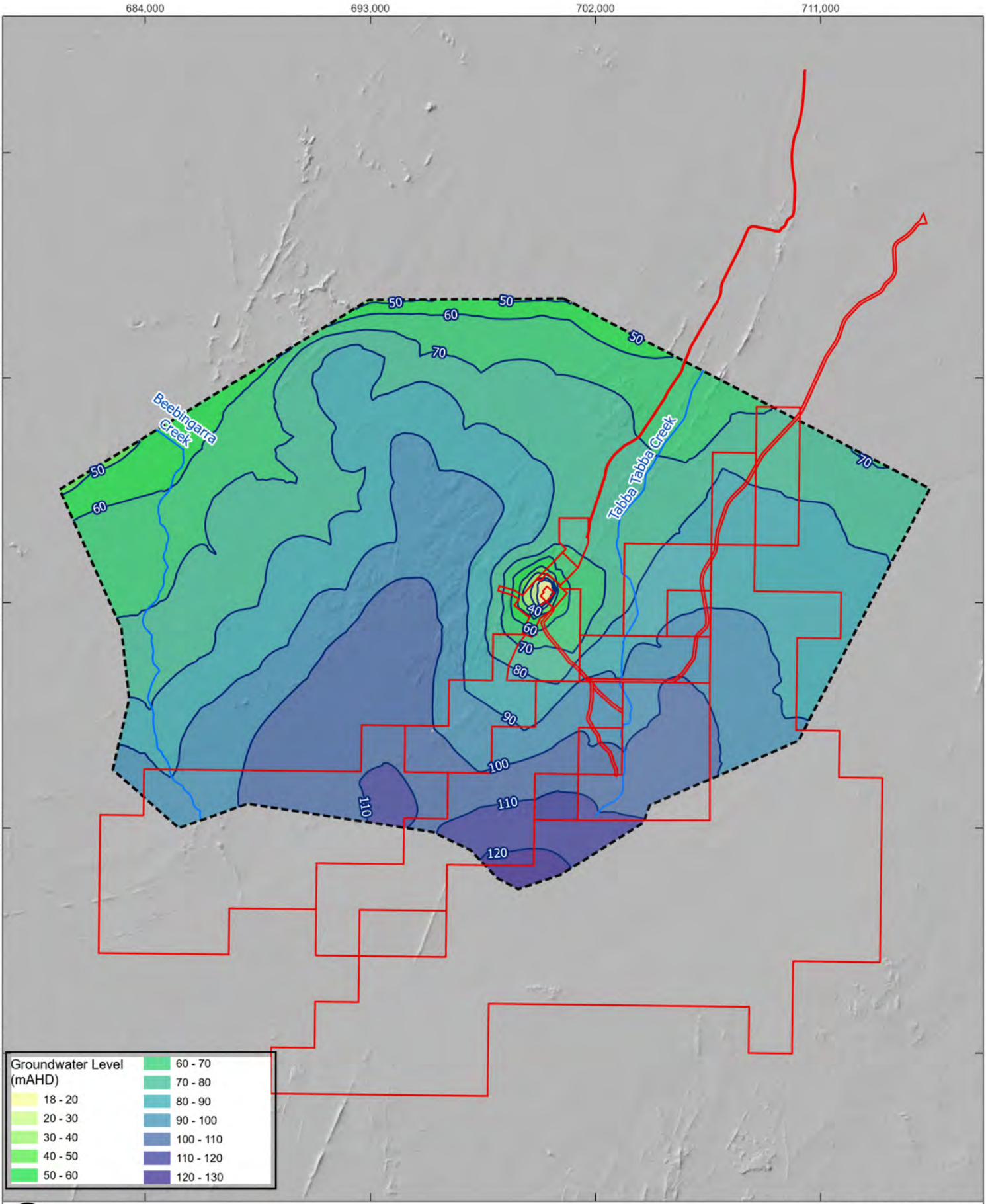
WATER TABLE ELEVATION – END OF MINING

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FIGURE 4-1

Path: H:\Local Resources\Mining Advisory\ADVGIS\03-Projects\Australia-WA\TabbaTabbaLithium\ADVAU00796\01-ESRI\ADVAU00796.aprx\GW - Figure 4 1 Water Table Elevation – End of Mining



0 1 2 km

Coordinate System:	GDA 1994 MGA Zone 50
Scale:	1:200,000 at A4
Project Number:	620.042733
Date Drawn:	5/19/2026
Drawn by:	DC

LEGEND

- Major Drainage System
- Groundwater Level Contour (mAHD)
- Mining Tenements
- Model Boundary

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WATER TABLE ELEVATION – POST MINING EQUILIBRIUM

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FIGURE 4-2

Path: H:\Local Resources\Mining Advisory\ADVGIS\03-Projects\Australia-WA\TabbaTabbaLithium\ADVAU00796\01-ESRI\ADVAU00796.aprx\GW - Figure 4 2 Water Table Elevation – Post Mining Equilibrium

4.2.2 Mine Induced Drawdown

Drawdown induced by the mining activity, which include the open pit mines, the underground mine and the water supply bores, is calculated as the differential between the “no mining scenario” and the “Project’ scenario (refer to **Section 4.1.2**).

Drawdown is estimated as:

- Maximum drawdown: The maximum drawdown simulated at any time during the mining and post mining periods;
- Transient drawdown: Drawdown assessed at a specific time, and;
- Residual drawdown: Drawdown at the end of the post mining period (i.e. at post mining equilibrium).

4.2.2.1 Maximum Drawdown

The maximum water table drawdown (1 m drawdown) extends more than 20 km in the alignment of Tabba Tabba Creek and 19 km along the dyke (**Figure 4-3**). The greater magnitude of drawdown is simulated within the dyke area, with estimated drawdown greater than 200 m. Drawdown greater than 100 m is limited to the mine, the dyke and the borefield. The 50 m drawdown contour is essentially limited to the mine development envelope and the dyke (**Figure 4-3**).

4.2.2.2 Transient Drawdown

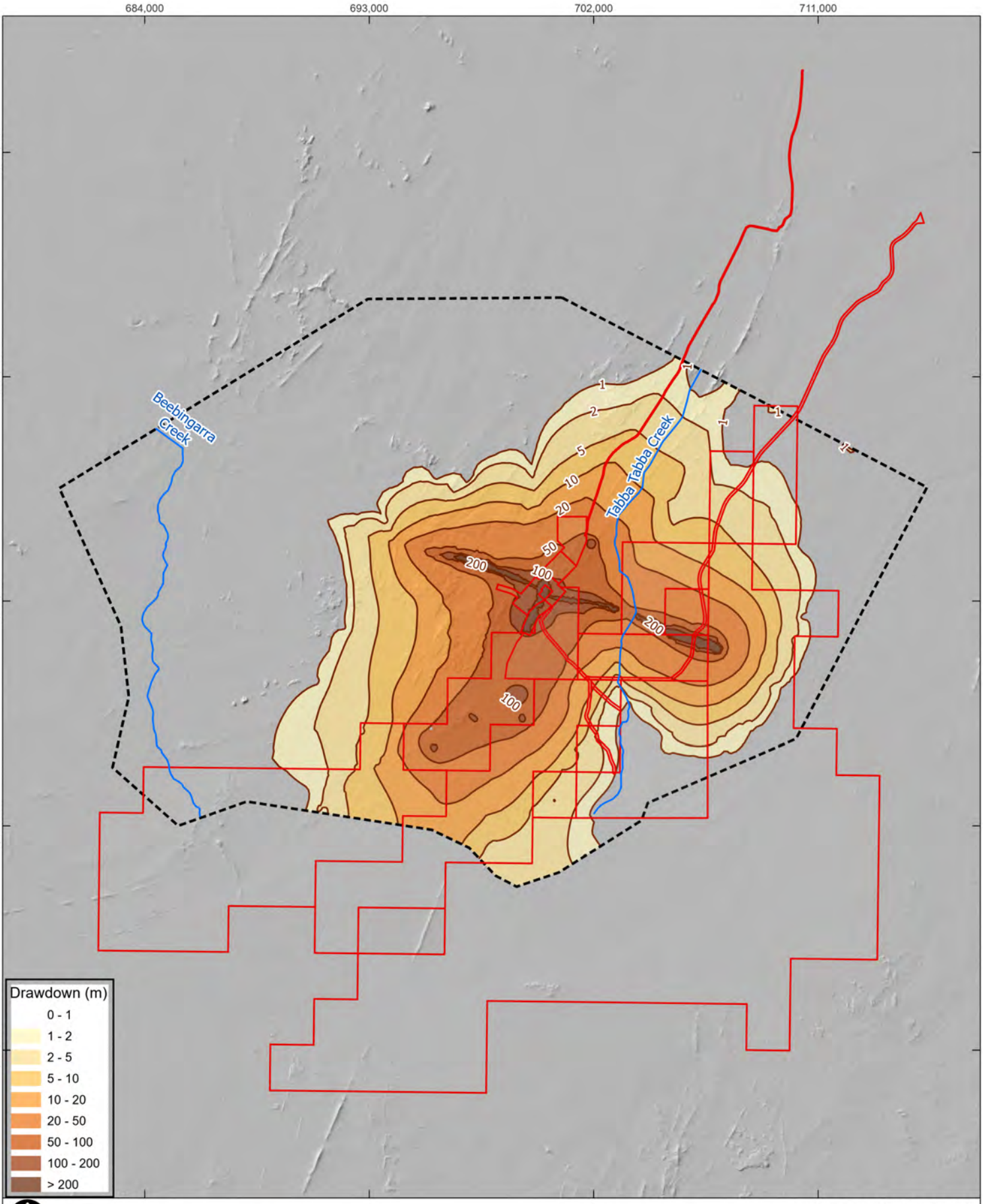
Transient drawdown was assessed at the end of the following mining year:

- Mining year 1 (**Figure B1**, **Appendix B**)
- Mining year 5 (**Figure B2**, **Appendix B**)
- Mining year 10 (**Figure B3**, **Appendix B**)
- Mining year 14 (**Figure B4**, **Appendix B**)

Drawdown first develop around the mine and southern borefields (**Figure B1**, **Appendix B**). By mining year 5, the drawdown is near maximum drawdown (**Figure B2**, **Appendix B**). From year 5 to the end of mining (year 14), the drawdown only expands marginally along the dyke and the Tabba Tabba shear zone (**Figures B3 and B4**, **Appendix B**).

4.2.2.3 Residual Drawdown

The 1 m residual water table drawdown contour extends for 18 km in the alignment of Tabba Tabba Creek and 8 km along the dyke. Drawdown greater than 50m is limited to the main final void. The residual drawdown contour reduces to less than 10 m approximately 2 km away from the main final void (**Figure 4-4**).



Coordinate System:	GDA 1994 MGA Zone 50
Scale:	1:200,000 at A4
Project Number:	620.042733
Date Drawn:	5/19/2026
Drawn by:	DC

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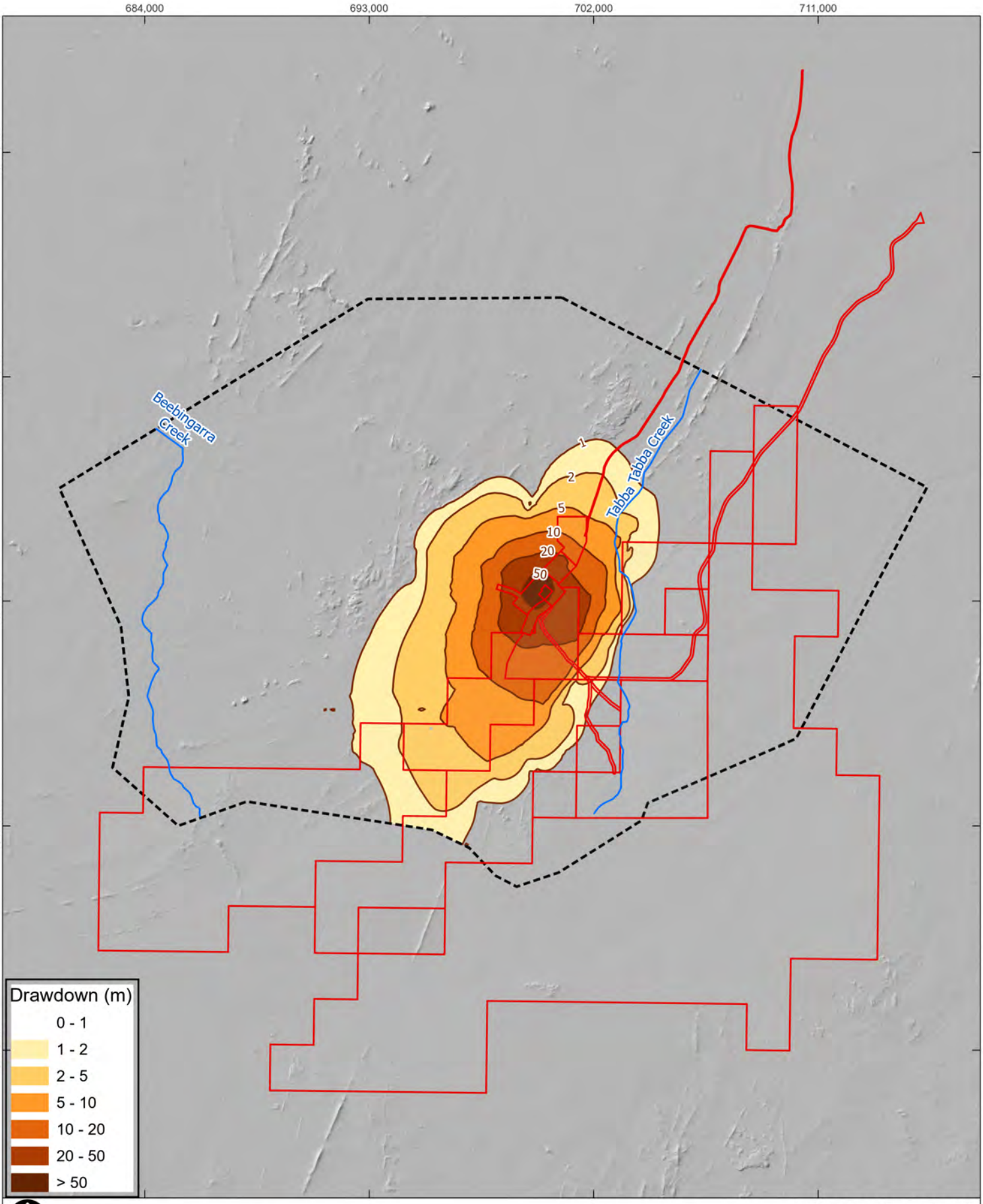
MAXIMUM WATER TABLE DRAWDOWN

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FIGURE 4-3

Path: H:\Local Resources\Mining Advisory\ADVGIS\03-Projects\Australia-WA\TabbaTabbaLithium\ADVAU00796\01-ESRI\ADVAU00796.aprx\GW - Figure 4 3 Maximum Water table Drawdown



LEGEND

- Major Drainage System
- Drawdown Contour (m)
- Mining Tenements
- Model Boundary

Coordinate System:	GDA 1994 MGA Zone 50
Scale:	1:200,000 at A4
Project Number:	620.042733
Date Drawn:	5/19/2026
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RESIDUAL WATER TABLE DRAWDOWN

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FIGURE 4-4

Path: H:\Local Resources\Mining Advisory\ADVGIS\03-Projects\Australia-WA\TabbaTabbaLithium\ADVAU00796\01-ESRI\ADVAU00796.aprx\GW - Figure 4 4 Residual Water Table Drawdown

4.2.2.4 Residual Drawdown

4.2.3 Groundwater Take

Groundwater take includes inflow to the open pit mines, the underground mine and abstraction at the water supply bores. The simulated groundwater take indicates that the mine inflow will peak in 2030 at 0.6 GL/y. The total extracted volume of groundwater is simulated to be approximately 5.5 GL/y for the first 6 years of mining, before progressively decreasing to 3 GL/year by the end of mining (**Figure 4-5**).

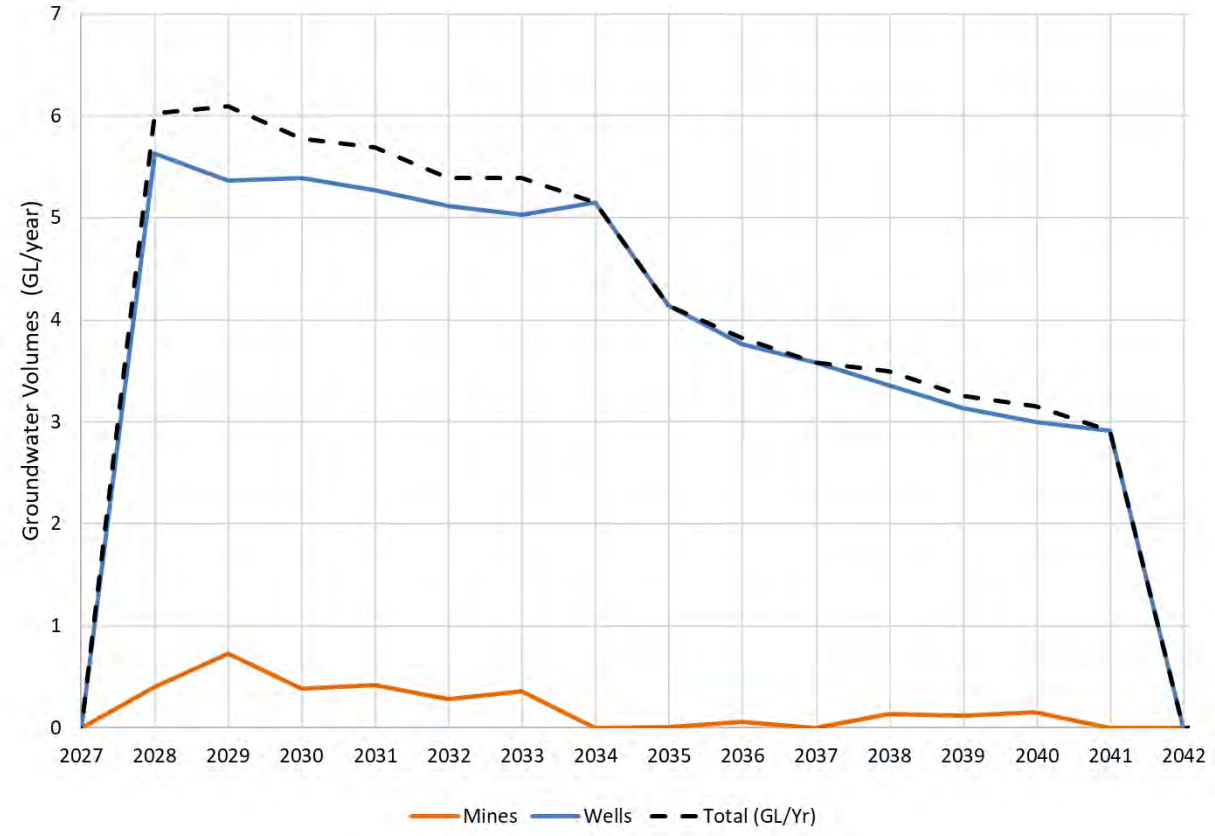


Figure 4-5 Total Extracted Groundwater (GL/y)

4.2.4 Final Void Equilibrium

4.2.4.1 Final Void Lake Elevation

Post mining, final void lake develops and reach an equilibrium driven by fluxes to the voids (rainfall and groundwater inflows) and outflow (Evaporation). As described in **Section 7.2**, final void modelling was simulated within the groundwater model to provide an indicative lake equilibrium level. Additional water balance modelling will be required to properly assess the final void lake elevation and any potential for seasonal overtopping.

At the main pit, the pit lakes reach an equilibrium level of 19 mAHD, which is 73 m below spill level. Equilibrium level is reached approximately 400 years post mining.

At the Hutt pit, the pit lakes reach an equilibrium level of 64 mAHD, which is 32 m below spill level. Equilibrium level is reached approximately 300 years post mining.

At the Han pit, the pit lakes reach an equilibrium level of 53 mAHD, which is 43 m below spill level. Equilibrium level is reached approximately 400 years post mining (**Figure 4-6**).

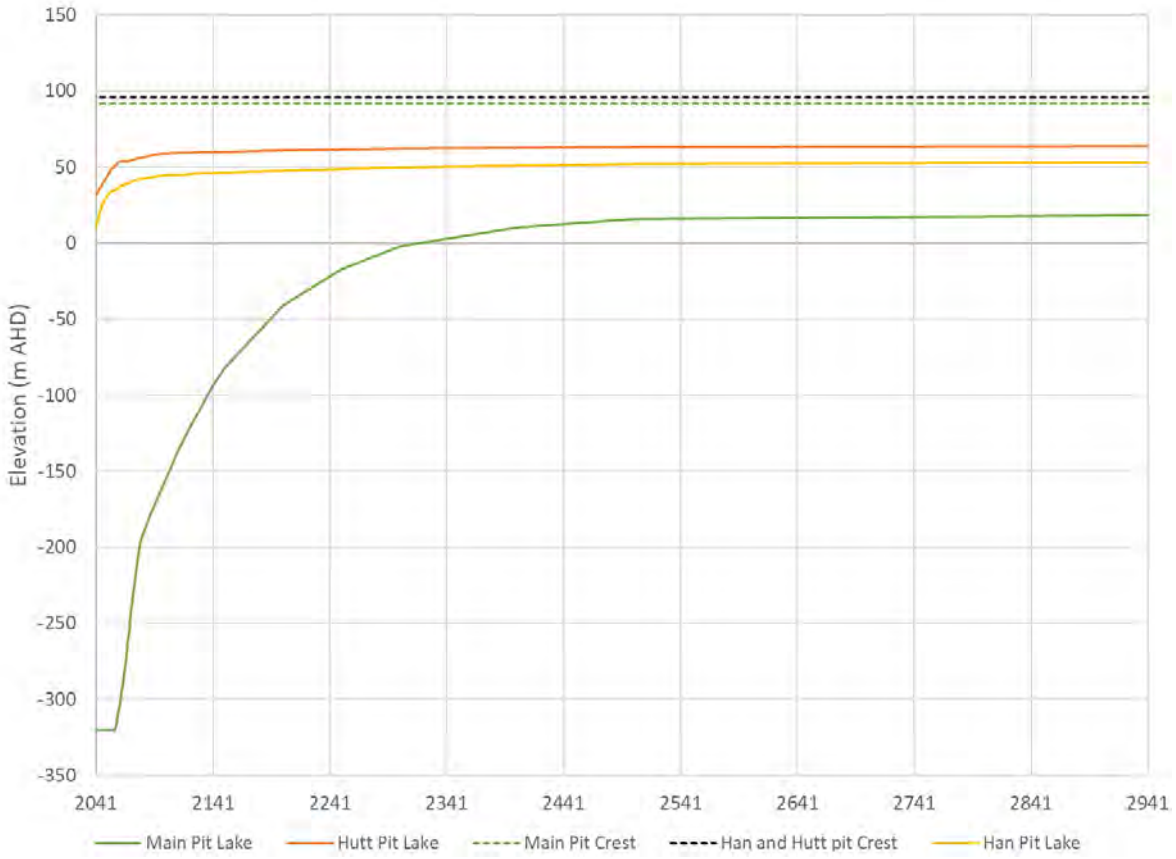


Figure 4-6 Final Void Lake Levels

5.0 Sensitivity Analysis

5.1 Sensitivity Analysis

5.1.1 Purpose

Quantifying the sensitivity of both calibration performance and model predictions to input parameters provides critical insight into model behaviour and uncertainty. The combined sensitivity analysis presented in this section supports two primary objectives:

1. **Assessing parameter conditioning through calibration sensitivity**: Parameters that have a strong influence on calibration performance metrics are more likely to be conditioned by the calibration process. In contrast, parameters with low sensitivity to calibration performance are less likely to be conditioned by the calibration process, meaning that their posterior distributions will likely remain broad regardless of the amount or quality of calibration data.
2. **Understanding prediction sensitivity to parameter uncertainty**: When model predictions are highly sensitive to specific parameters, it indicates that uncertainties in those parameters have a strong influence on predictive outcomes. Conversely, if predictions are insensitive to a given parameter, then uncertainty in that parameter has limited influence on the modelled forecast.

Comparing calibration and prediction sensitivity allows for distinguishing between parameters that are constrained during calibration, and parameters that drive predictive uncertainty, which may or may not overlap. Such insights support decision-making in model refinement, data collection prioritisation, and risk-based scenario analysis.

5.1.2 Methodology

To evaluate how variations in model parameters affect calibration and prediction outcomes, SLR employed two complementary global sensitivity analysis methods:

- Spearman rank correlation.
- Standardised linear regression coefficients.

These two methods assess different aspects of the input–output relationship and are well-suited to the often non-linear and complex behaviour of hydrogeological systems. They are commonly used in hydrological and environmental modelling due to their simplicity, interpretability, and relatively low computational demand (Saltelli et al., 2008; Pianosi et al., 2016).

5.1.2.1 Data Aggregation and Standardisation

Parameter and observation data were pre-processed and standardised. Parameters using a log normal distribution were converted to log 10 values.

Calibration performance was represented by Phi (sum of squared residuals) for head targets. For predictive sensitivity, predictive data included three groups: total area with drawdown > 1 m, total mine groundwater inflow (active mining) and total well abstraction.

Parameter values (one group), calibration data (one group) and prediction data (three groups) were standardised (zero mean, unit variance) independently (i.e. per group) to enable consistent comparison across variables and groups.

5.1.2.2 Spearman Rank Correlation Coefficient

Spearman rank correlation measures the monotonic relationship between input parameters and model outputs. It identifies whether changes in a parameter consistently increase or decrease a model output, regardless of the exact functional form of the relationship. This is especially useful in groundwater models where non-linearities are common due to boundary conditions, storage terms, or non-linear recharge responses (van Griensven et al., 2006).

Given a parameter vector X and a model response vector Y, Spearman's rank correlation coefficient ρ is calculated as:

$$\rho = 1 - \frac{6\sum_{i=1}^{n}(R_i - S_i)^2}{n(n^2-1)}$$

Where:

- R_i is the rank of parameter X for sample *i*.
- S_i is the rank of the corresponding model output Y.
- *n* is the number of realisations.

5.1.2.3 Linear Regression Sensitivity Coefficient

Linear regression sensitivity quantifies how much the output changes *on average* with a unit change in a parameter, assuming a linear relationship. It describes the *magnitude* of influence a parameter has on model outputs under the assumption of a linear relationship.

The relationship is represented as:

$$Y = X\beta + \epsilon$$

Where:

- *Y* is the model output.
- *X* is a matrix of standardized parameter values.
- β is the vector of estimated sensitivity coefficients.
- ϵ is the model error.

The coefficient β represents the average change in model output (*Y*) for a one standard deviation change in model parameter (*X*) and is interpreted as a direct measure of sensitivity magnitude, specifically how the variance of the parameter uncertainty contributes to the variance of the predictive or calibration uncertainty. This method assumes linearity and additivity but remains useful as a first-order sensitivity metric (Helton et al., 2006).

5.1.2.4 Interpretation

There is no single universally accepted threshold for Spearman or regression coefficients in sensitivity analysis. However, some thresholds are often used as pragmatic benchmarks based on the practical significance of parameter influence rather than strict statistical cutoffs. For this analysis, moderate sensitivity was selected for an absolute ρ score greater than 0.2 and for an absolute β value greater than 0.1.

This dual-method framework supports robust sensitivity diagnostics by capturing both the consistency and strength of parameter influence. The combined use of both metrics enables us to distinguish between parameters that:

- have a strong and consistent effect;
- have an effect only in a narrow range (local sensitivity); or
- behave non-monotonically and inconsistently.

A comparison of the interpretive value of each method is provided in **Table 5-1**:

Table 5-1 Comparison of Spearman and Regression in Sensitivity Analysis

Sensitivity Scenario	Impact of Parameter Changes on Model Outcome	Spearman	Regression	Interpretation
S1	Strong, consistent linear effect	>0.2	>0.1	Parameter is influential and predictable
S2	Consistent but nonlinear effect	>0.2	<0.1	Parameter is influential but not well described by linear models
S3	Local or inconsistent effect	<0.2	>0.1	Large effect in a narrow range
S4	Non-influential	<0.2	<0.1	Parameter has minimal influence

5.1.3 Results

The results are presented as bar charts and discussed in **Section 5.1.3.1** for:

- Spearman rank correlation coefficient: hydraulic conductivity (**Figure 5-1**), storage parameters (**Figure 5-2**) and boundary conditions and spoil parameters (**Figure 5-3**).
- Linear regression sensitivity coefficient: hydraulic conductivity (**Figure 5-4**), storage parameters (**Figure 5-5**) and boundary conditions and spoil parameters (**Figure 5-6**).

5.1.3.1 Calibration Sensitivity (Parameter Conditioning)

Parameter with a ρ score greater than 0.2 and/or a β value greater than 0.1 (scenarios S1, S2 or S3 in **Table 5-1**) are likely to be conditioned through the calibration process.

As presented on **Figure 5-1** to **Figure 5-6**, the calibration process is likely to be conditioning the majority of parameters associated with zones that includes target heads. This is obvious for all the parameters associated with the Tabba Tabba shear zone, for the upper fractured rock aquifer, where the majority of the bores are located (Kx_z03 and Sy_z03). Some zones in direct hydraulic connection with these zones are also likely to be conditioned by the calibration process (e.g. Kx_z02, regolith). Conversely, zones that are completely disconnected from the zones associated with head targets are unlikely to be conditioned by the calibration process.

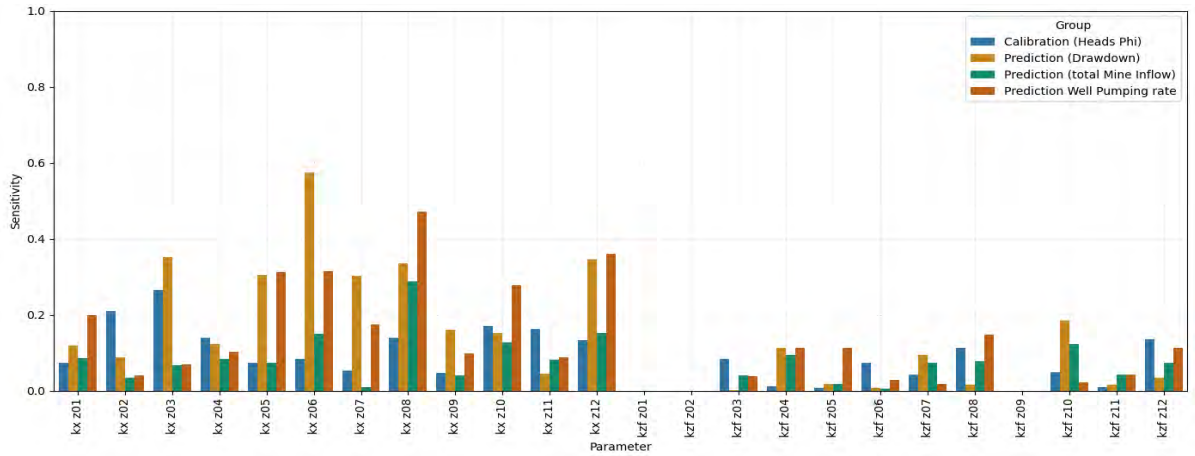


Figure 5-1 Spearman Rank Correlation Coefficient (Absolute Value) – Hydraulic Conductivity

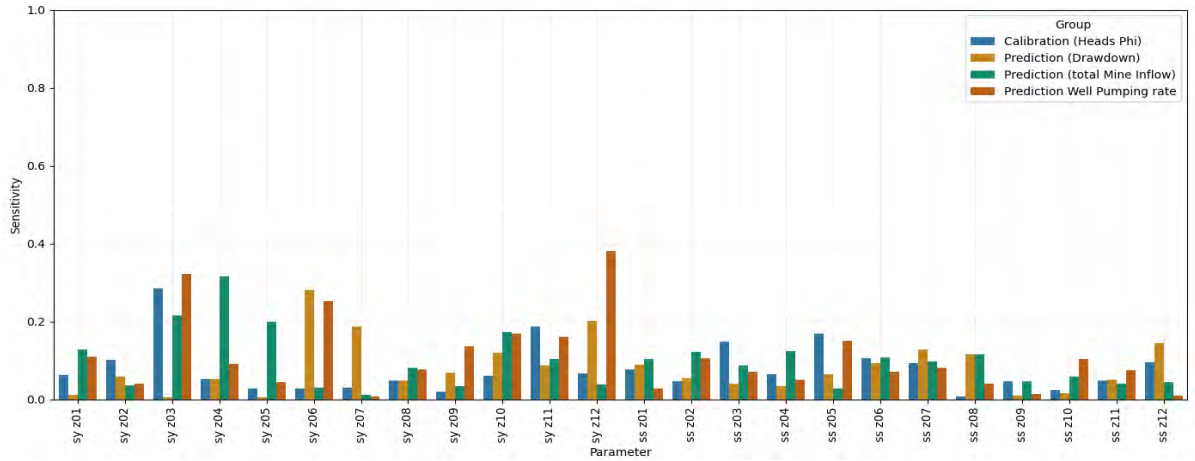


Figure 5-2 Spearman Rank Correlation Coefficient (Absolute Value) – Storage Parameters

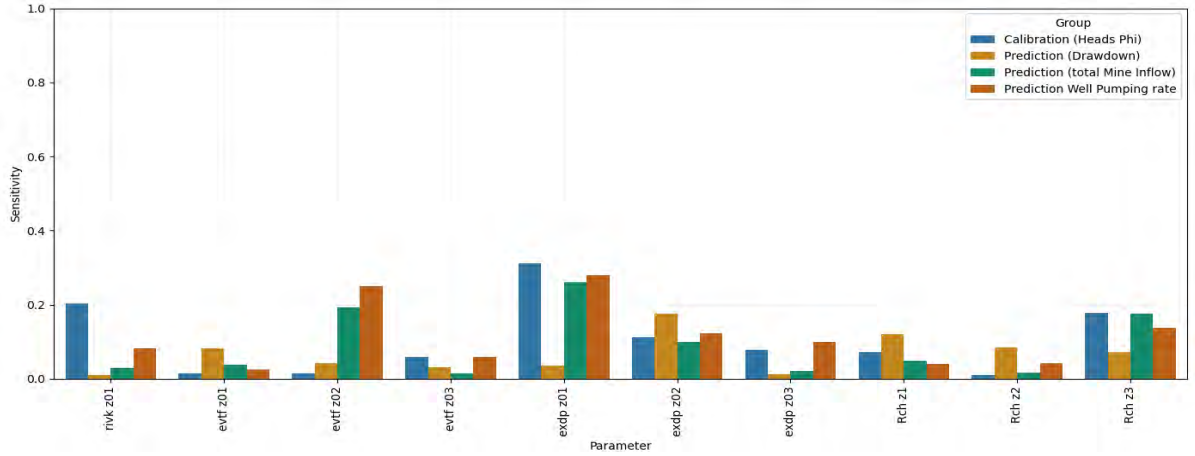


Figure 5-3 Spearman Rank Correlation Coefficient (Absolute Value) – Boundary Conditions

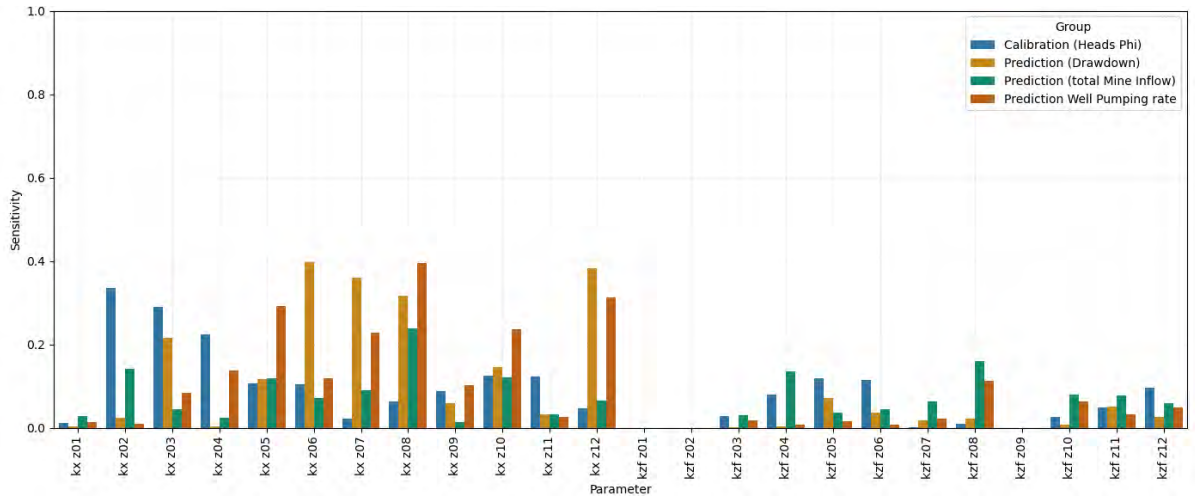


Figure 5-4 Linear Regression Sensitivity Coefficient (Absolute Value) – Hydraulic Conductivity

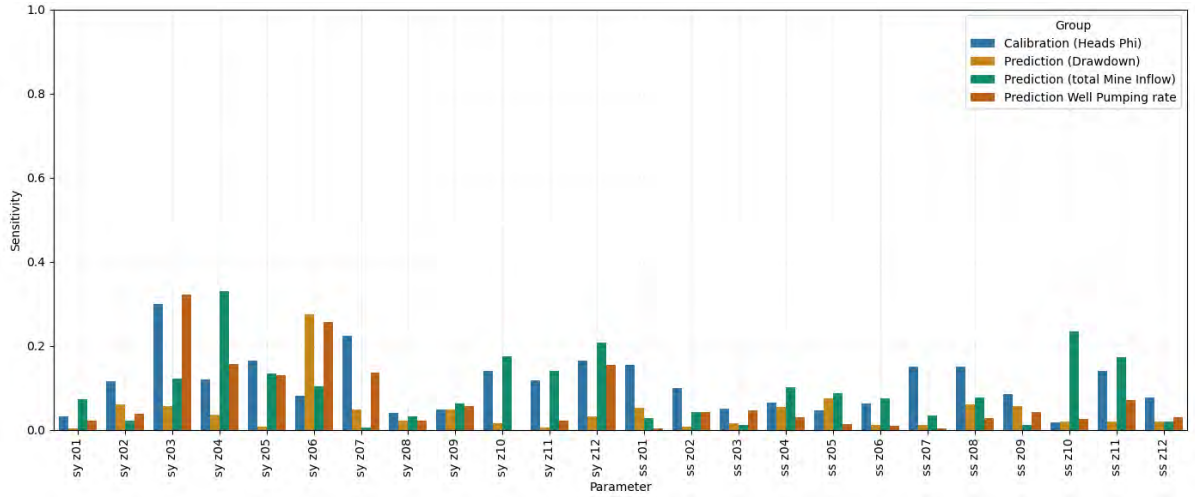


Figure 5-5 Linear Regression Sensitivity Coefficient (Absolute Value) – Storage Parameters

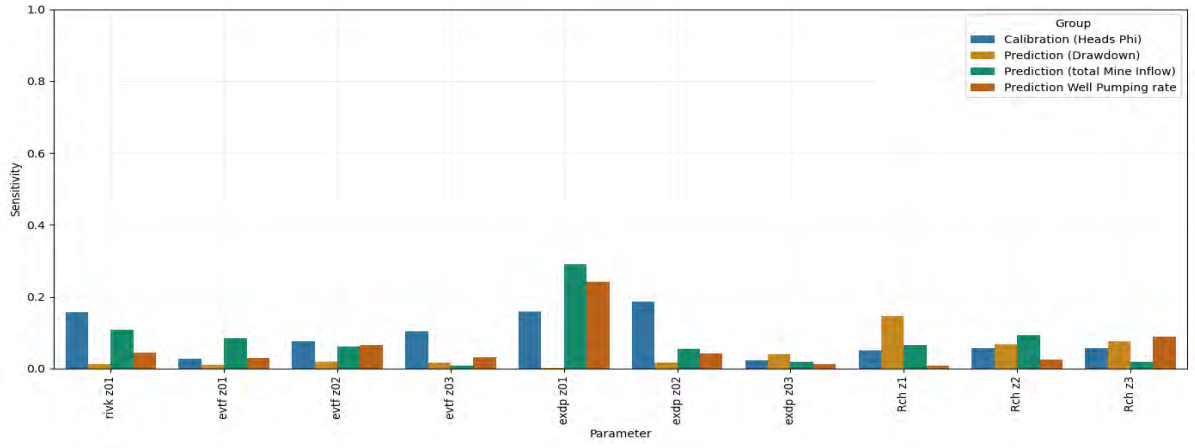


Figure 5-6 Linear Regression Sensitivity Coefficient (Absolute Value) – Boundary Conditions

5.1.3.2 Type I-IV Analysis

The Murray Darling Basin Modelling Guidelines (Murray Darling Basin Commission [MDBC], 2000) recommends classifying sensitivity by the resultant changes (or contribution) to the model calibration and predictions. According to this process models can be classified as one of the four main types:

- Type I: Insignificant changes to calibration (low calibration sensitivity) and prediction (low predictive sensitivity);
- Type II: Significant changes to calibration (high calibration sensitivity) – insignificant changes to predictions (low predictive sensitivity);
- Type III: Significant changes to calibration (high calibration sensitivity) –significant changes to predictions (high predictive sensitivity); and
- Type IV: Insignificant changes to calibration (low calibration sensitivity) –significant changes to predictions (high predictive sensitivity).

Types I-III are of less concern, as these Types have an insignificant impact on model predictions or conditioned by calibration. Type IV is classed as 'a cause for concern' as non-uniqueness in a model input might allow a range of valid calibrations but the choice of value impacts significantly on a prediction (MDBC, 2000).

To classify the sensitivity contribution to the model calibration and predictions for each model parameter, the calibration and prediction sensitivities were compared against each other for each parameter.

To allow comparing calibration and prediction sensitivity in one graph, a combined sensitivity value was calculated for each sensitivity group as:

$$\text{Combined}_{(i,g)} = 0.5 * |\beta_{(i,g)}| + 0.5 * |\rho_{(i,g)}|$$

where:

- $\beta_{(i,g)}$ is the standardised regression coefficient for parameter *i* and group *g*.
- $\rho_{(i,g)}$ is the Spearman rank correlation coefficient between parameter *i* and group *g*.

For this analysis, the threshold value for a sensitive parameter was set at 0.15, as the average of the threshold for *β and ρ* (see **Section 5.1.2.4**).

Comparison plots are presented for the mine inflows (**Figure 5-7**), drawdown (**Figure 5-8**) and well extraction (**Figure 5-9**).

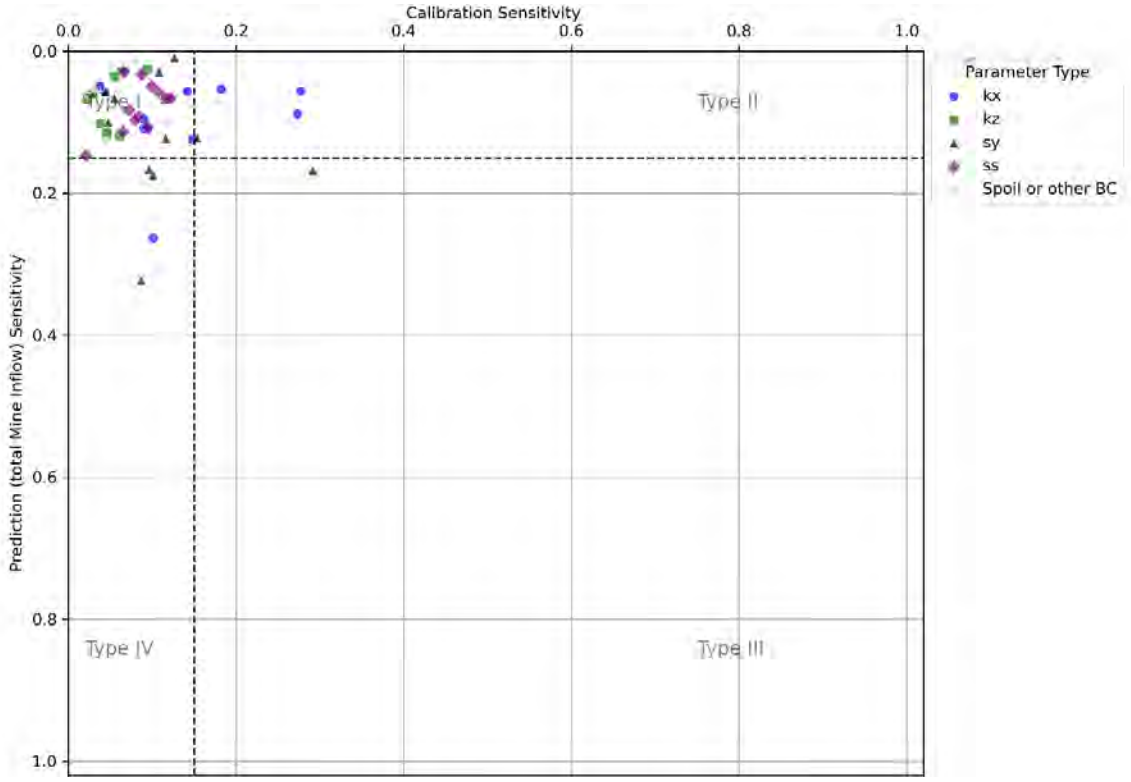


Figure 5-7 Predictive Sensitivity (Mine Inflow) Versus Calibration Sensitivity

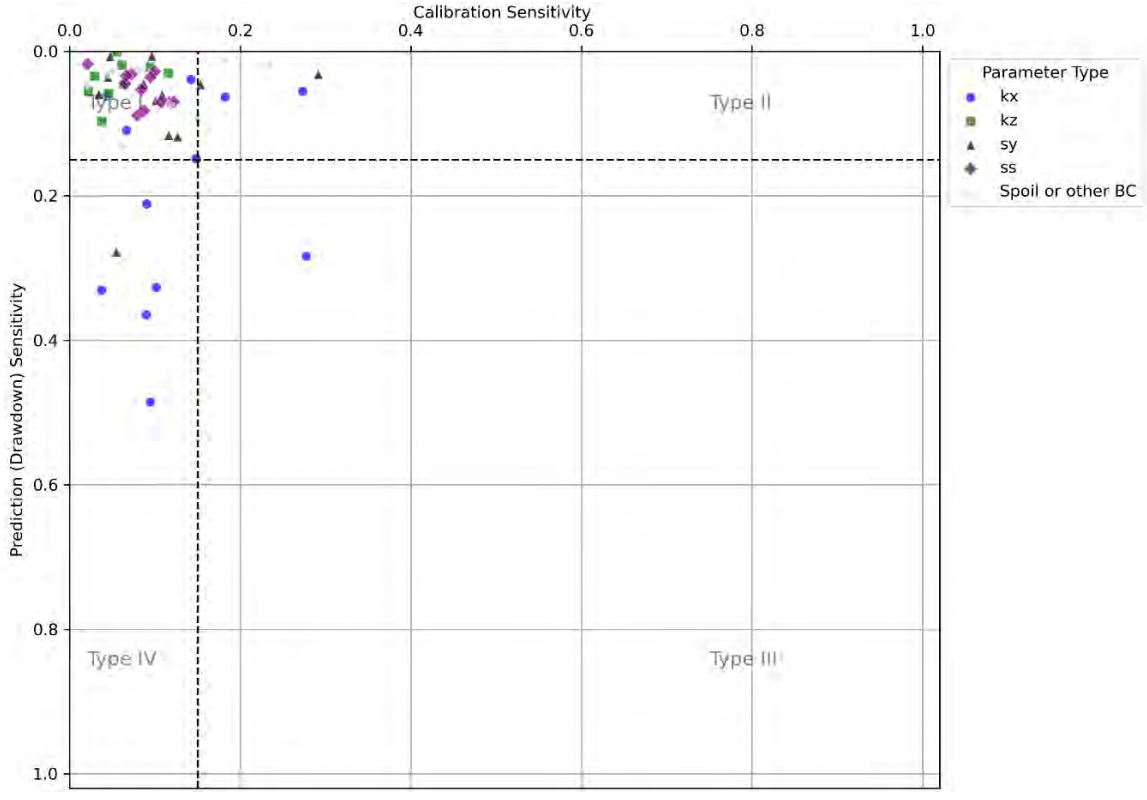


Figure 5-8 Predictive Sensitivity (Drawdown) Versus Calibration Sensitivity

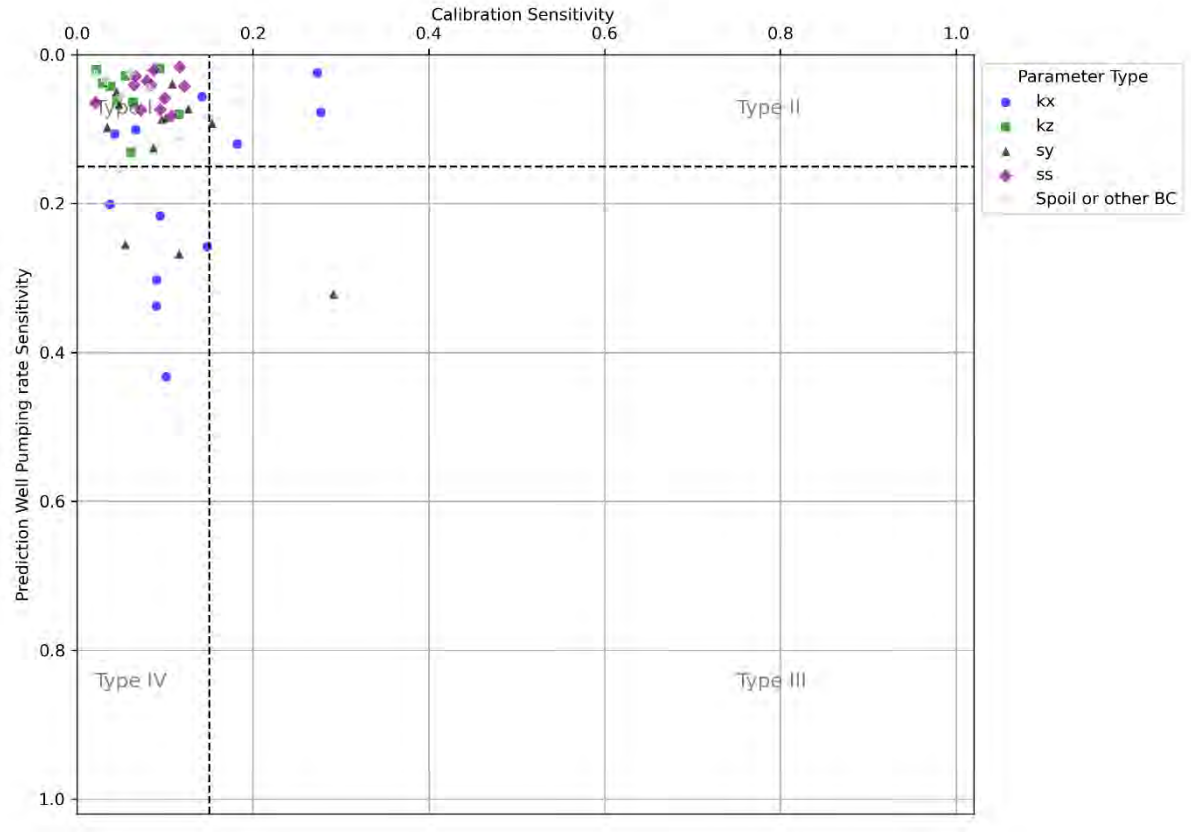


Figure 5-9 Predictive Sensitivity (Well Extraction) Versus Calibration Sensitivity

Type IV parameters are summarised in **Table 5-2.**

Table 5-2 Type IV Parameters

Parameter	Description	Associated Prediction
kx_z05	Layer 5 - Fractured rock Tabba Shear zone - low	Drawdown, Well Pumping rate
kx_z06	Layer 3 - Fractured rock - high fracture	Drawdown, Well Pumping rate
kx_z07	Layer 4 - Fractured rock - med fracture	Drawdown, Well Pumping rate
kx_z08	Layer 5 - Fractured rock - Low fracture	Drawdown, Total Mine Inflow, Well Pumping rate
kx_z12	Layer 3 to layer 7 - Dolerite Dyke	Drawdown, Well Pumping rate
sy_z06	Layer 3 - Fractured rock - high fracture	Drawdown, Well Pumping rate
sy_z04	Layer 4 - Fractured rock Tabba Shear zone - med	Total Mine Inflow
sy_z05	Layer 5 - Fractured rock Tabba Shear zone - low	Total Mine Inflow
sy_z10	Layer 7 - Basement - middle	Total Mine Inflow
kx_z10	Layer 7 - Basement - middle	Well Pumping rate
sy_z12	Layer 3 to layer 7 - Dolerite Dyke	Well Pumping rate
evtf_z02	Shear zone	Well Pumping rate

5.1.4 Conclusion

The sensitivity analysis highlighted several parameters that contribute to predictive uncertainty and that are likely to be poorly conditioned by the calibration process (Type IV parameters). These parameters are generally associated with zones that are:

- directly or indirectly stressed by the mining process (i.e. zones of active dewatering or zones adjacent to active dewatering) and;
- not associated with head targets (and thus not able to be conditioned by the calibration process).

A predictive uncertainty was conducted to quantify the uncertainty associated with model parameters, including the type IV parameters identified above (See **Section 6.0**).

6.0 Uncertainty Analysis

A Type 3 Monte Carlo uncertainty analysis was undertaken to estimate the uncertainty in the future impacts predicted by the model. This method operates by using the calibrated realisations presented in **Section 3.0**, executing the model independently for each realisation, and then aggregating the results for statistical analysis.

The 127 calibrated realisations were selected for this uncertainty analysis. The predictions included in the uncertainty analysis were:

- Water Table Drawdown,
- Mine Inflows (active mining),
- Pumping Well Volumes, and
- Final Void Lake Elevation.

6.1.1 Uncertainty Convergence

Statistical analyses of predictive results were conducted to assess if additional realisations were likely to provide results that would significantly change reported results. The 5th and 95th percent confidence interval for the main predictive results (drawdown and mine groundwater inflow (active mining)) was calculated using the Bootstrap method (Efron & Tibshirani, 1993).

The confidence intervals are calculated sequentially as more realisations are added, creating a sequential progression of confidence intervals; for example, the confidence interval of the mine groundwater inflow (active mining) rates was calculated using the results from 10 realisations, 20 realisations, sequentially, up to the total number of realisations.

6.1.1.1 Methodology

Given a dataset of values $X = \{x_1, x_2, \ldots, x_n\}$ we compute percentile confidence intervals as follows:

- We perform 500 bootstrap iterations. In each iteration b = 1, ... , 500, we draw a sample with replacement from the data.
- The percentiles are recalculated for each bootstrap sample
- The 95th confidence interval is estimated using the 2.5th and 97.5th percentiles of the bootstrap estimates.

This method allows for non-parametric estimation of confidence intervals on percentiles, accounting for sampling variability.

6.1.1.2 Results

Figure 6-1 and **Figure 6-2** shows percentile for the 5th, median and 95th as well as the 5th and 95th confidence intervals as more realisations are added, for mine groundwater inflows and drawdown. As indicated in **Figure 6-1** and **Figure 6-2**, additional realisations are unlikely to significantly increase or decrease the confidence intervals of predictions. This conclusion is drawn based upon the combination of two factors:

- The rate of change per additional realisation is small.
- The magnitudes of the confidence interval are small and well below the reasonable expectations of the predictive ability of a numerical model.

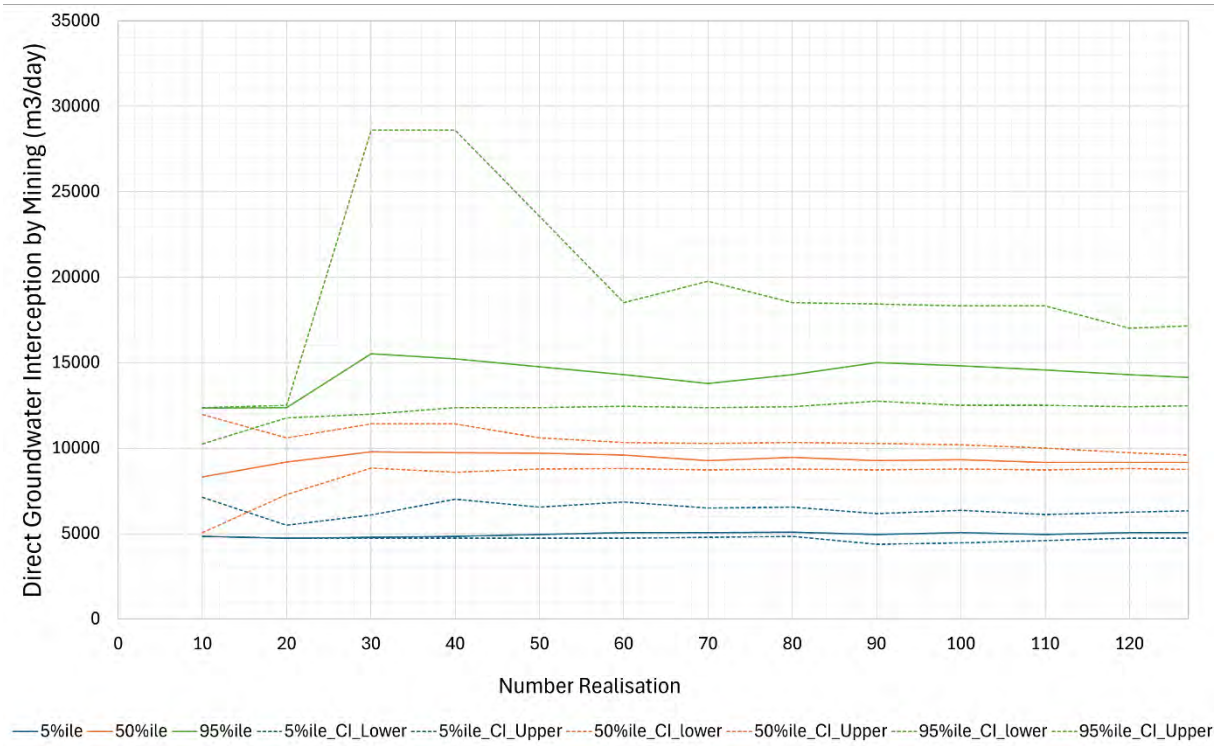
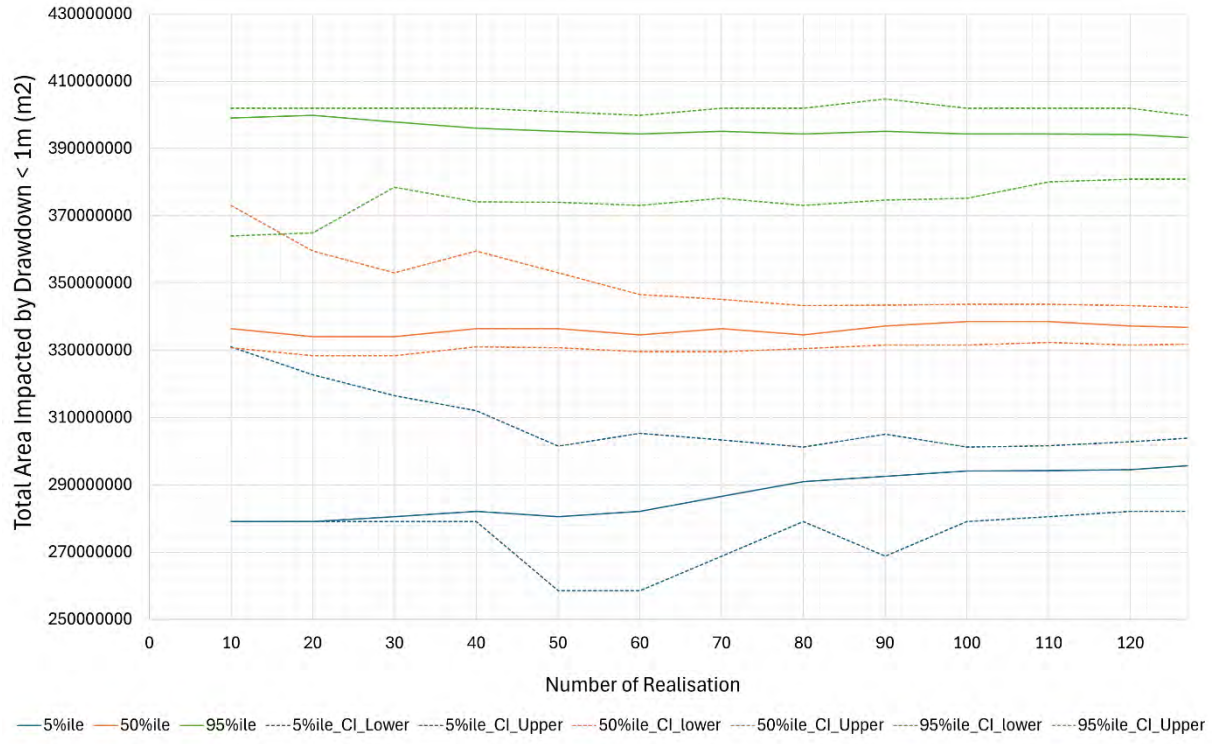


Figure 6-1 Predictive Uncertainty Convergence – Mine Groundwater Inflows (Active Mining)

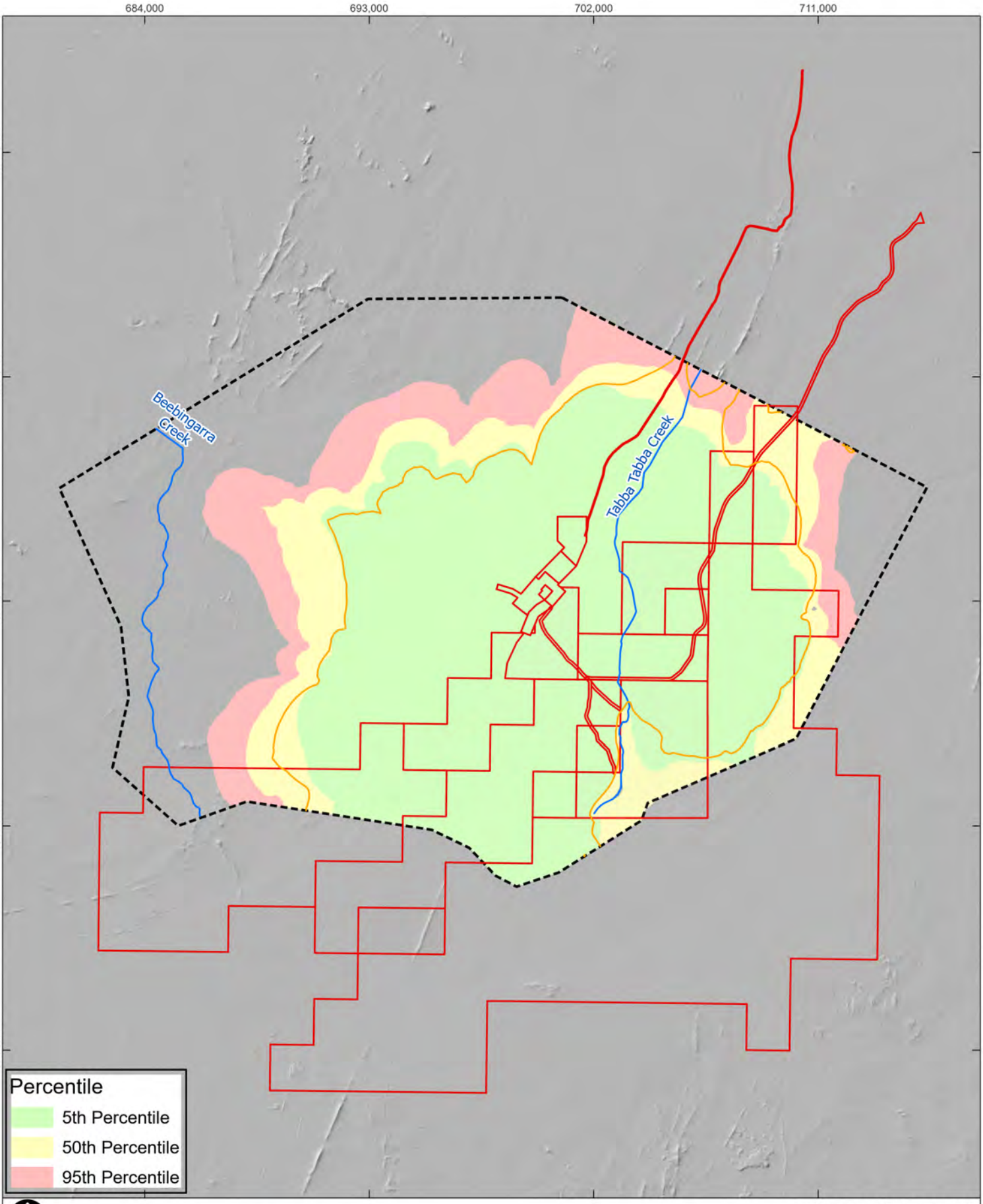


Note: m^2 = square metres

Figure 6-2 Predictive Uncertainty Convergence – Drawdown

6.1.2 Uncertainty of Drawdown

To illustrate the level of uncertainty in the extent of predicted mine induced drawdown (1 m contours), the calibrated prediction model maximum drawdown (incremental) and the 50th percentile maximum drawdown extent were compared to the maximum drawdown extent for the 5th and 95th percentiles (**Figure 6-3**). Overall, the results indicate that the Best Calibrated Model 1 m contour mostly fits in between the 5th percentile and the median.



0 1 2 km

Coordinate System:	GDA 1994 MGA Zone 50
Scale:	1:200,000 at A4
Project Number:	620.042733
Date Drawn:	5/19/2026
Drawn by:	DC

LEGEND

- Best Calibrated Model
- Major Drainage System
- Mining Tenements
- Model Boundary

TABBA TABBA LITHIUM MINE PROJECT, GROUNDWATER MODELLING TECHNICAL REPORT

UNCERTAINTY IN PREDICTED MAXIMUM WATER TABLE DRAWDOWN (INCREMENTAL)

SLR

DISCLAIMER: All information within this document may be based on external sources. SLR Consulting Pty Ltd makes no warranty regarding the data's accuracy or reliability for any purpose.

FIGURE 6-3

Path: H:\Local Resources\Mining Advisory\ADVGIS\03-Projects\Australia-WA\TabbaTabbaLithium\ADVAU00796\01-ESRI\ADVAU00796.aprx\GW - Figure 6-3 Uncertainty in Predicted Maximum Water Table Drawdown (Incremental)

6.1.3 Uncertainty of Mine Groundwater Inflows

The uncertainty of mine groundwater inflow (active mining) into the Project pit (active take) from the start of Project mining (2027) to the end of mining (2040), is shown for the incremental scenario in **Figure 6-4**. The figures show the predicted mine groundwater inflows (active mining) for the Best Calibrated Model and different prediction ranges. These represent:

- 5th – 33th indicates it is likely that the outcome is larger than this range.
- Median indicates it is as likely as not that the outcome is larger or smaller than this value.
- 33th – 67th indicates it is likely that the outcome is within that range.
- 67th – 95th indicates it is unlikely that the outcome is larger than this range.

The predicted uncertainty in mine groundwater inflows (active mining) is up to 2,700 m³/d deviation from the median for the incremental scenario. Overall, the results indicate that the Best Calibrated Model model generally tracks below the median throughout most of the period. It aligns with the lower percentile range (5th–33rd) during peak years (2027–2029) and again during the decline and low-flow period (2032–2037), before returning to the central range (33rd–67th) during the late recovery phase (2038–2040) (**Figure 6-4**).

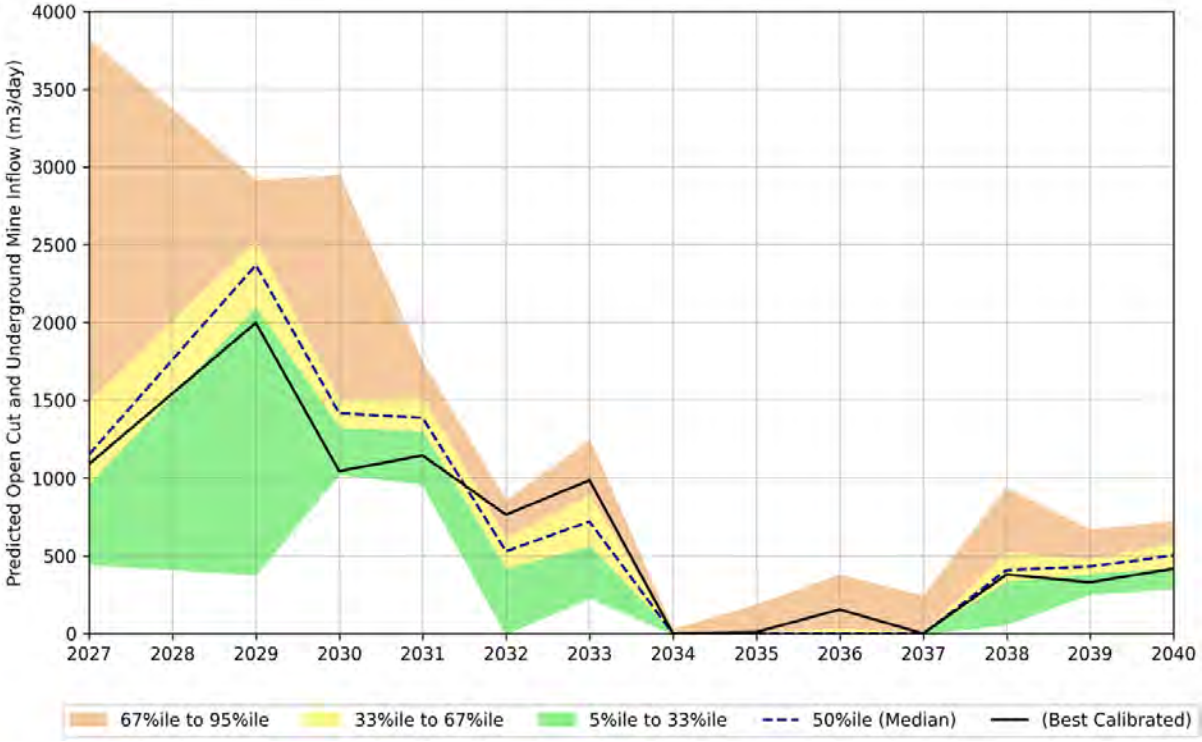


Figure 6-4 Uncertainty in Incremental Mine Groundwater Inflows (Active Mining)

6.1.4 Uncertainty of Predicted Pumping Rate (Well)

The uncertainty of predicted pumping rates at the selected well from 2027 to 2041 is shown for the incremental scenario in **Figure 6-5**. The figure presents the predicted pumping rates for the Best Calibrated Model and associated prediction ranges.

The predicted uncertainty in pumping rates is up to approximately 2,000 ML/year deviation from the median, particularly during peak conditions around 2034. Overall, the results indicate that the Best Calibrated Model consistently lies below the median and is predominantly within the 5th–33rd percentile range or close to the lower bound of the 5th–33rd percentile range throughout the assessment period (**Figure 6-5)**. The Best Calibrated Model results presented is therefore likely to underestimate pumping rates.

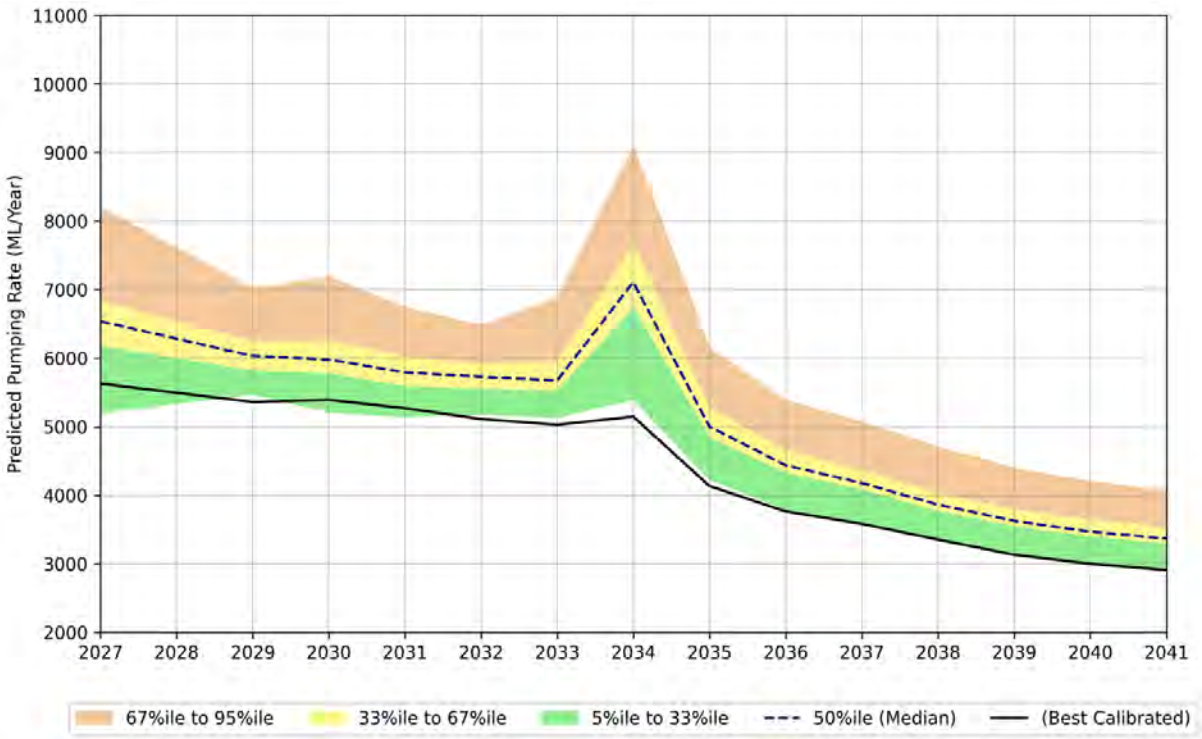


Figure 6-5 Uncertainty in Incremental Pumping Rates at the Selected Well

6.1.5 Uncertainty of Final Void Lake Elevation

The uncertainty of predicted final void lake water levels was quantified for all three final voids.

For Main pit, the results indicate that the Best Calibrated Model generally lies within the 5th–33th percentiles (**Figure 6-6**).

For the Han pit, the results indicate that the Best Calibrated Model generally lies close to the median. During period of maximum drawdown, the Best Calibrated Model tends to align closer to the maximum (**Figure 6-7**).

For the Hutt pit, the results indicate that the Best Calibrated Model generally lies within 67th–95th percentiles. During period of maximum drawdown, the Best Calibrated Model tends to align closer to the maximum (**Figure 6-8).**

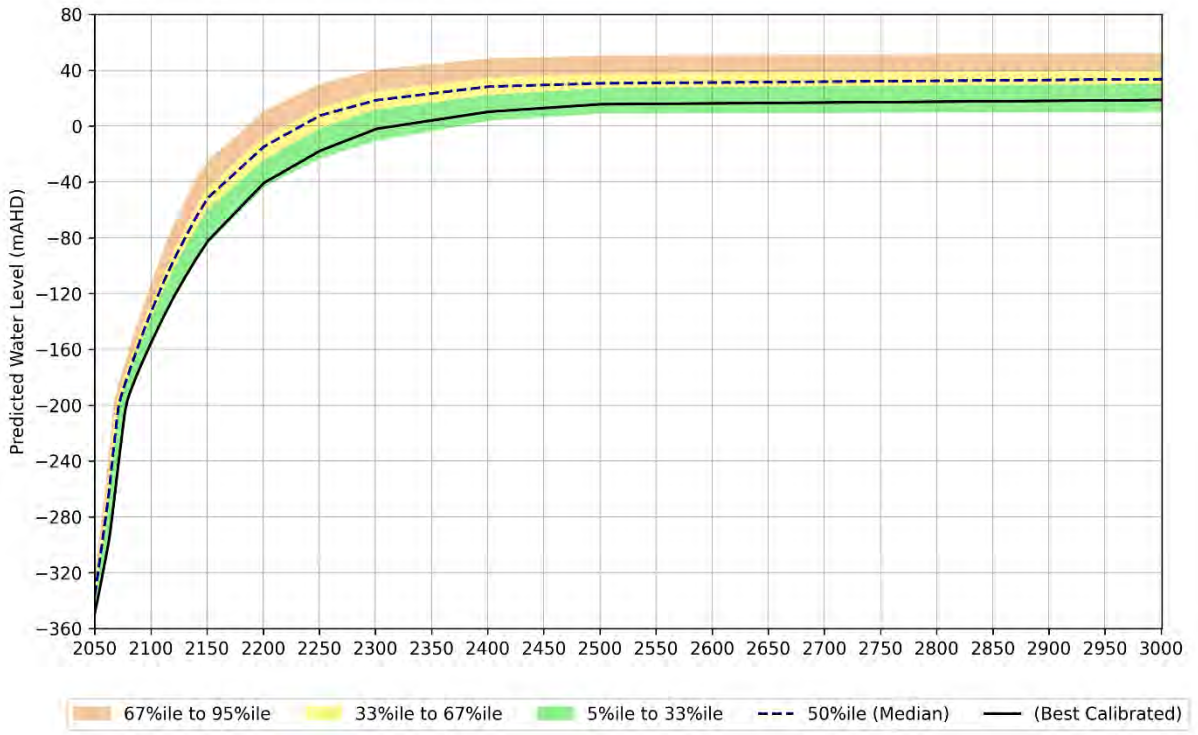


Figure 6-6 Uncertainty in Final Void lake level Elevation – Main Pit

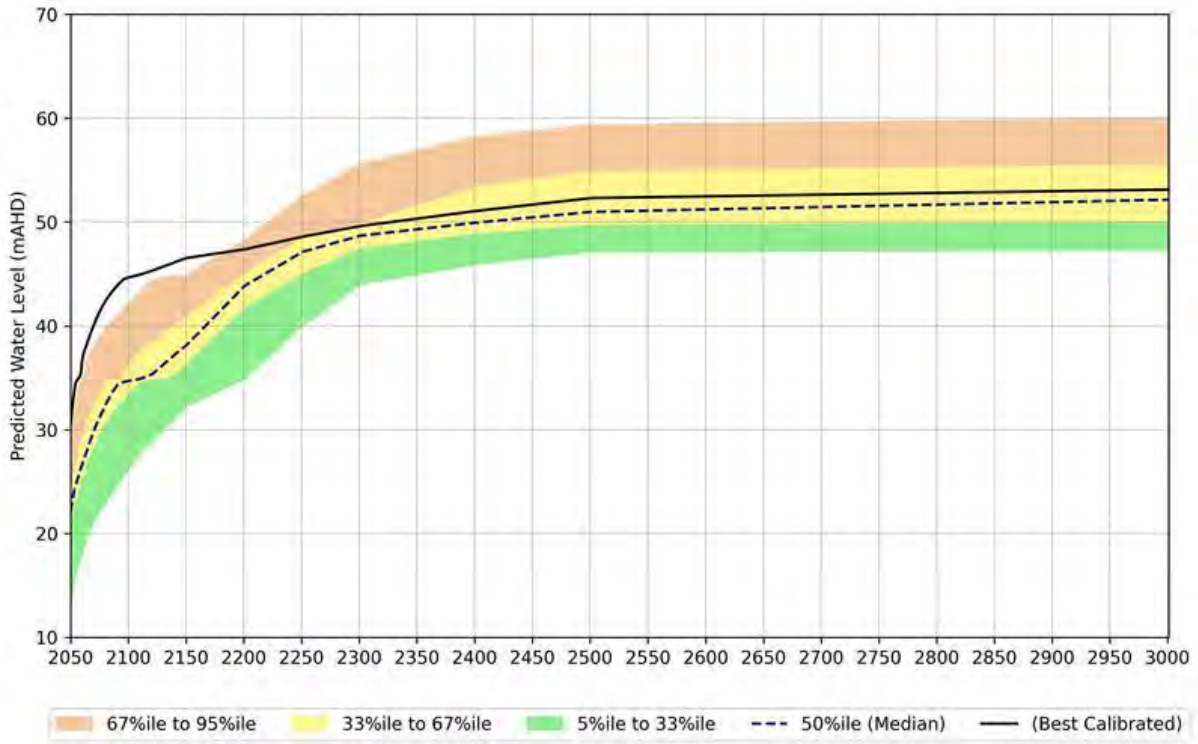


Figure 6-7 Uncertainty in Final Void lake level Elevation – Han pit

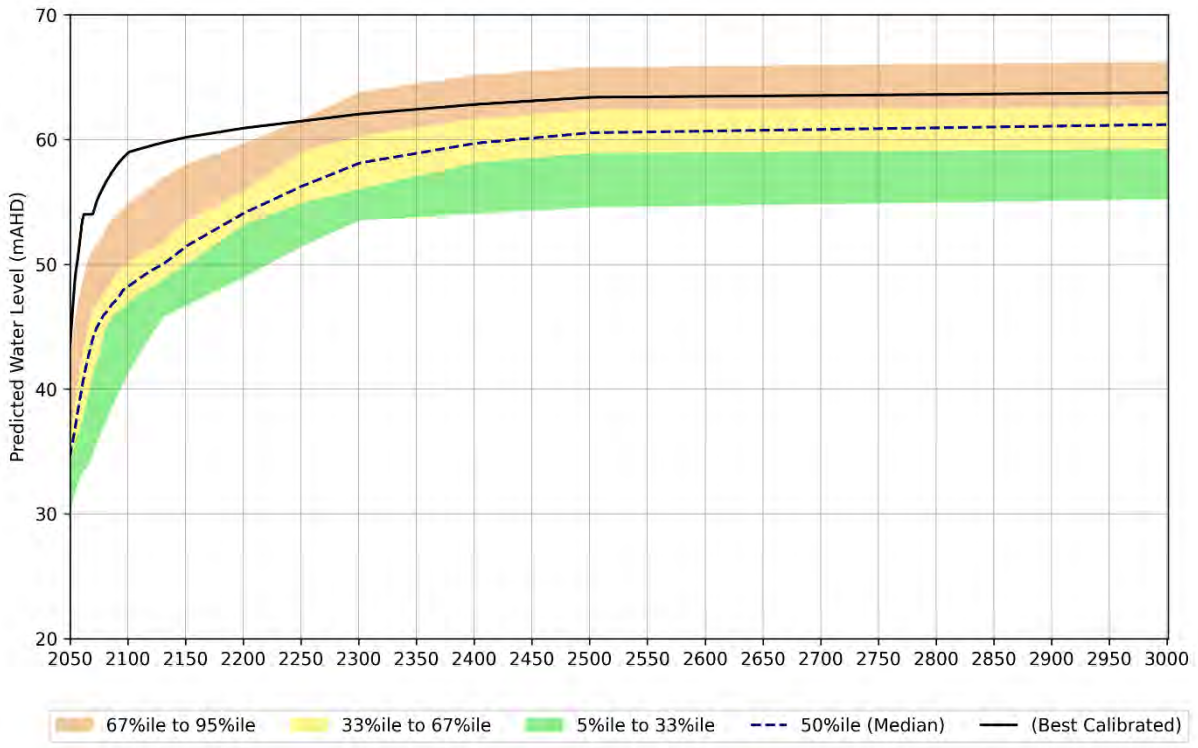


Figure 6-8 Uncertainty in Final Void lake level Elevation – Hutt pit

7.0 Assumptions and Limitations

7.1 Assumptions

This groundwater model has been developed based on the current conceptual understanding of the site and available data. The following assumptions were adopted in model construction, calibration and predictive simulations.

The conceptual hydrogeological model is considered an appropriate representation of the groundwater system at regional scale. Groundwater flow is assumed to be controlled by topography and structural features, with preferential flow through the Tabba Tabba shear zone and dolerite dyke.

The model discretisation and layering are considered sufficient to represent the main hydrostratigraphic units and vertical groundwater flow processes. The thickness of unconsolidated sediments near creek lines and associated GDV/ potential GDV areas was based on the CSIRO depth to regolith dataset (Australian wide dataset). As GDV/ potential GDV areas have been defined based on vegetation type, it is unclear if these systems are supported by localised perched systems or deeper regional water table in the weather/fractured rock. In the model, most of the GDV/ potential GDV areas have a very thin (<2 m) regolith cover which does not support simulating perched systems.

Hydraulic properties are represented using zonation and pilot point parameterisation. The calibrated parameter distributions are considered physically plausible and representative at the scale of the model. Subsurface heterogeneity is represented at the model scale and smaller-scale variability is not explicitly resolved.

Recharge is assumed to occur via rainfall infiltration, with enhanced recharge along drainage lines and structural features. Recharge estimates derived from AWRA-L deep drainage are assumed to be representative of long-term conditions and temporal variability. Evapotranspiration is represented using a simplified linear function and is considered to provide a reasonable approximation of groundwater discharge to the atmosphere.

Domain boundary conditions are assumed to adequately represent regional groundwater flow processes. General Head Boundaries simulate regional inflow and outflow. Surface water features are represented as drains only, consistent with their ephemeral nature.

Calibration is based on available groundwater level data and is considered sufficient to constrain key model parameters around the mine and represent regional groundwater conditions. The calibrated parameter sets are considered representative within the limits of available data.

Predictive simulations assume that the mining schedule, abstraction rates and infrastructure are accurately represented. Climatic conditions are assumed to be consistent with long-term historical averages. Mine dewatering is represented using drain boundary conditions. Post-mining processes, including pit lake development, are simulated using simplified recharge and evapotranspiration conditions.

7.2 Limitations

The model is subject to limitations that should be considered when interpreting model results.

Groundwater monitoring data are spatially limited and predominantly sourced from the upper fractured rock aquifer. Temporal coverage is limited, particularly prior to 2025, which reduces confidence in long-term system behaviour. Hydraulic property data are sparse and may not



fully represent aquifer heterogeneity. Data availability for deeper hydrostratigraphic units is limited.

The conceptual model includes simplifications. The Diorite Dyke is represented as a uniform zone and may not capture local variability or complex hydraulic connectivity. Recharge processes are simplified and may not fully represent episodic recharge typical of arid environments. Surface water–groundwater interactions are simplified and do not include transient flow processes.

The numerical model is regional in scale and does not resolve local-scale variability. Unsaturated zone processes are simplified and not explicitly represented. Mine dewatering and underground workings are simplified representations and do not capture all operational complexities. Final void modelling is limited to large stress period and provided only as an indicative lake equilibrium level. Additional water balance modelling will be required to properly assess the final void lake elevation and any potential for seasonal overtopping

Calibration results indicate an acceptable regional fit; however, local discrepancies remain. Parameter non-uniqueness means that multiple parameter combinations may provide a similar calibration outcome, resulting in predictive uncertainty. Model predictions are sensitive to parameters that are not well constrained by the calibration dataset.

Predictive scenarios assume no change in climate conditions over time. Mining configurations and abstraction rates are based on current designs and may change. Cumulative impacts from other developments are not explicitly included. Long-term predictions, particularly post-mining equilibrium conditions, are subject to increased uncertainty due to extrapolation beyond available data.

Model predictions are sensitive to a subset of parameters that are not strongly constrained by calibration (Type IV parameters), particularly those associated with deeper fractured rock units, structural features and storage properties. Variability in these parameters results in a range of plausible predictive outcomes.

Uncertainty is reflected in the spread of model results (for example between the 5th and 95th percentiles), which represent a range of potential system responses rather than a single deterministic outcome. The best calibrated model typically falls within but not necessarily at the centre of this range.

7.3 Use of Model Results

Model outputs represent regional-scale groundwater responses and should not be interpreted at a local scale. Predictions are most reliable for comparison between scenarios rather than absolute values. The model is suitable for impact assessment and regulatory evaluation. Additional data collection and model refinement would reduce uncertainty and improve confidence in predictions.

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9.0 Closure

Sincerely,

SLR Consulting Australia Pty Ltd



Louis Bouchet
Principal Groundwater Modeller

Appendix A Parameters Distributions

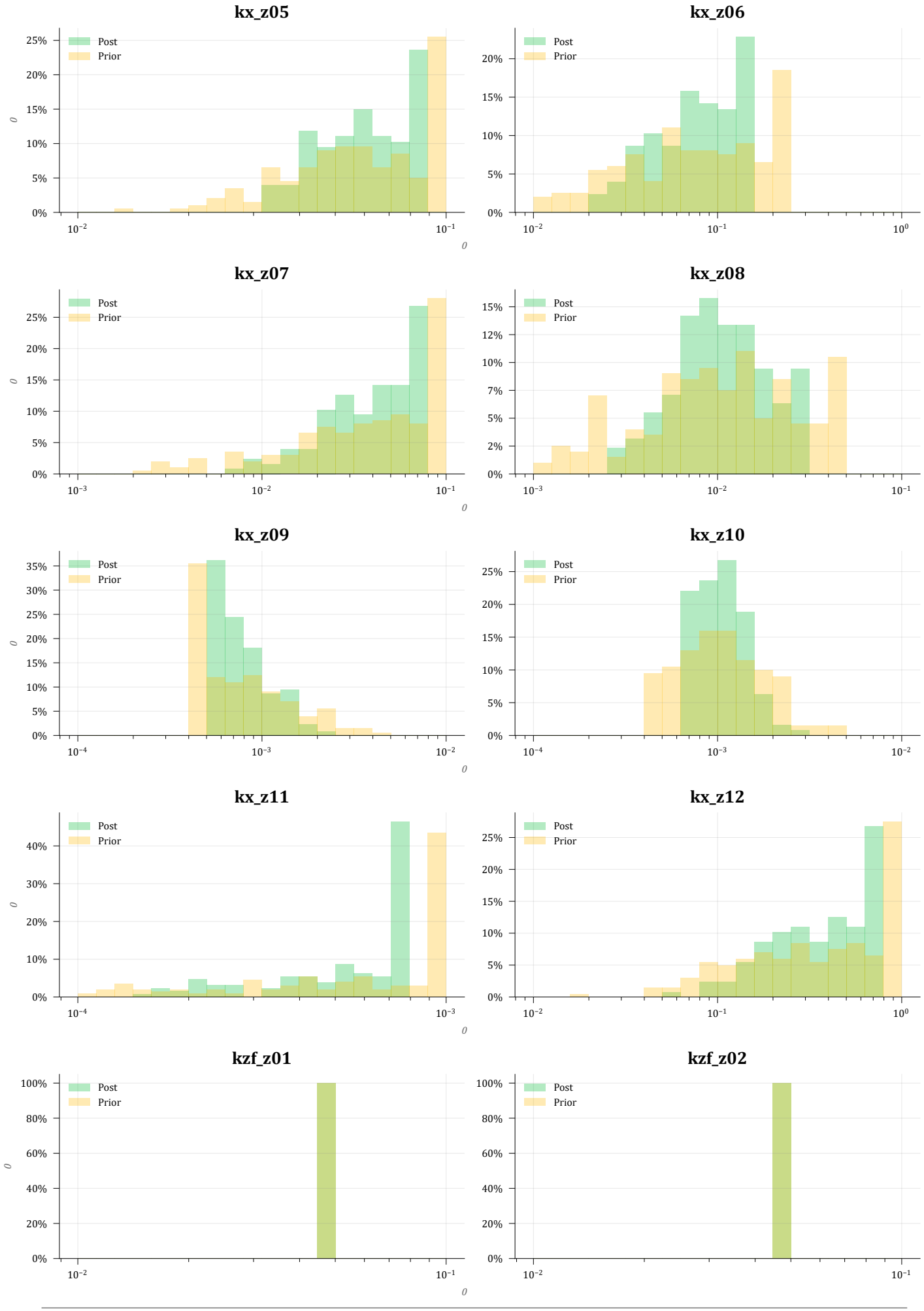
Tabba Tabba Lithium Mine Project

Groundwater Modelling Technical Report

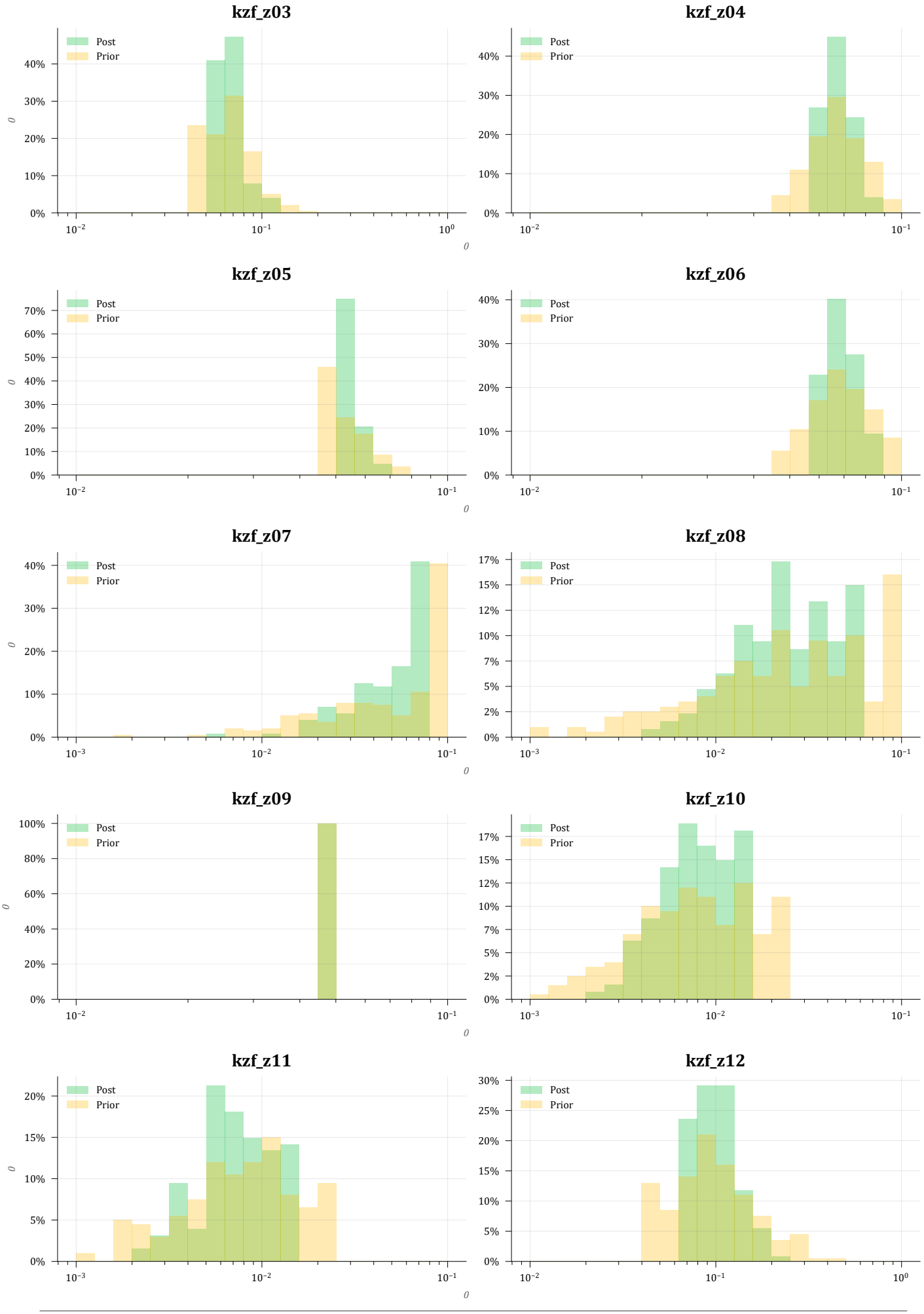
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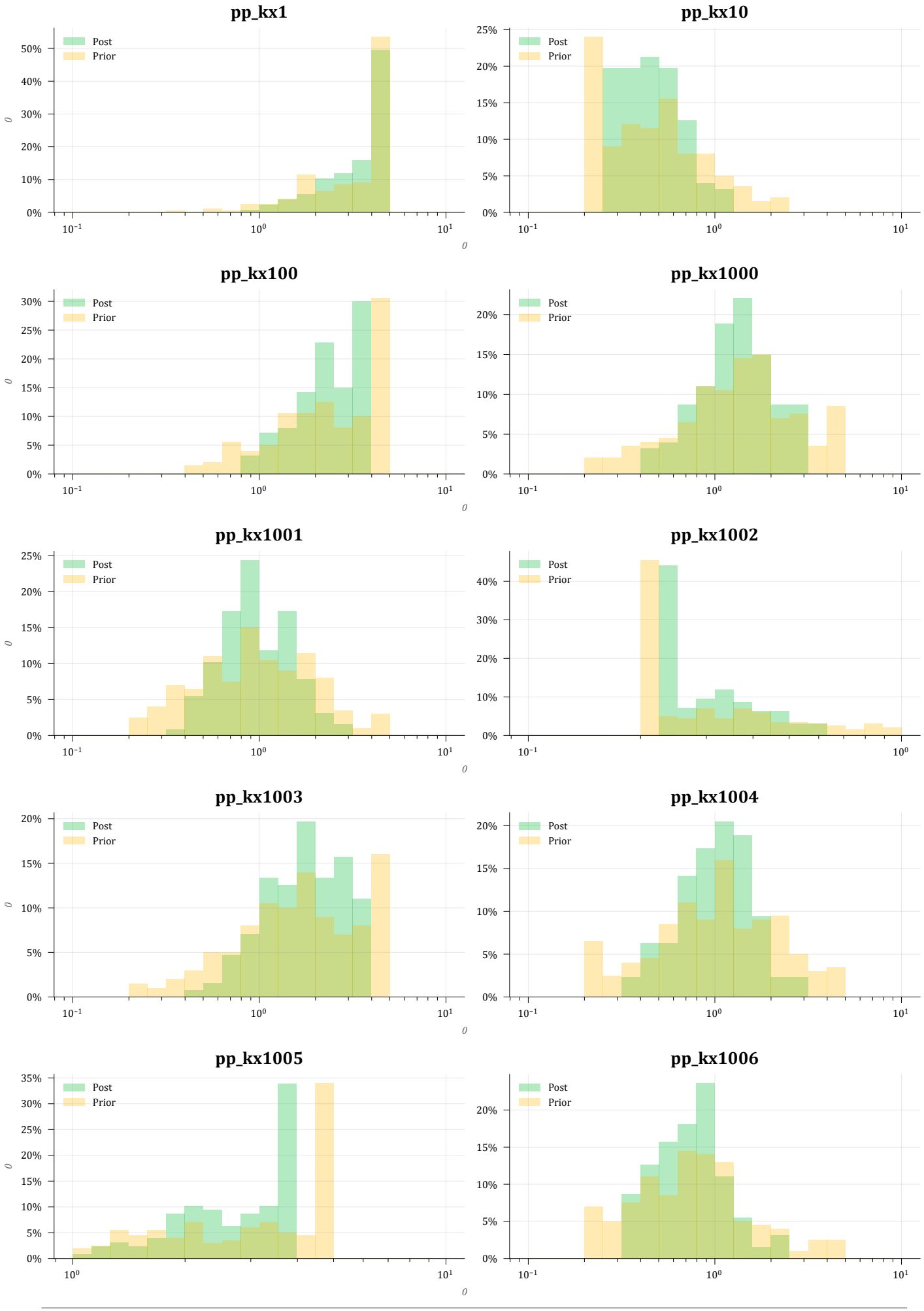
SLR Project No.: 620.042733.00001


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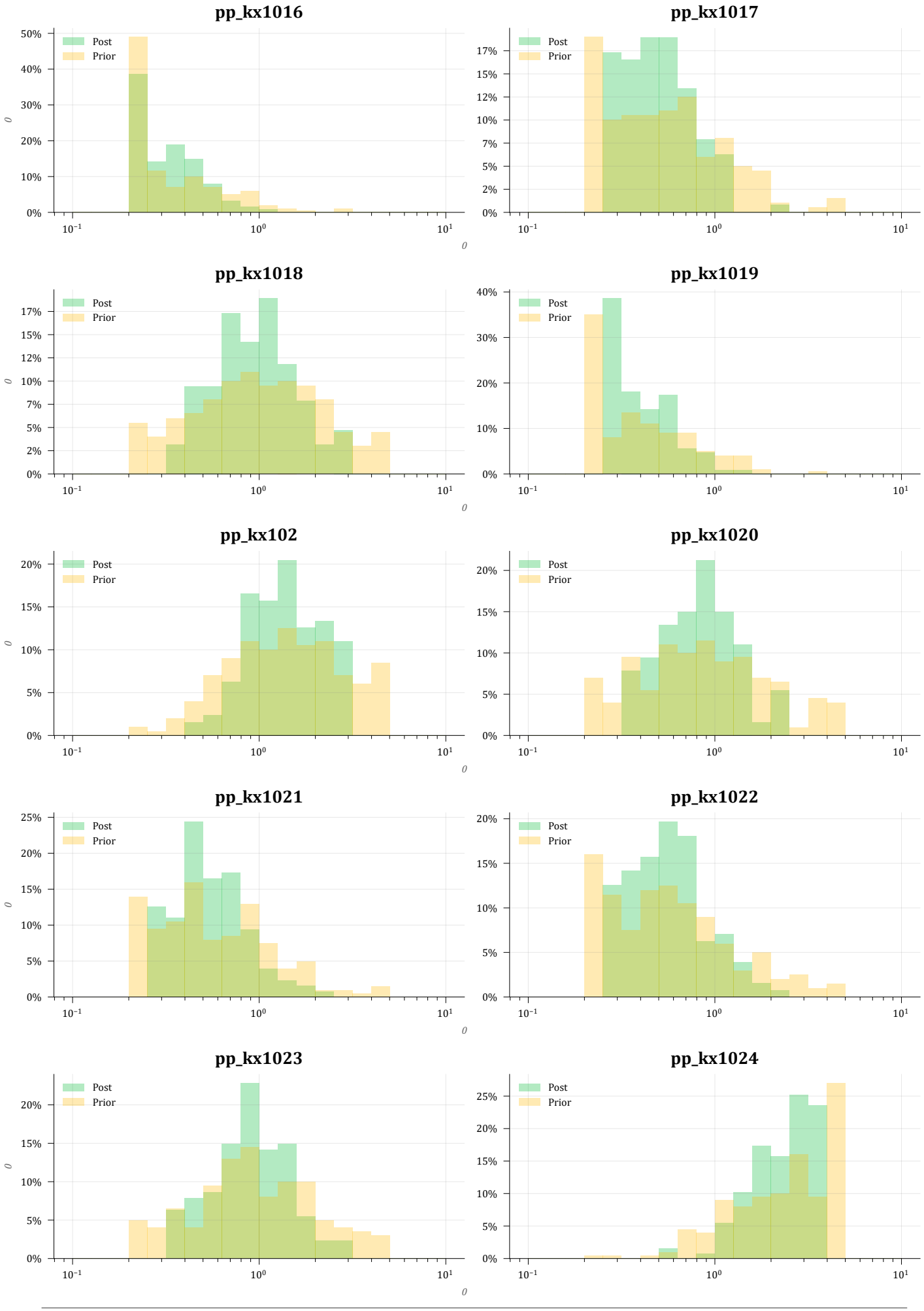

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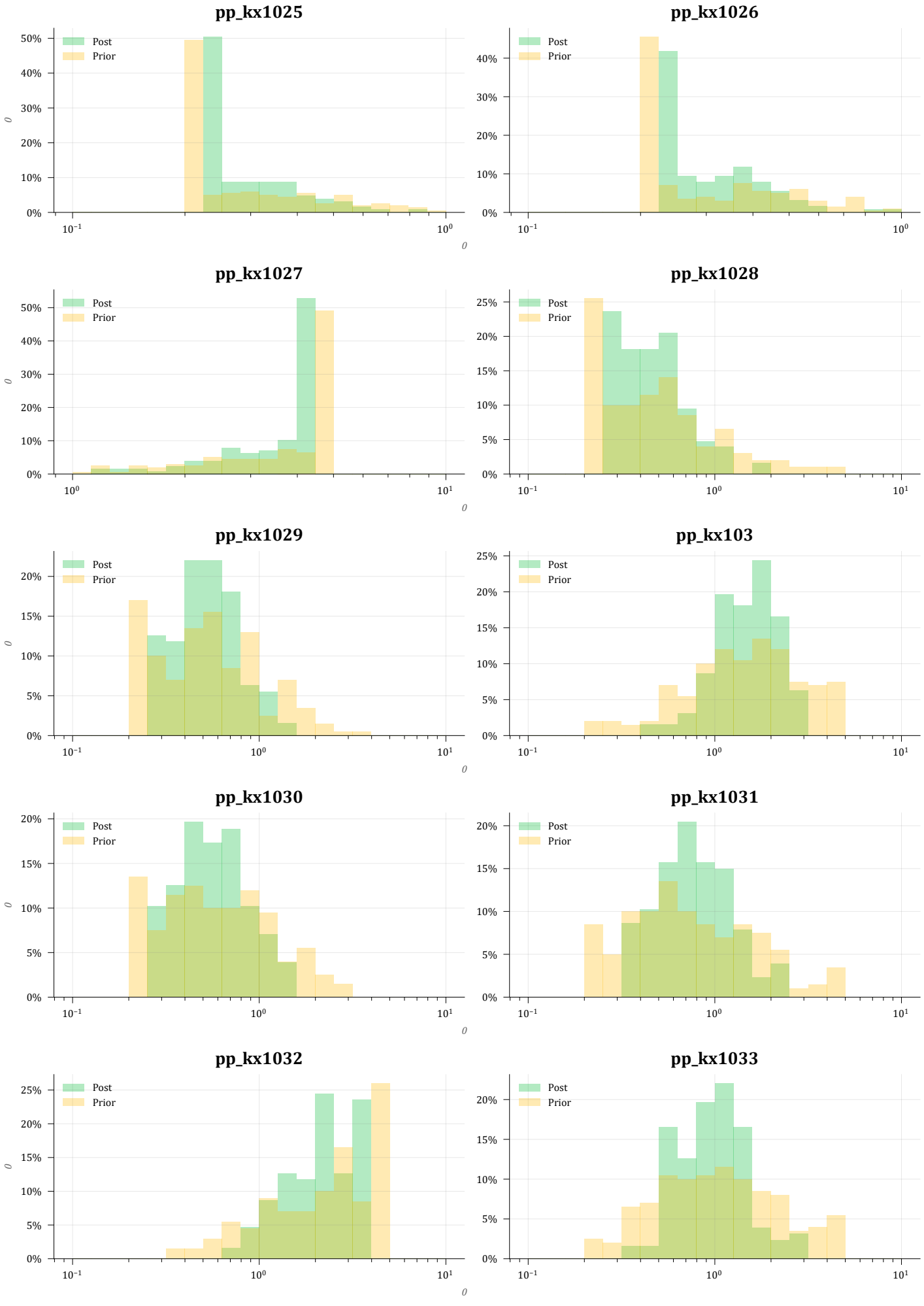
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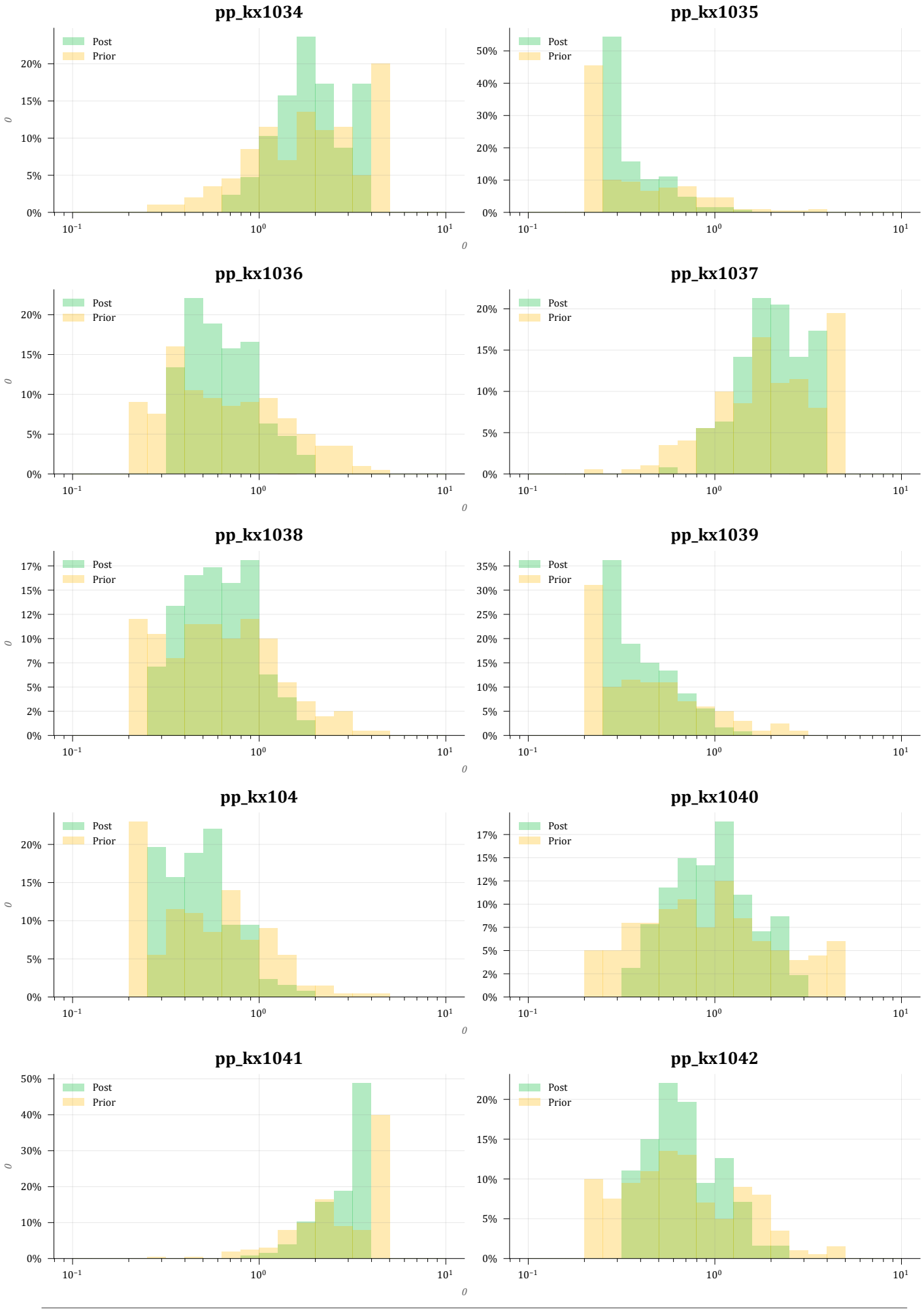

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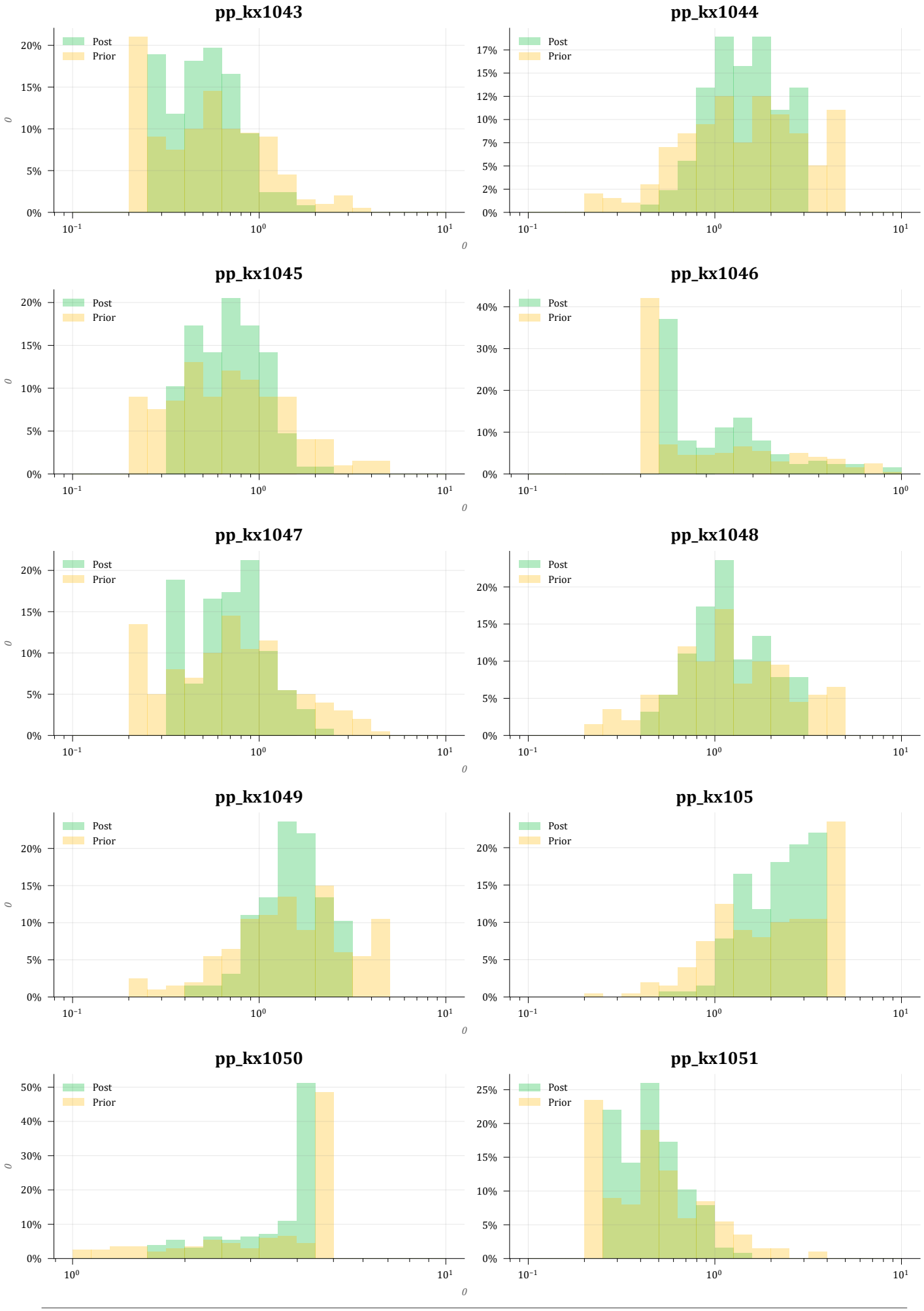

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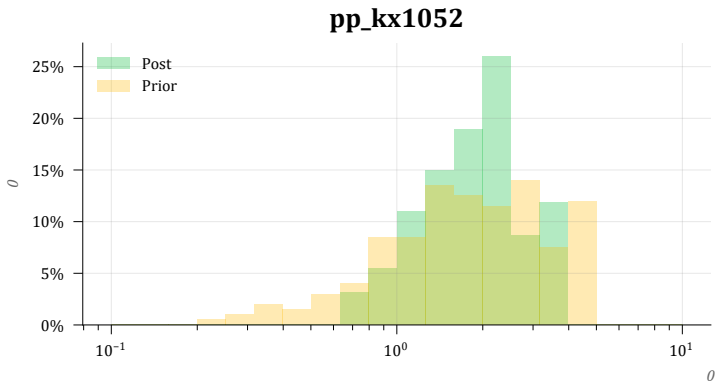

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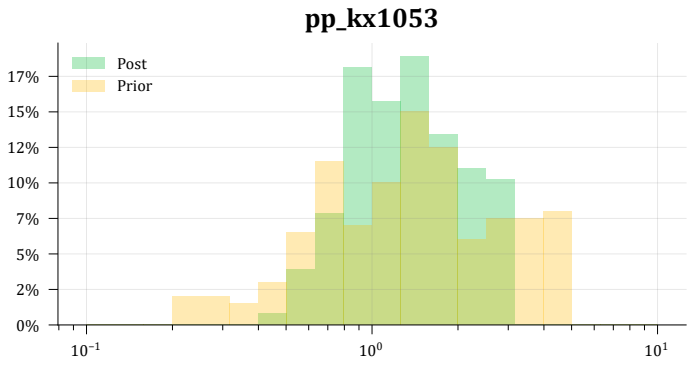

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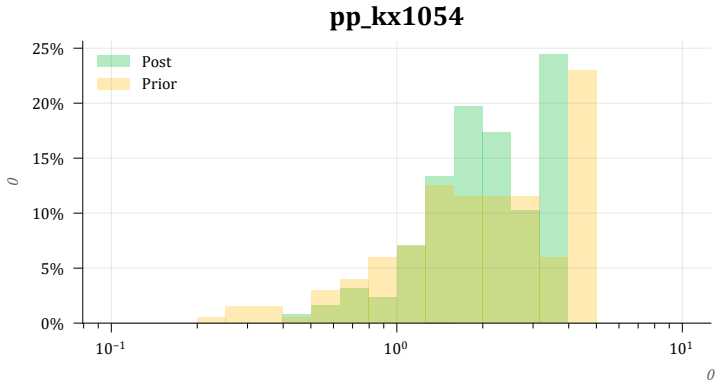

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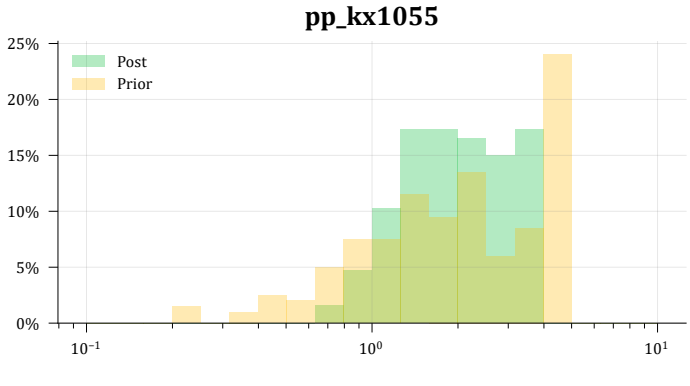

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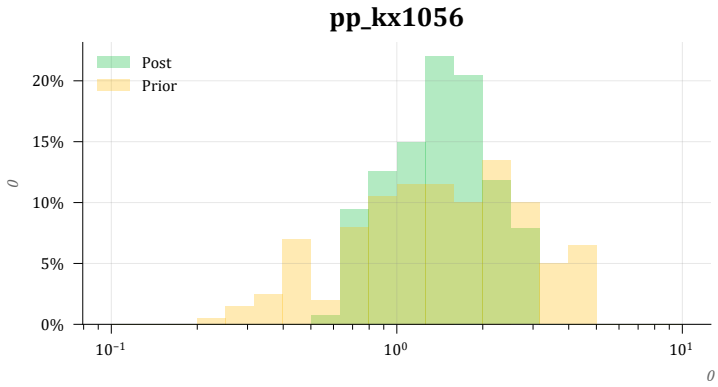

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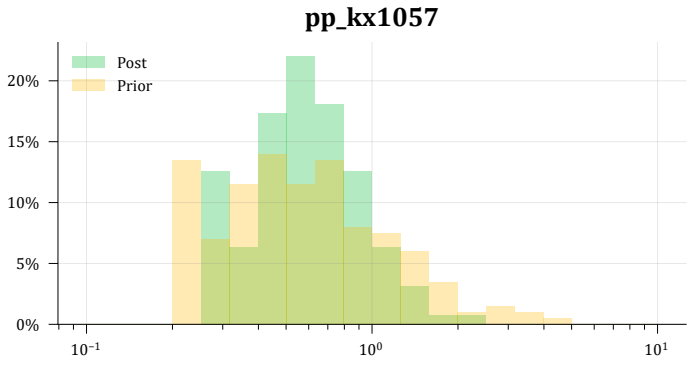

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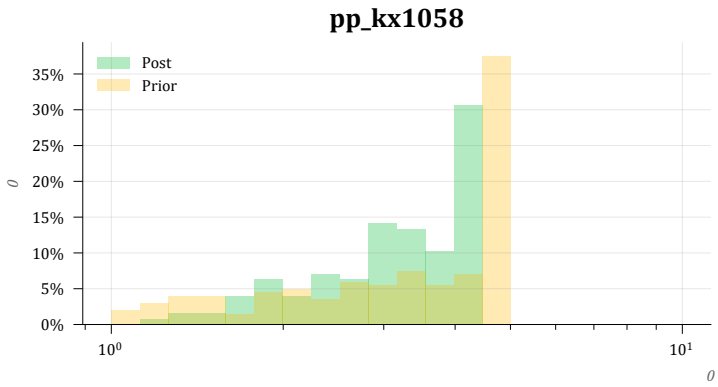

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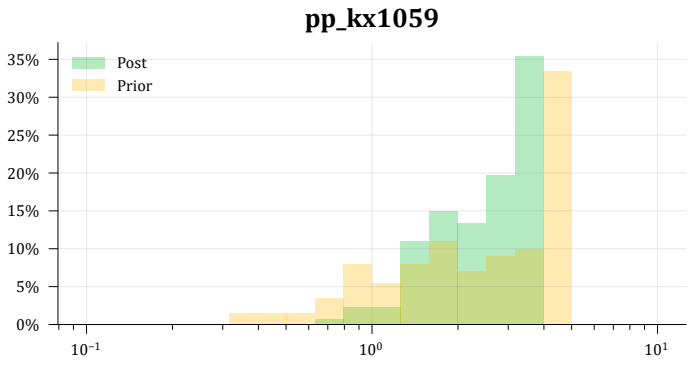

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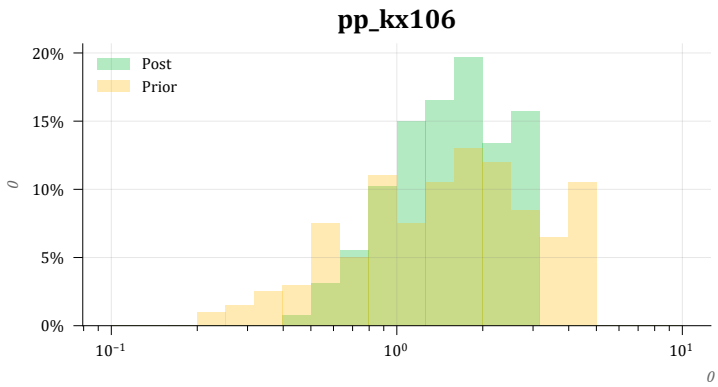

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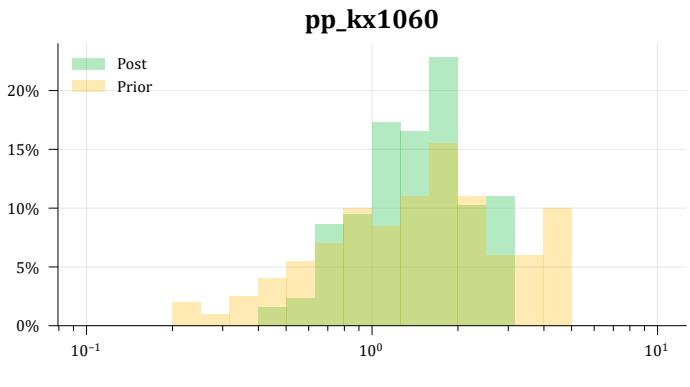

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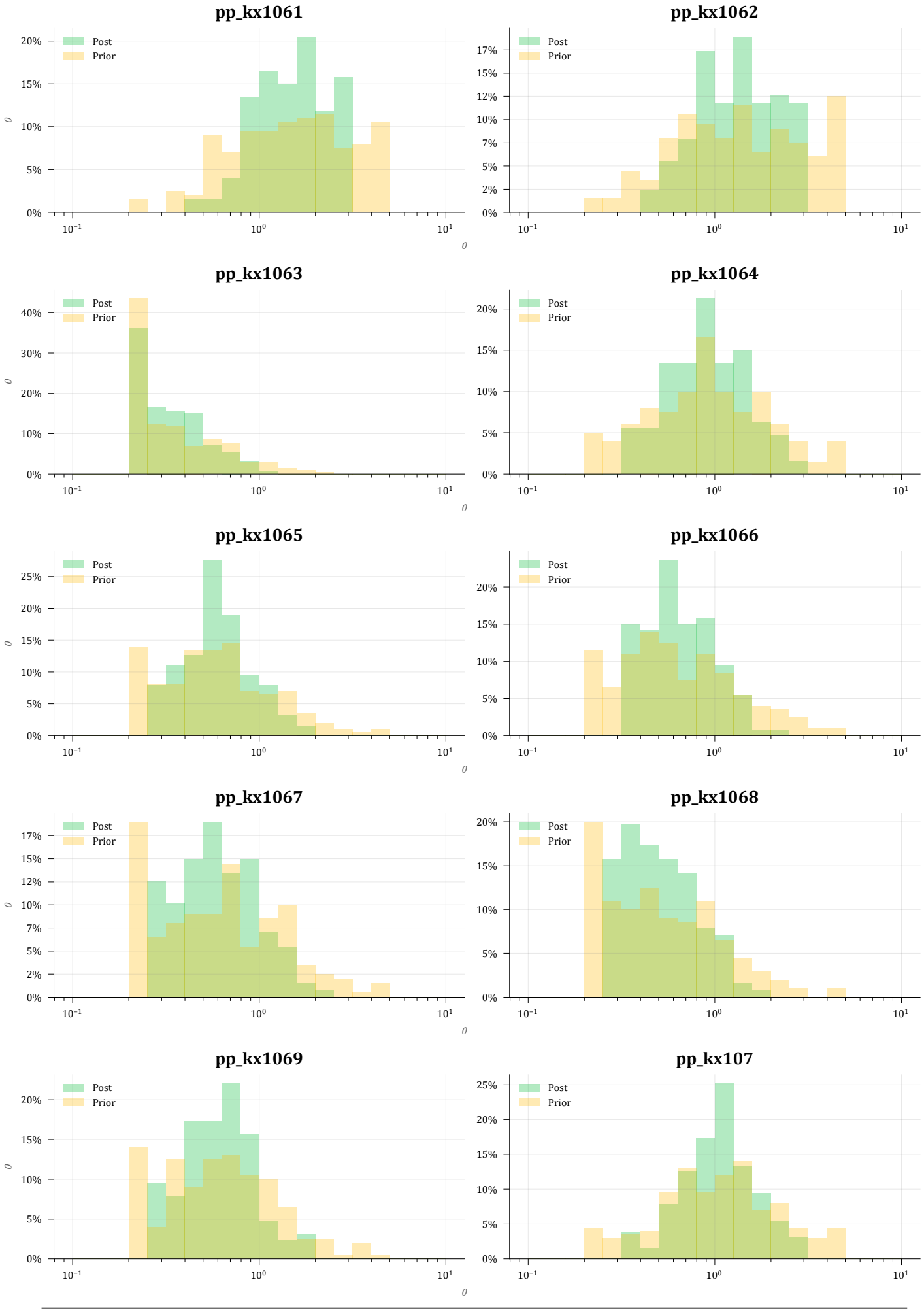

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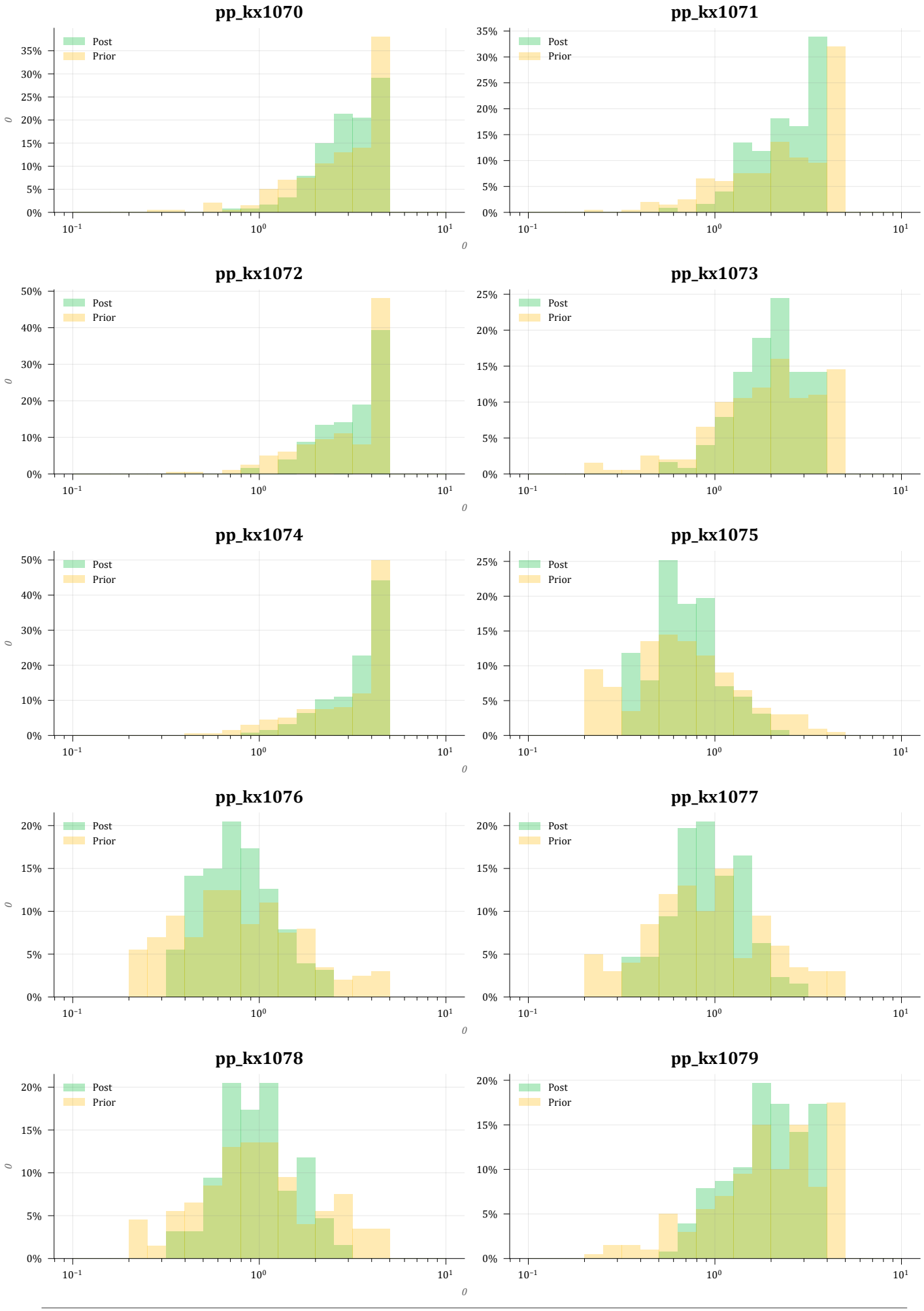

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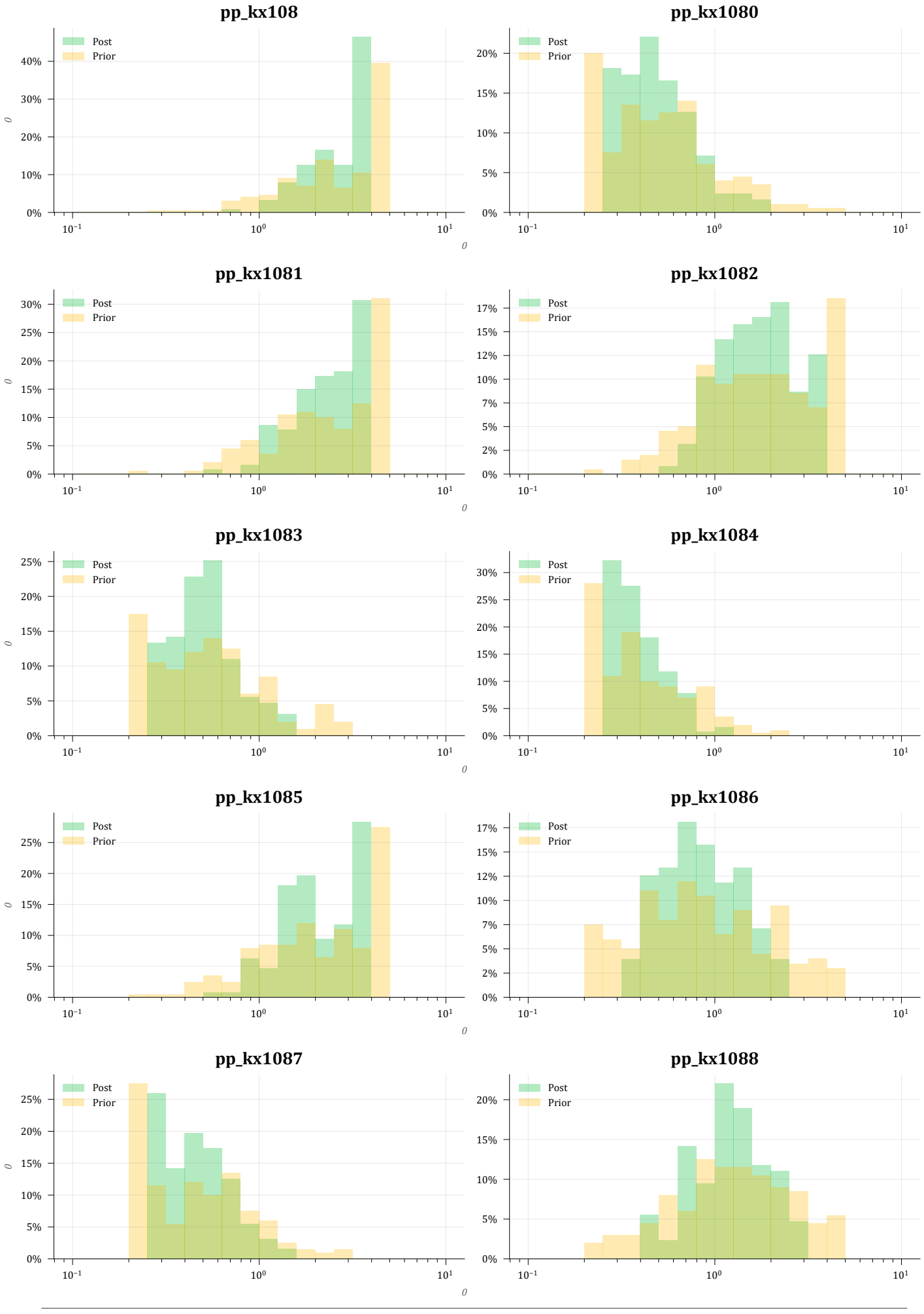

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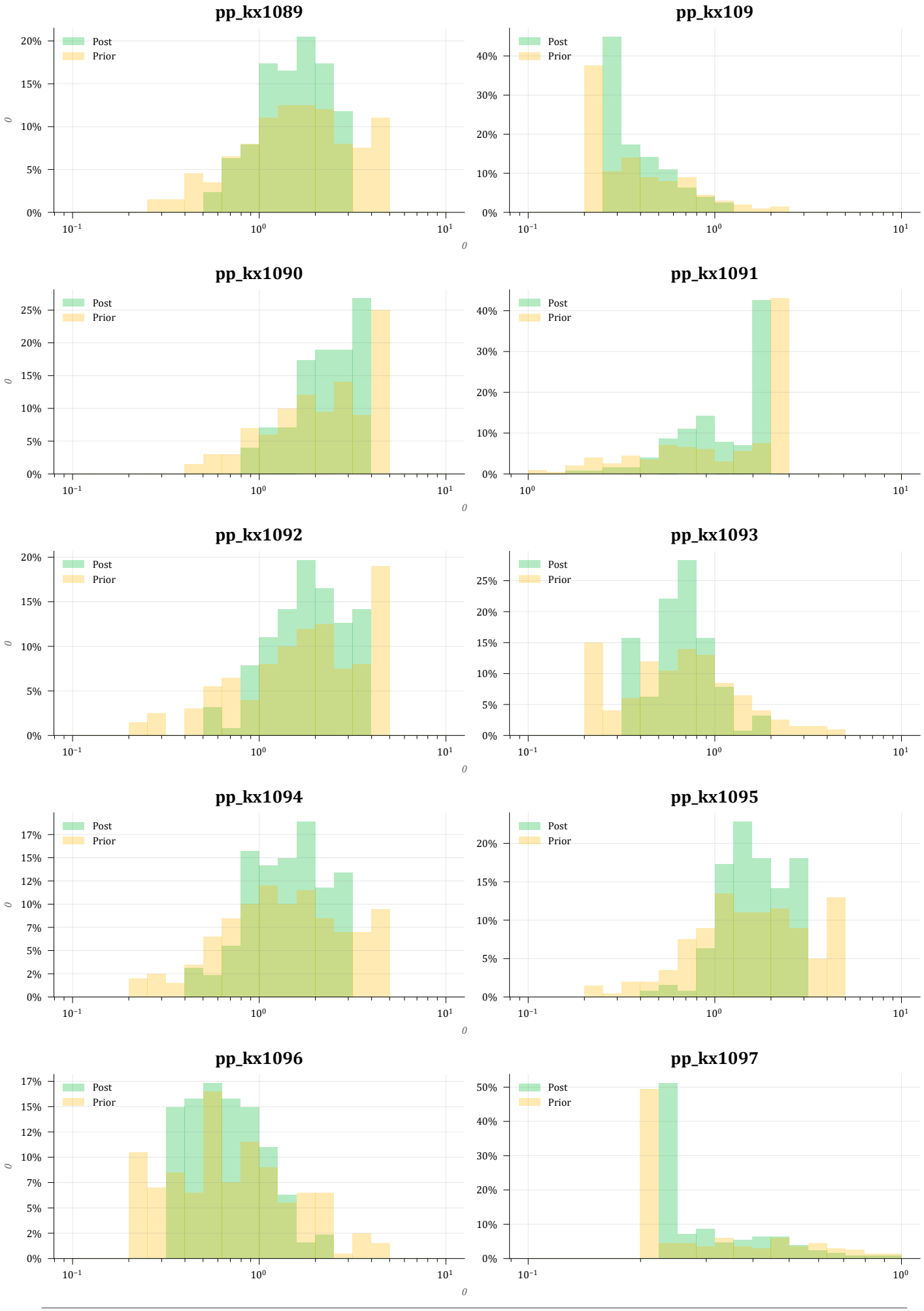

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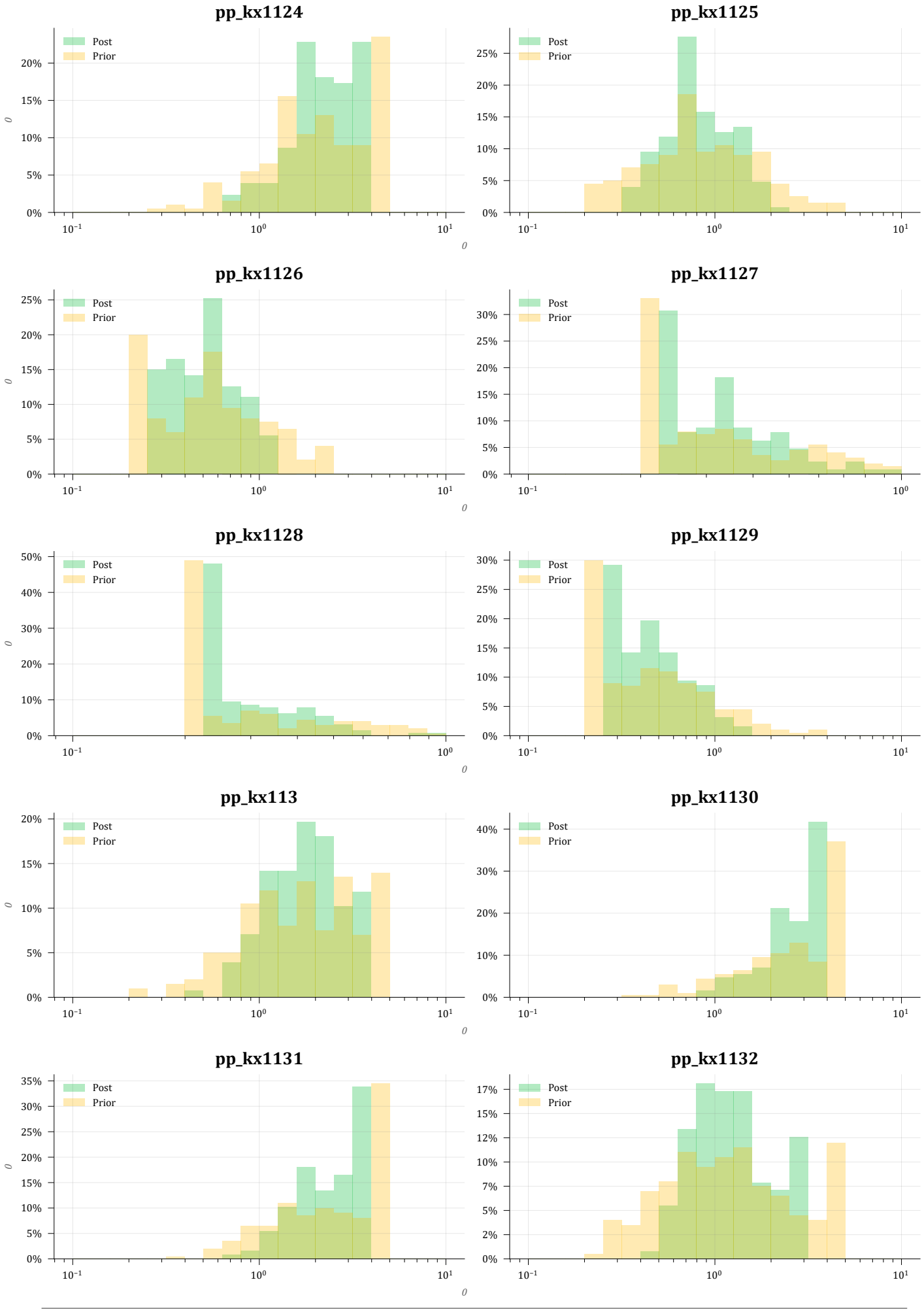

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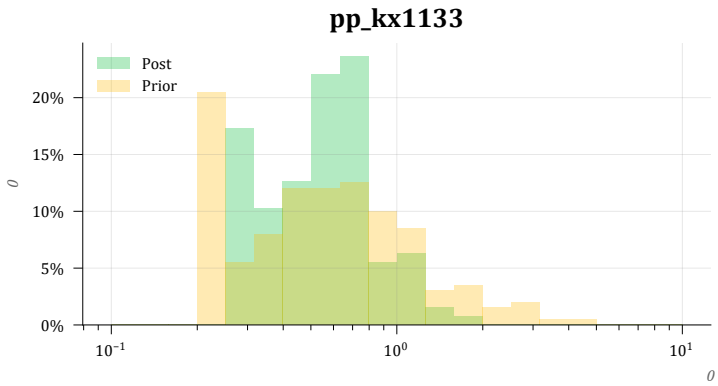

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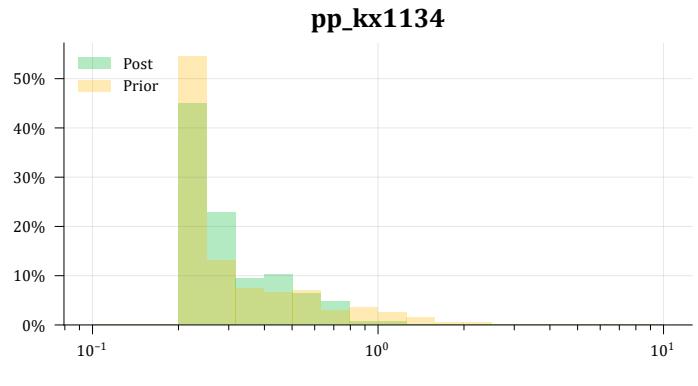

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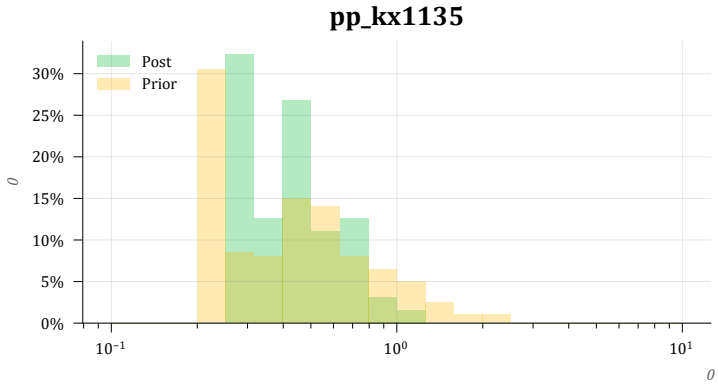

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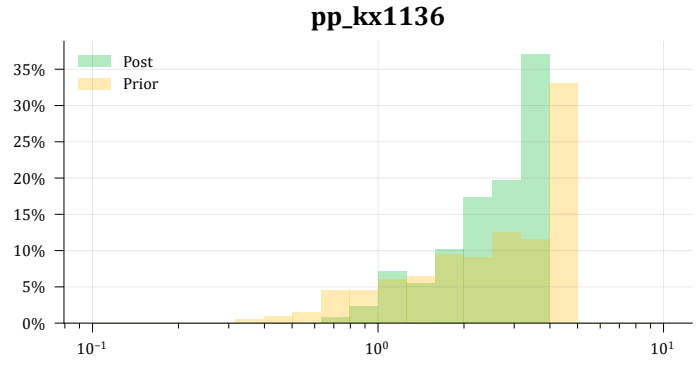

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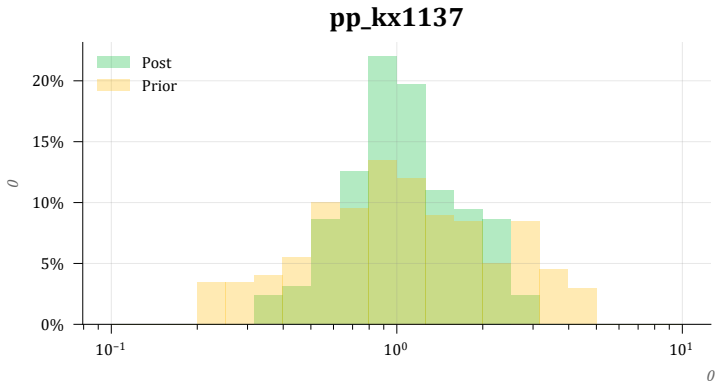

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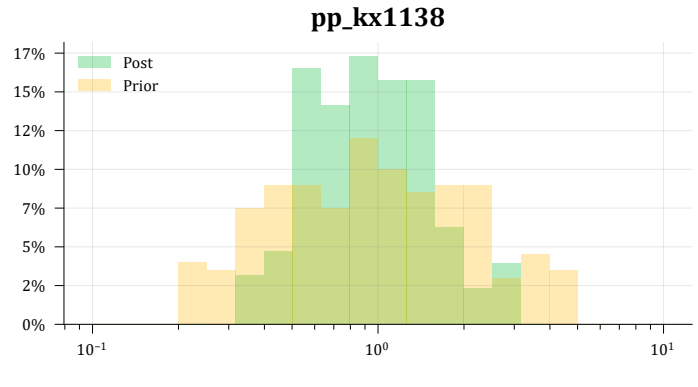

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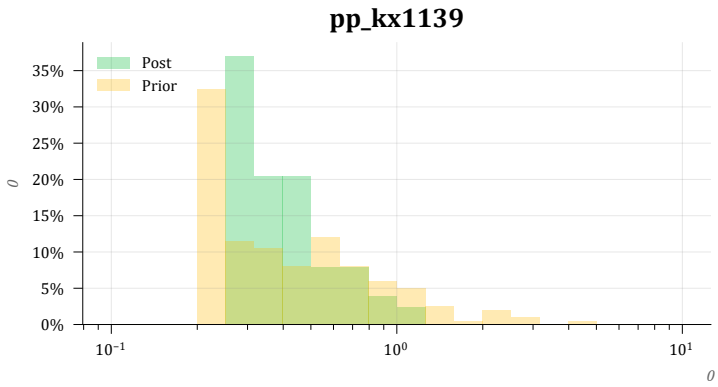

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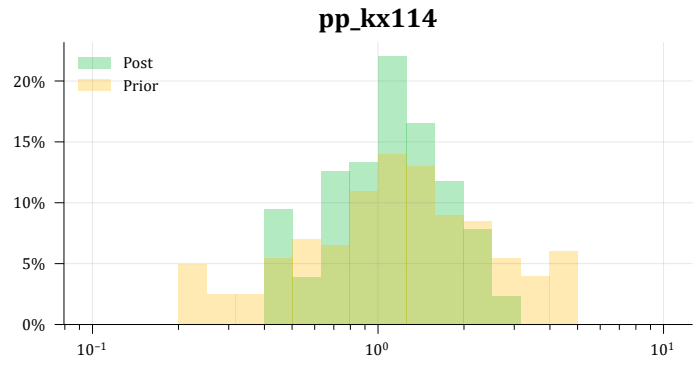

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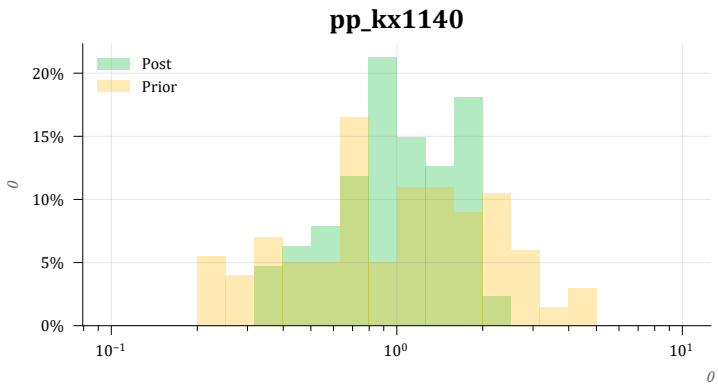

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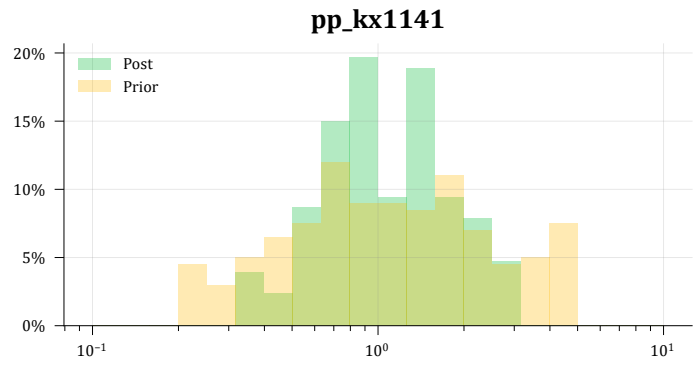

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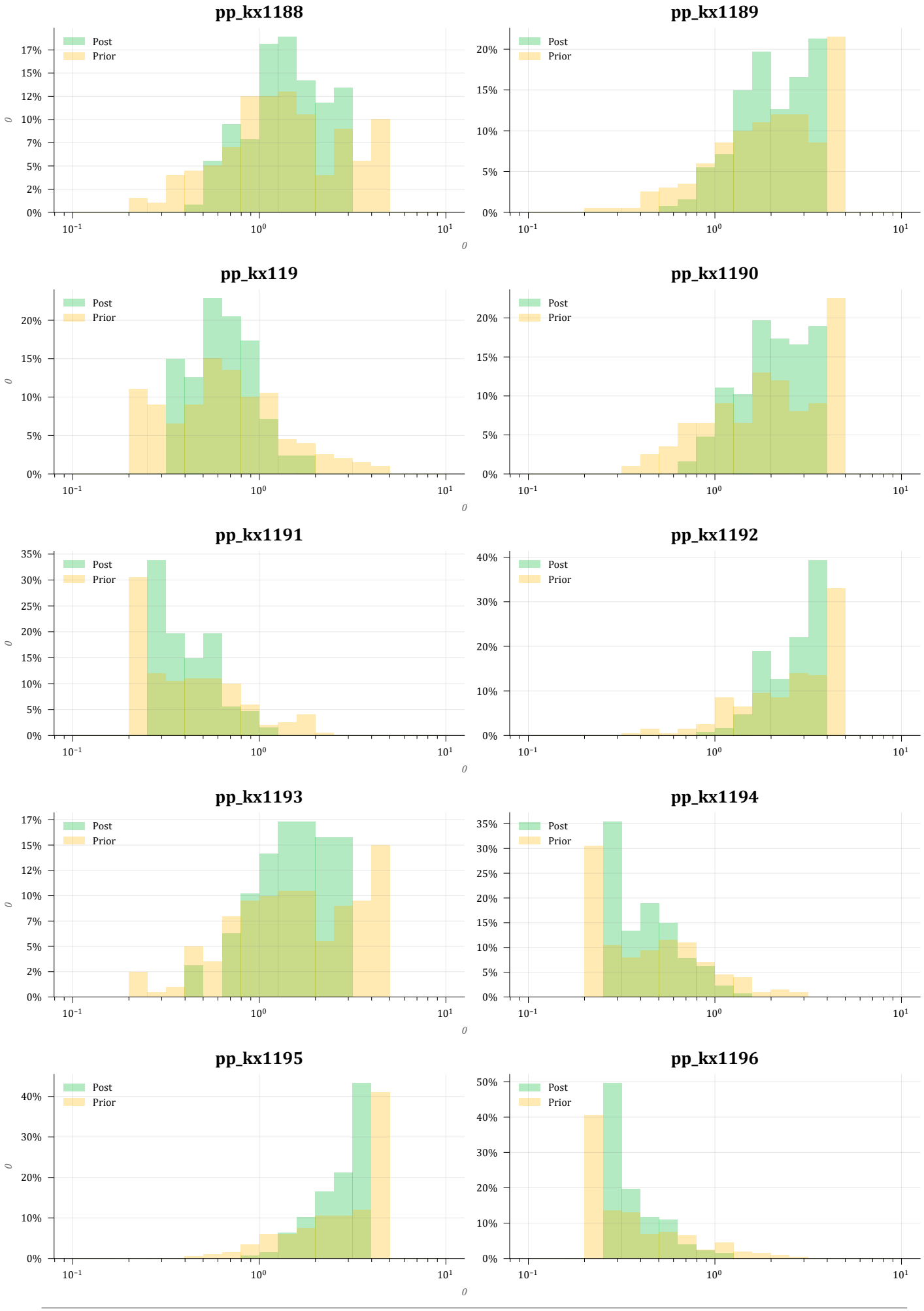

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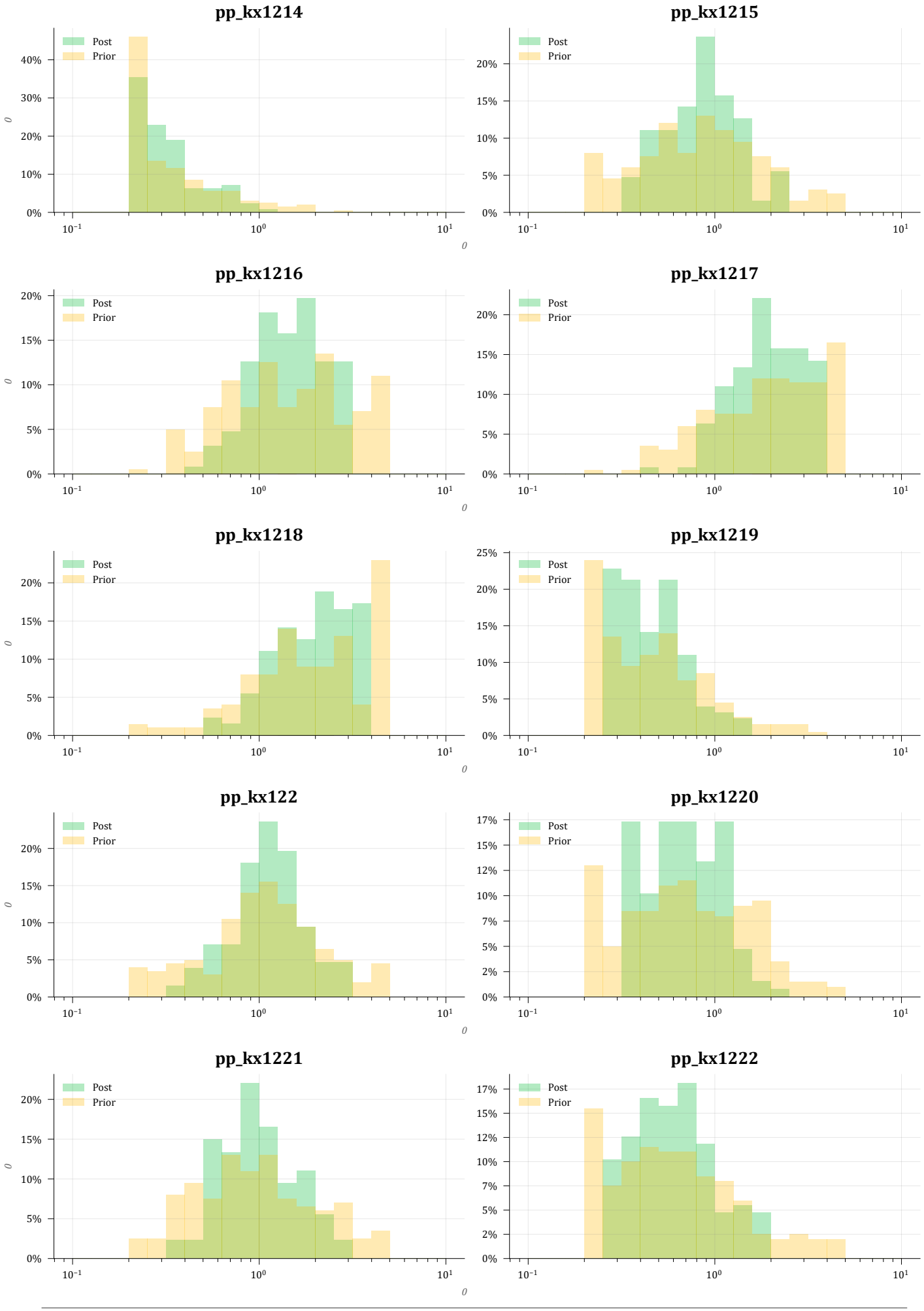

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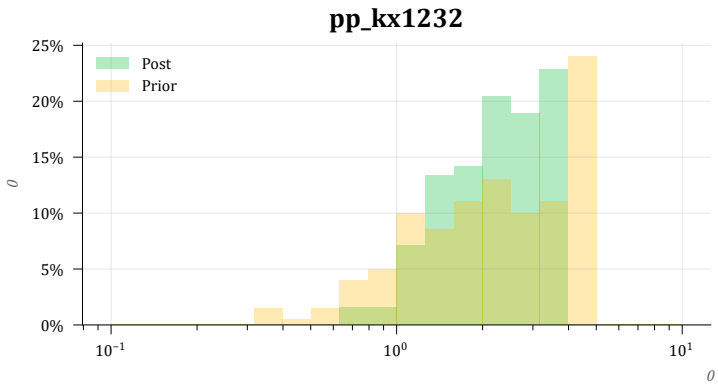

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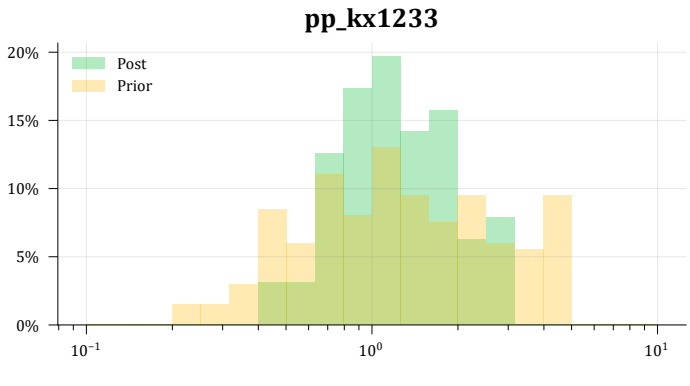

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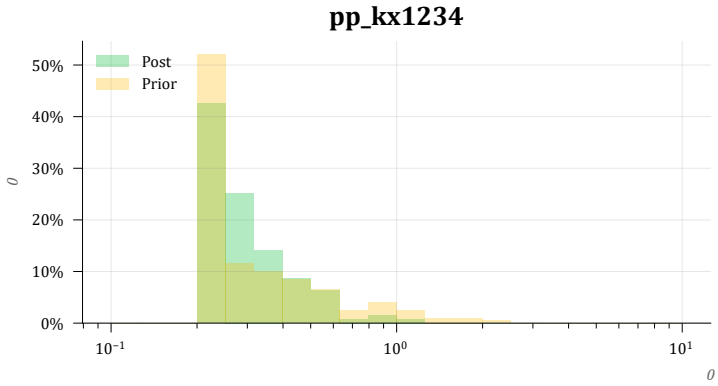

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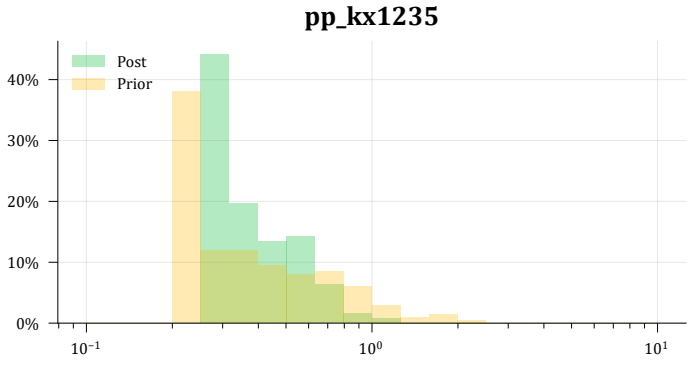

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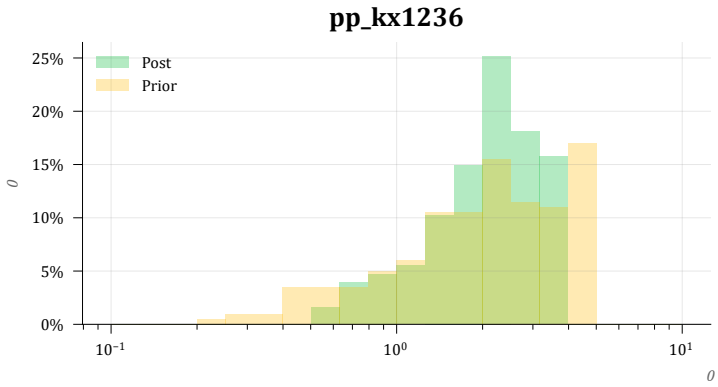

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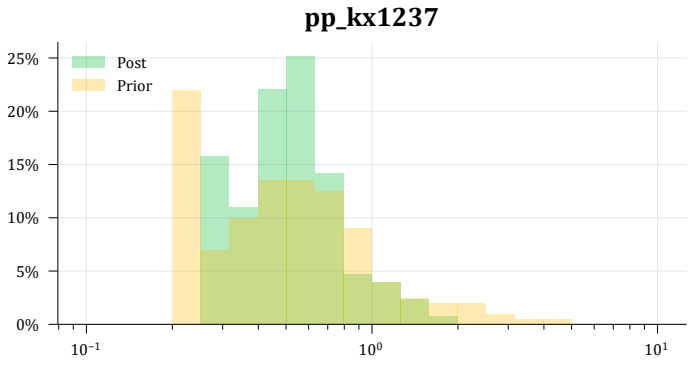

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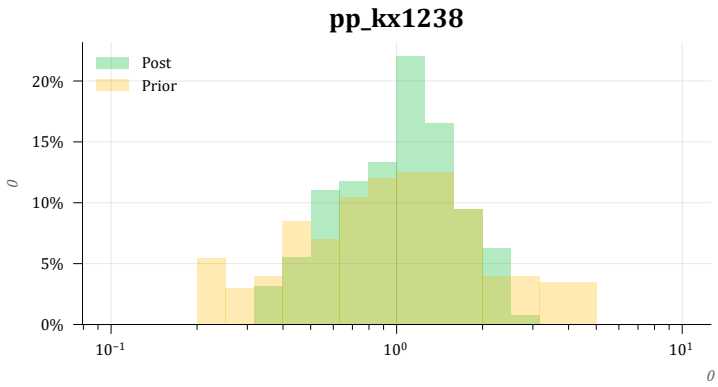

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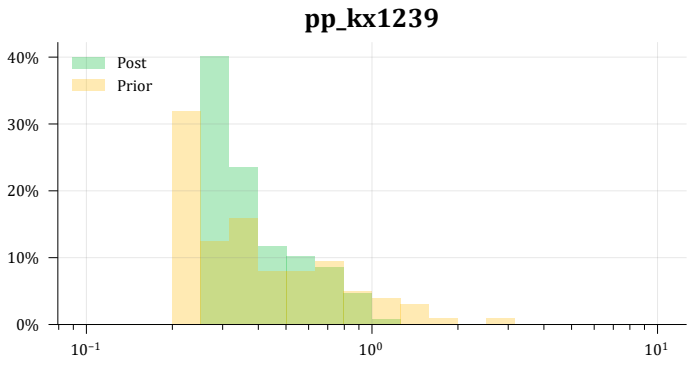

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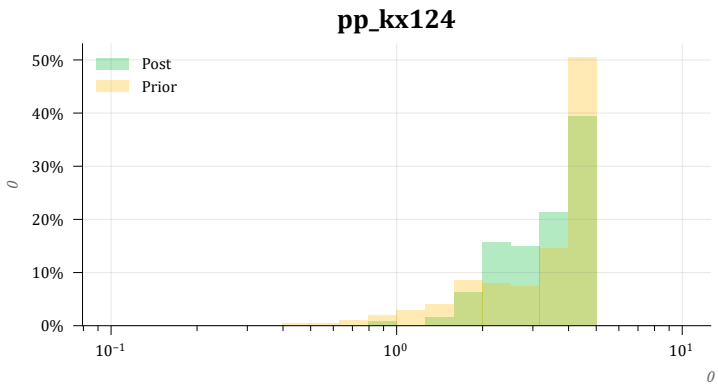

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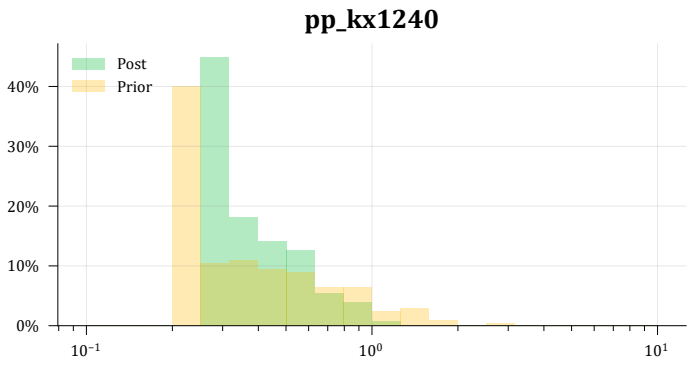

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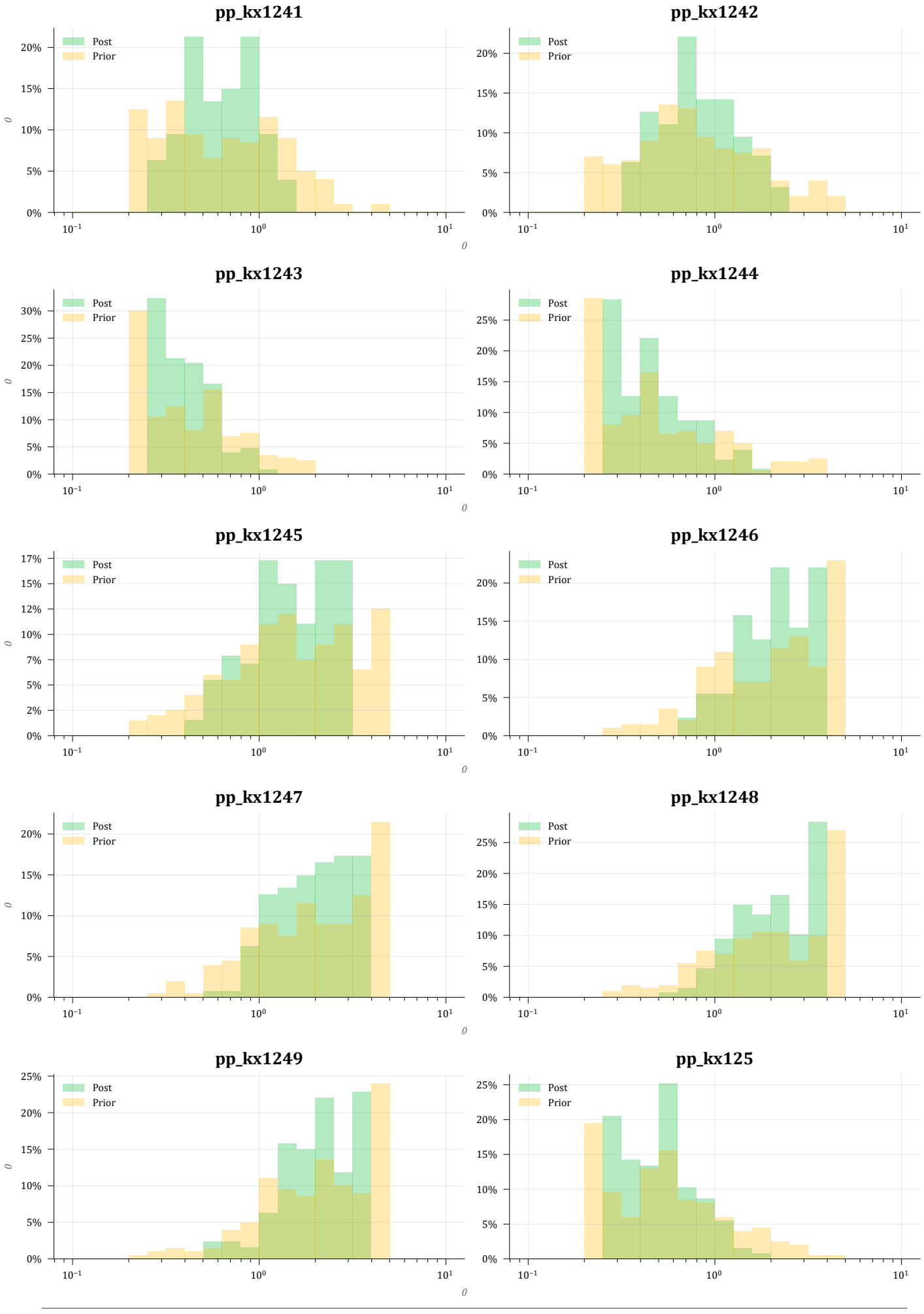

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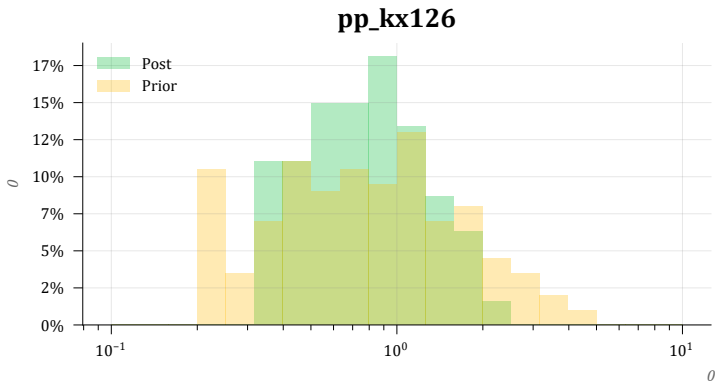

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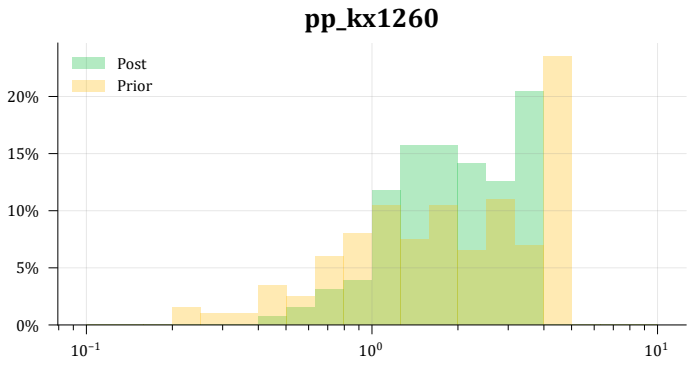

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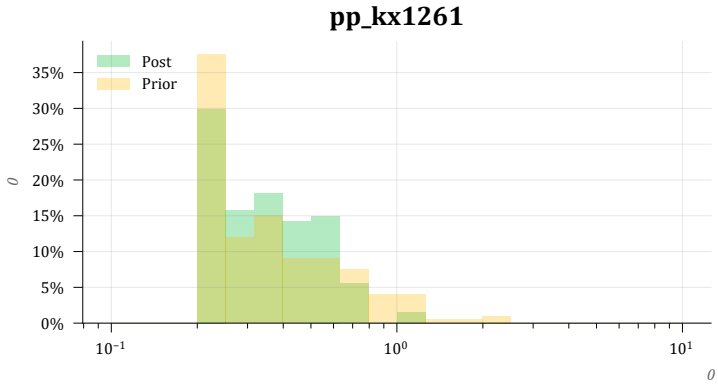

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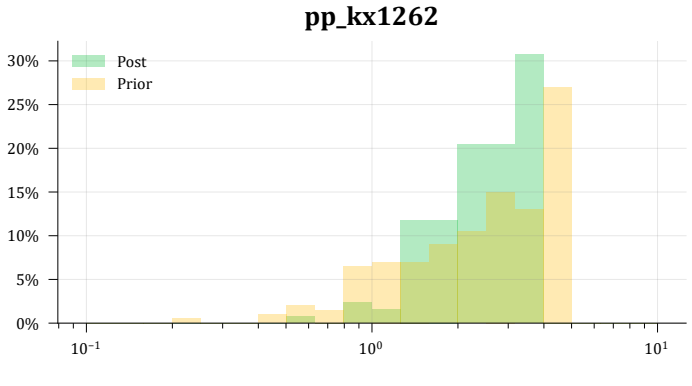

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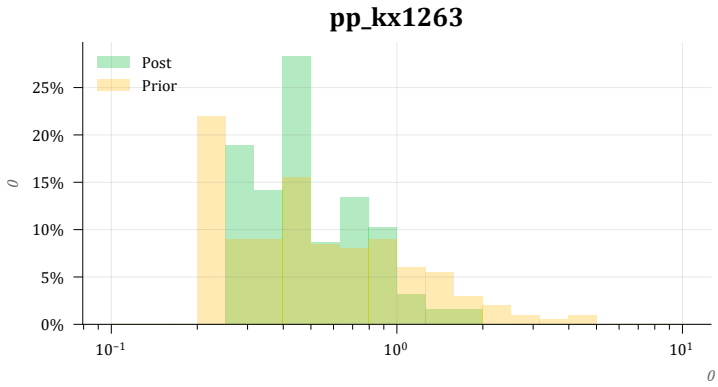

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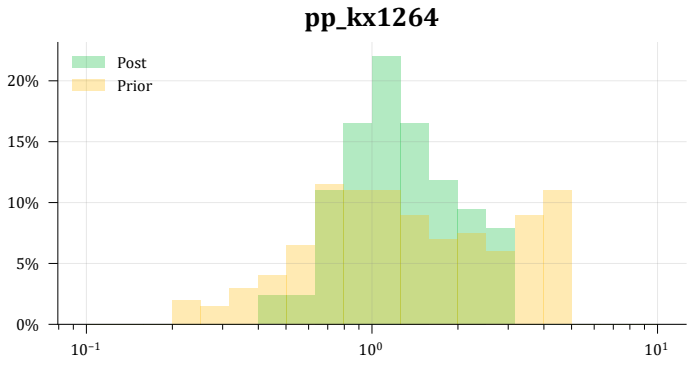

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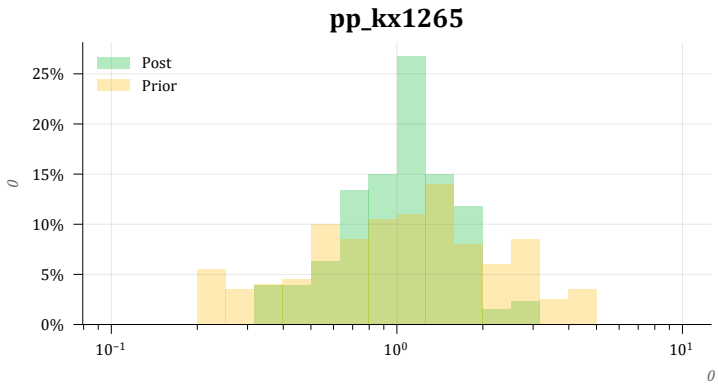

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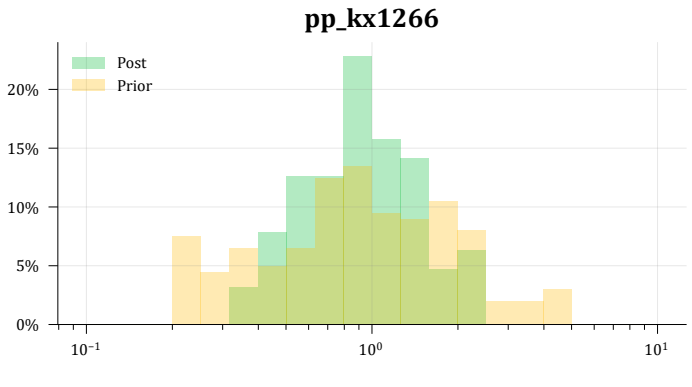

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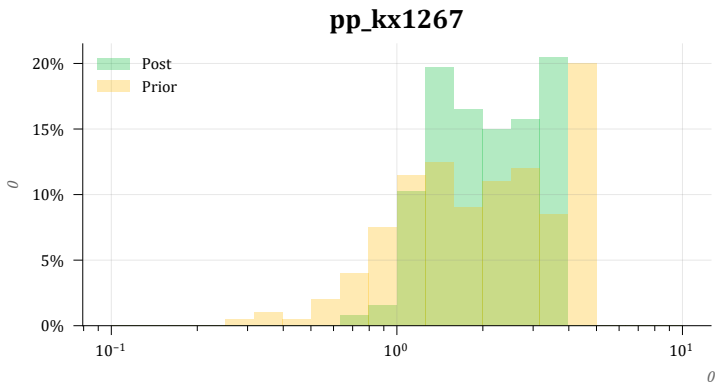

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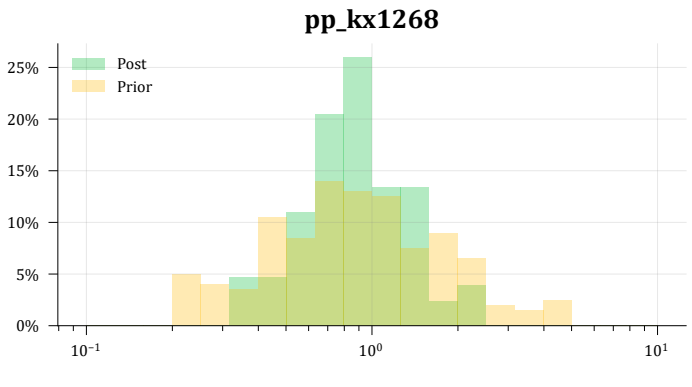

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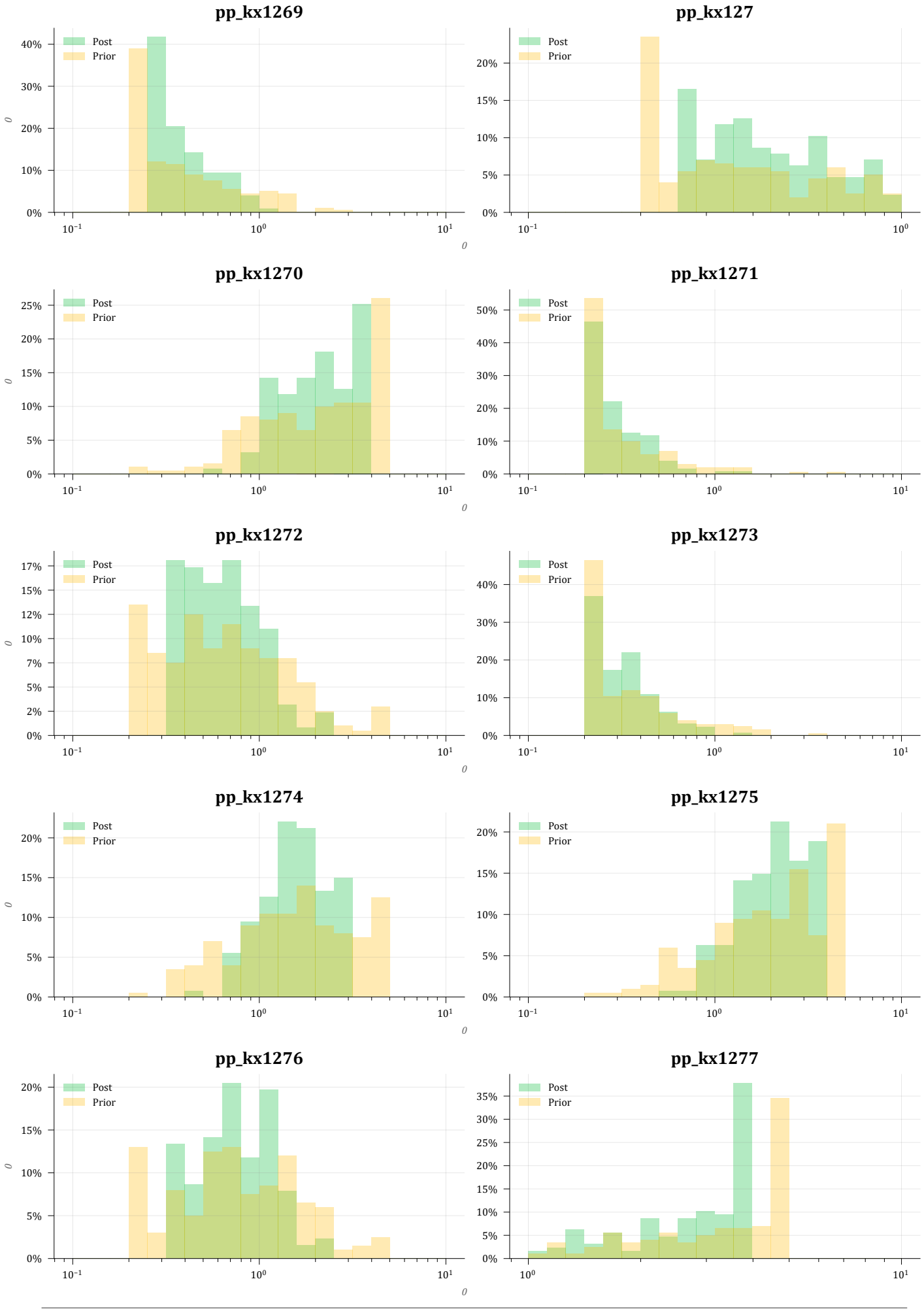

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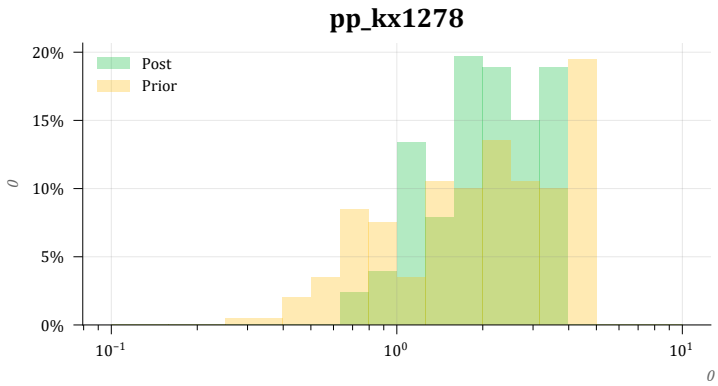

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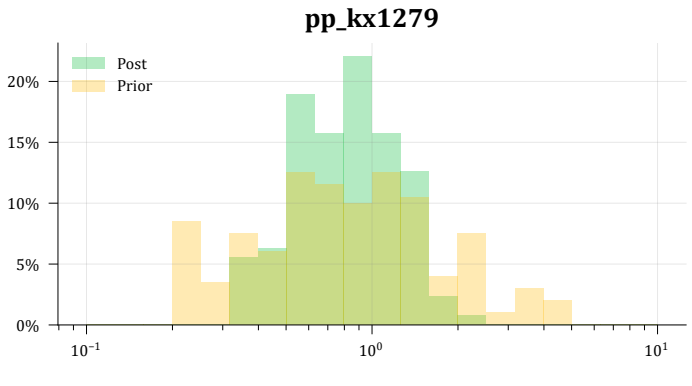

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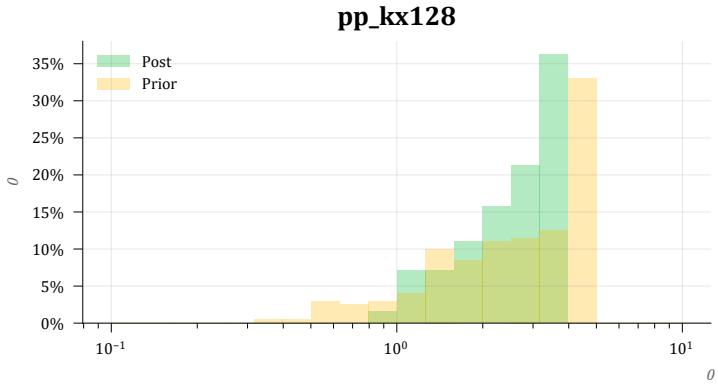

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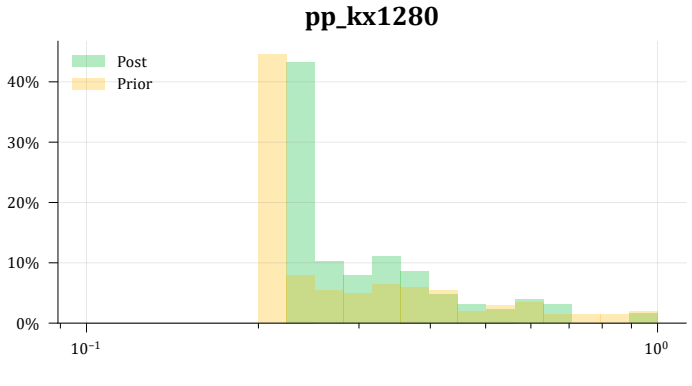
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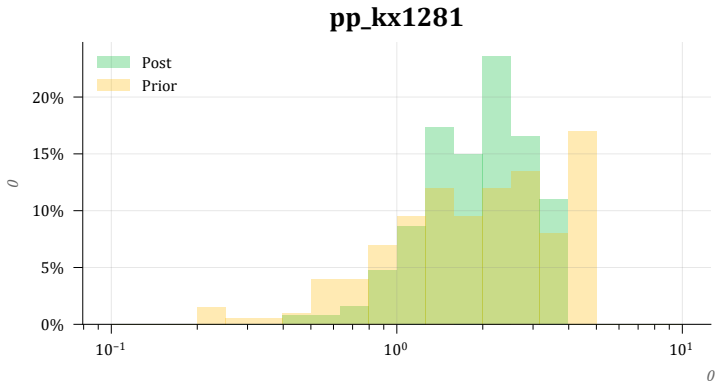

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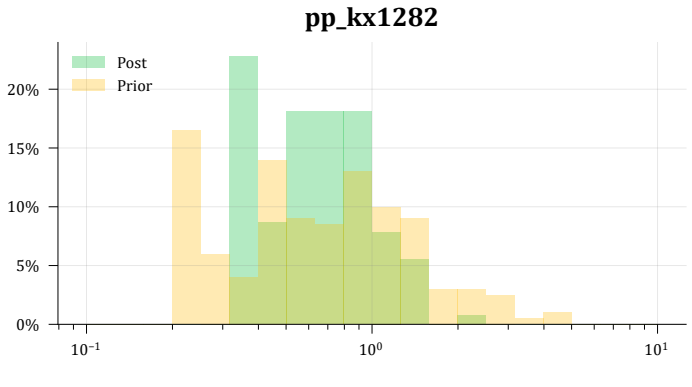

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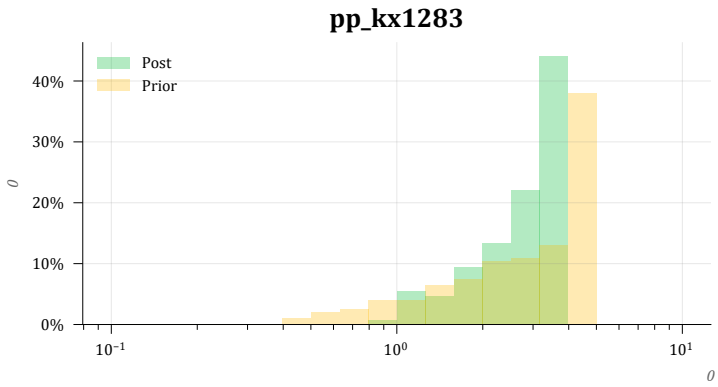

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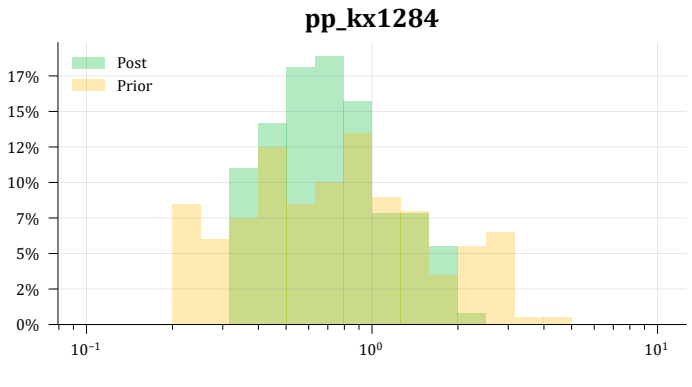

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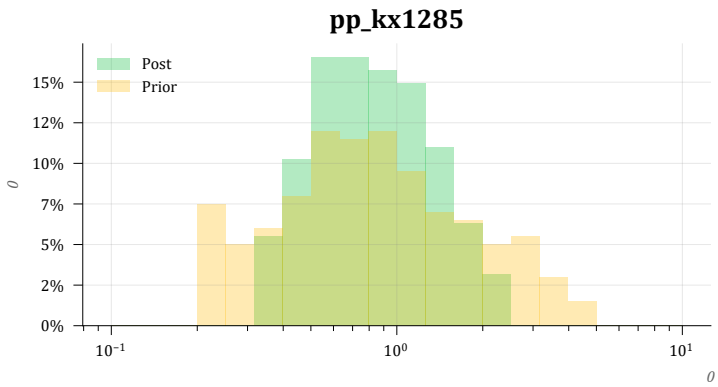

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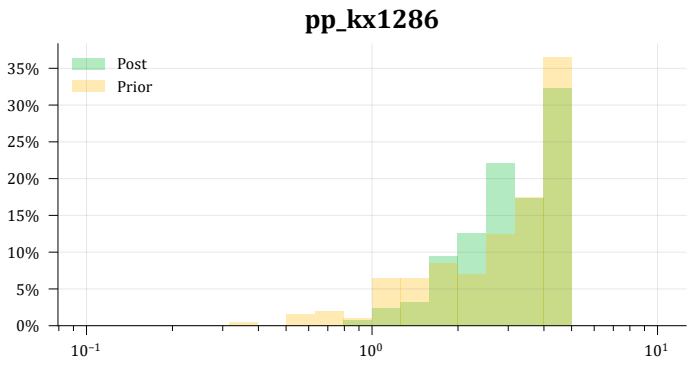

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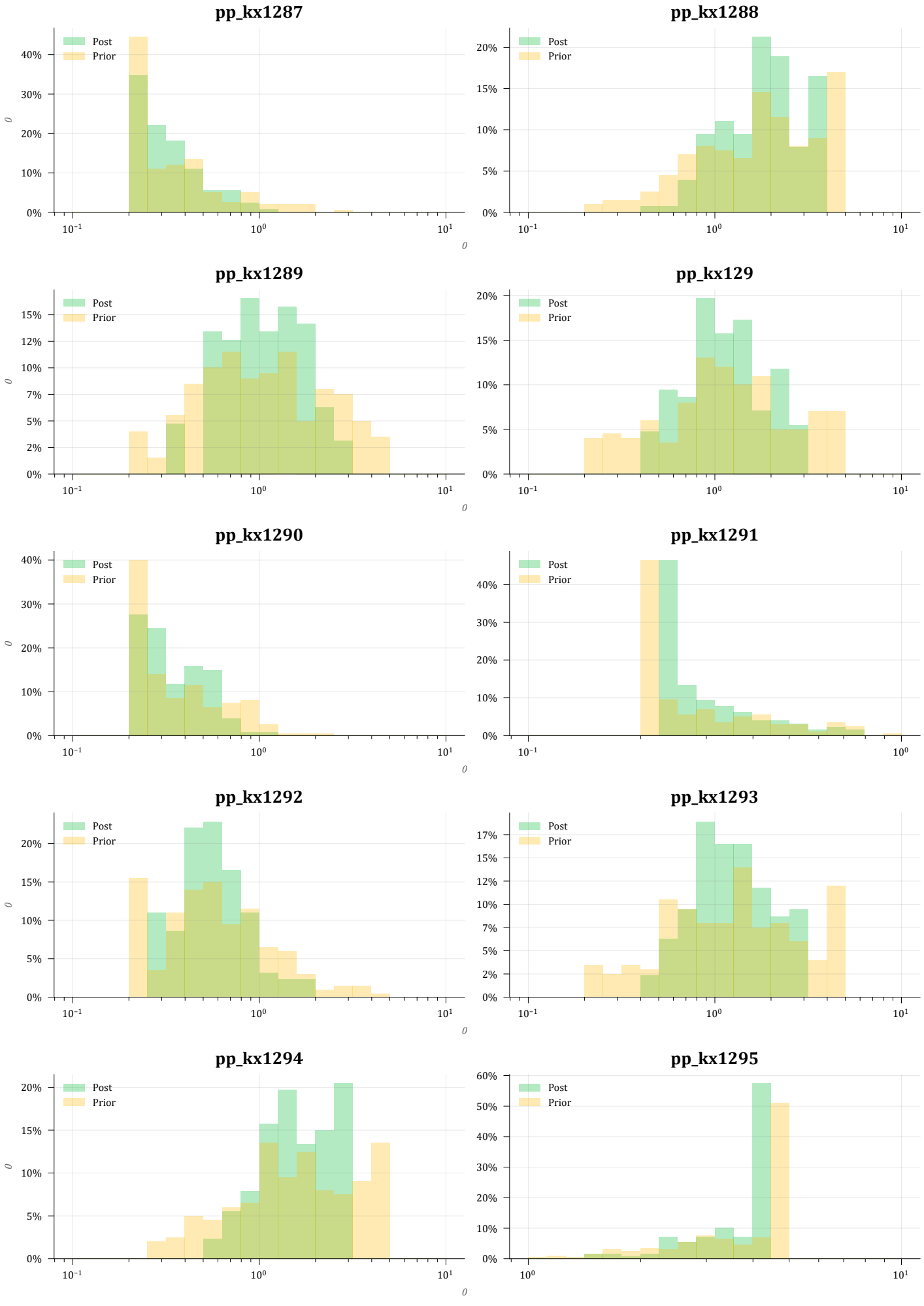

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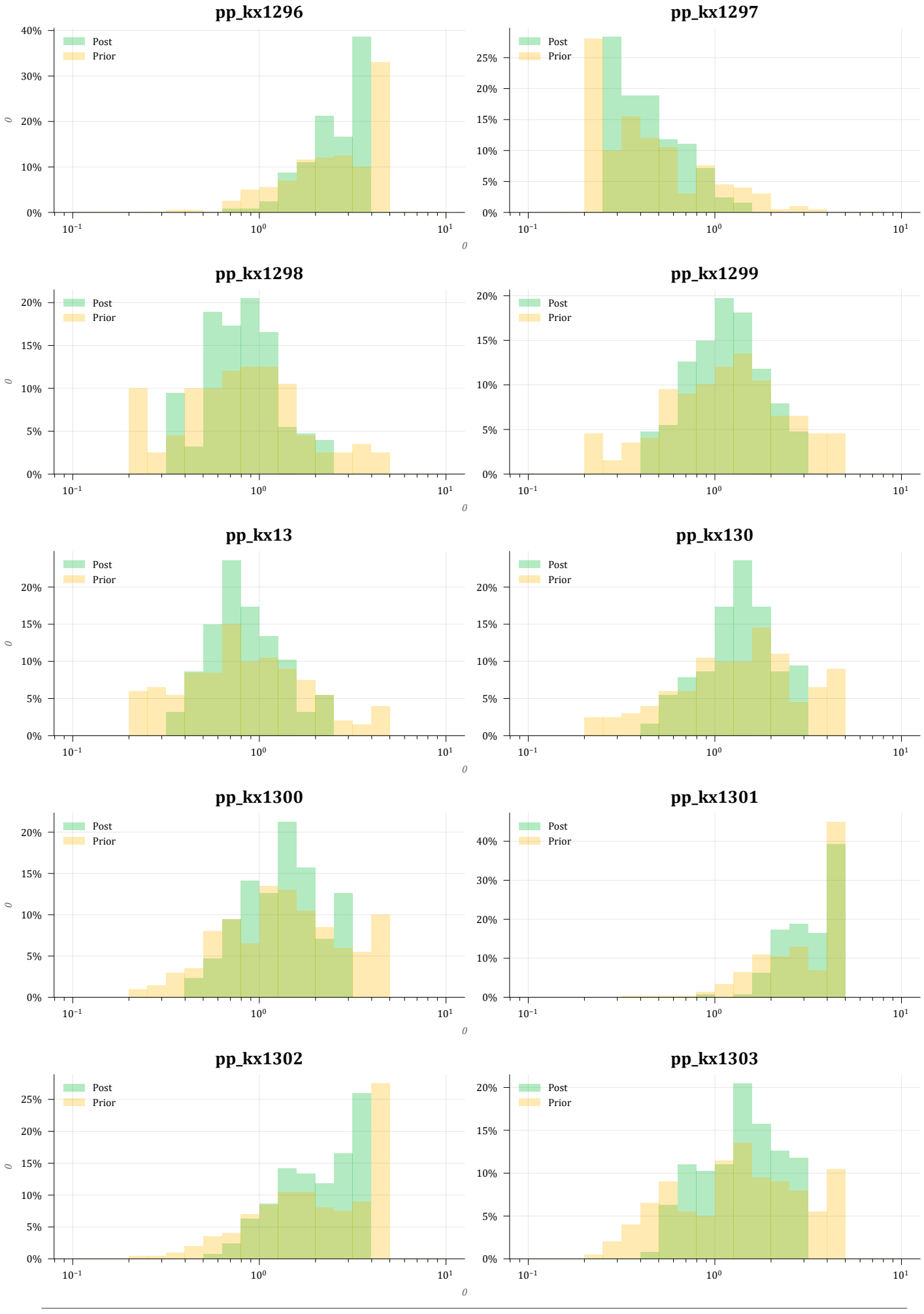

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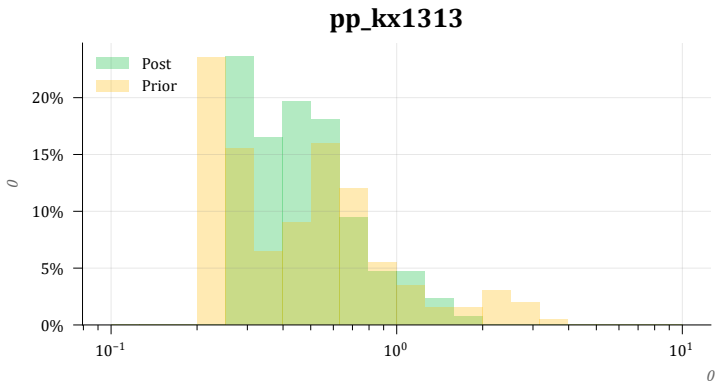

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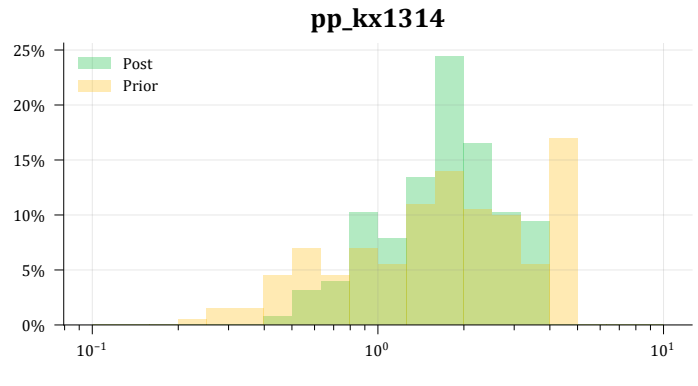

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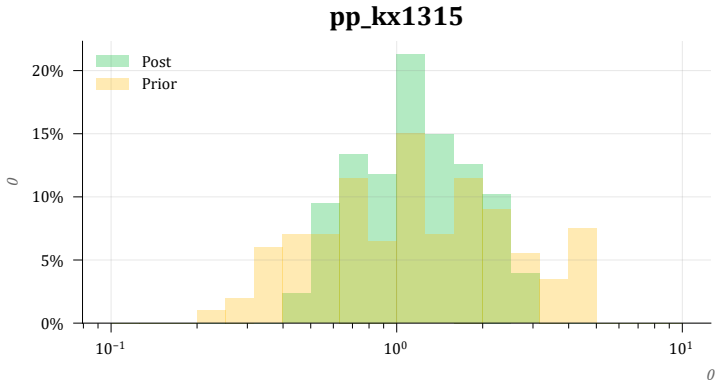

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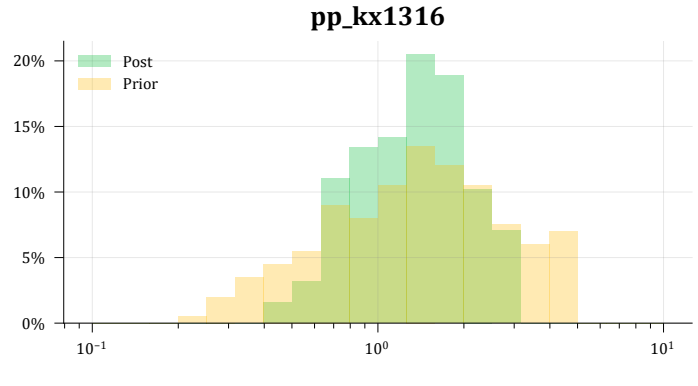

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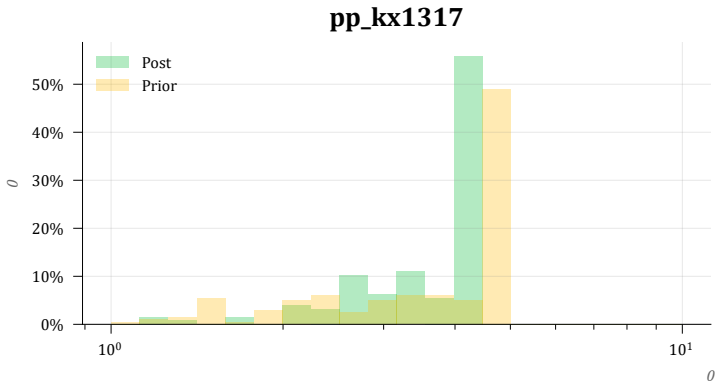

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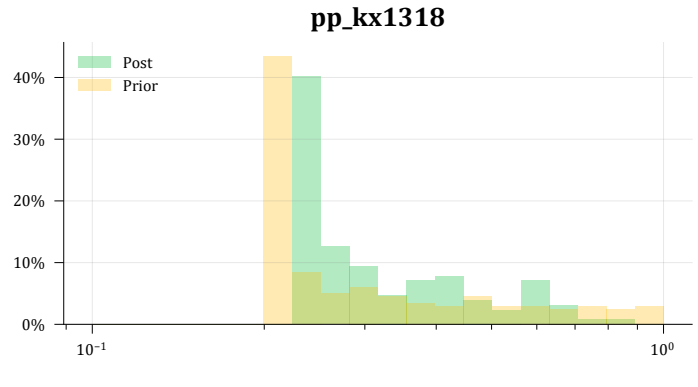

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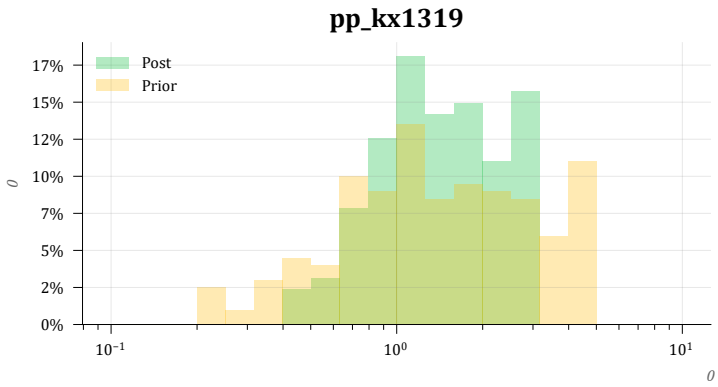

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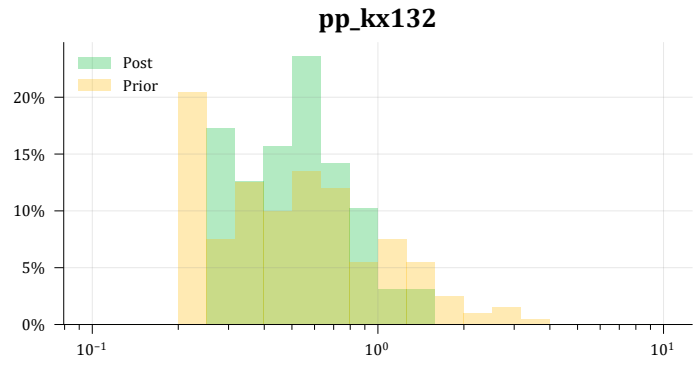

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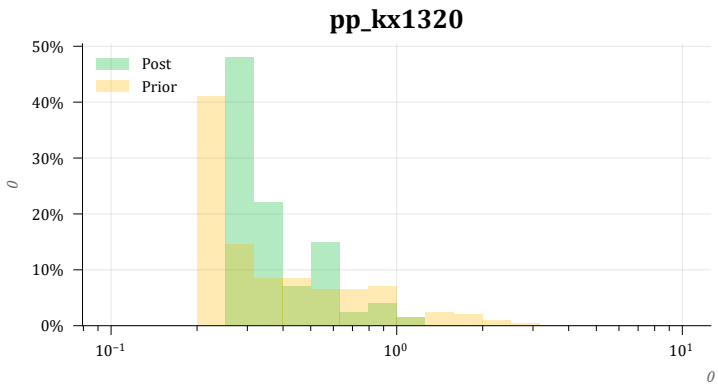

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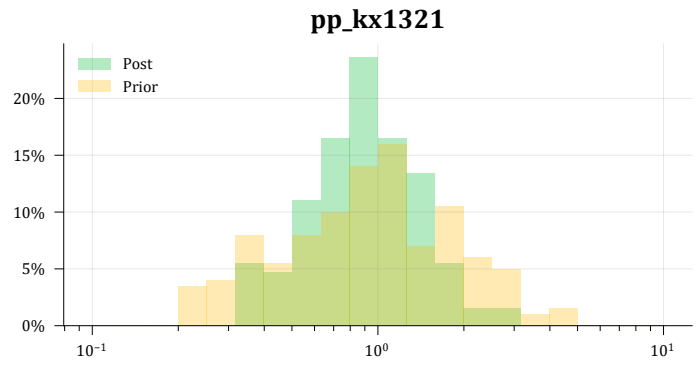

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pp_kx1318
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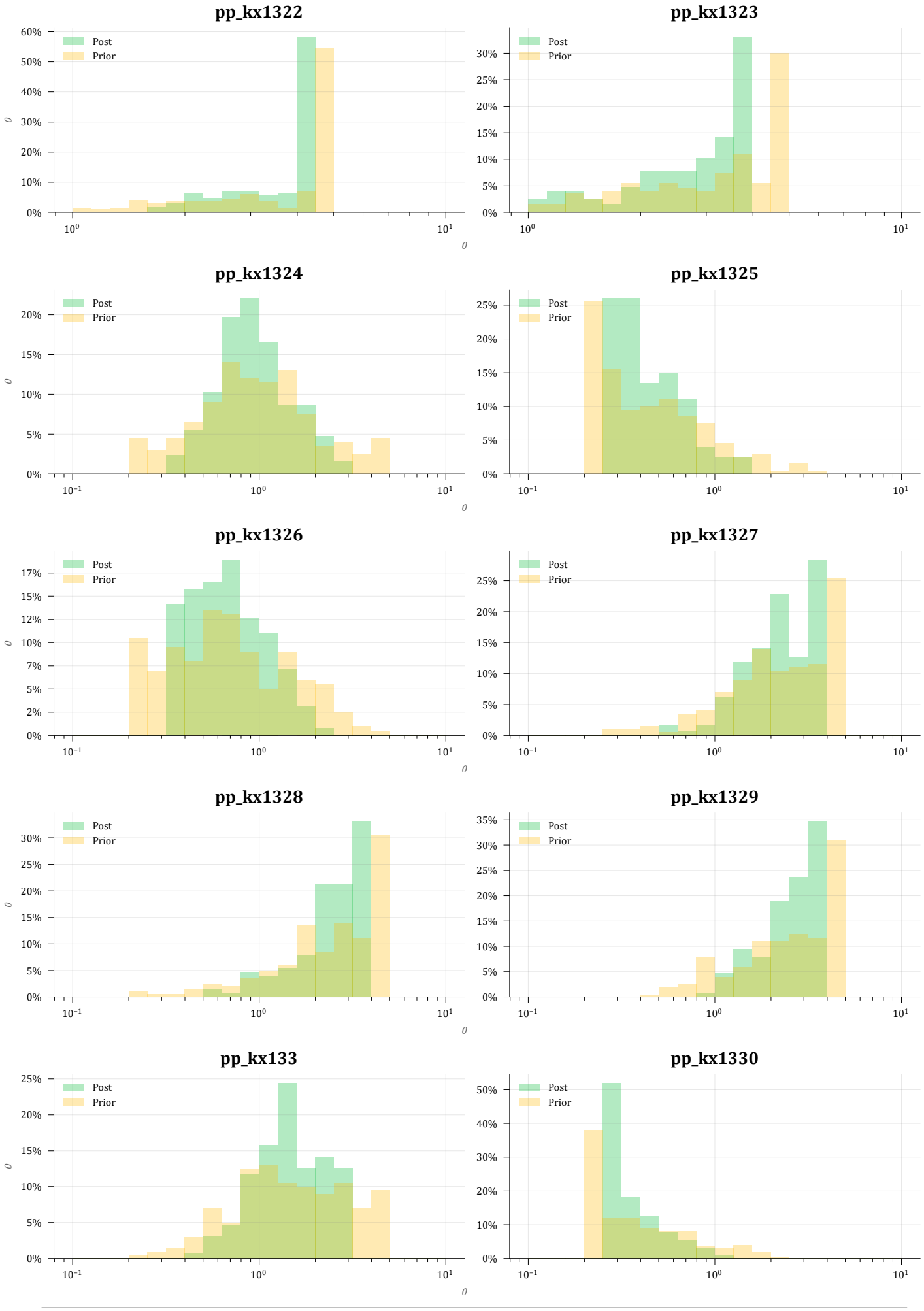

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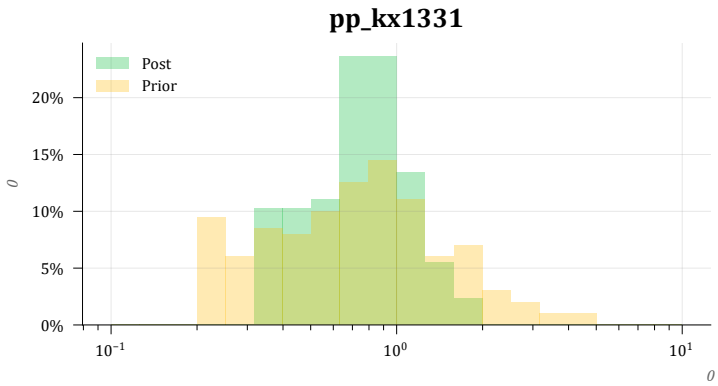

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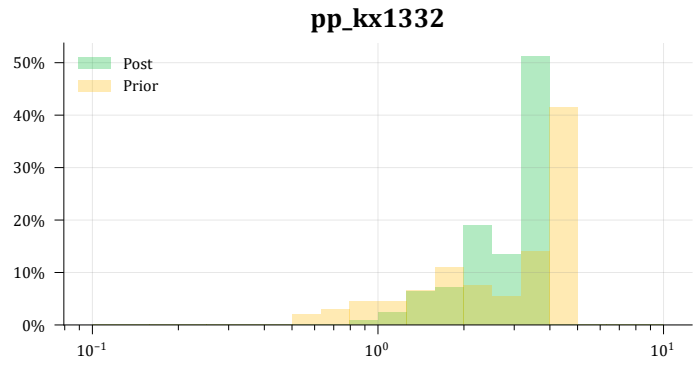

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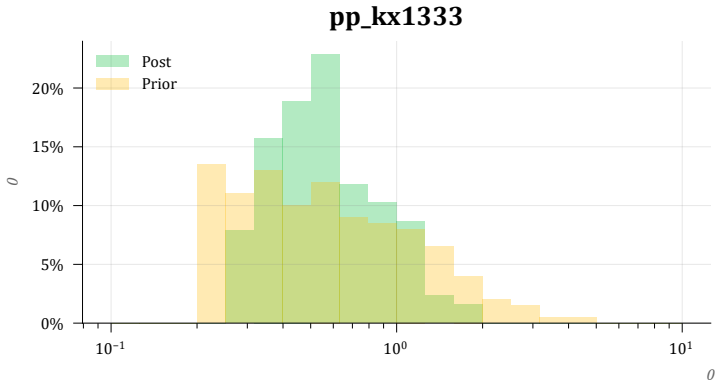

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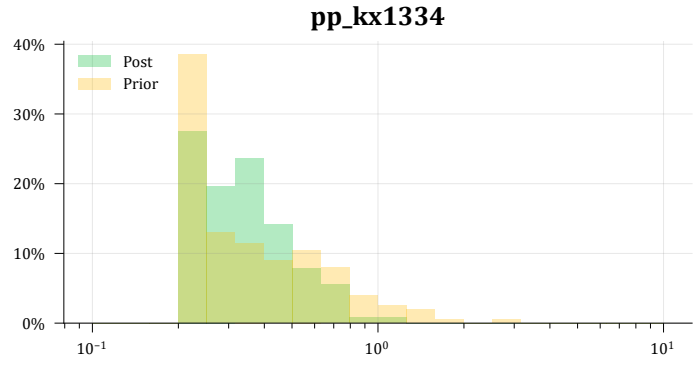
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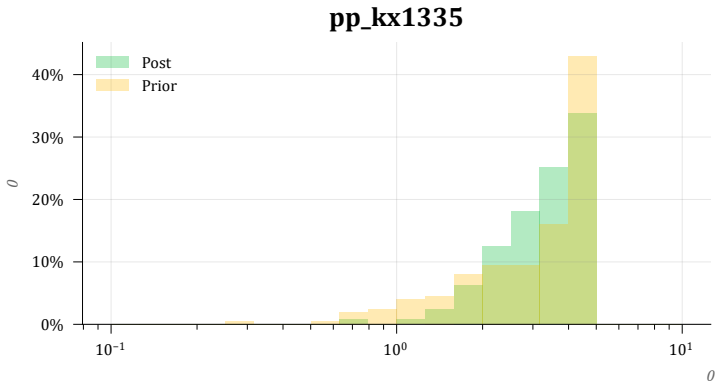

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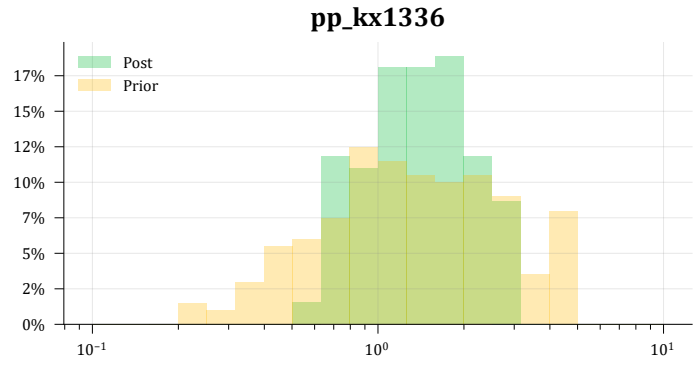

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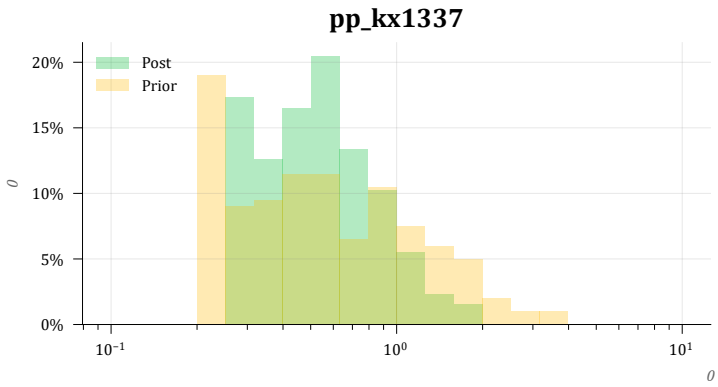

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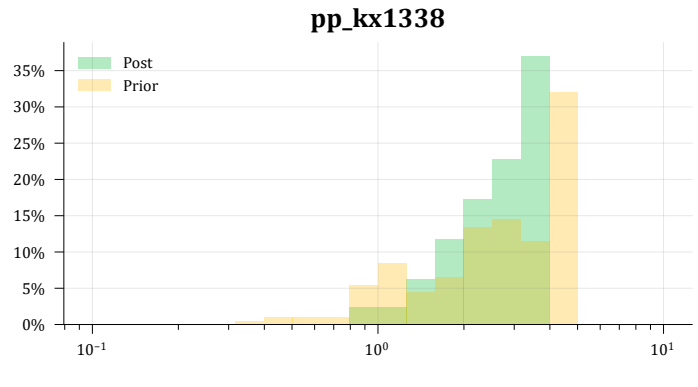

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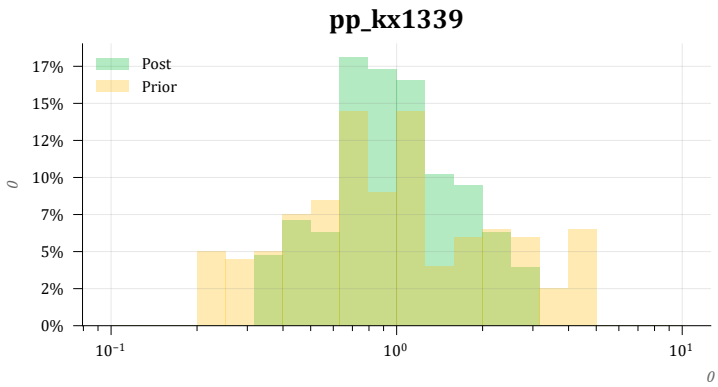

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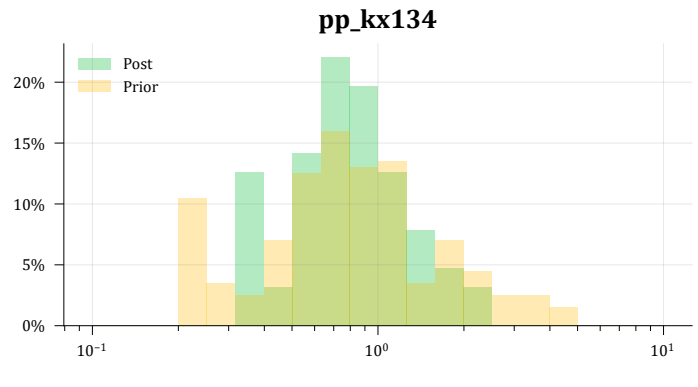

pp_kx1335
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Prior
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10^{1}
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pp_kx1336
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Prior
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2%
0%
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10^{1}

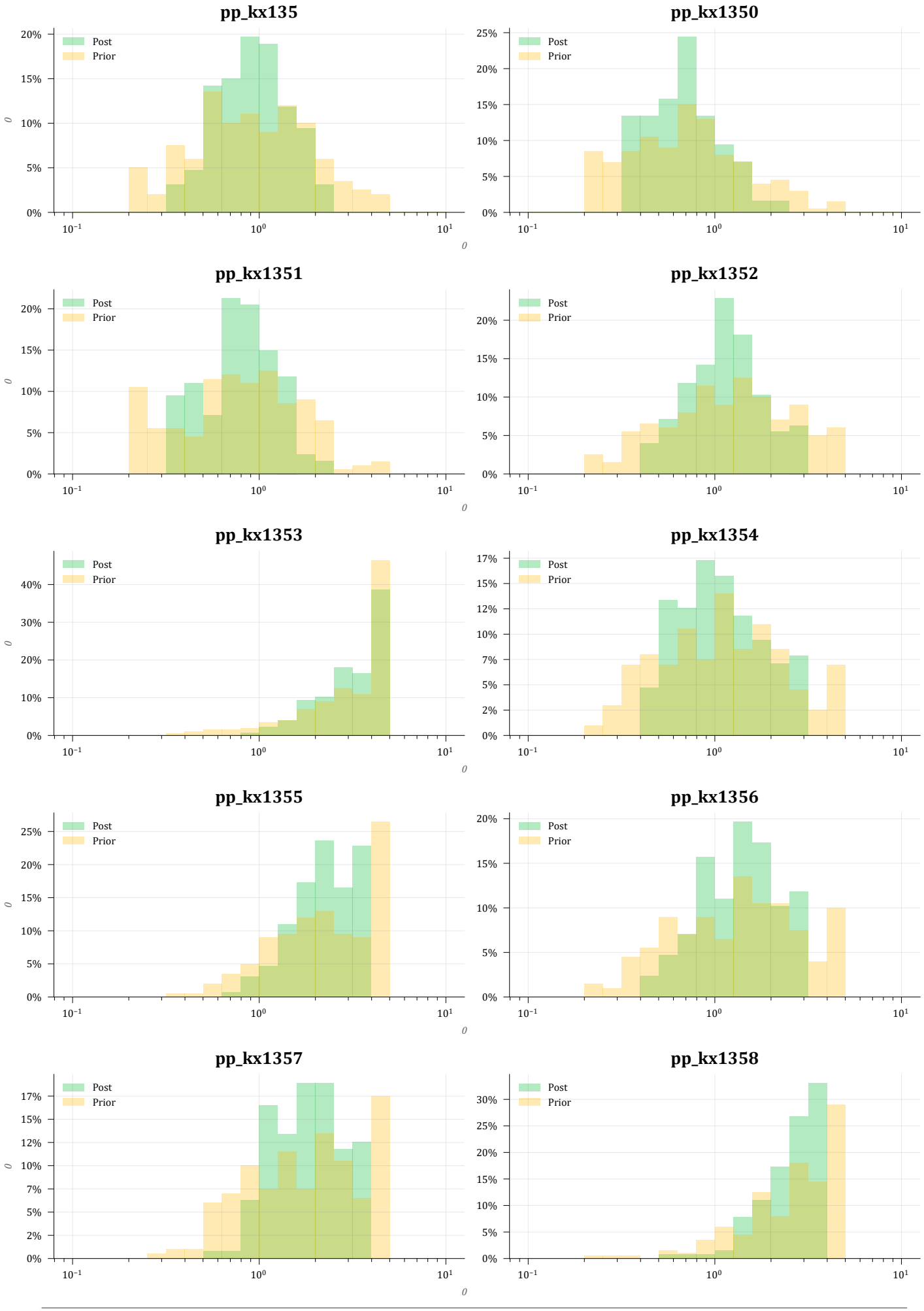

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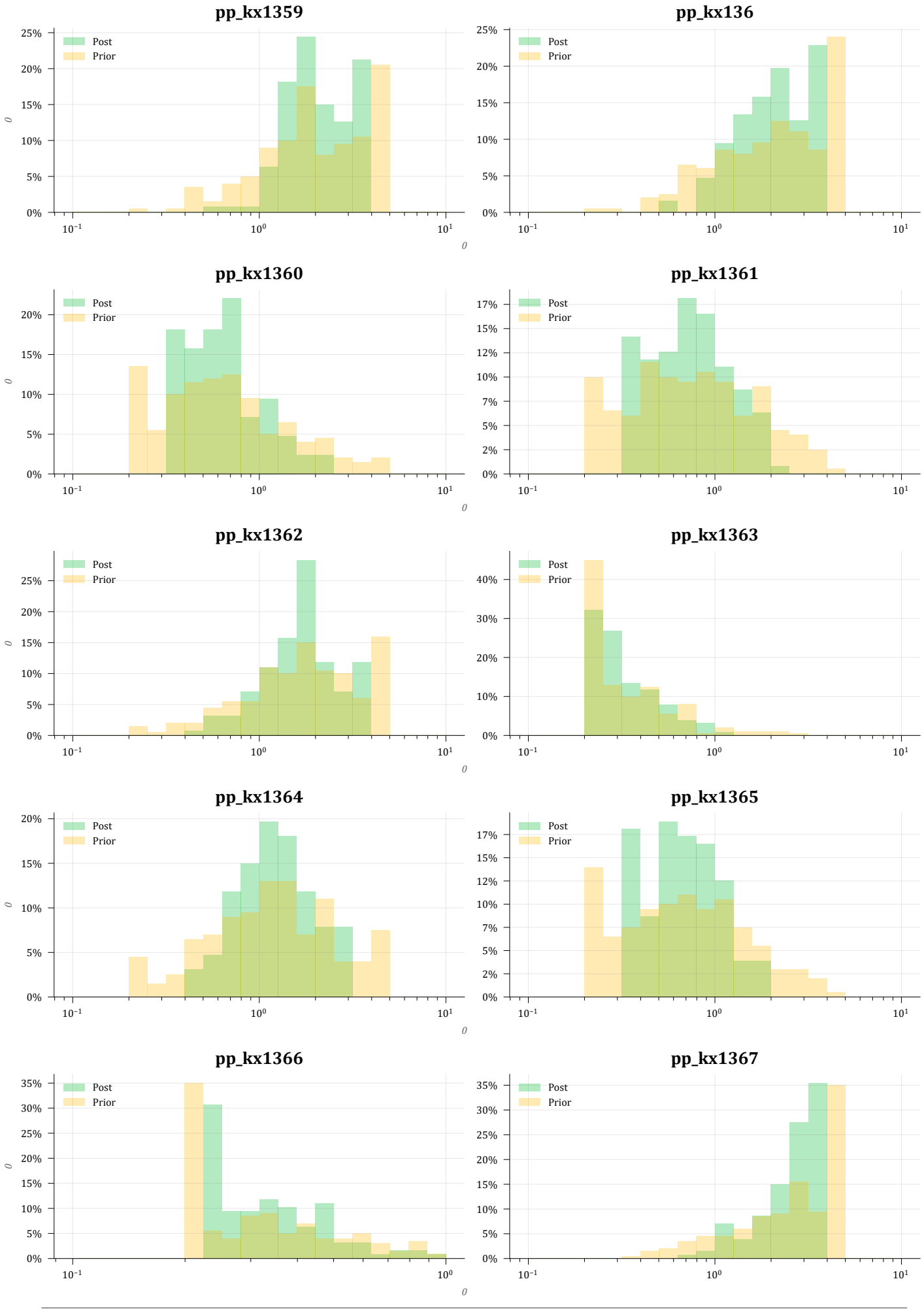

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10^{1}


pp_kx1339
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12%
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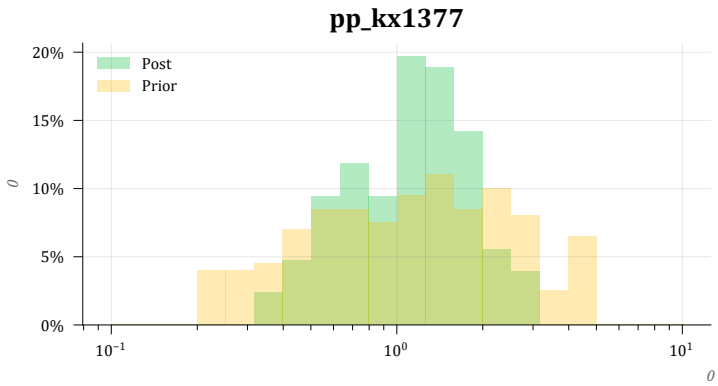

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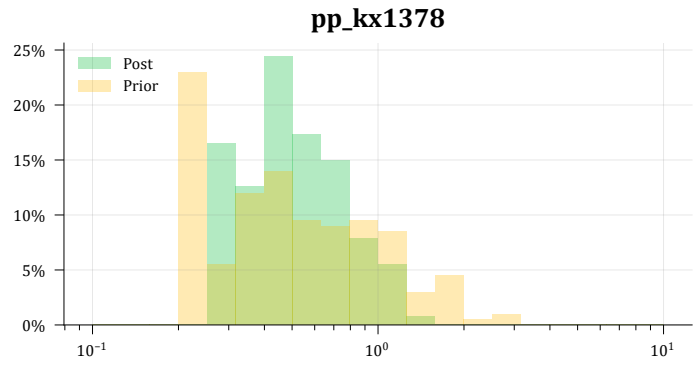

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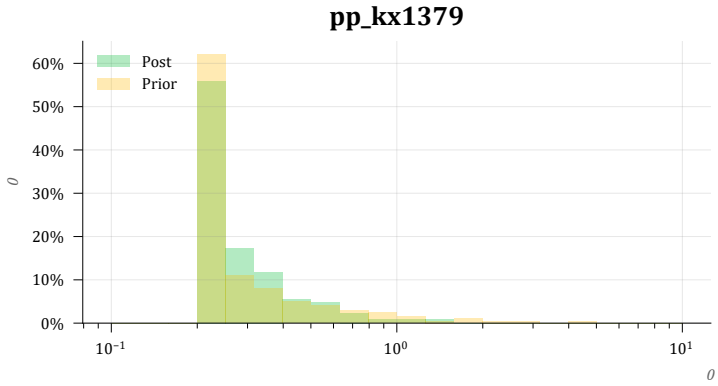

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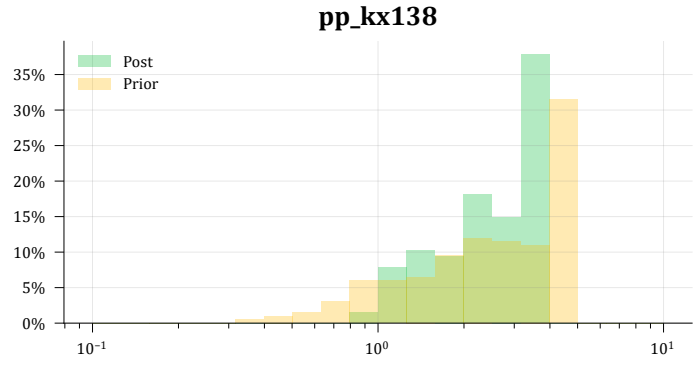

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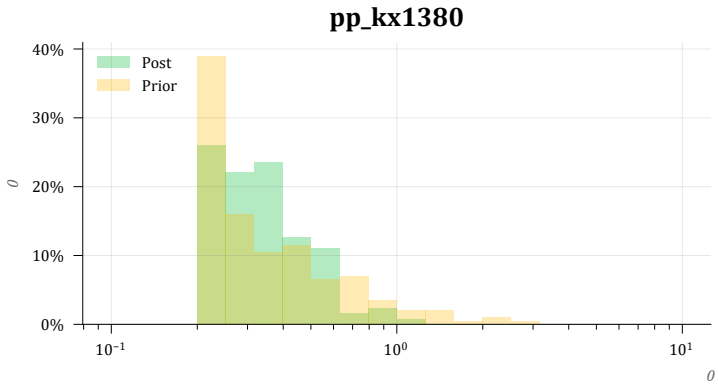

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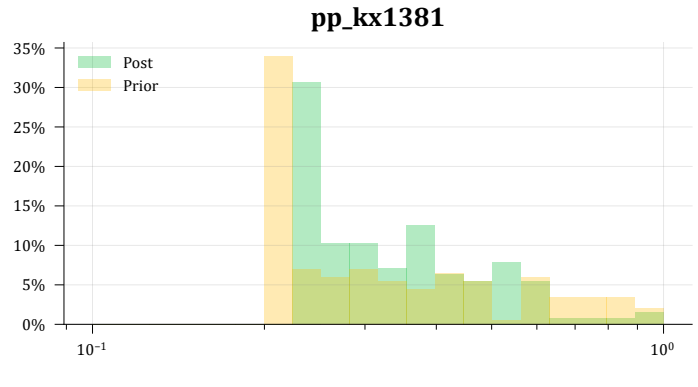

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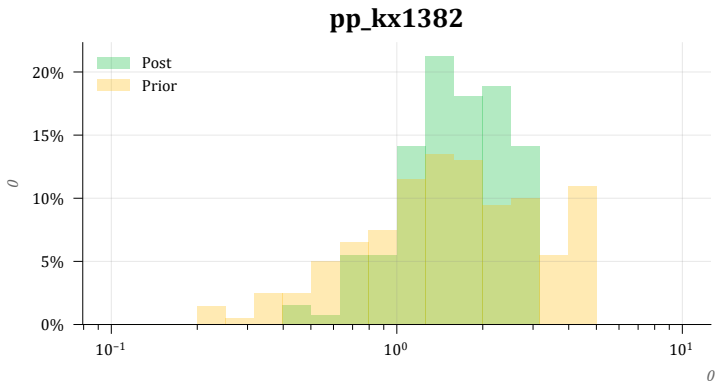

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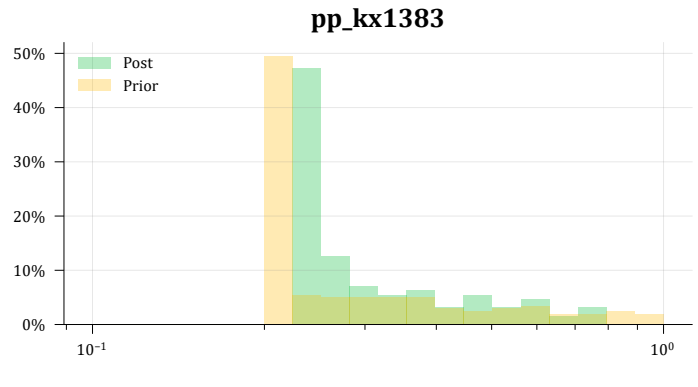

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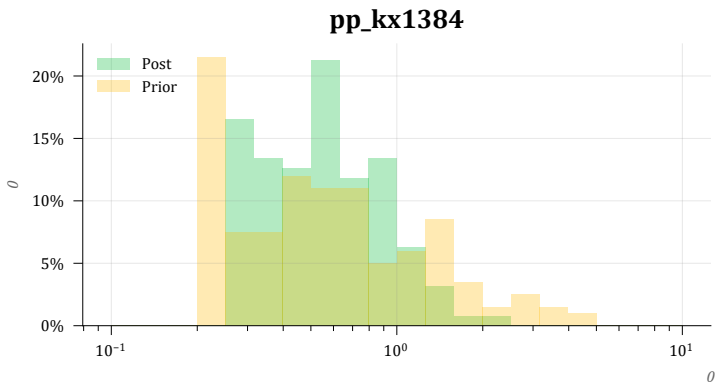

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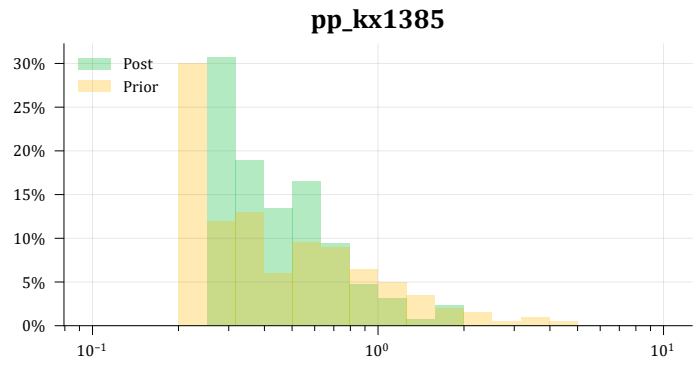

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10^{0}
10^{1}
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pp_kx1381
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Prior
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30%
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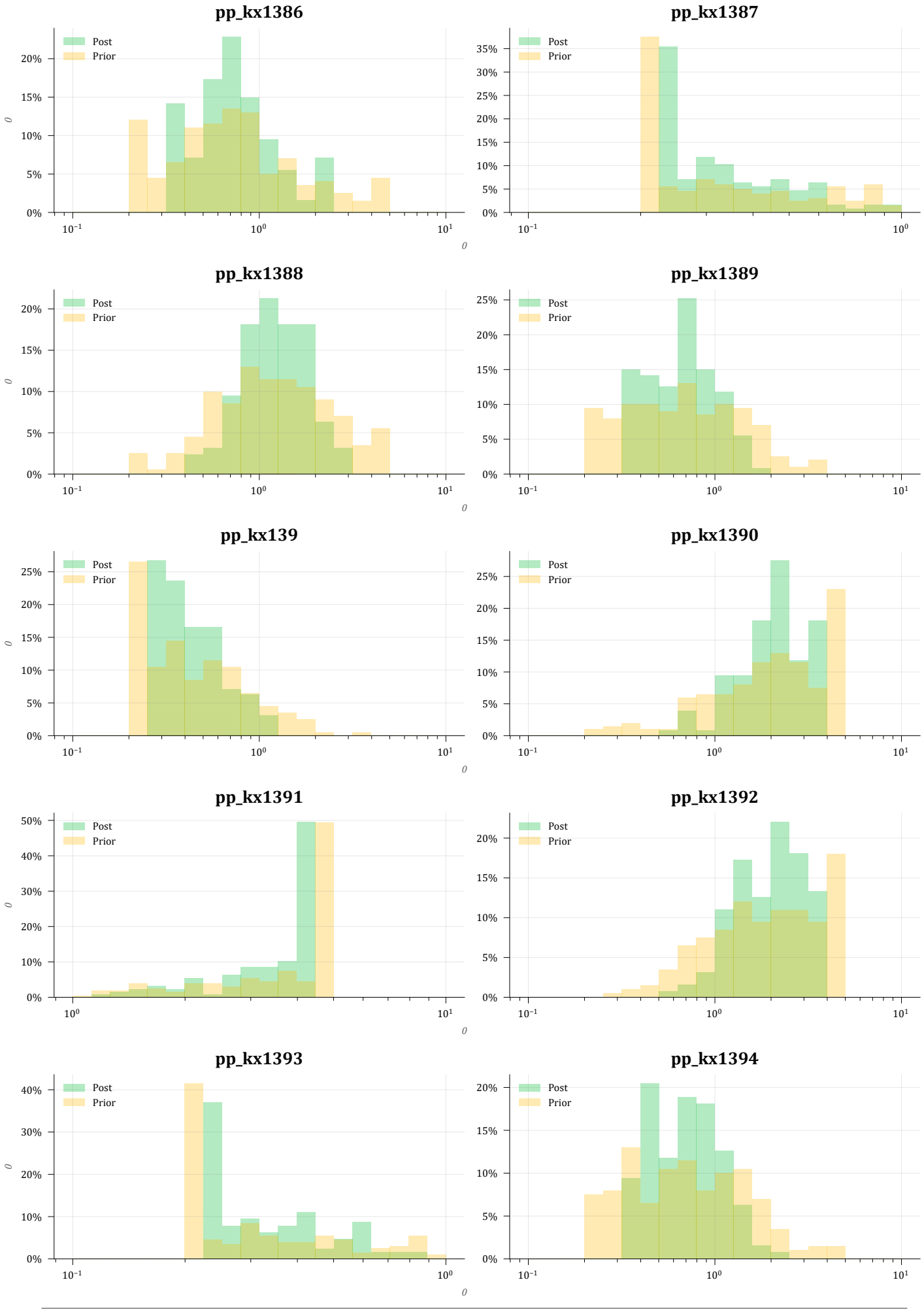

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pp_kx1383
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Prior
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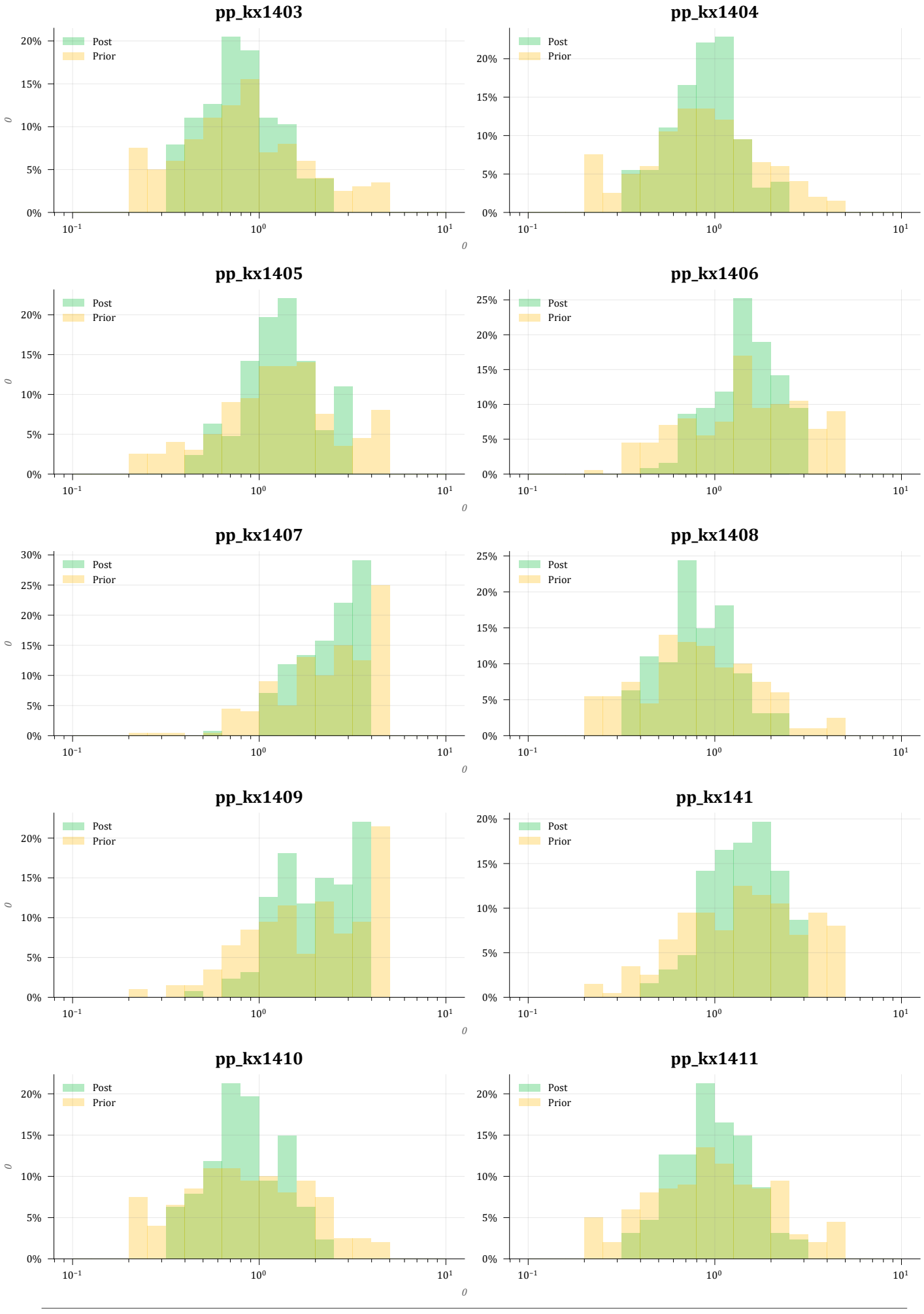

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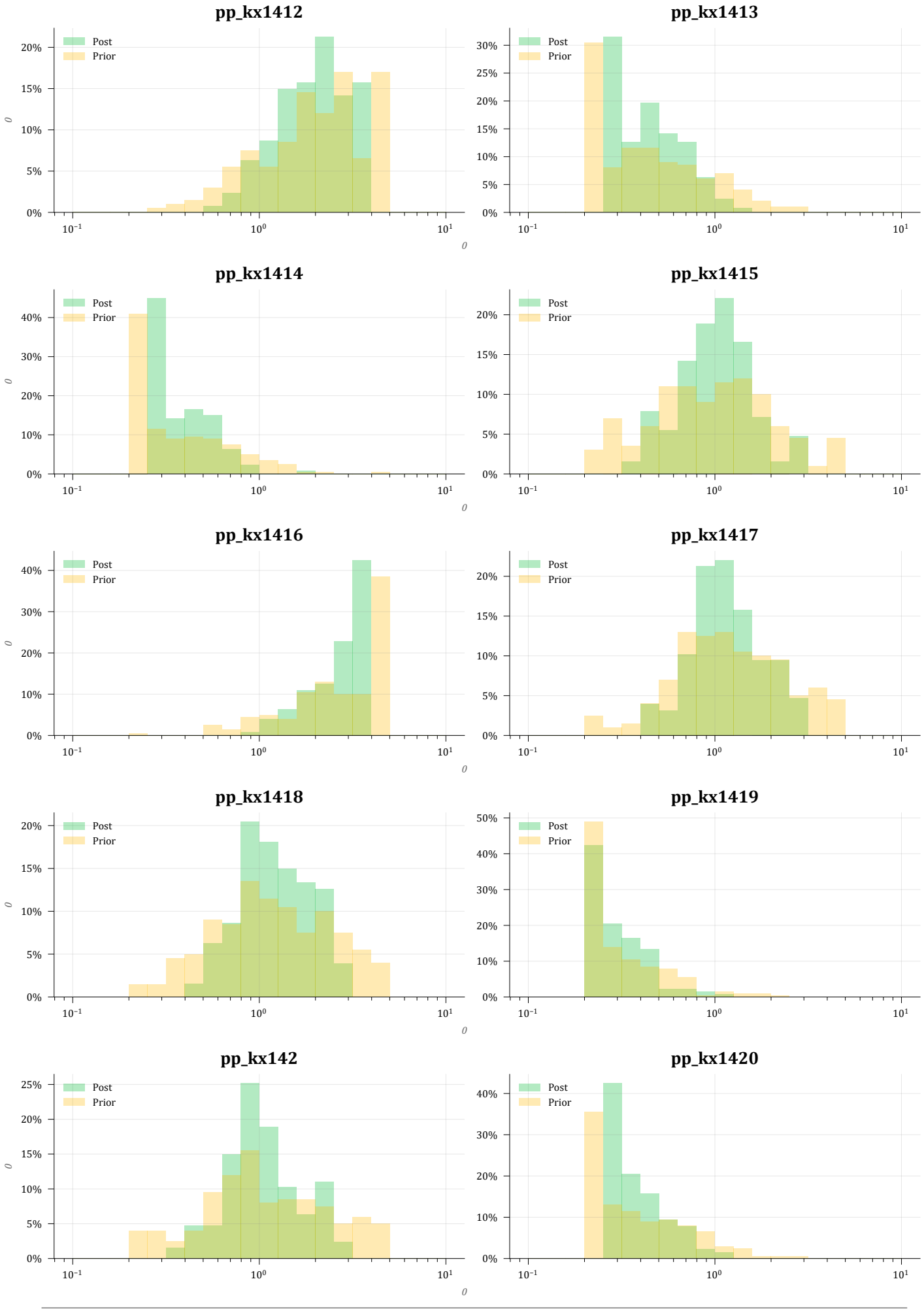

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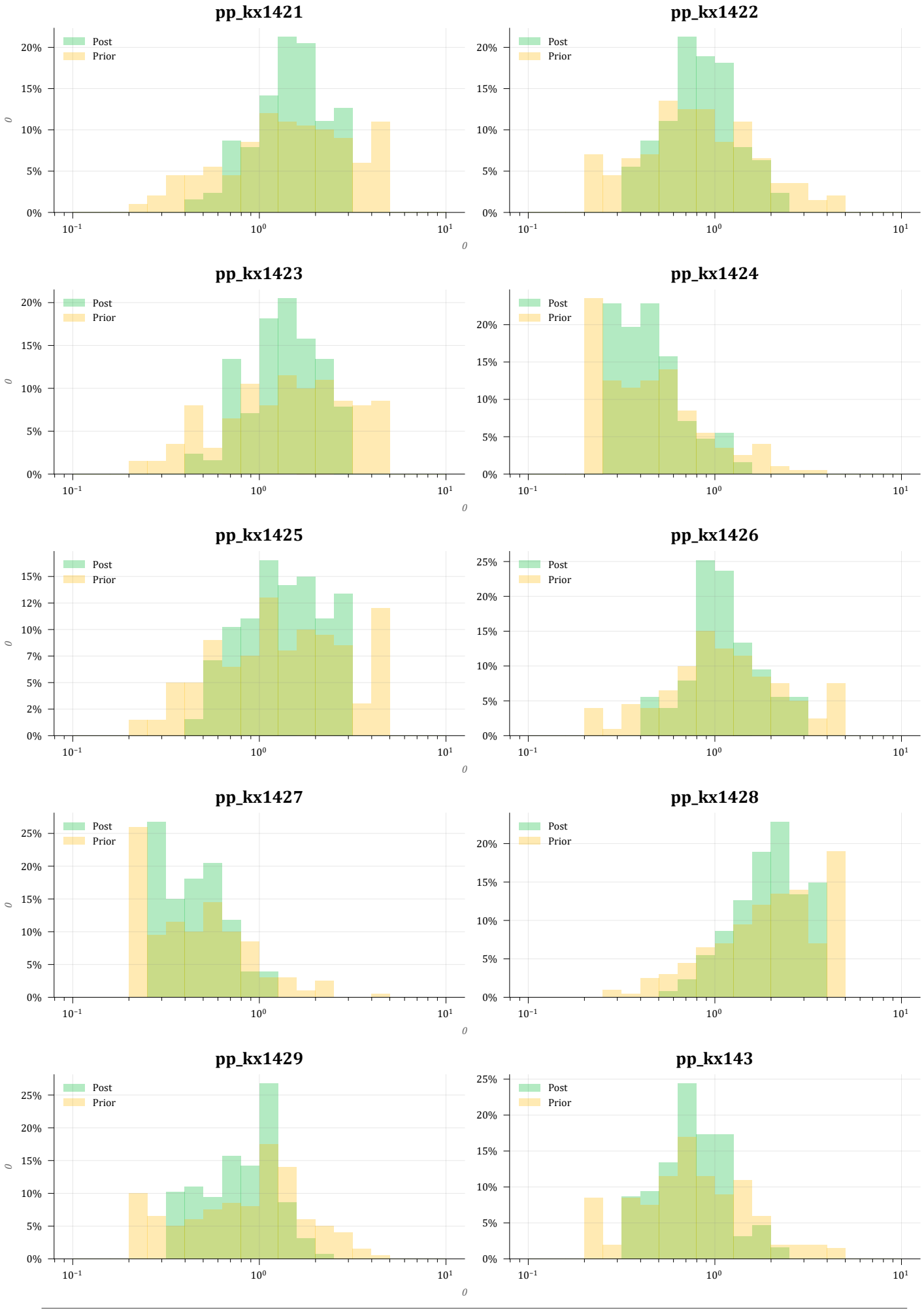
Parameters


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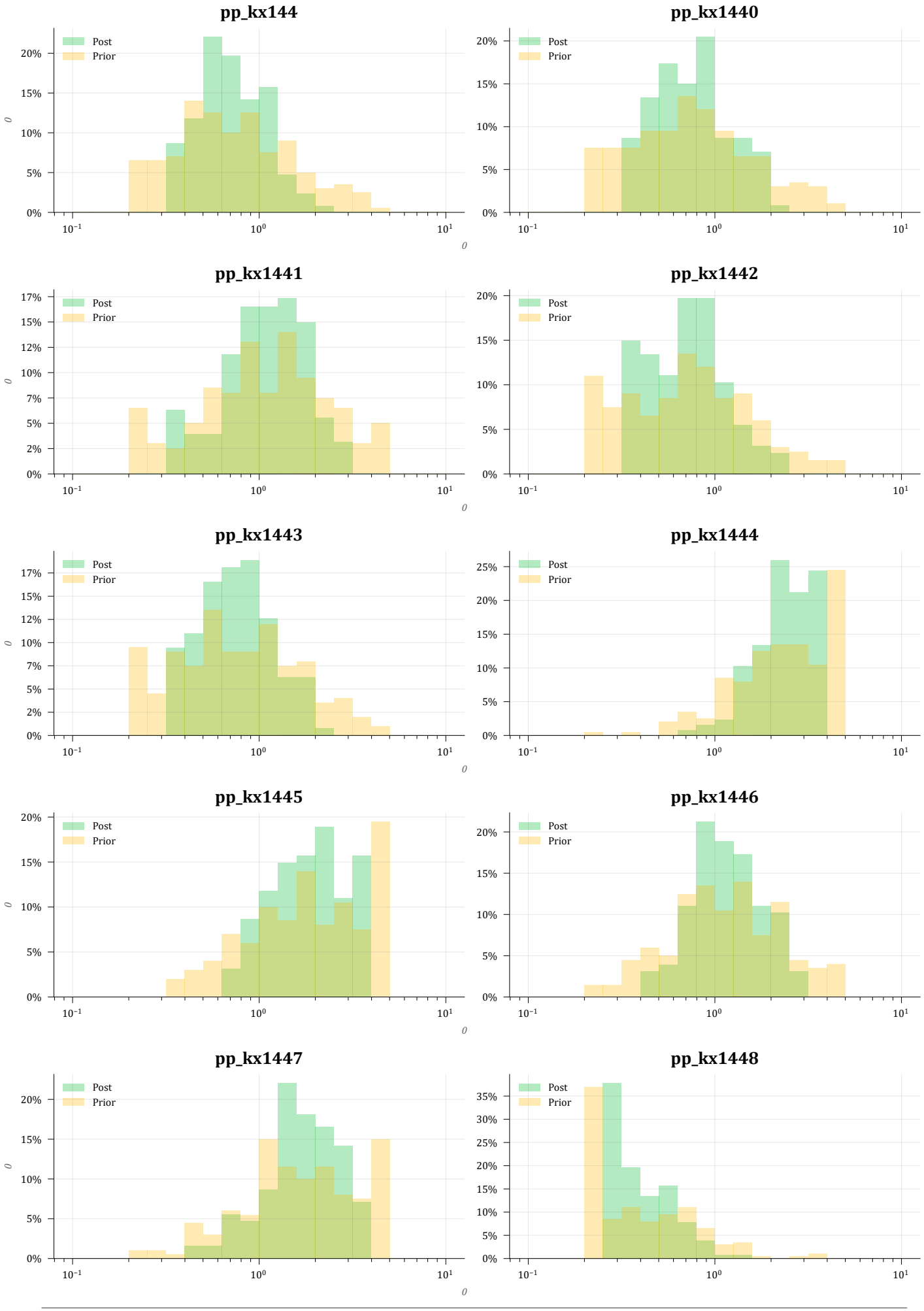

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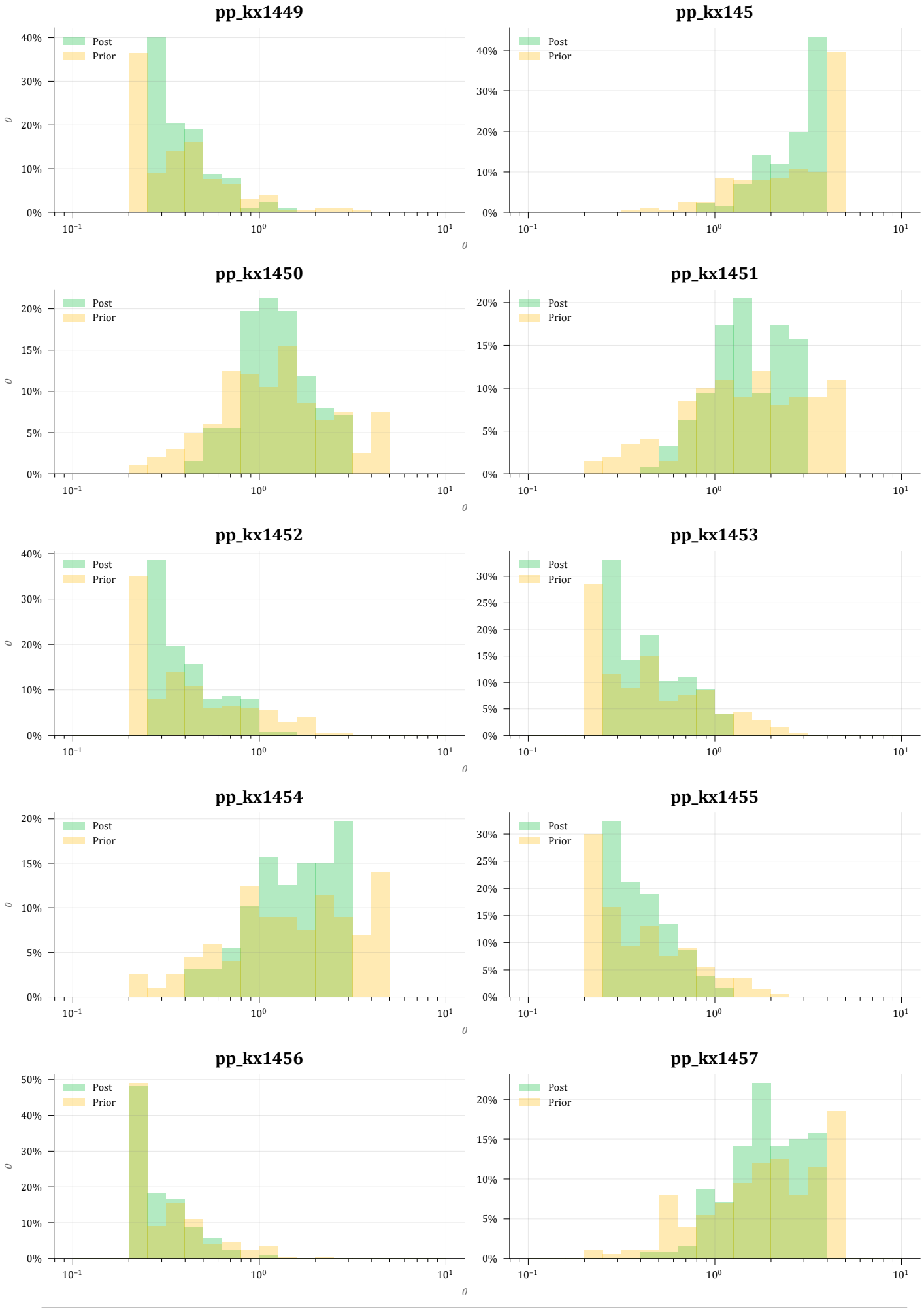

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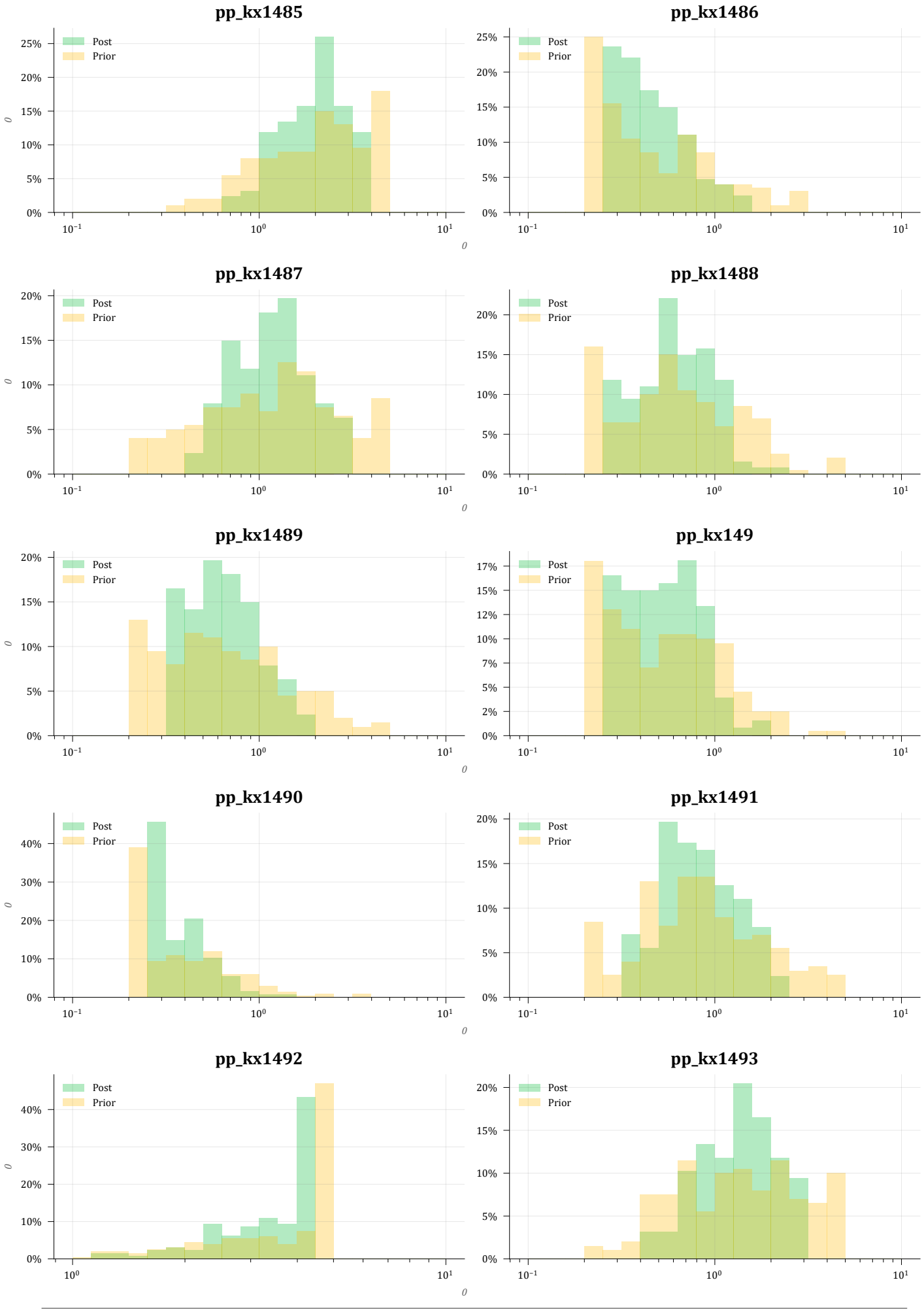

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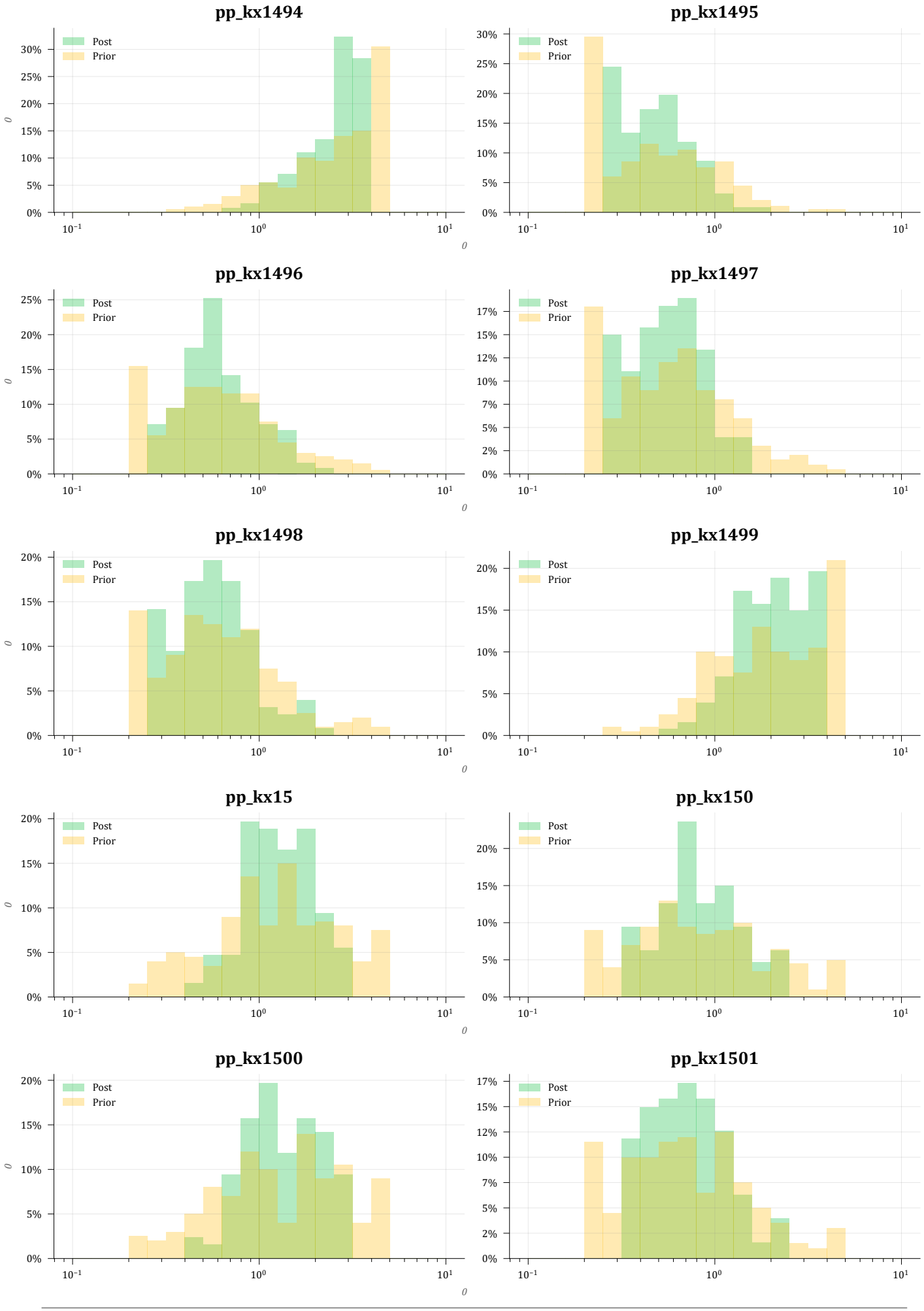

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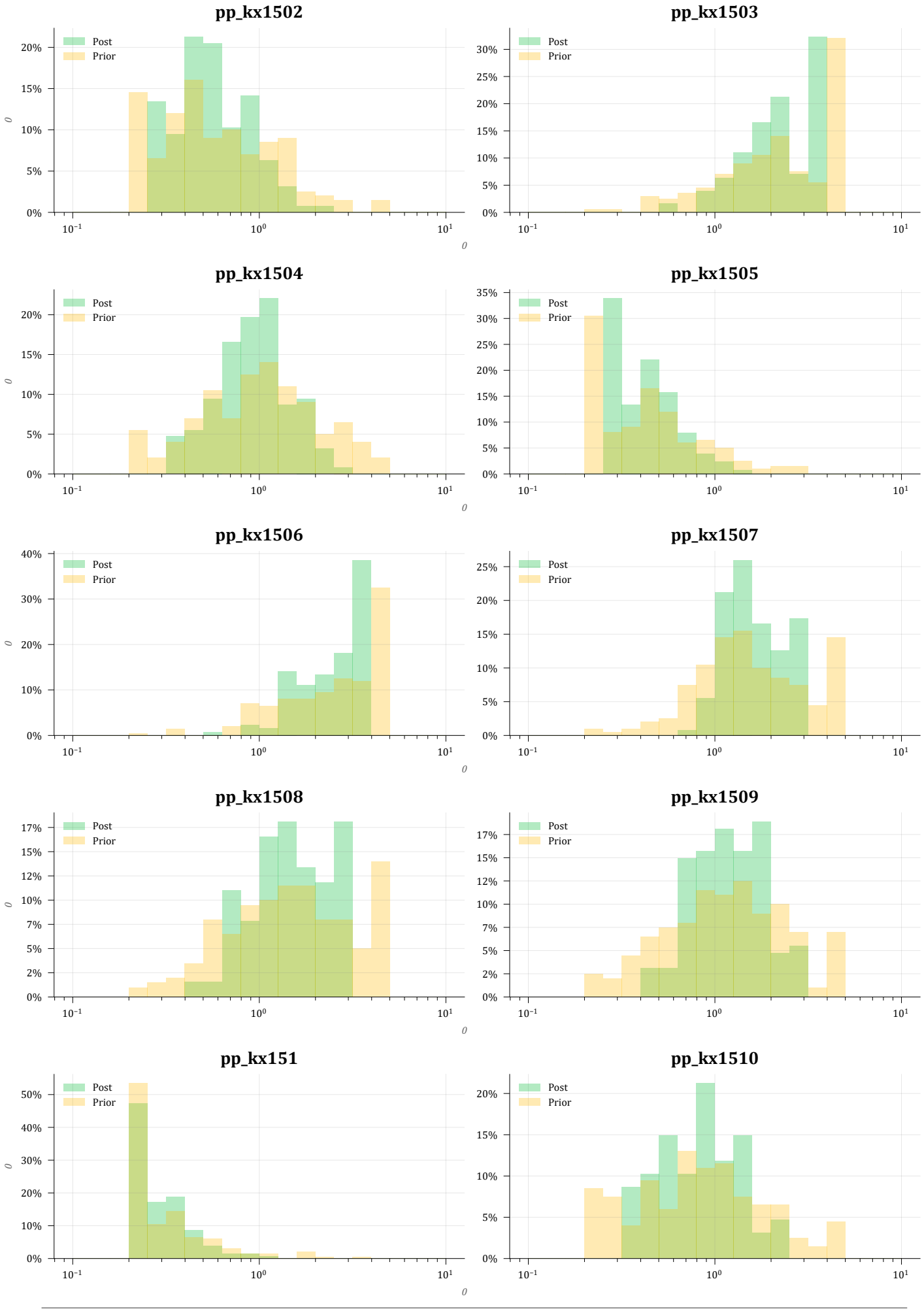

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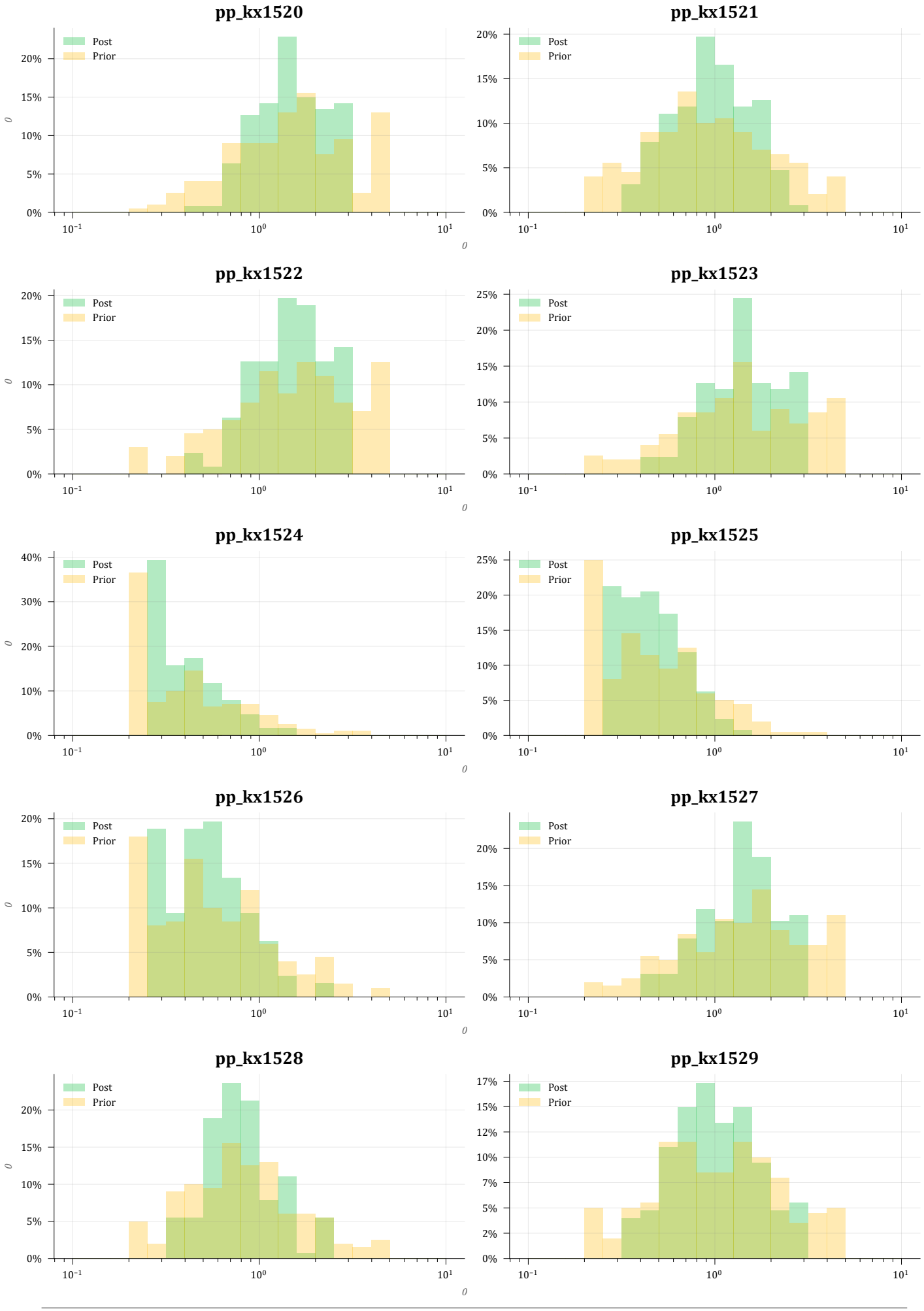

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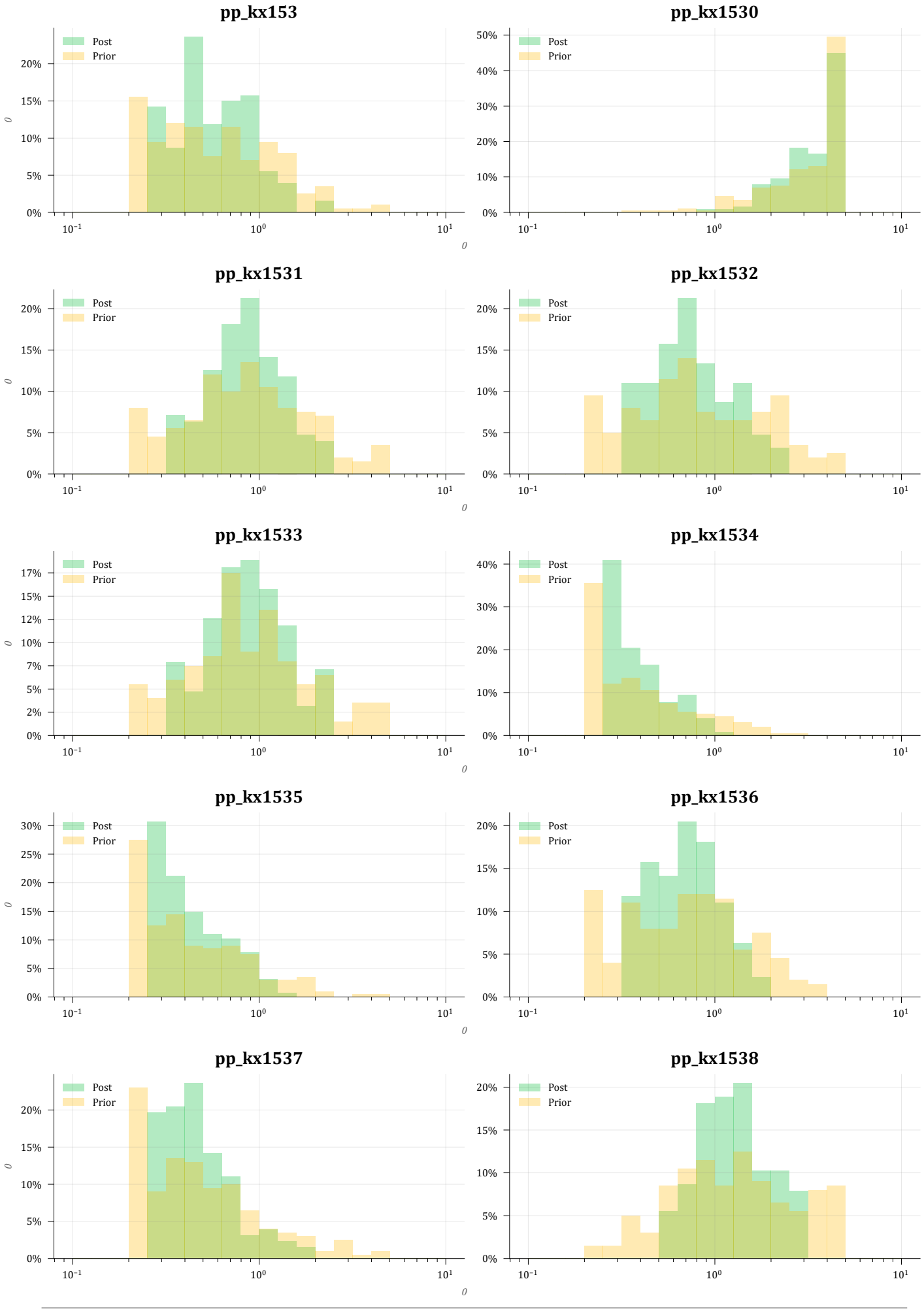

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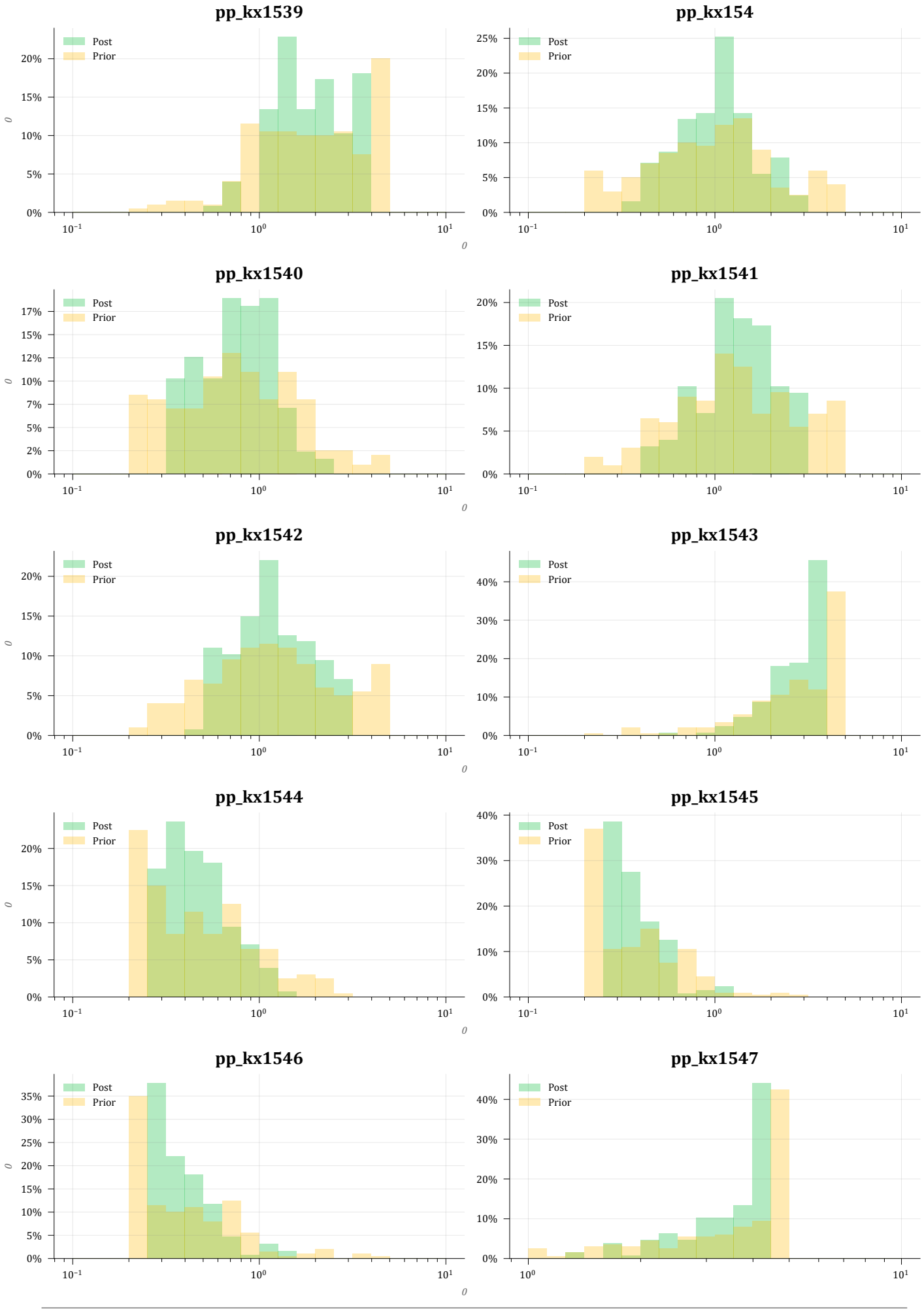

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Parameters


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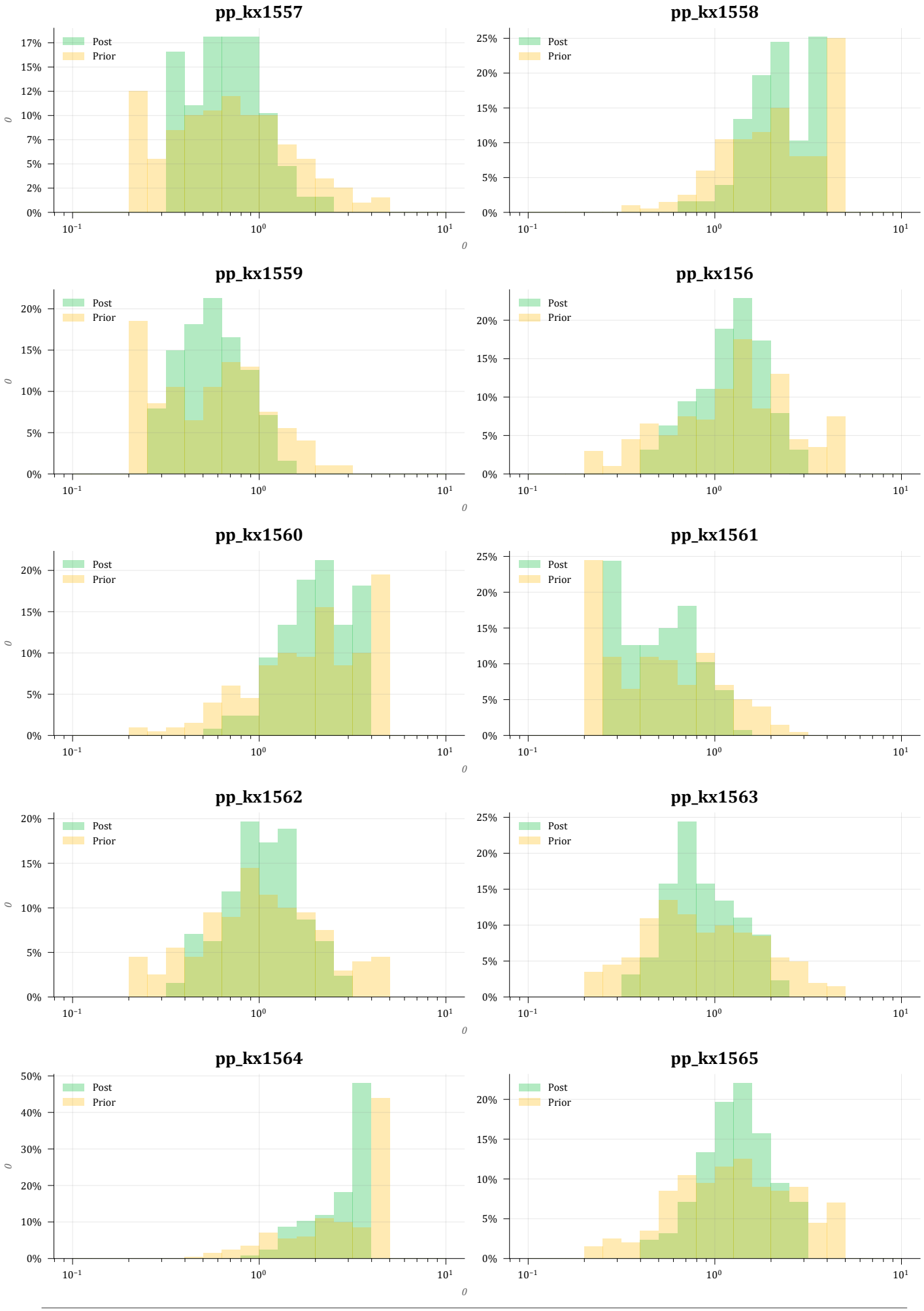

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Post
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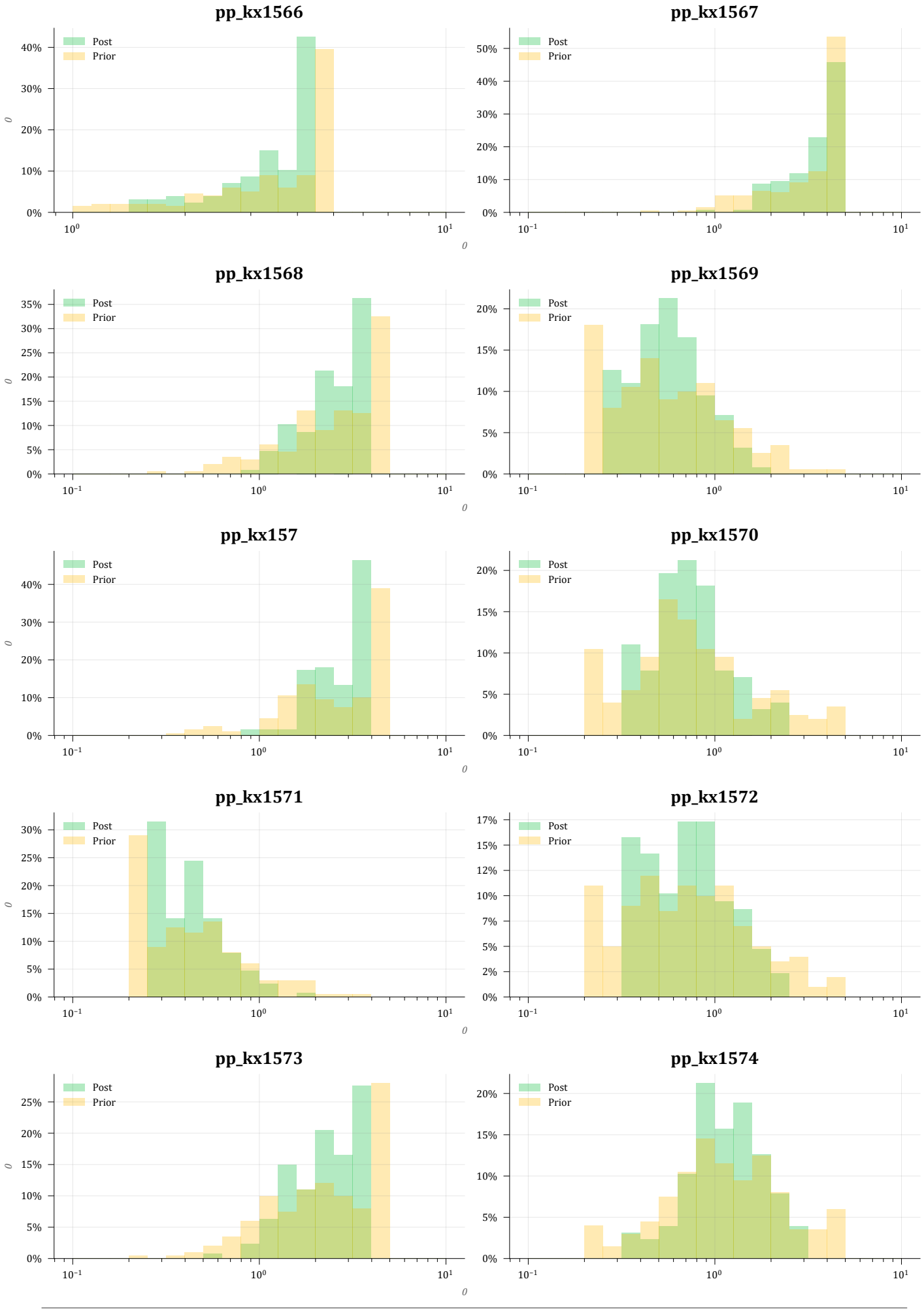

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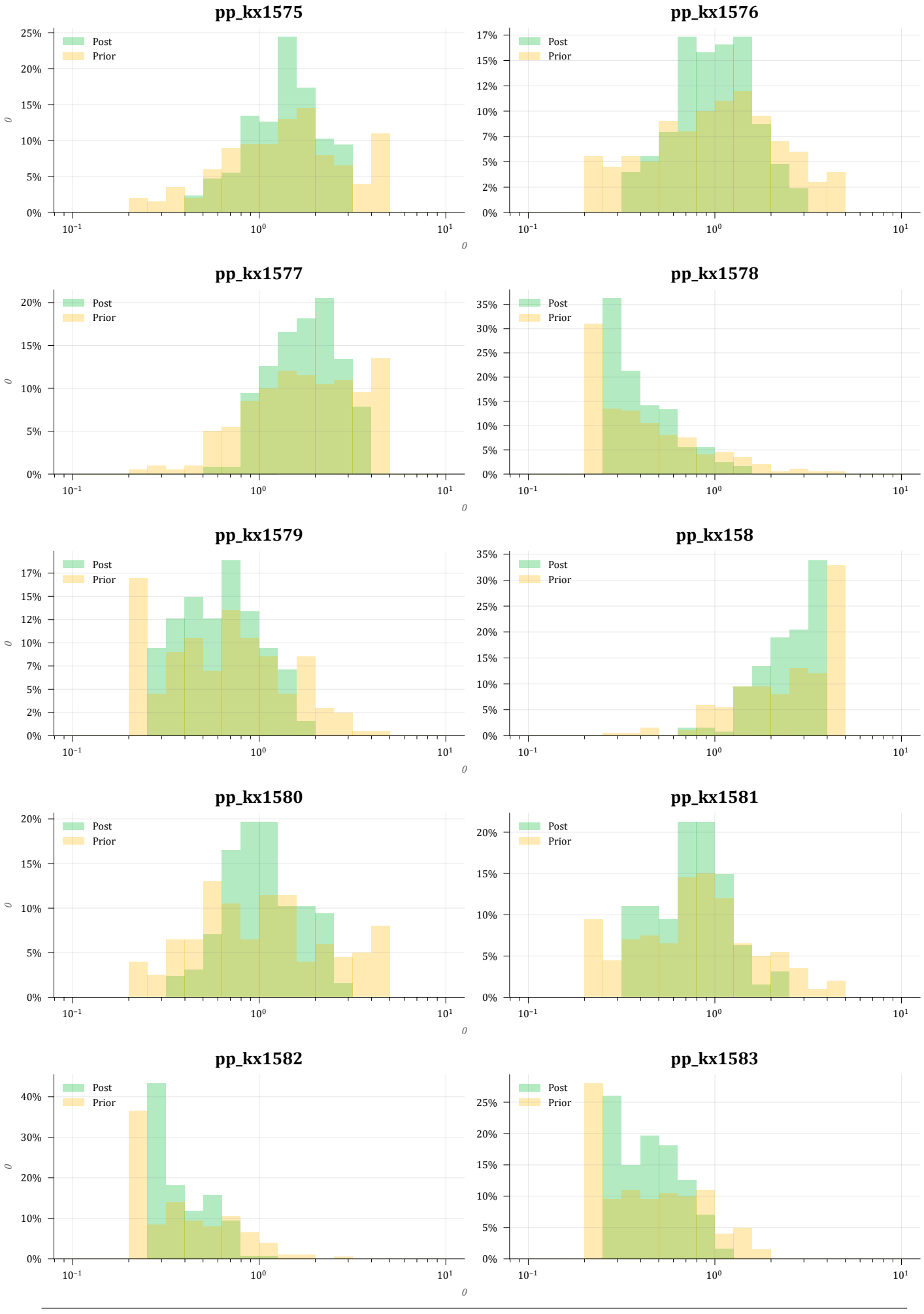

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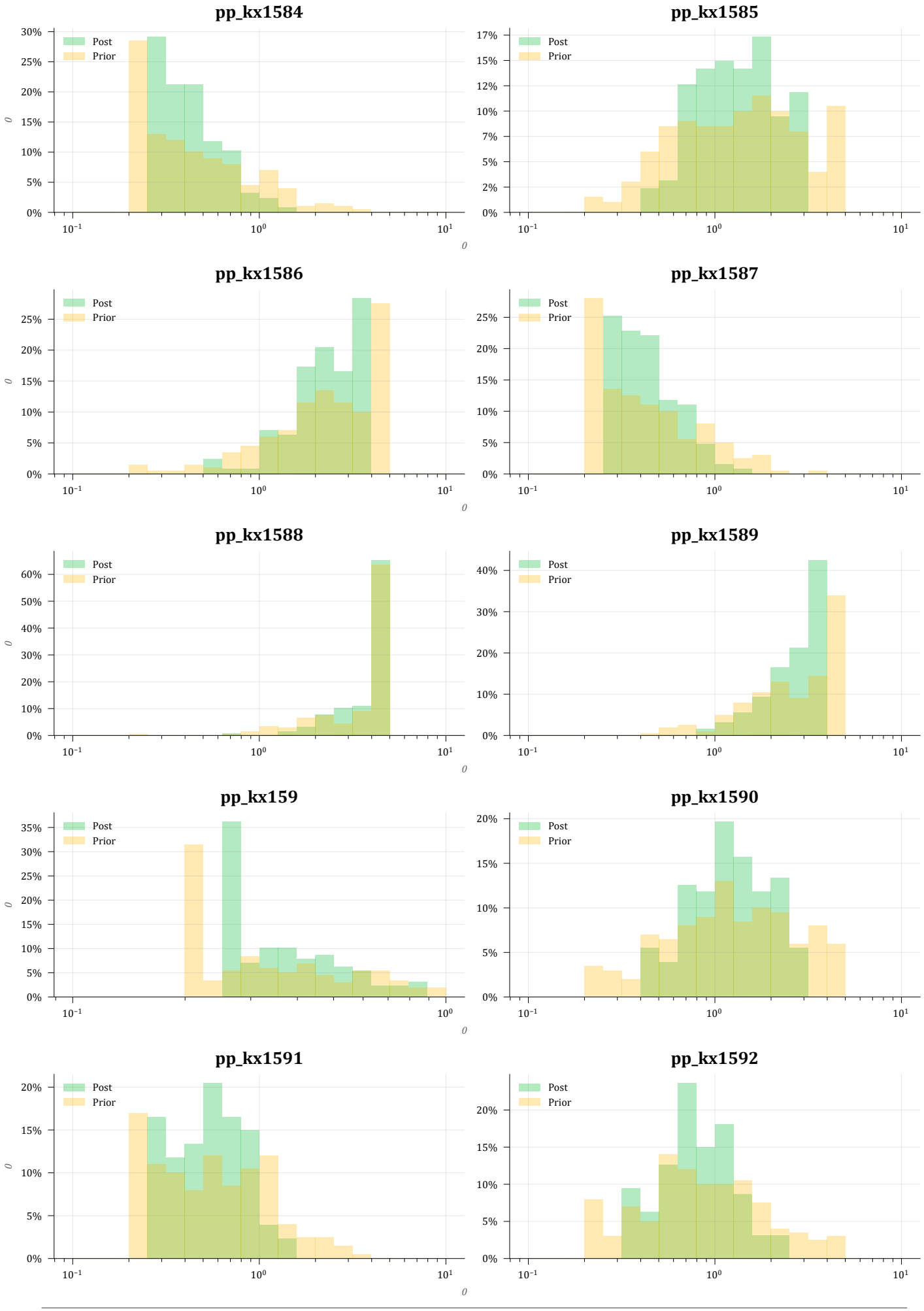

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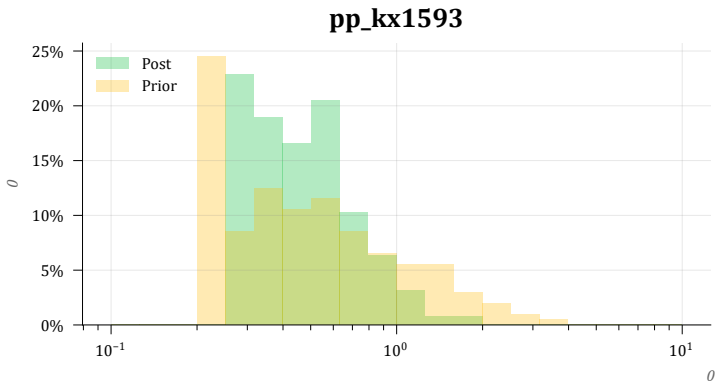

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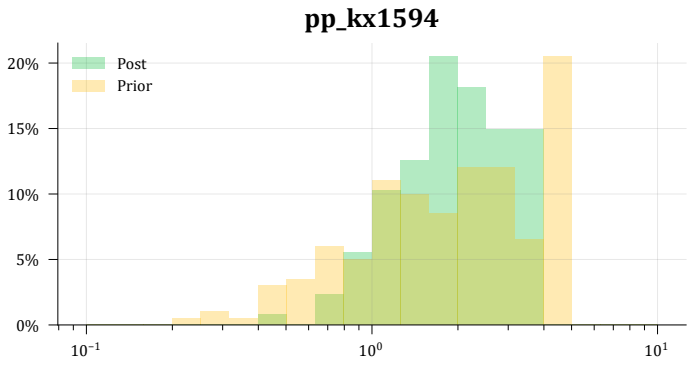

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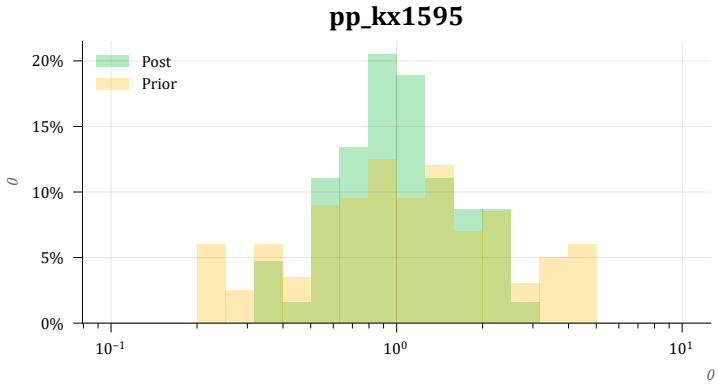

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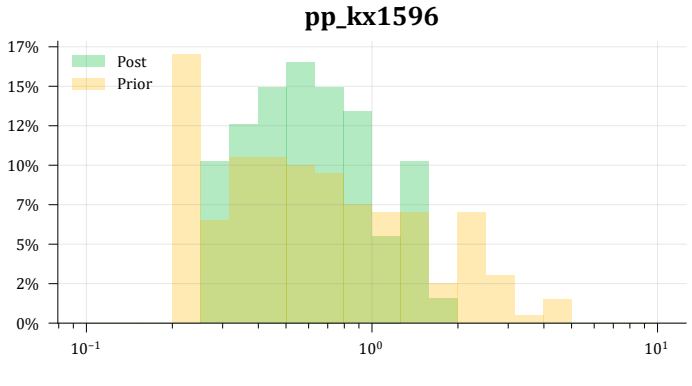

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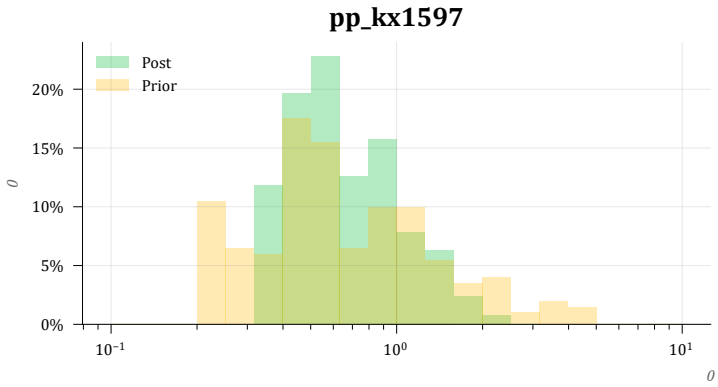

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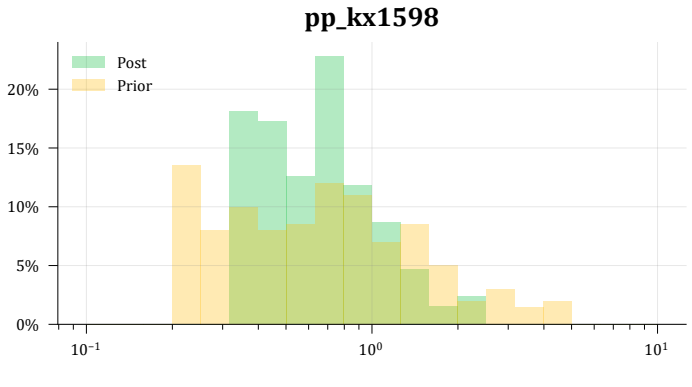

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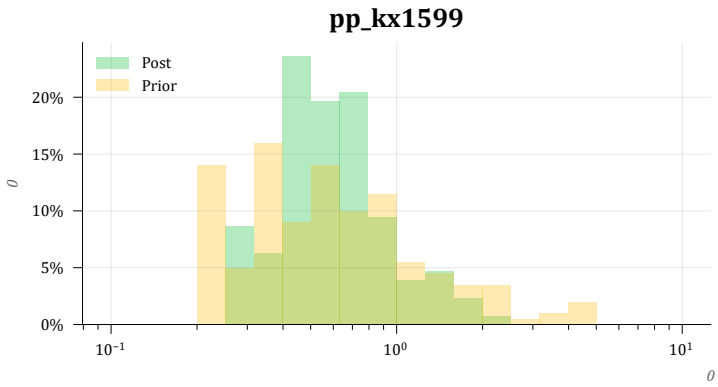

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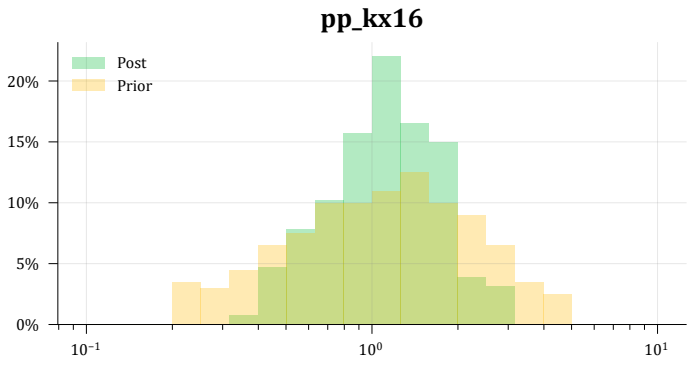

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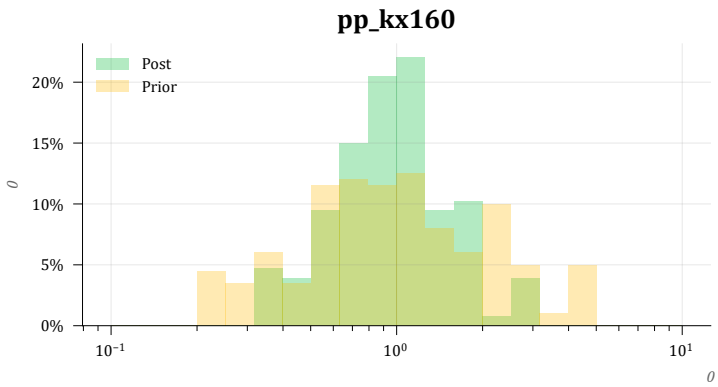

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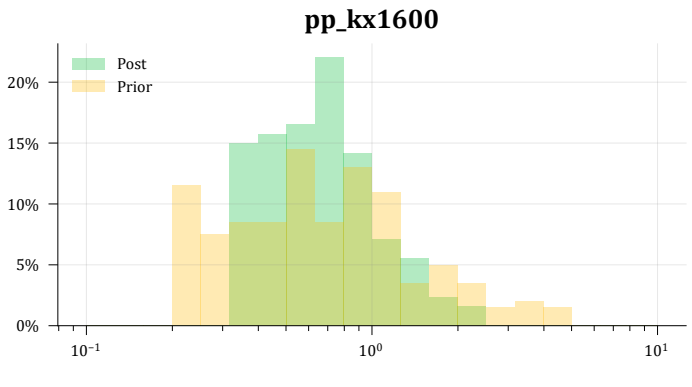

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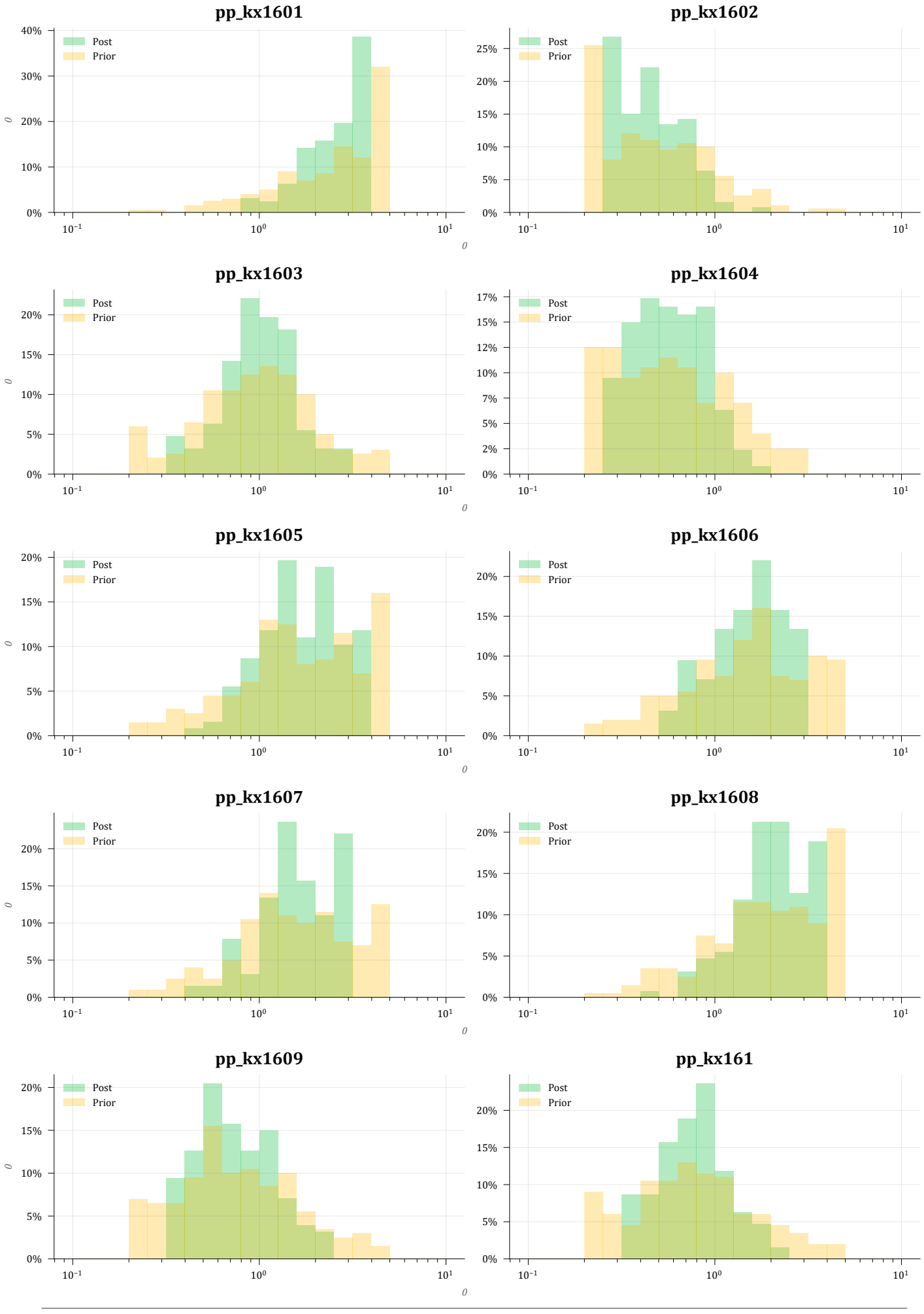

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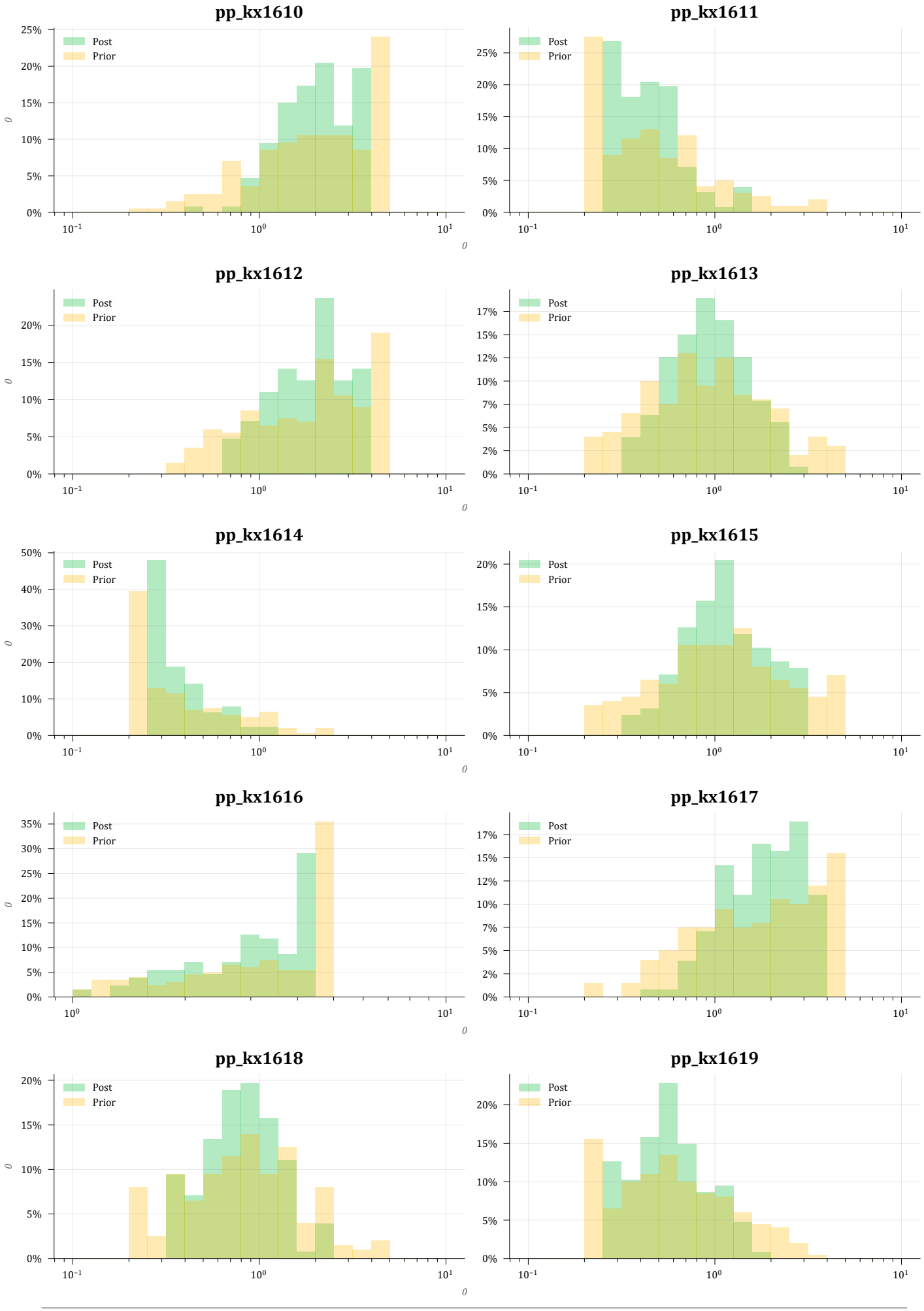

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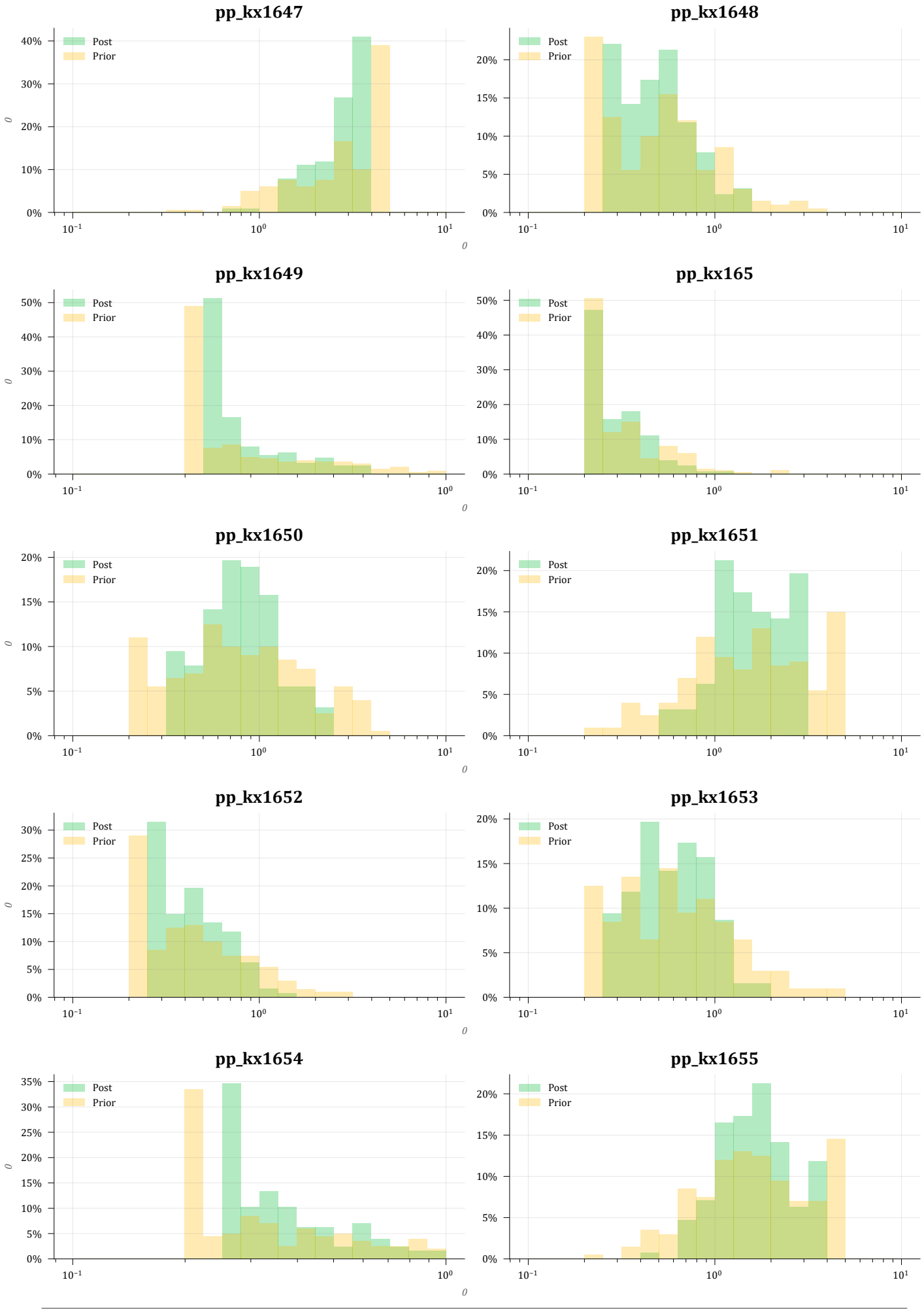

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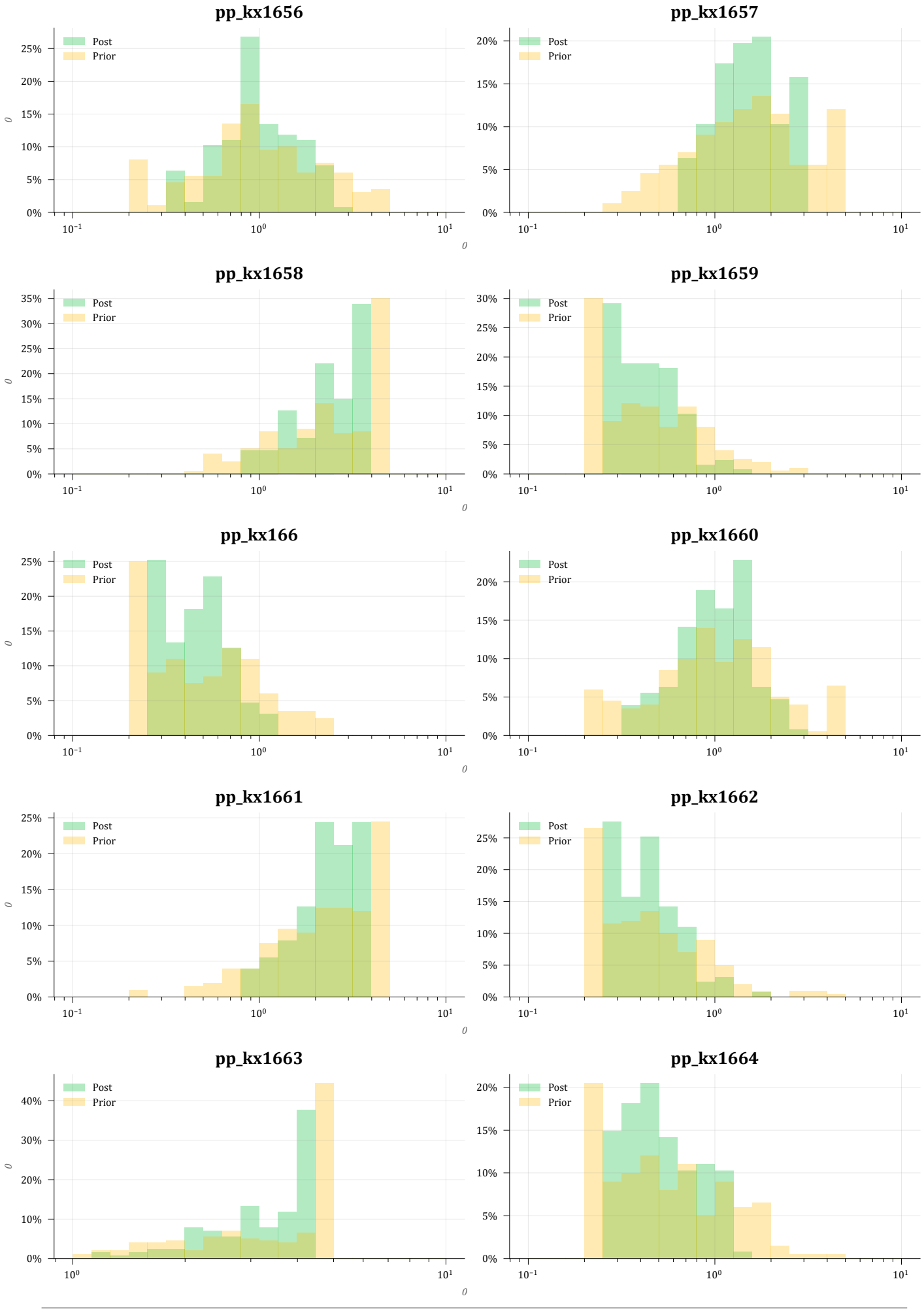

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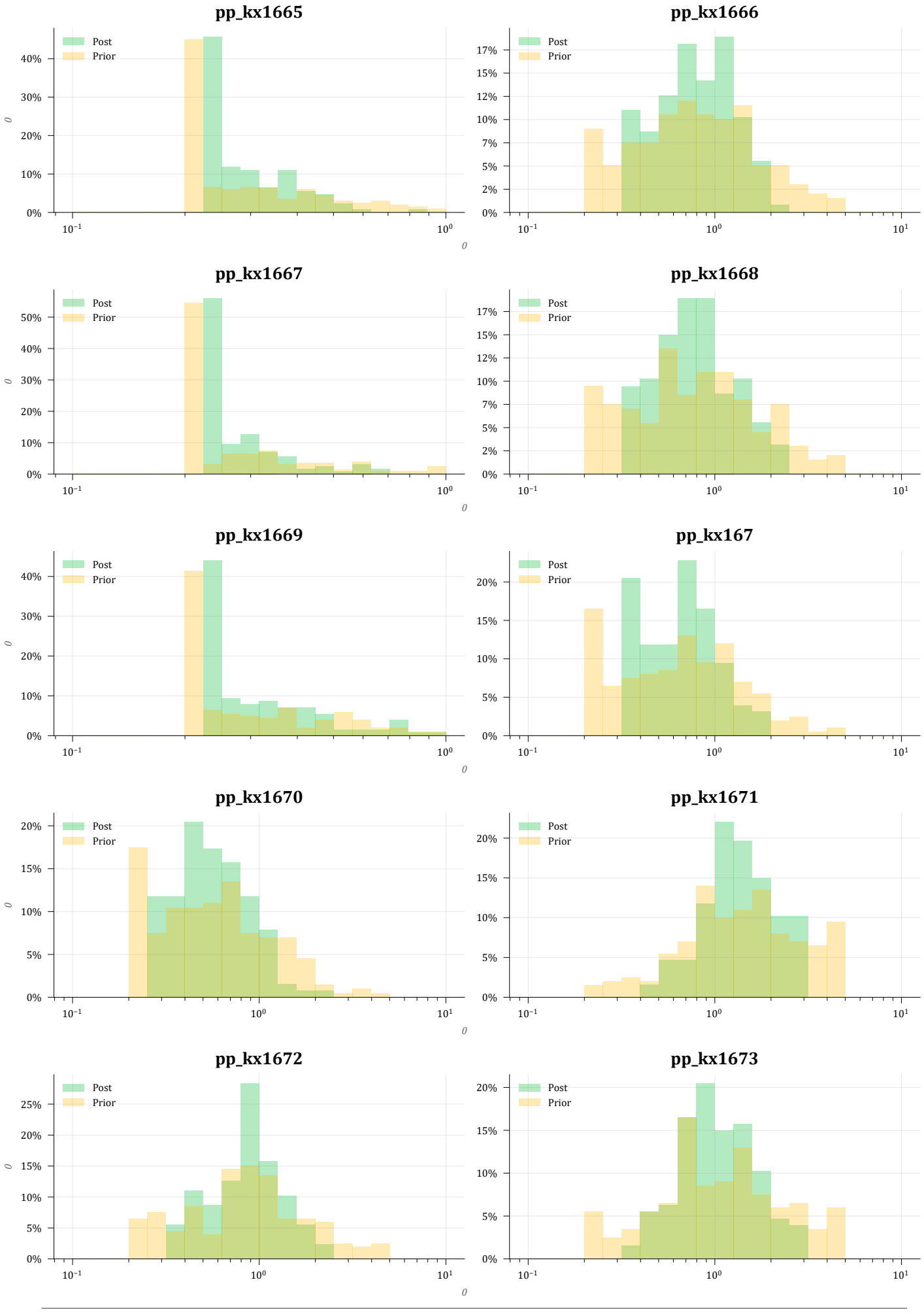

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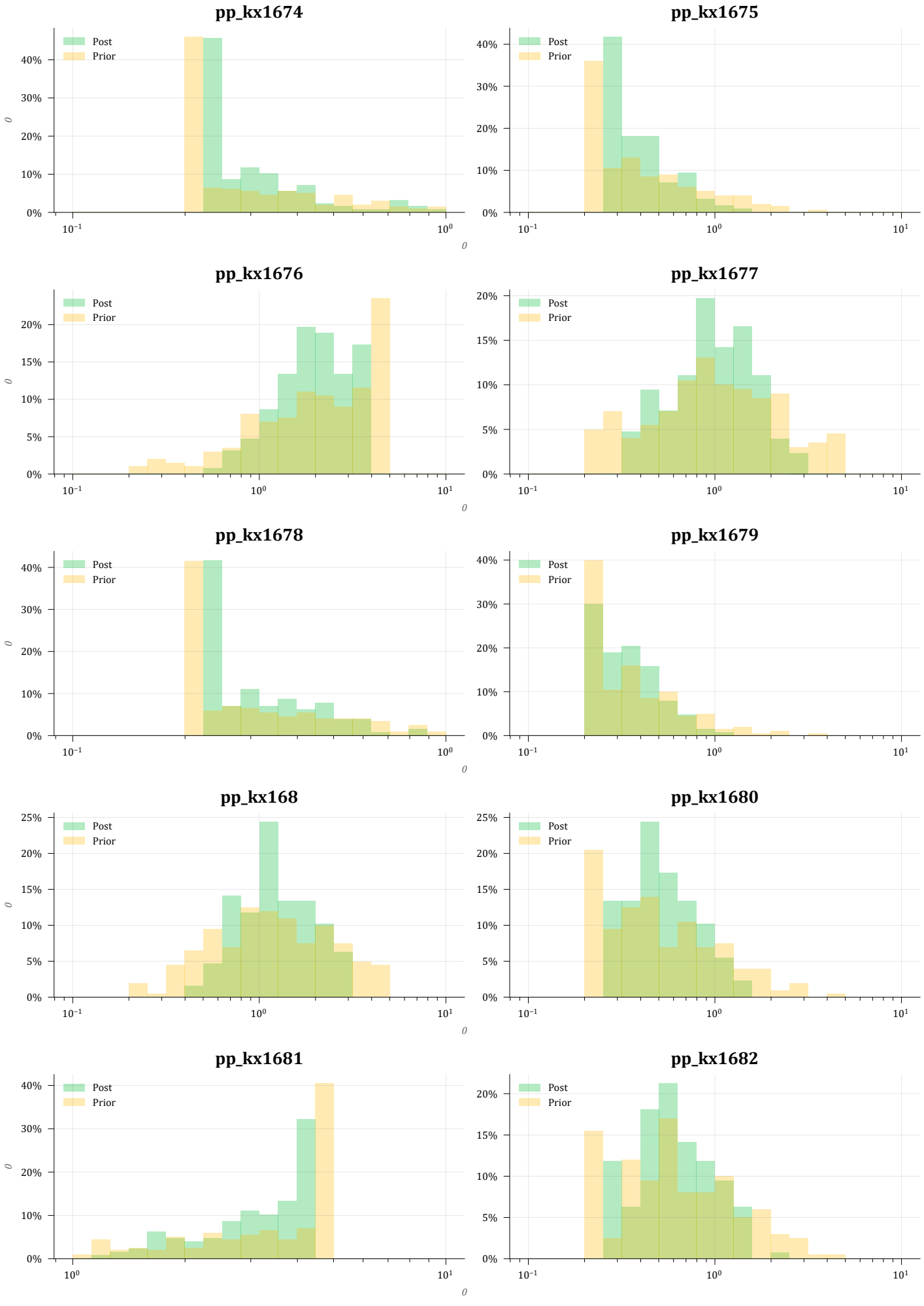

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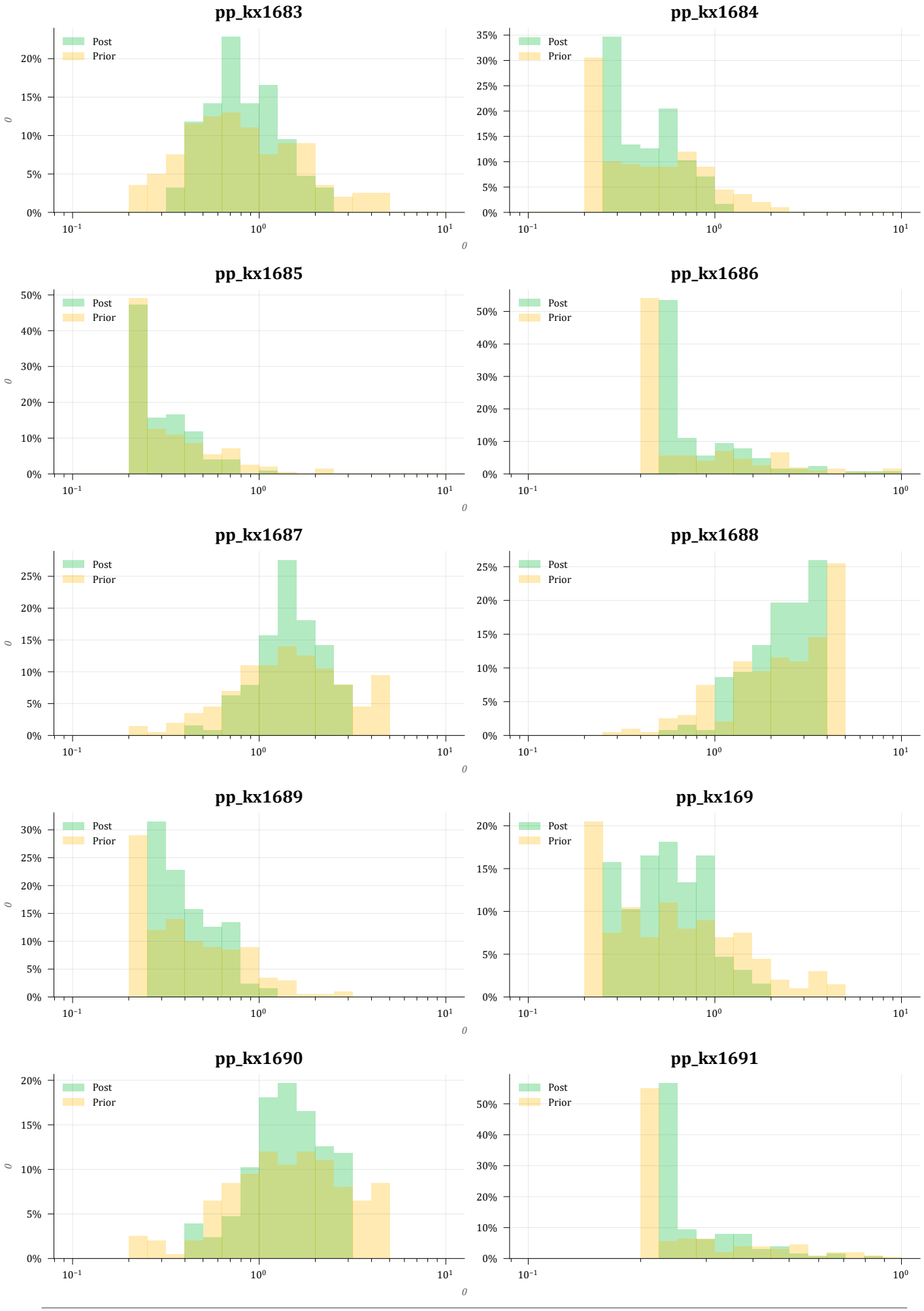

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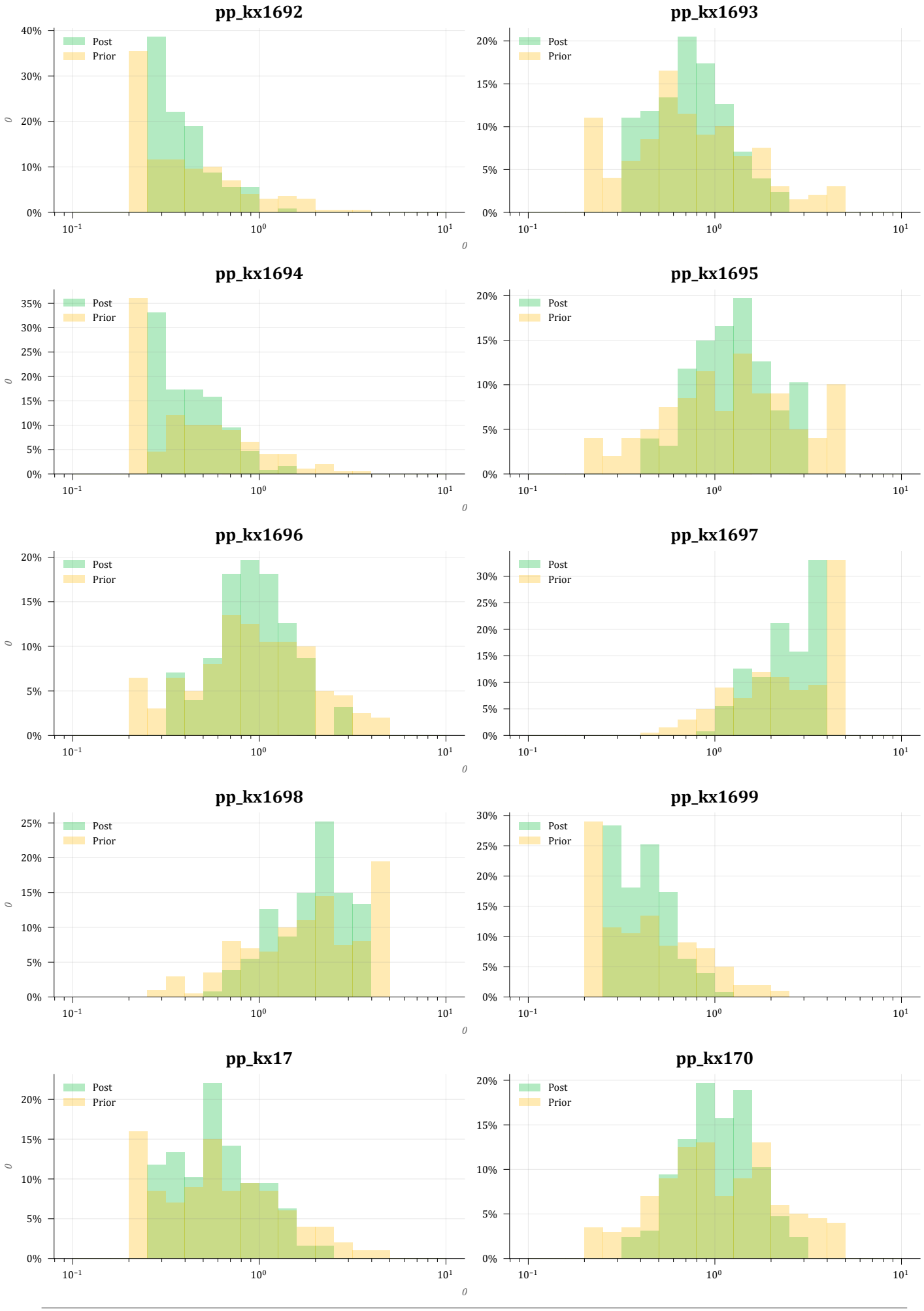

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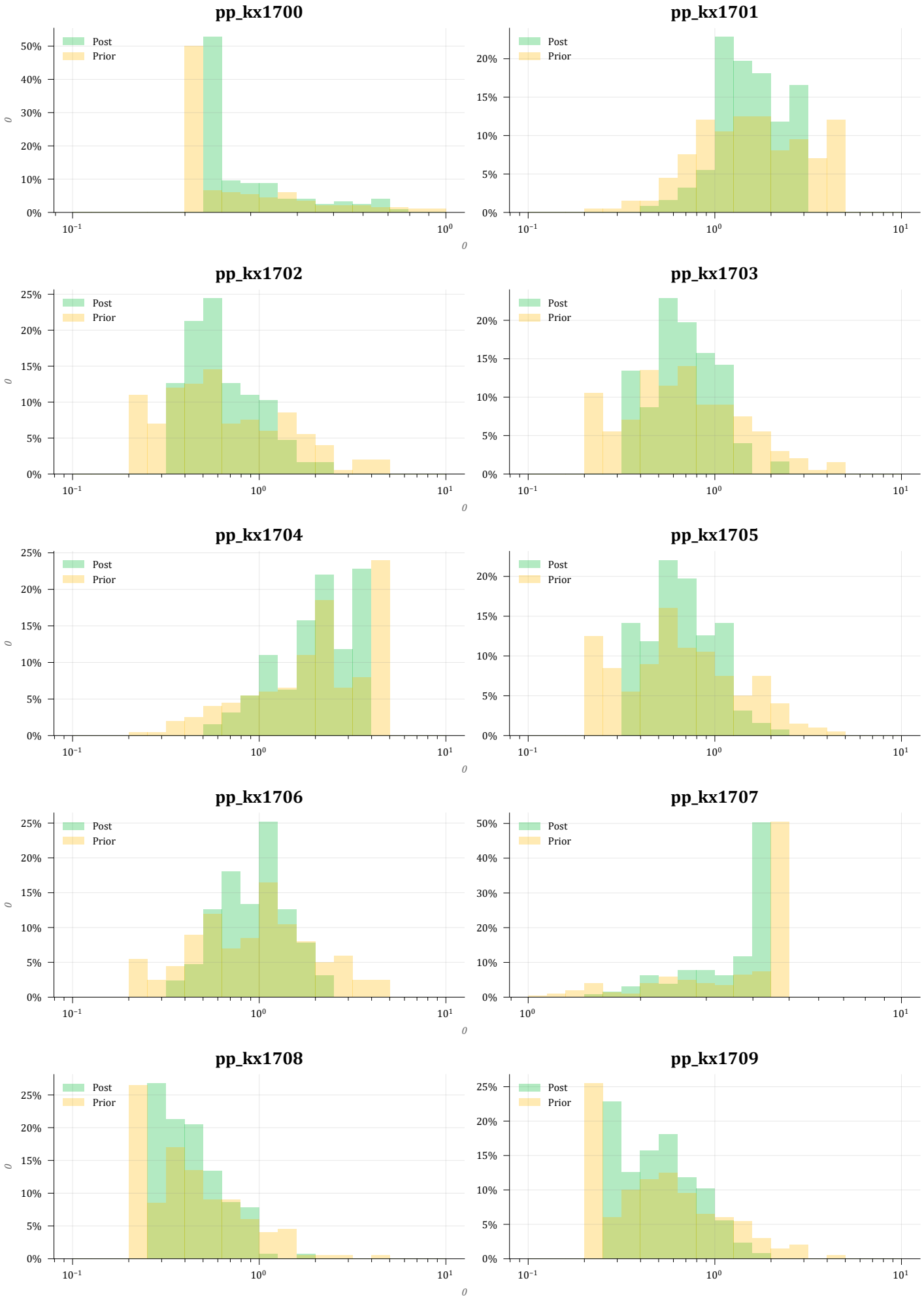

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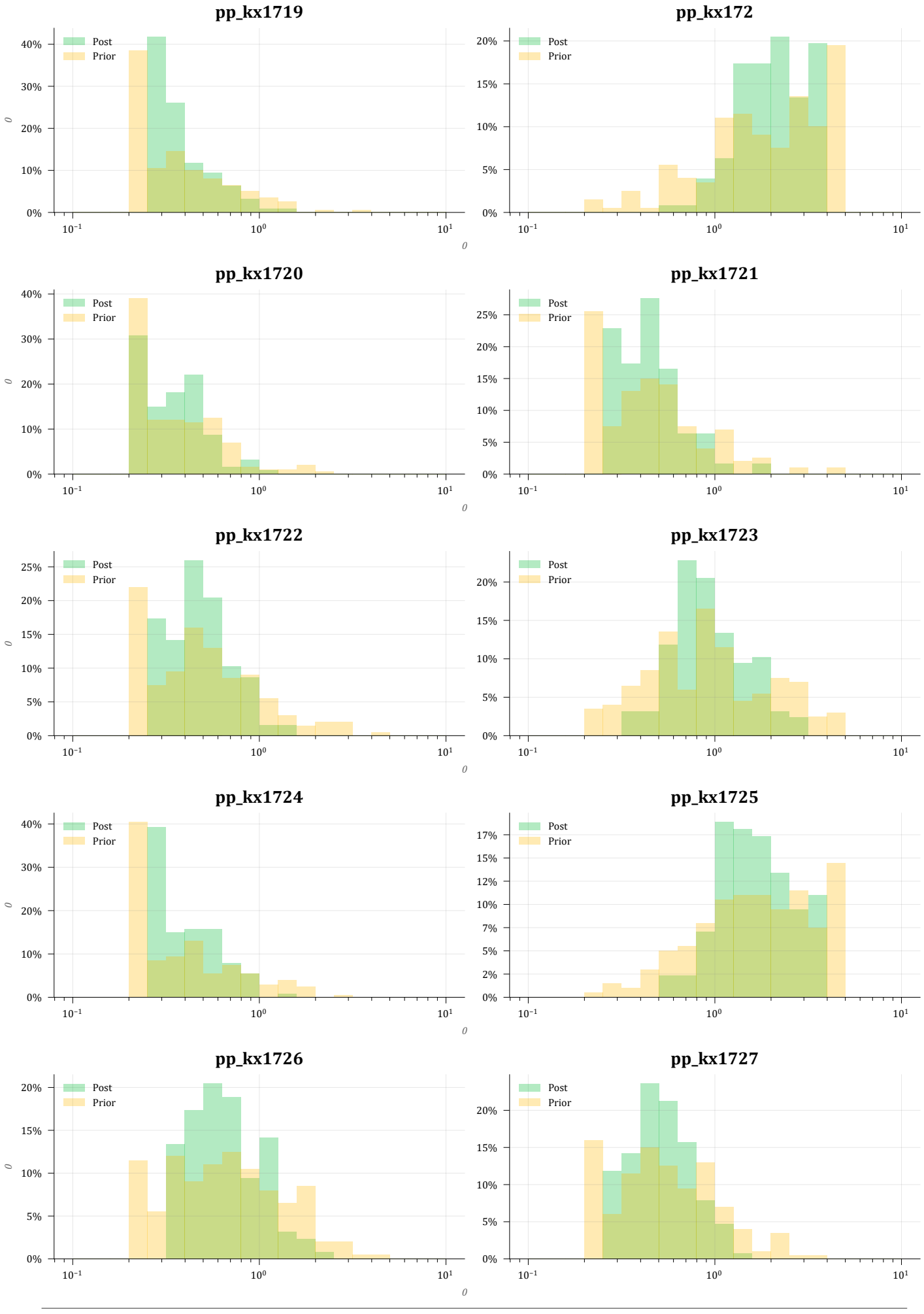

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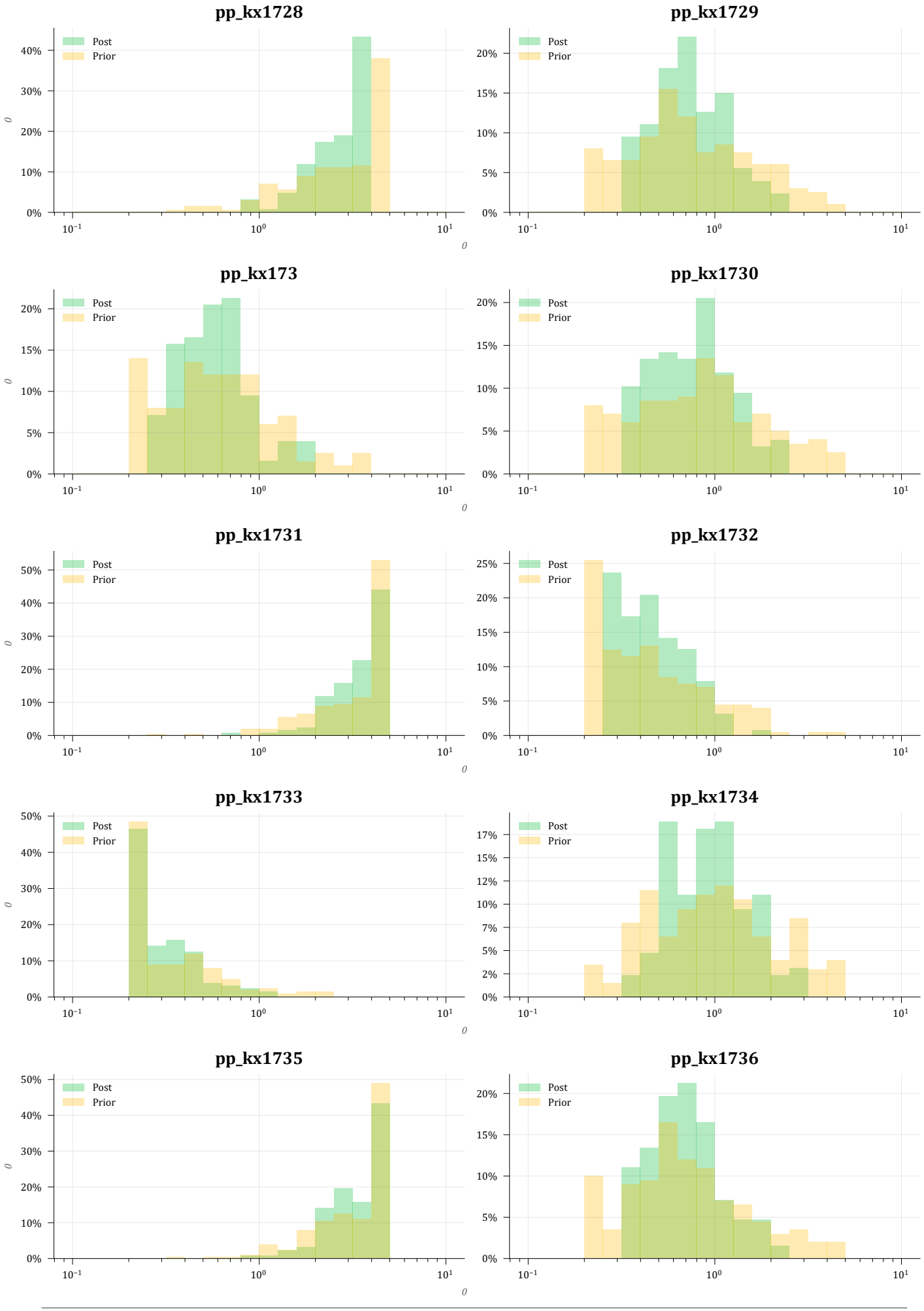

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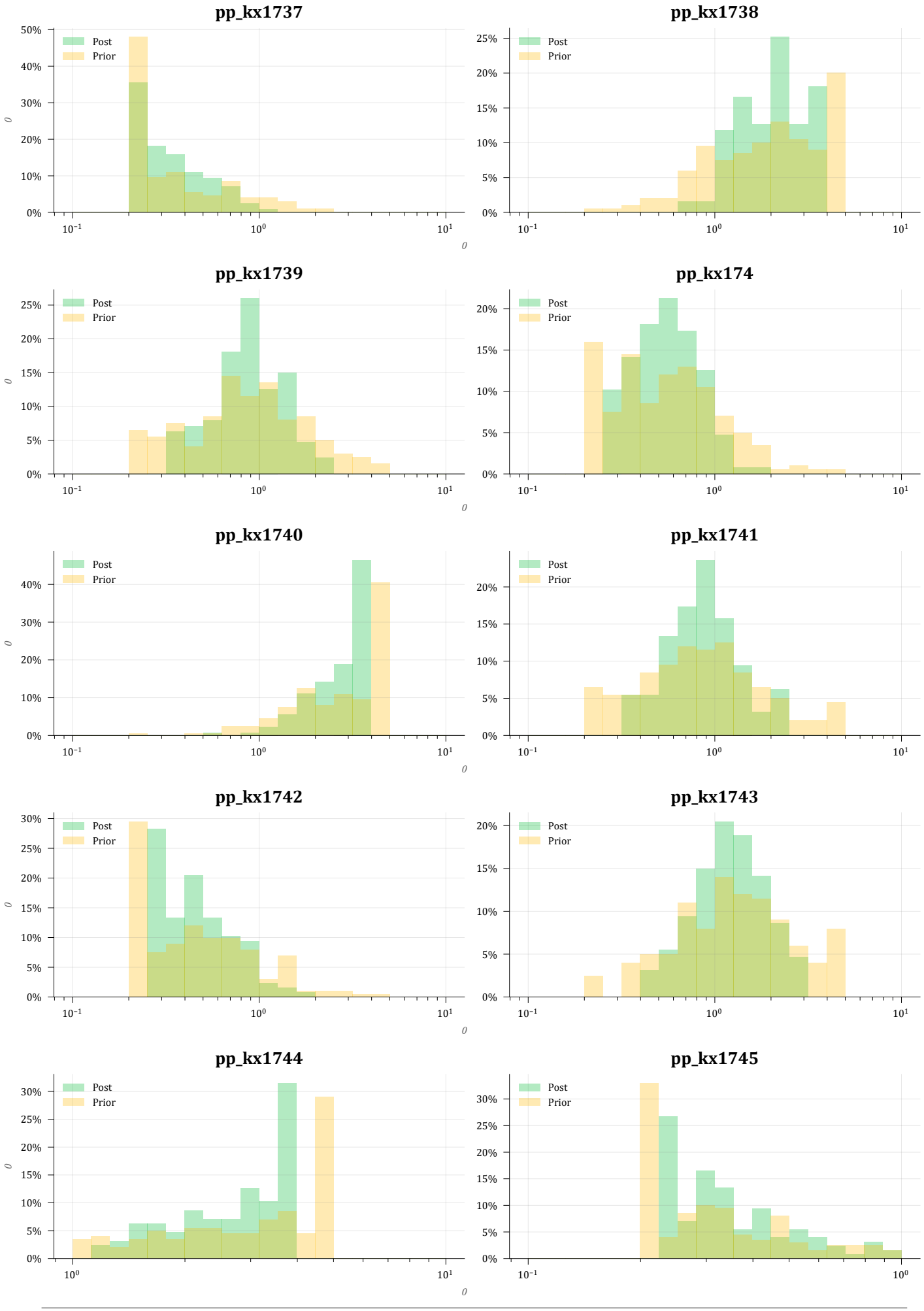

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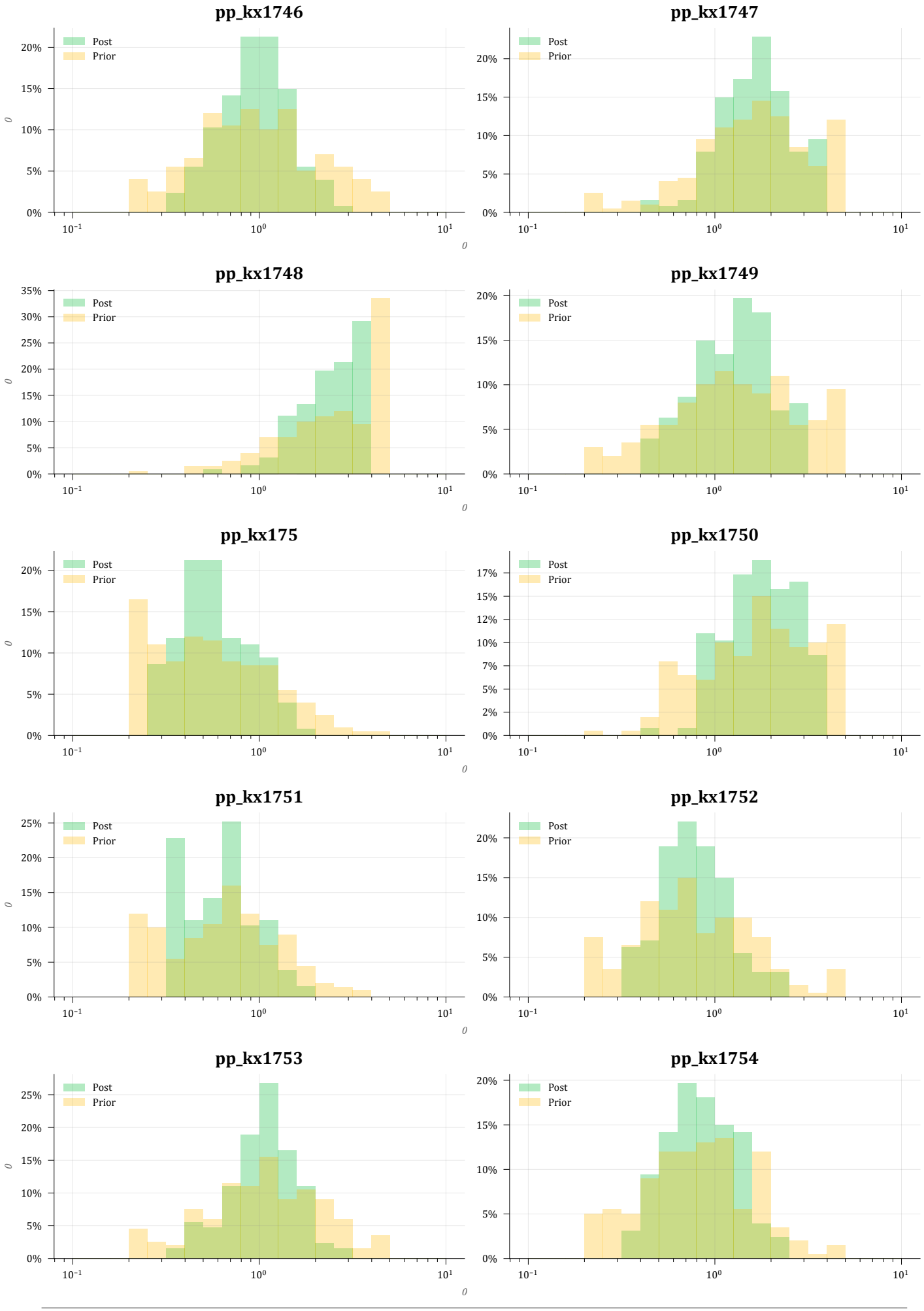

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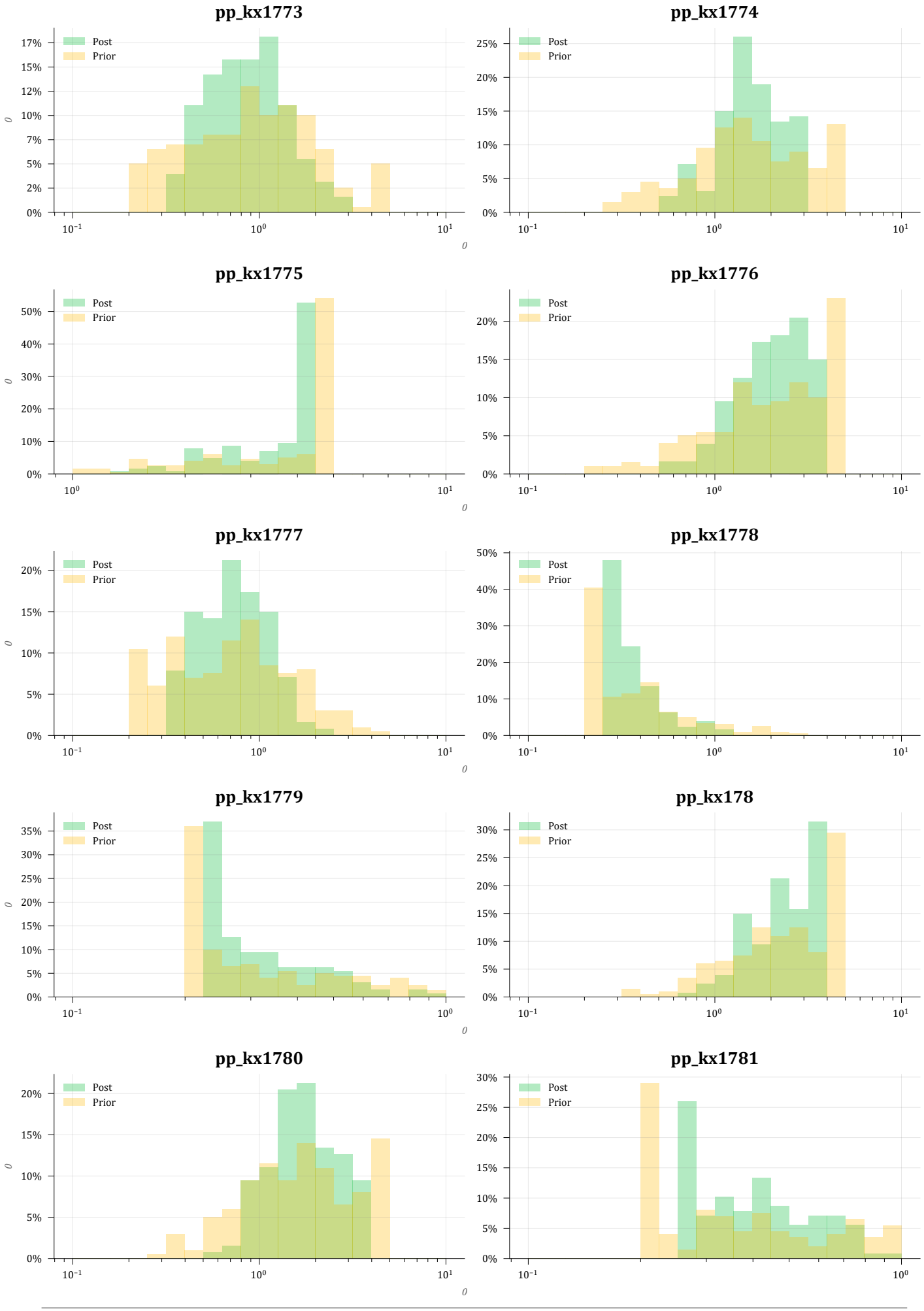

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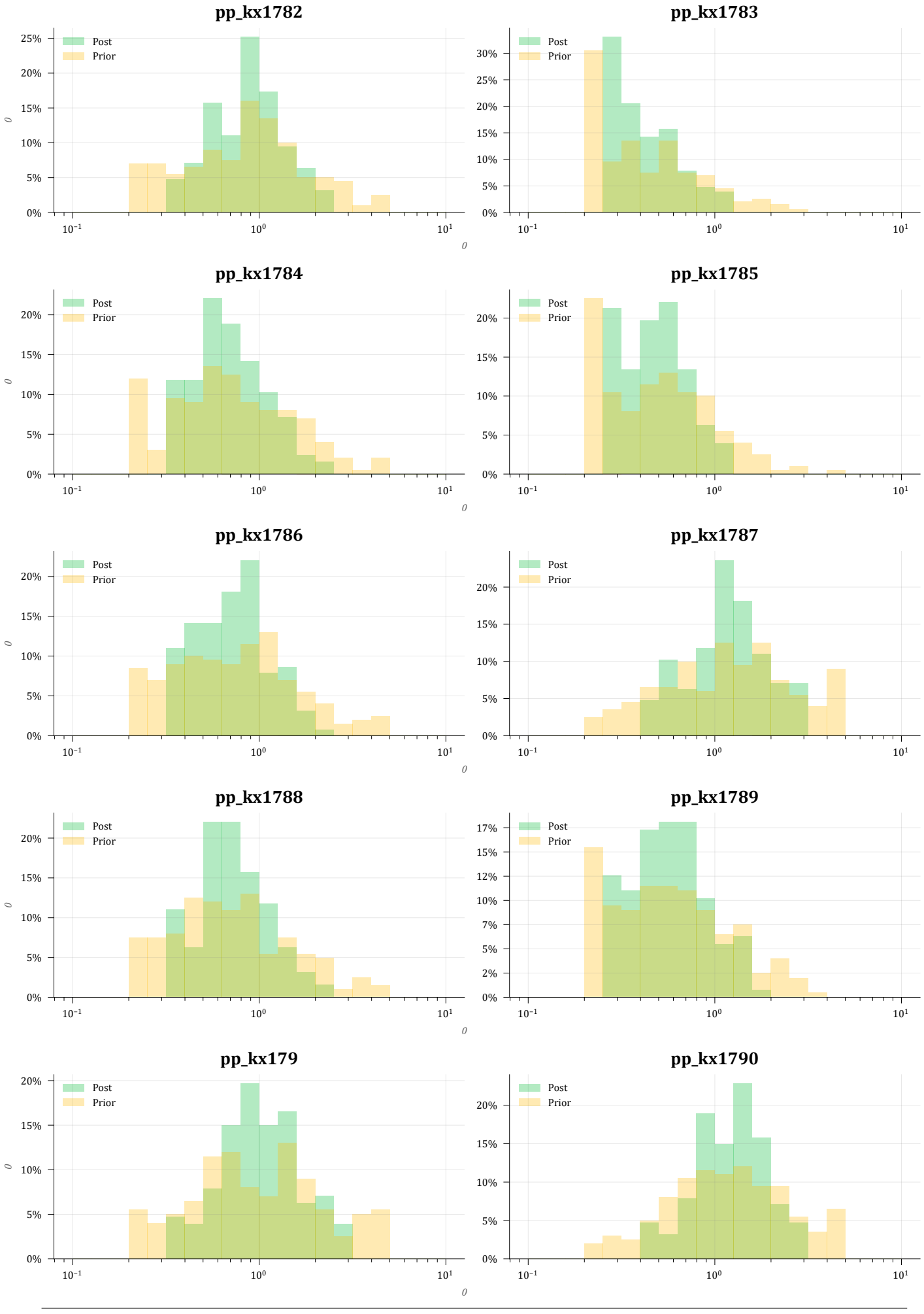

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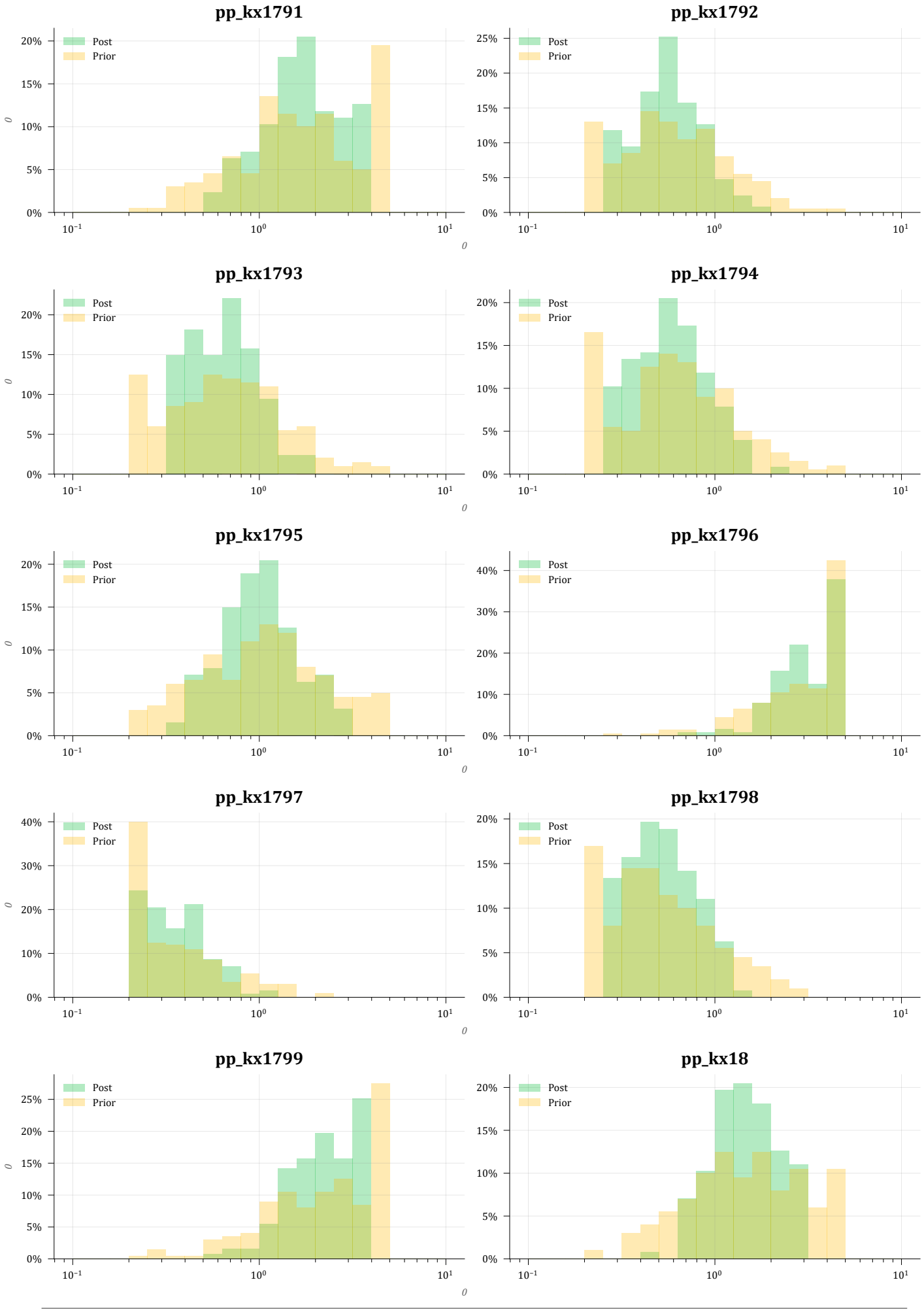

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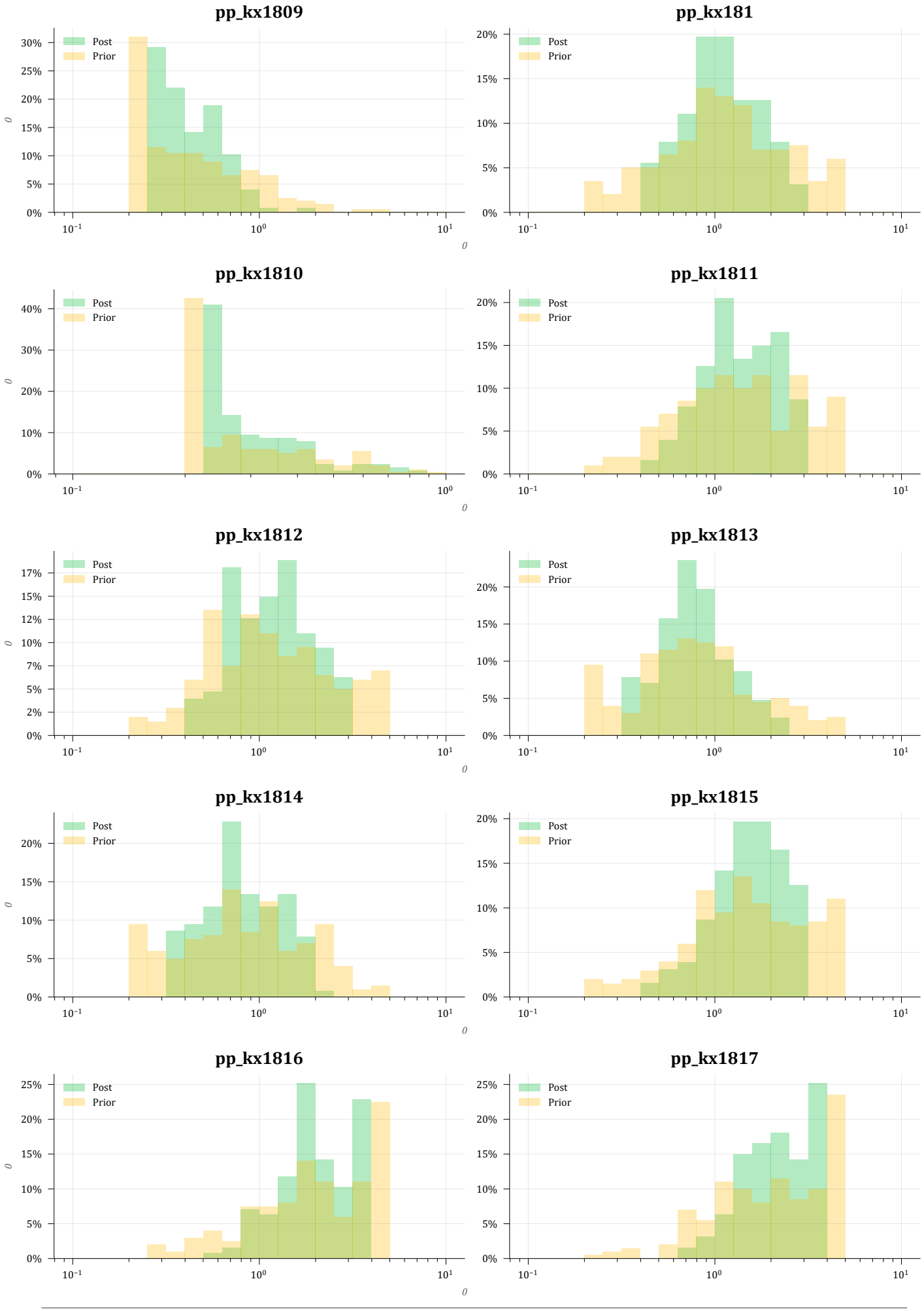

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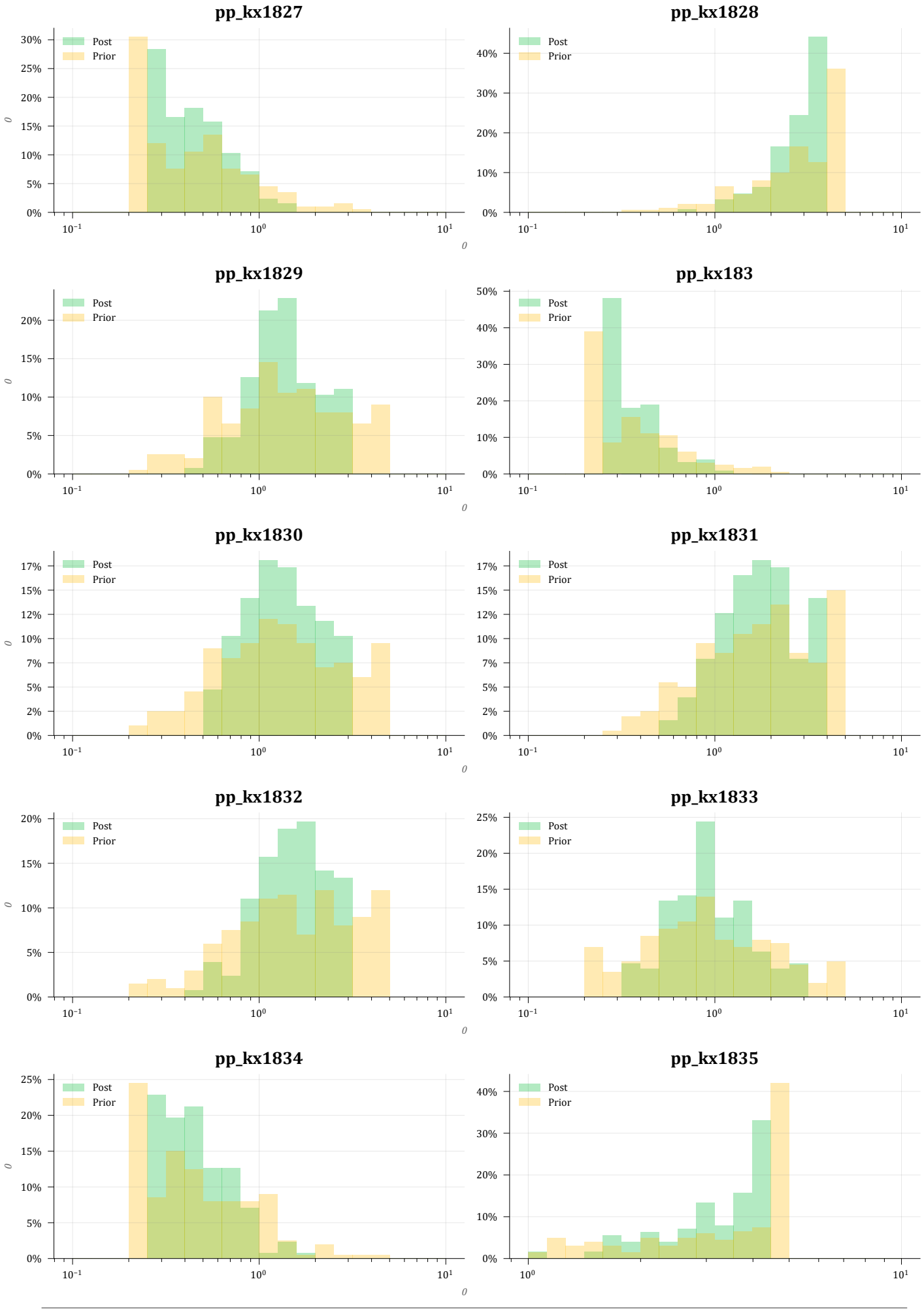

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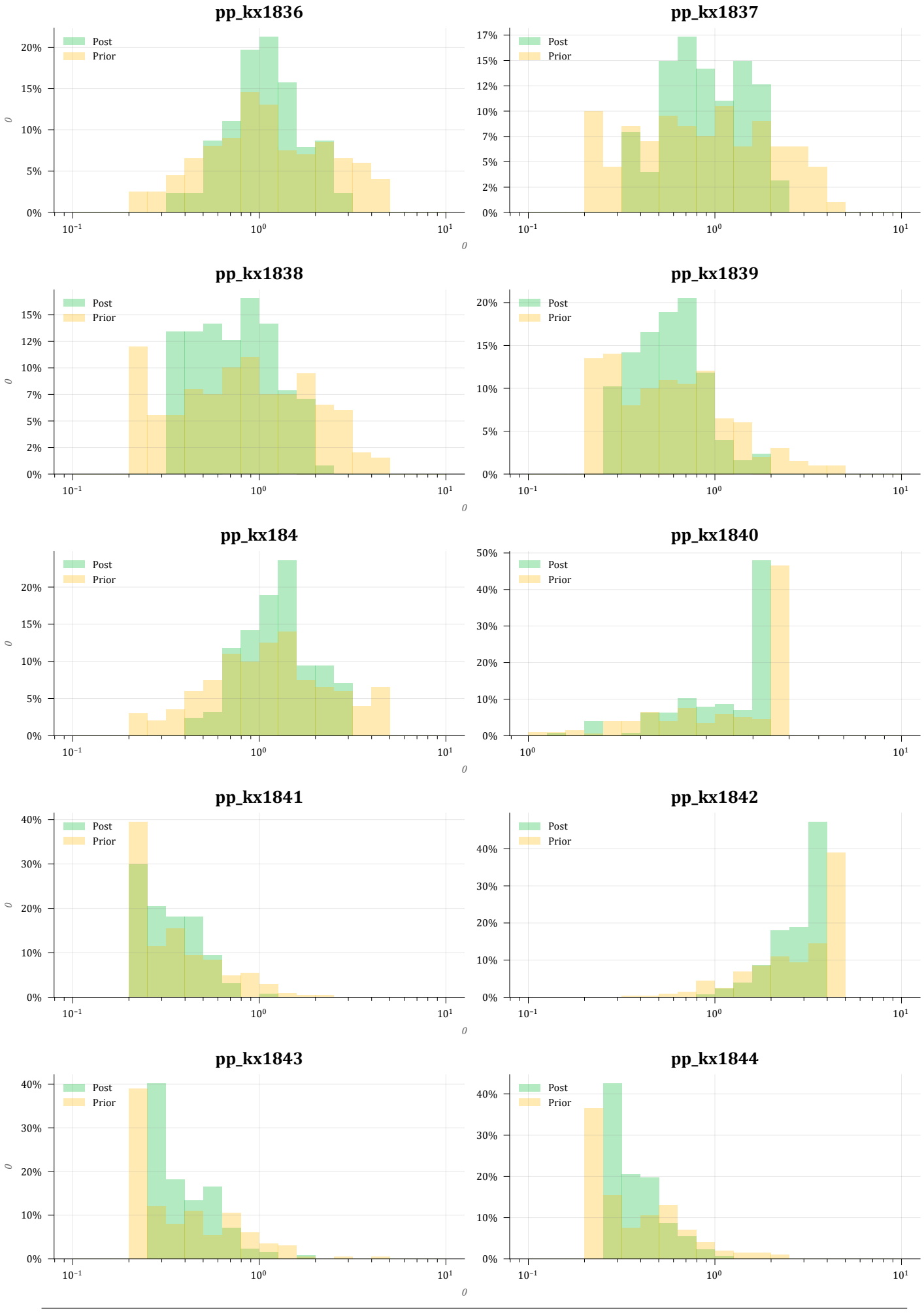

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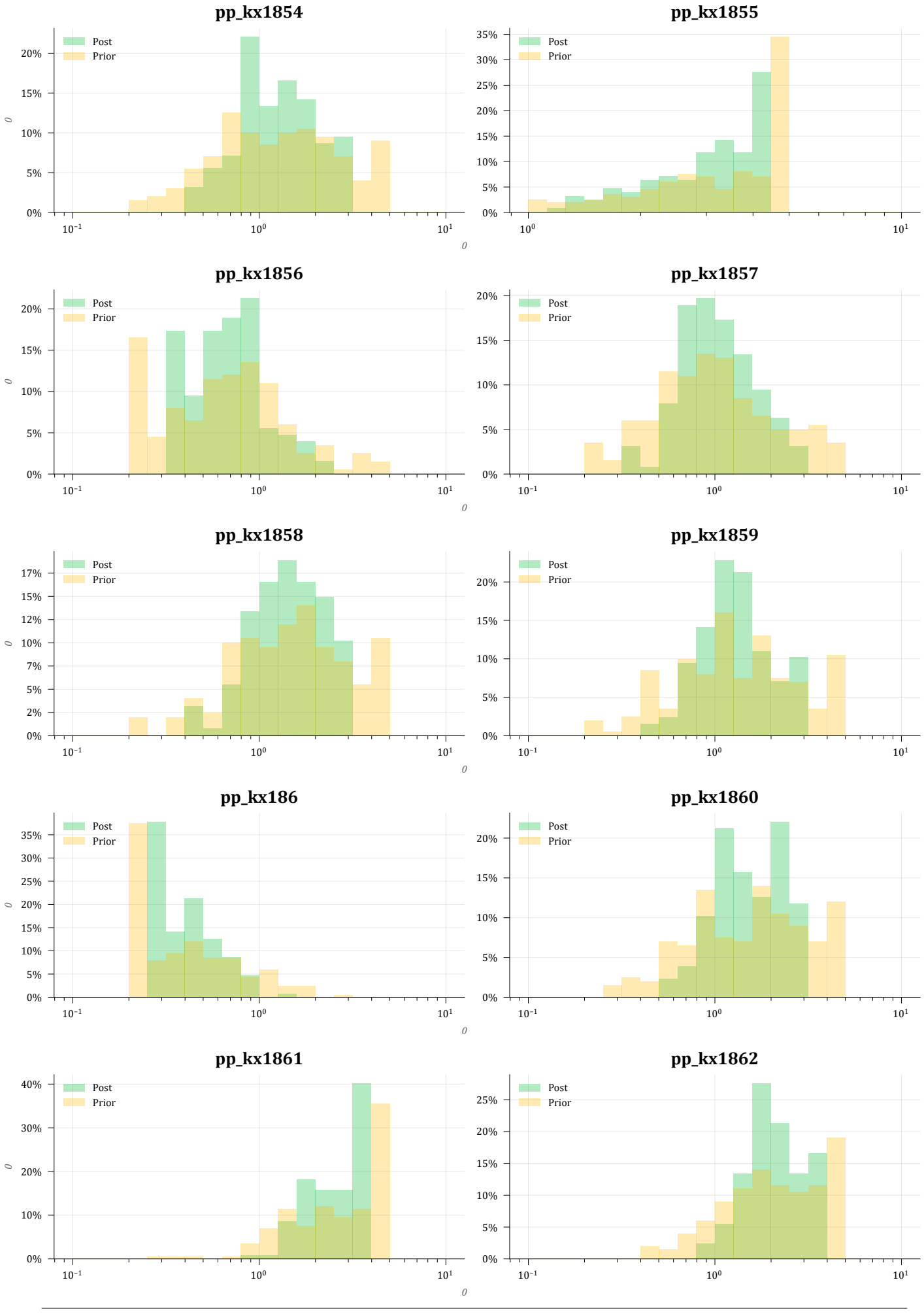

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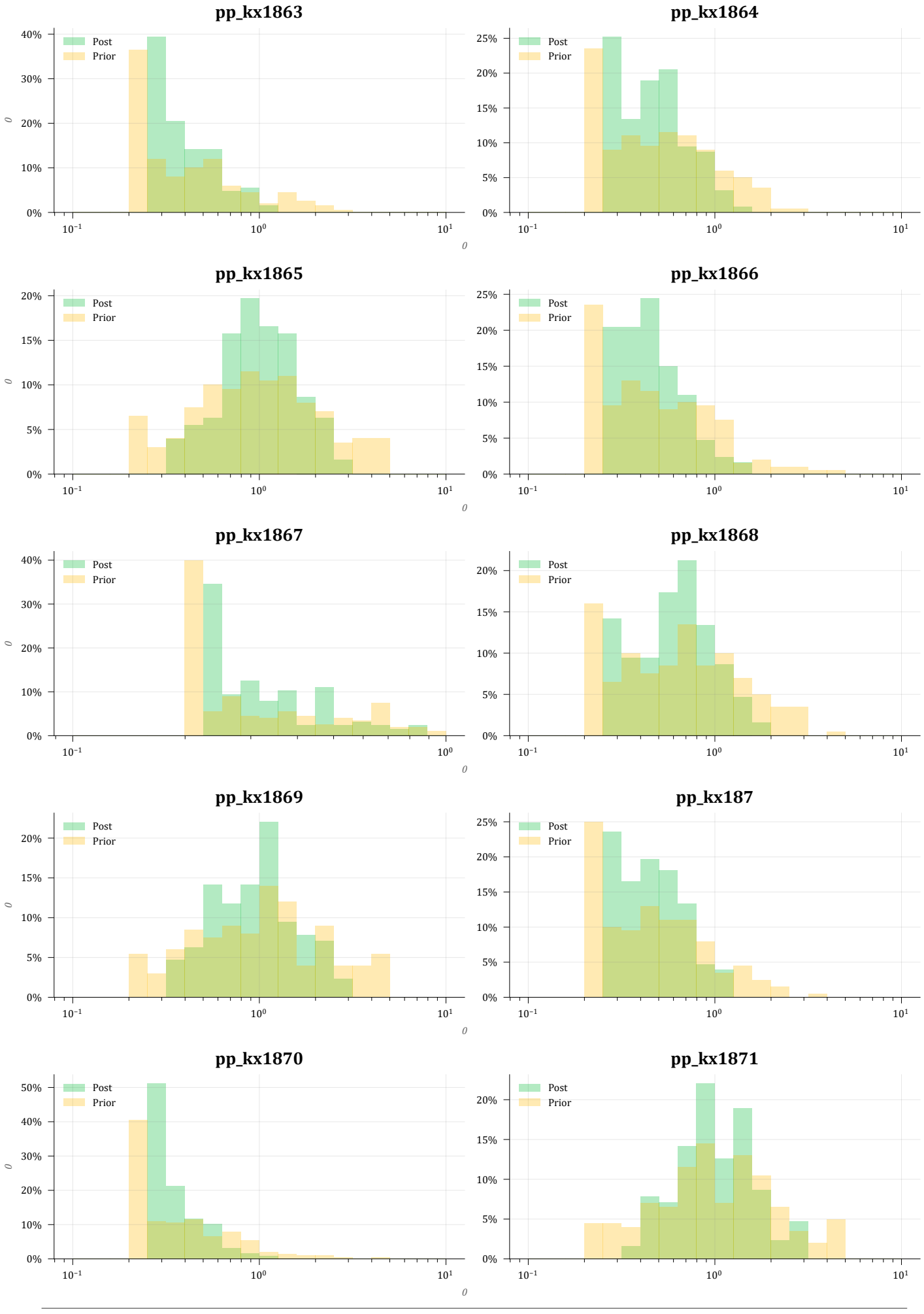

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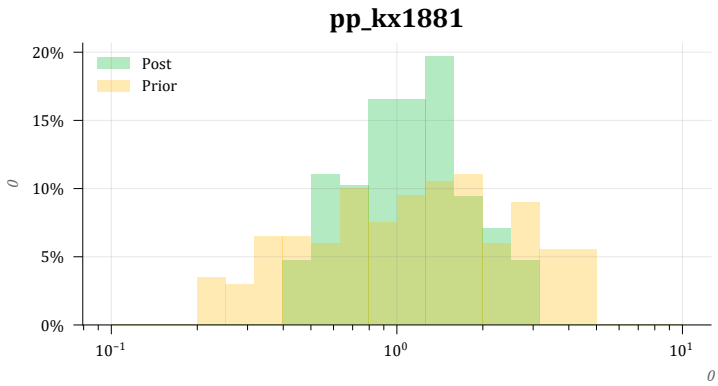

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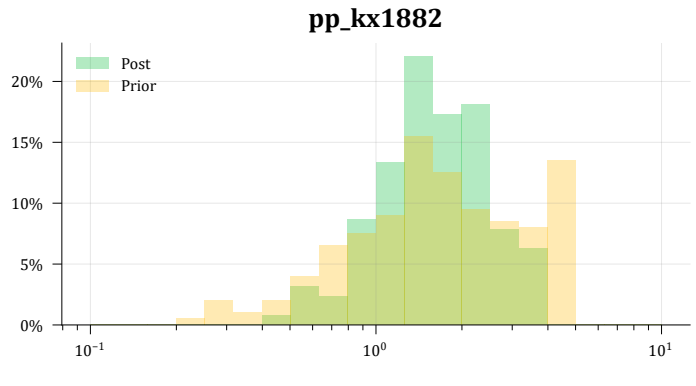

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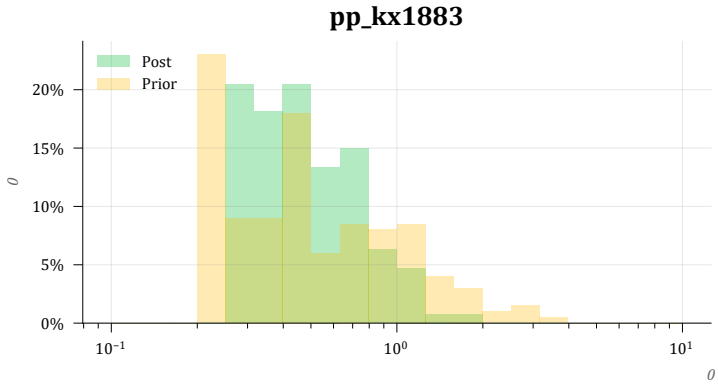

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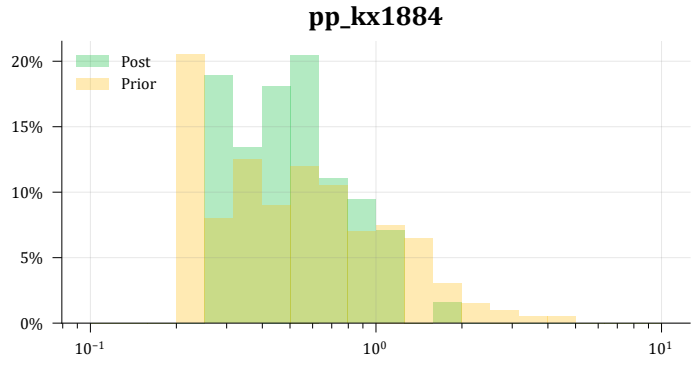

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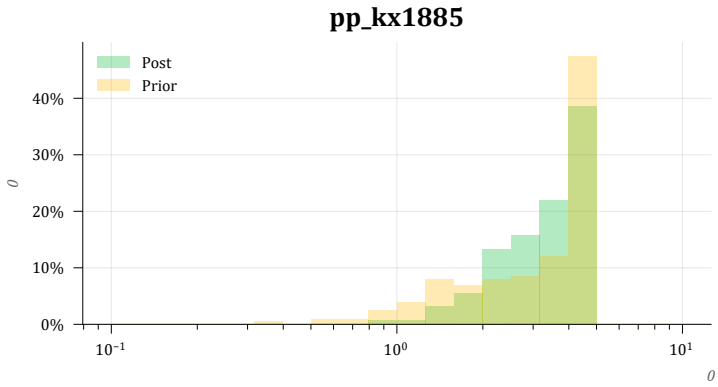

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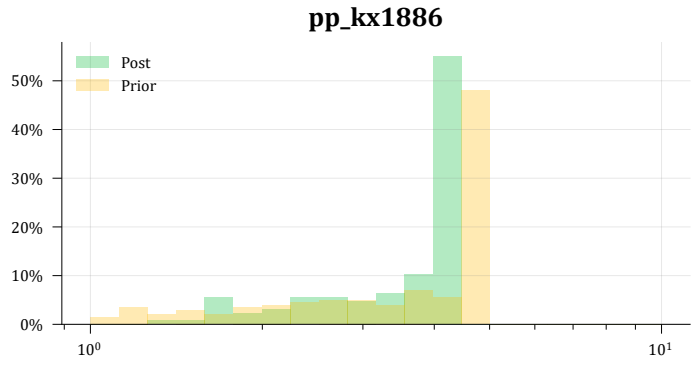

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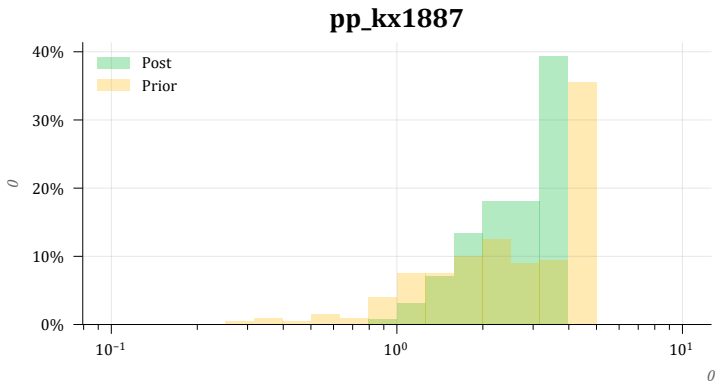

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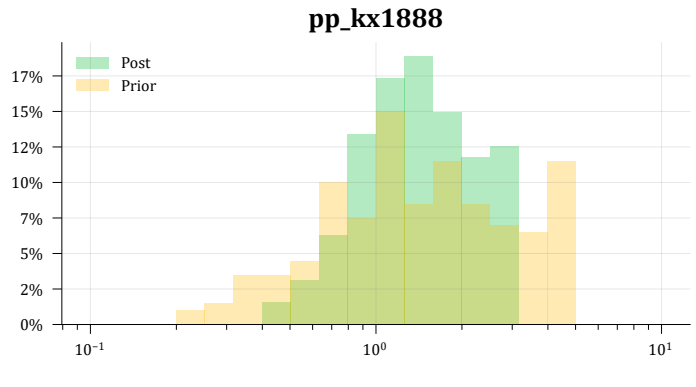

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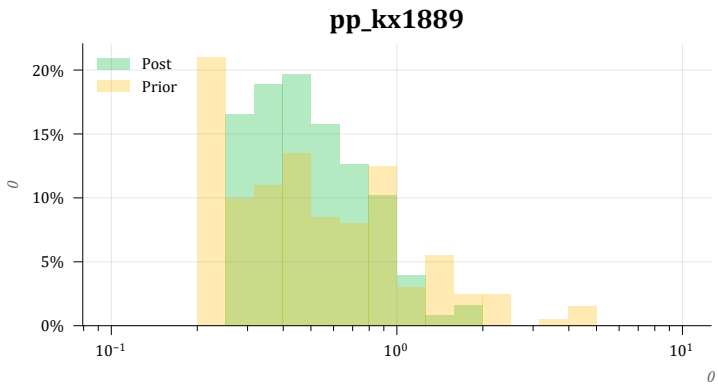

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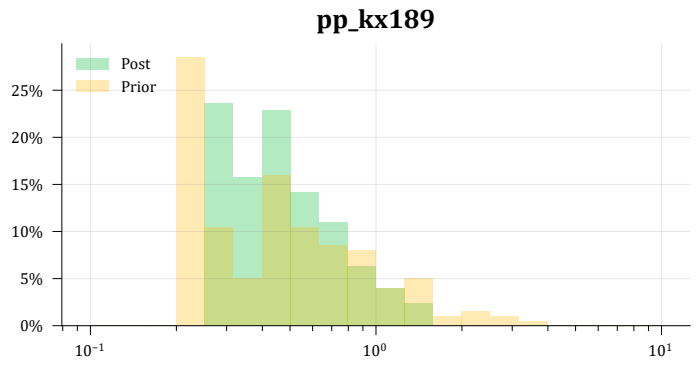

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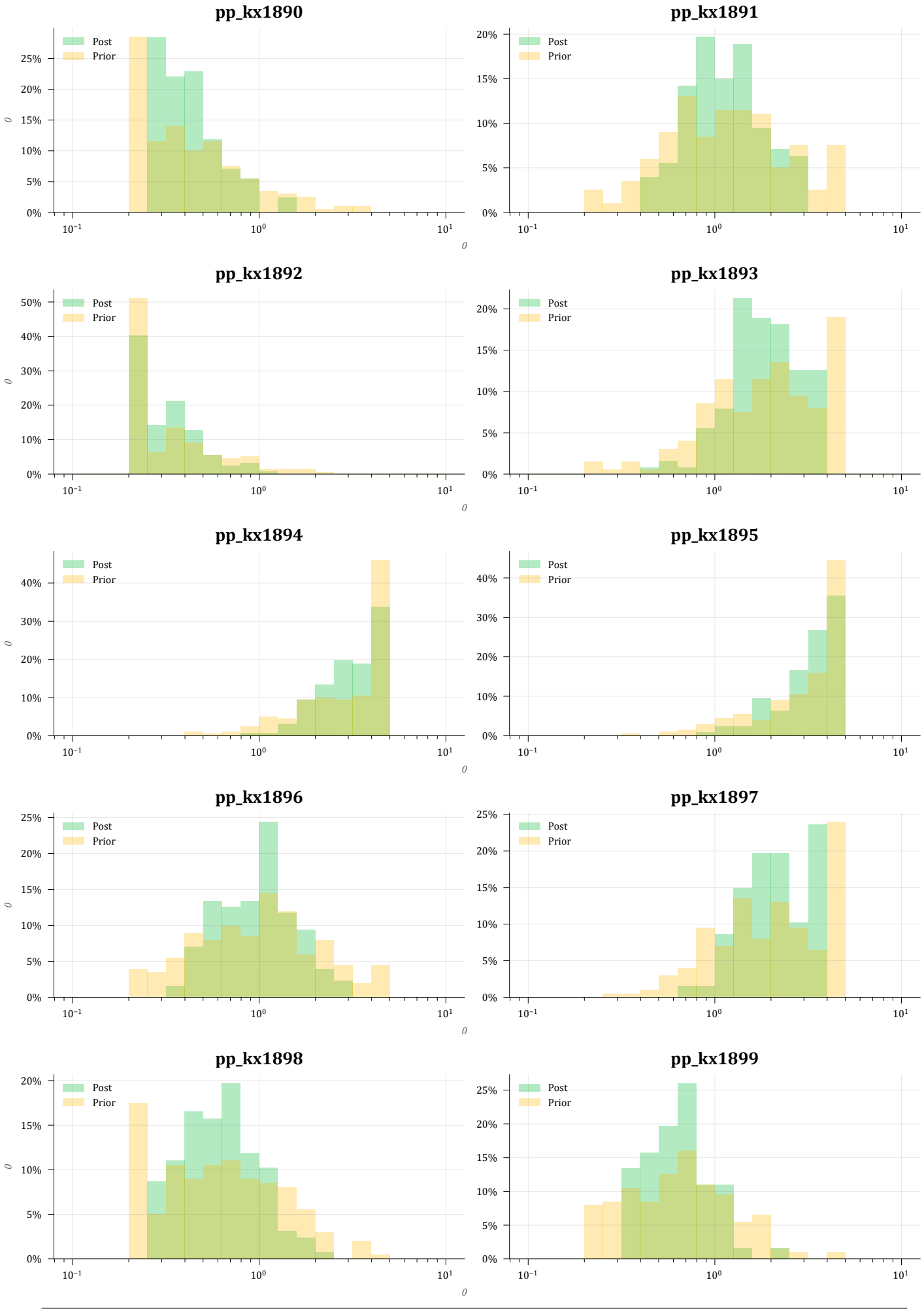

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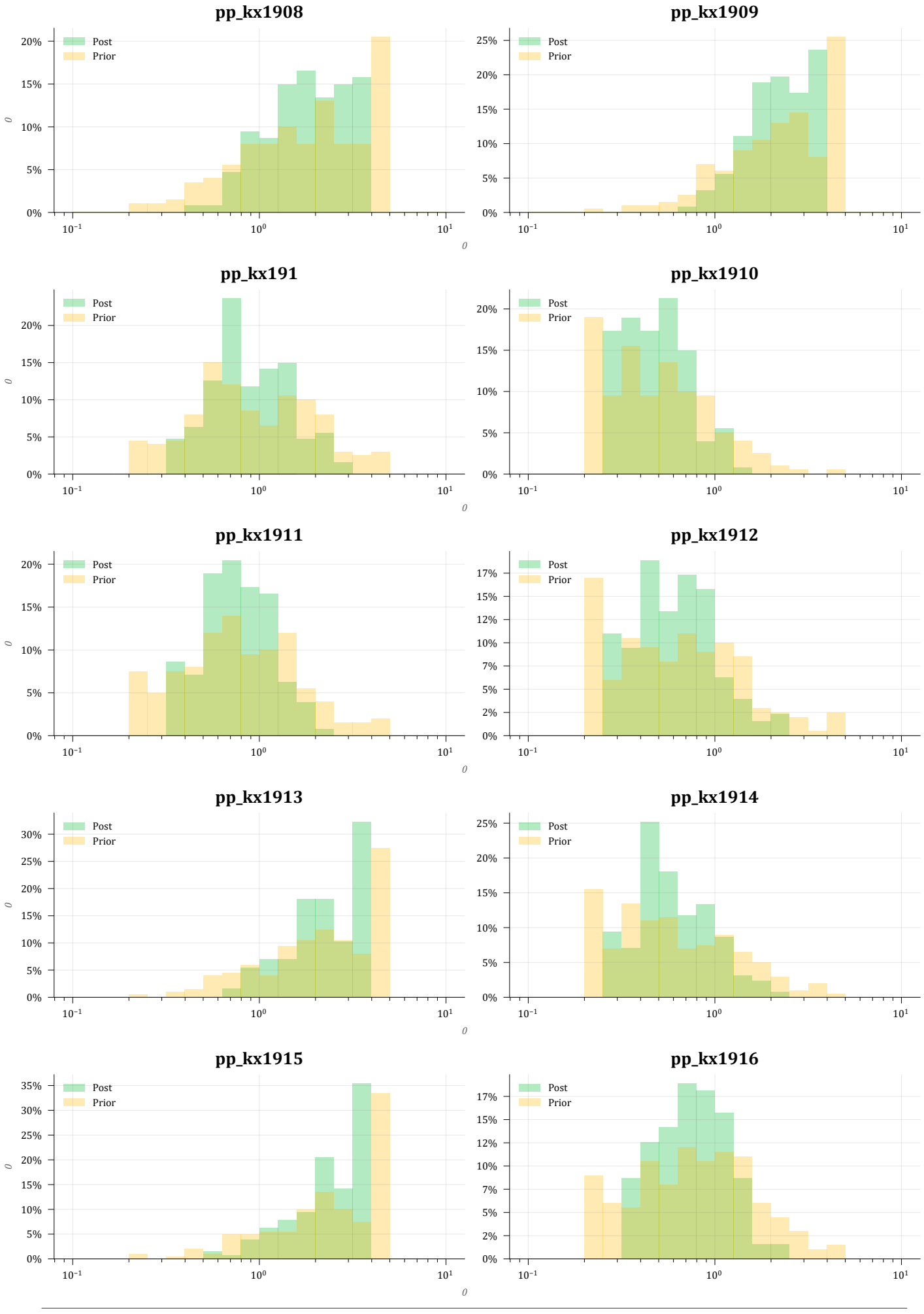

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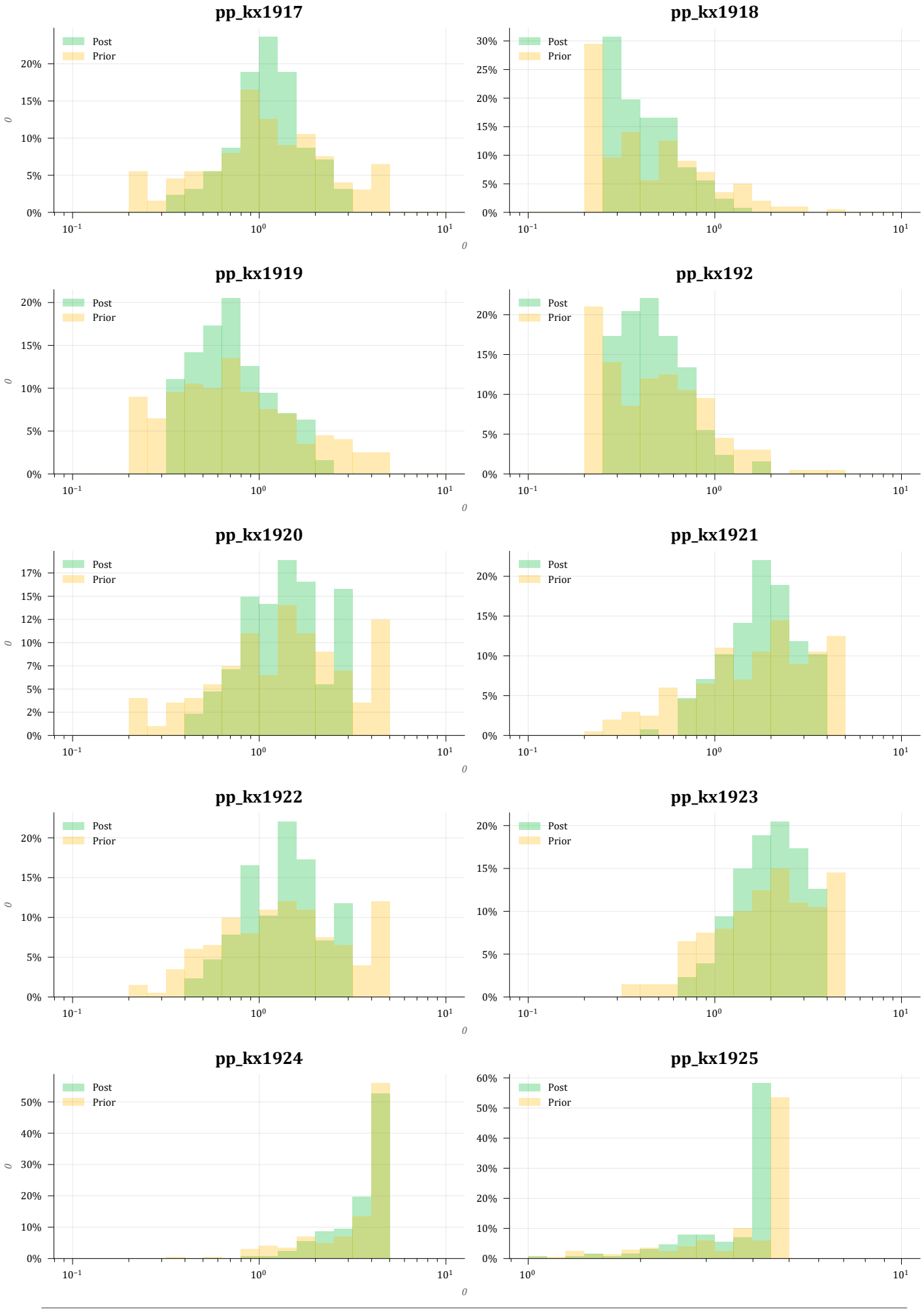

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pp_kx189
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pp_kx1893
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Prior
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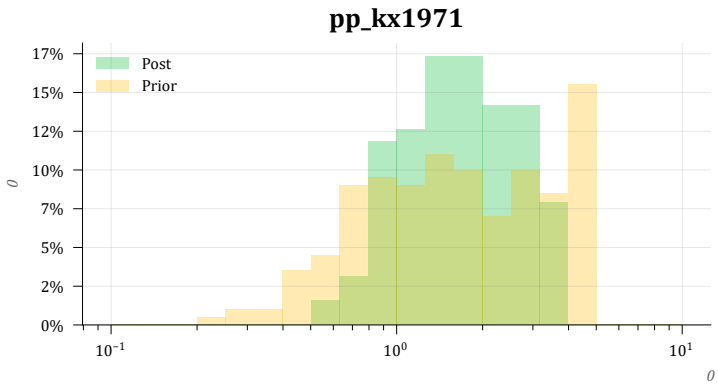

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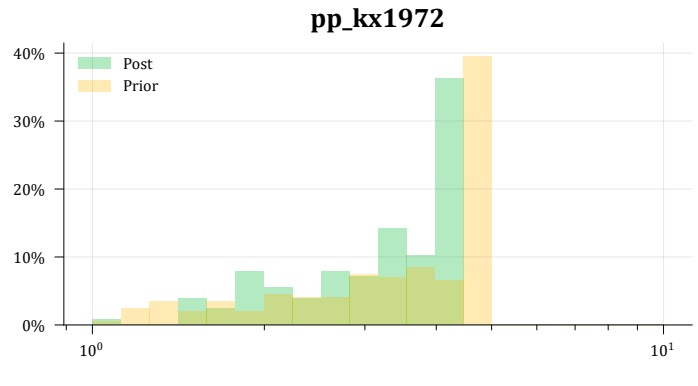

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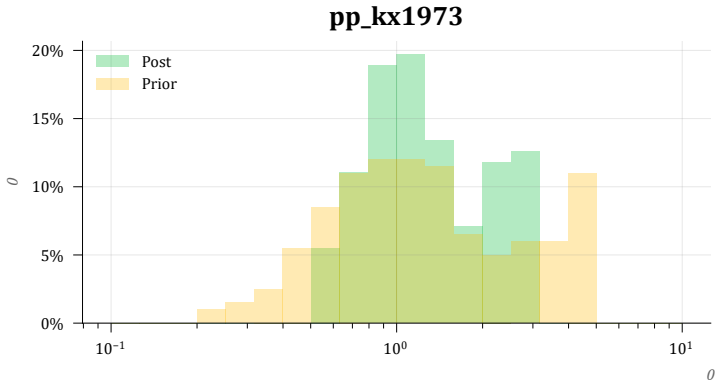

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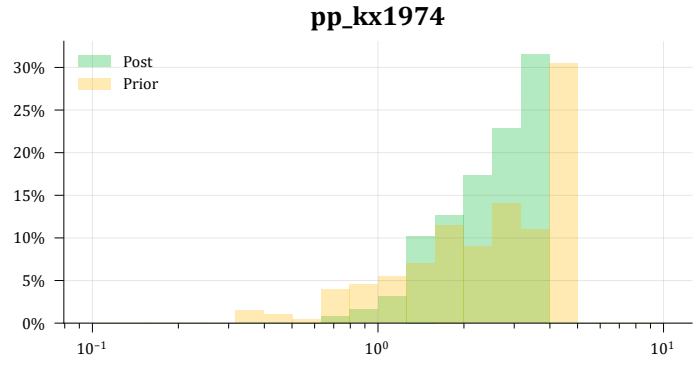

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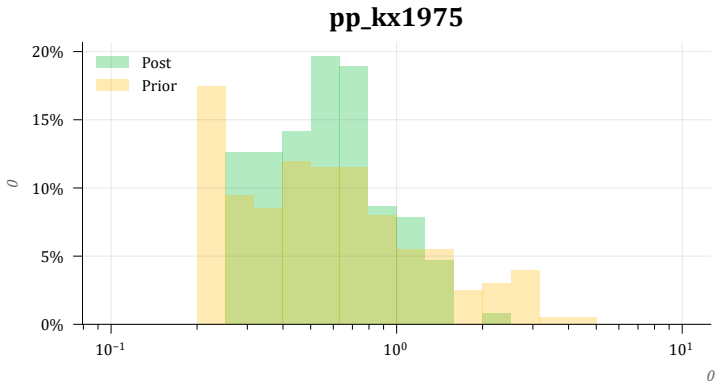

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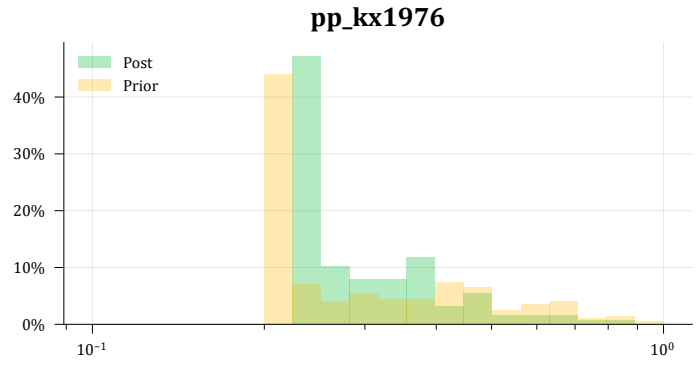

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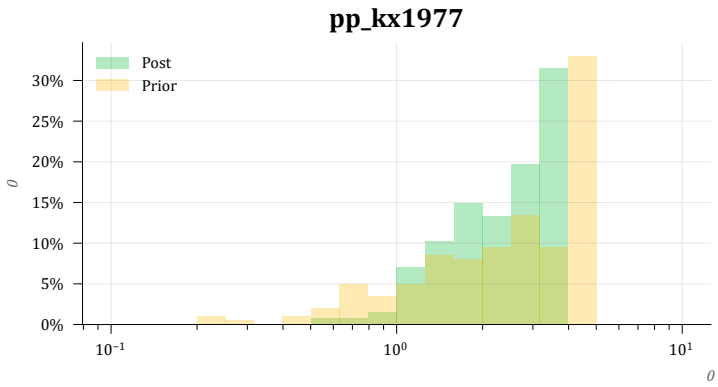

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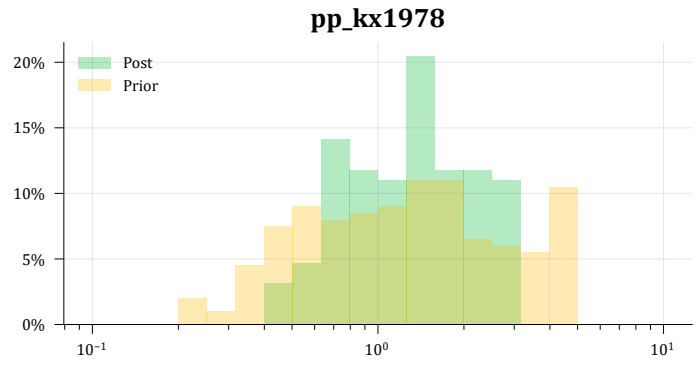

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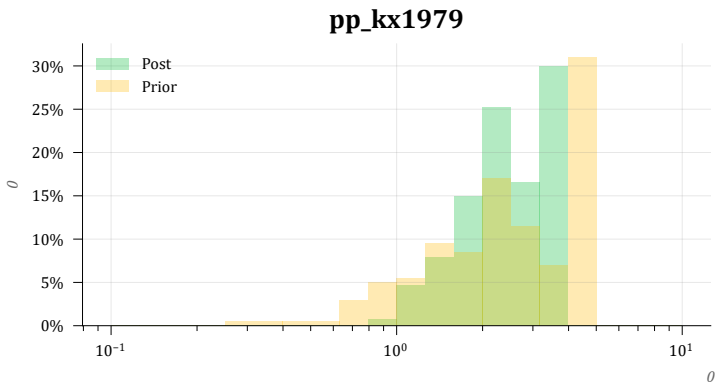

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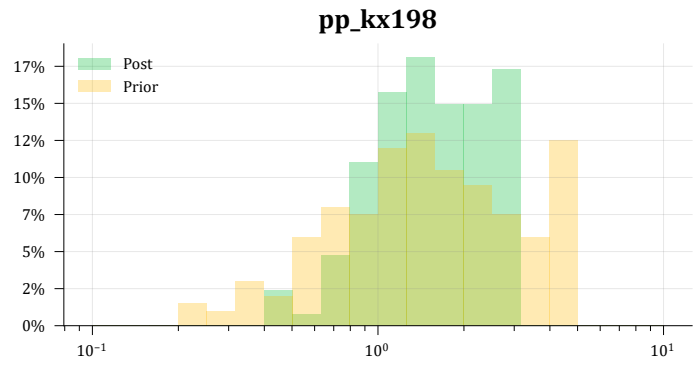

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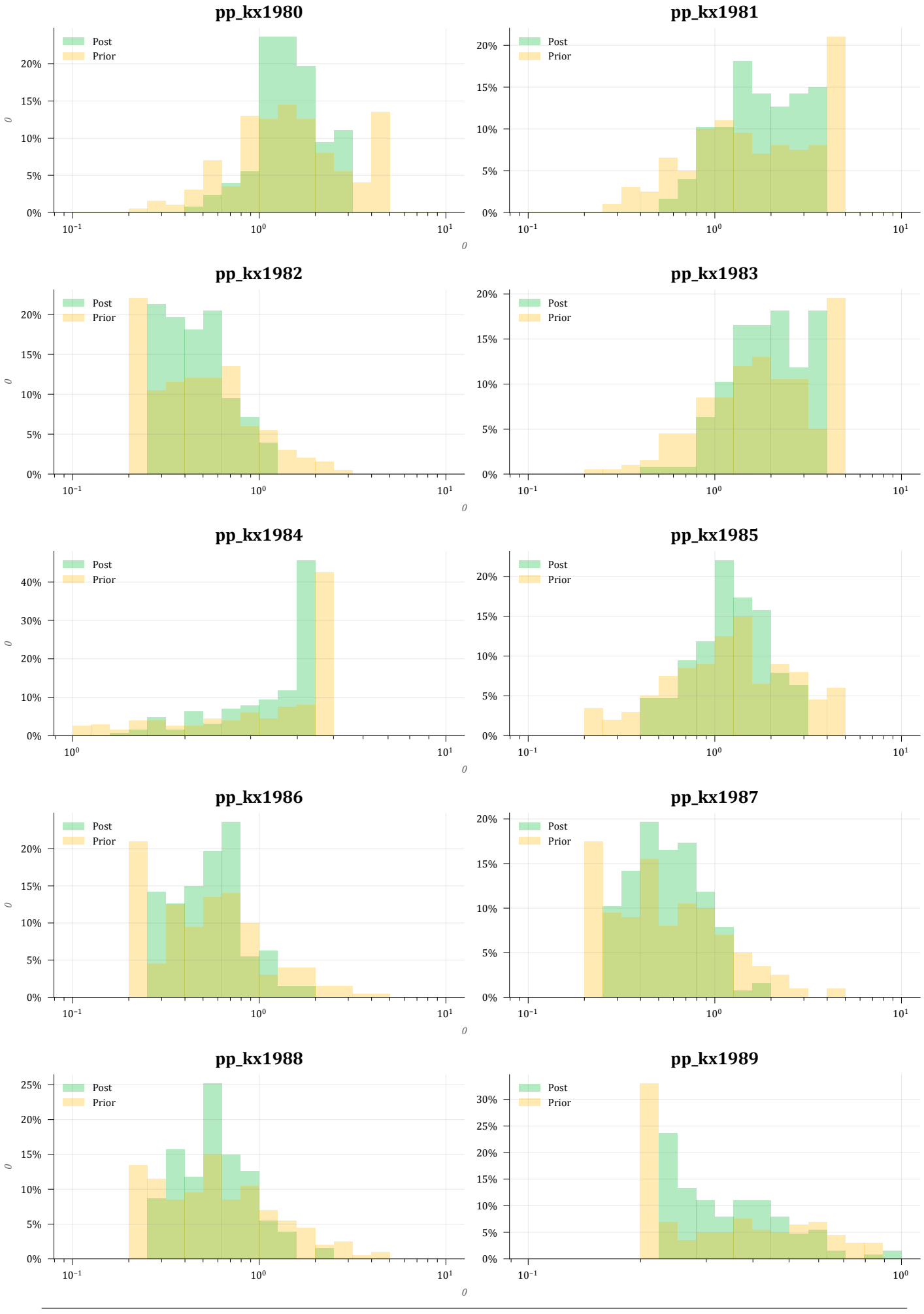

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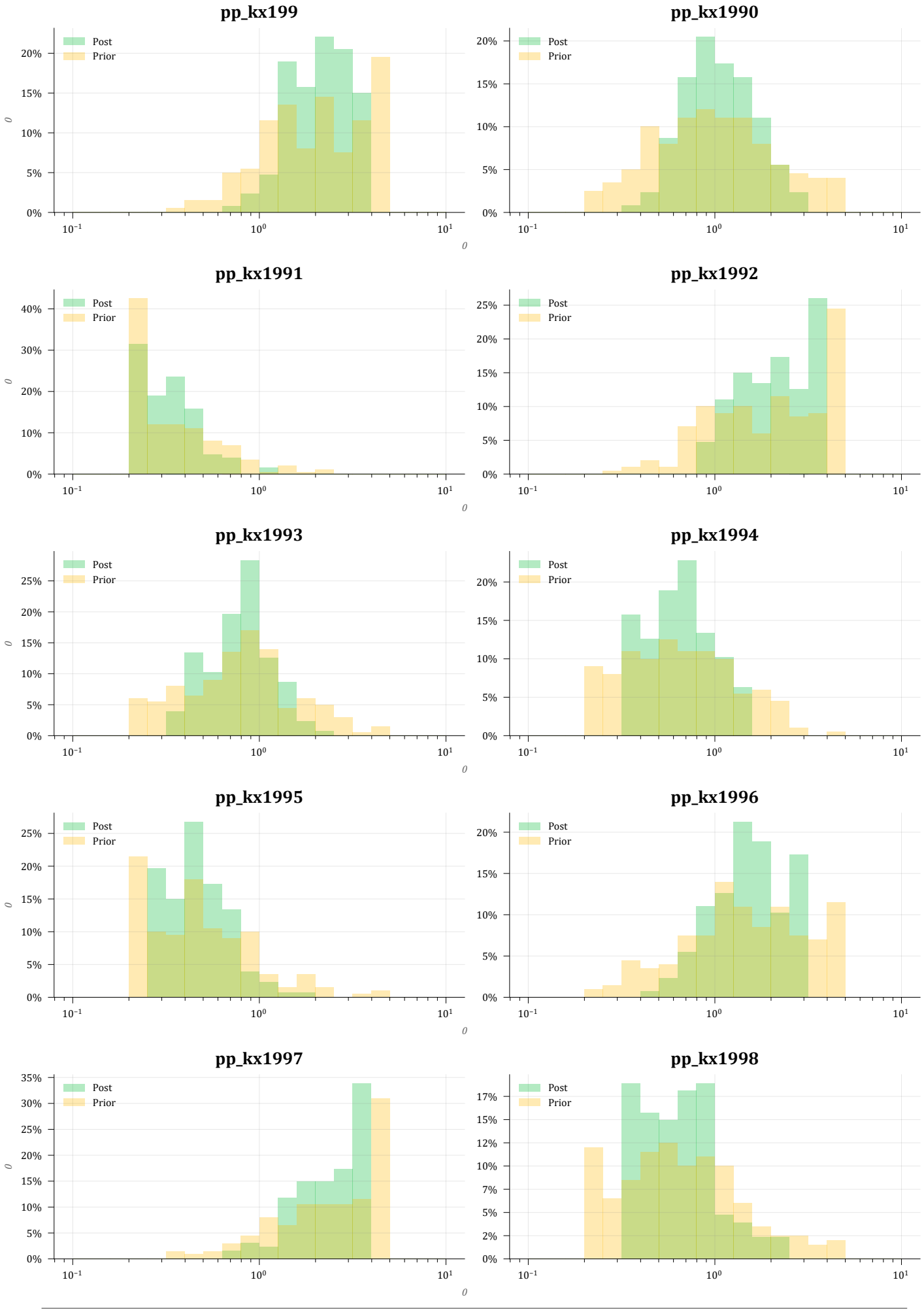

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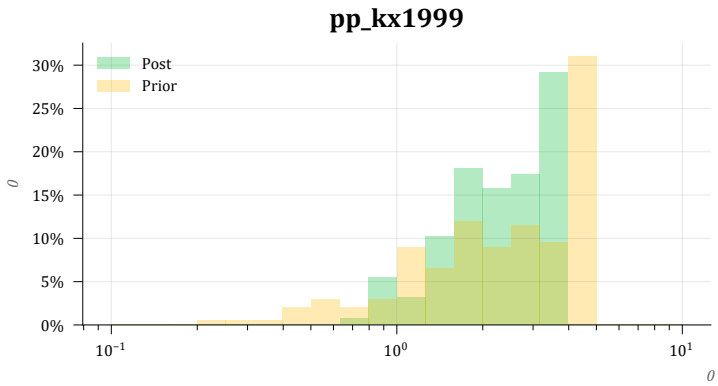

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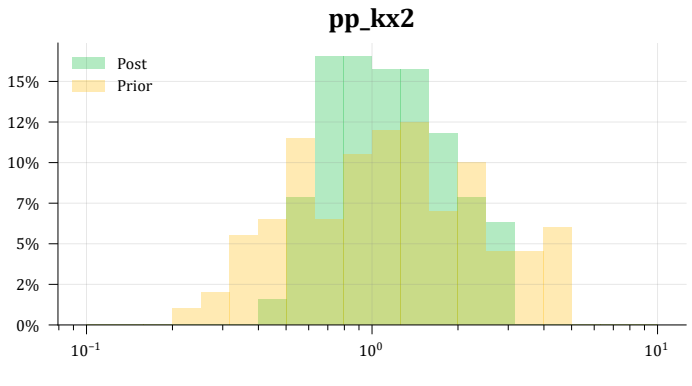

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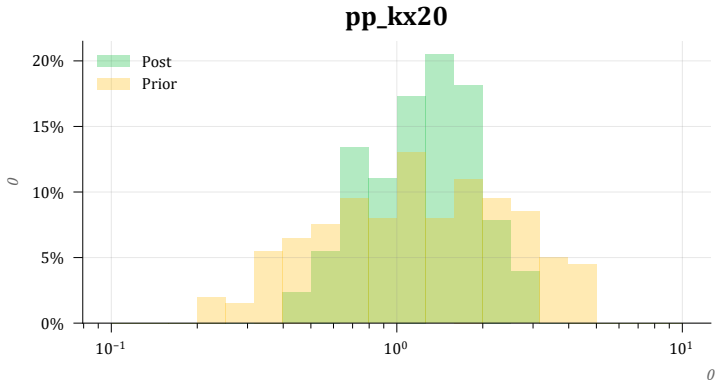

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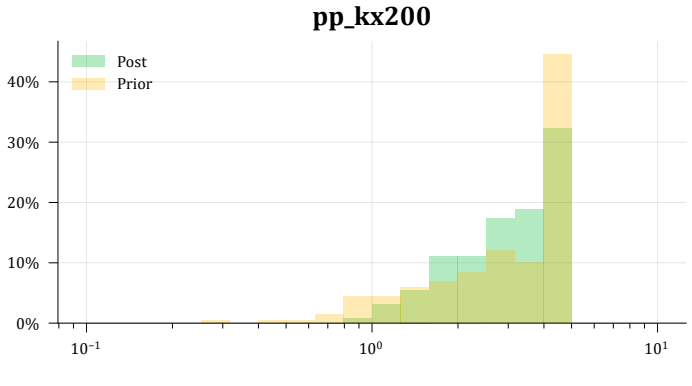

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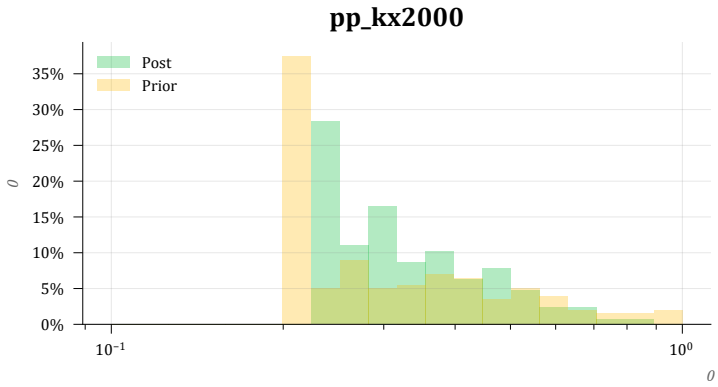

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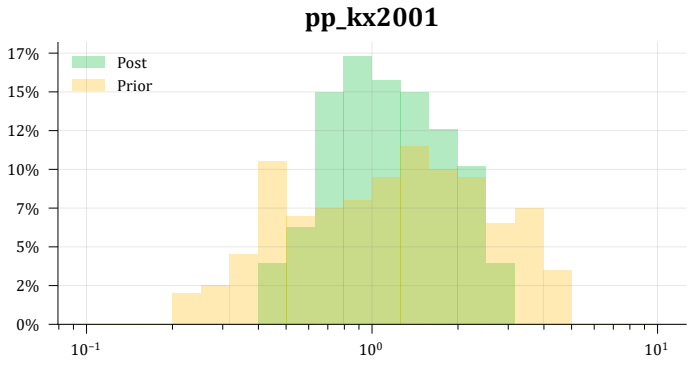

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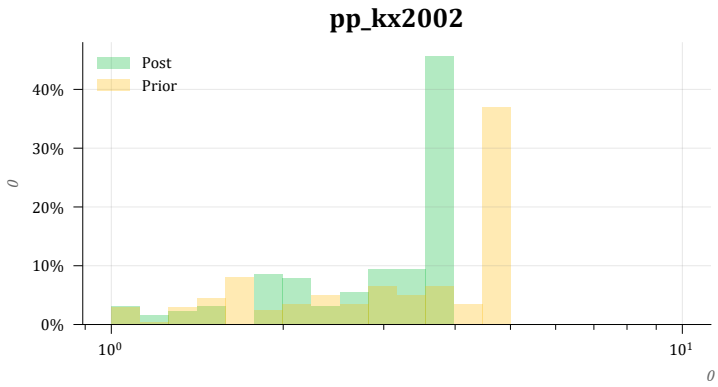

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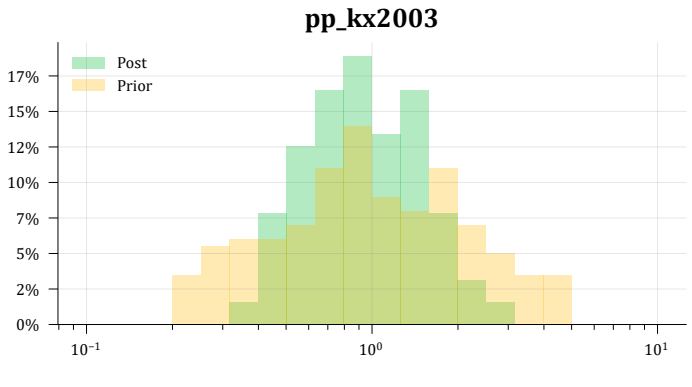

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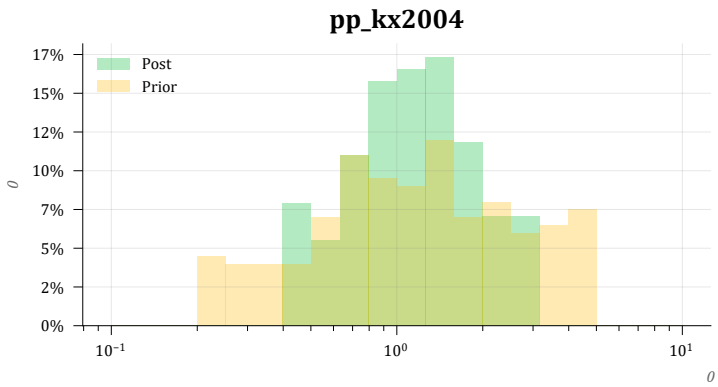

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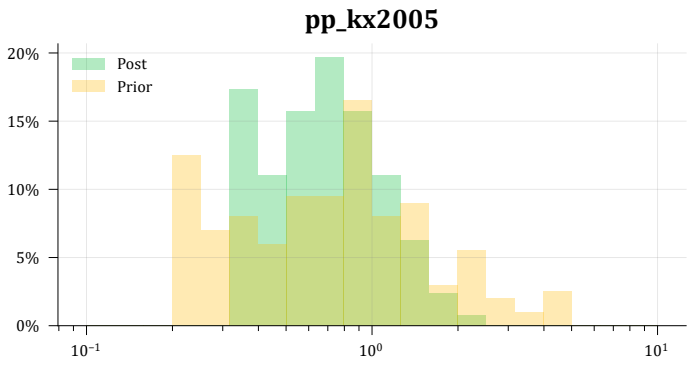

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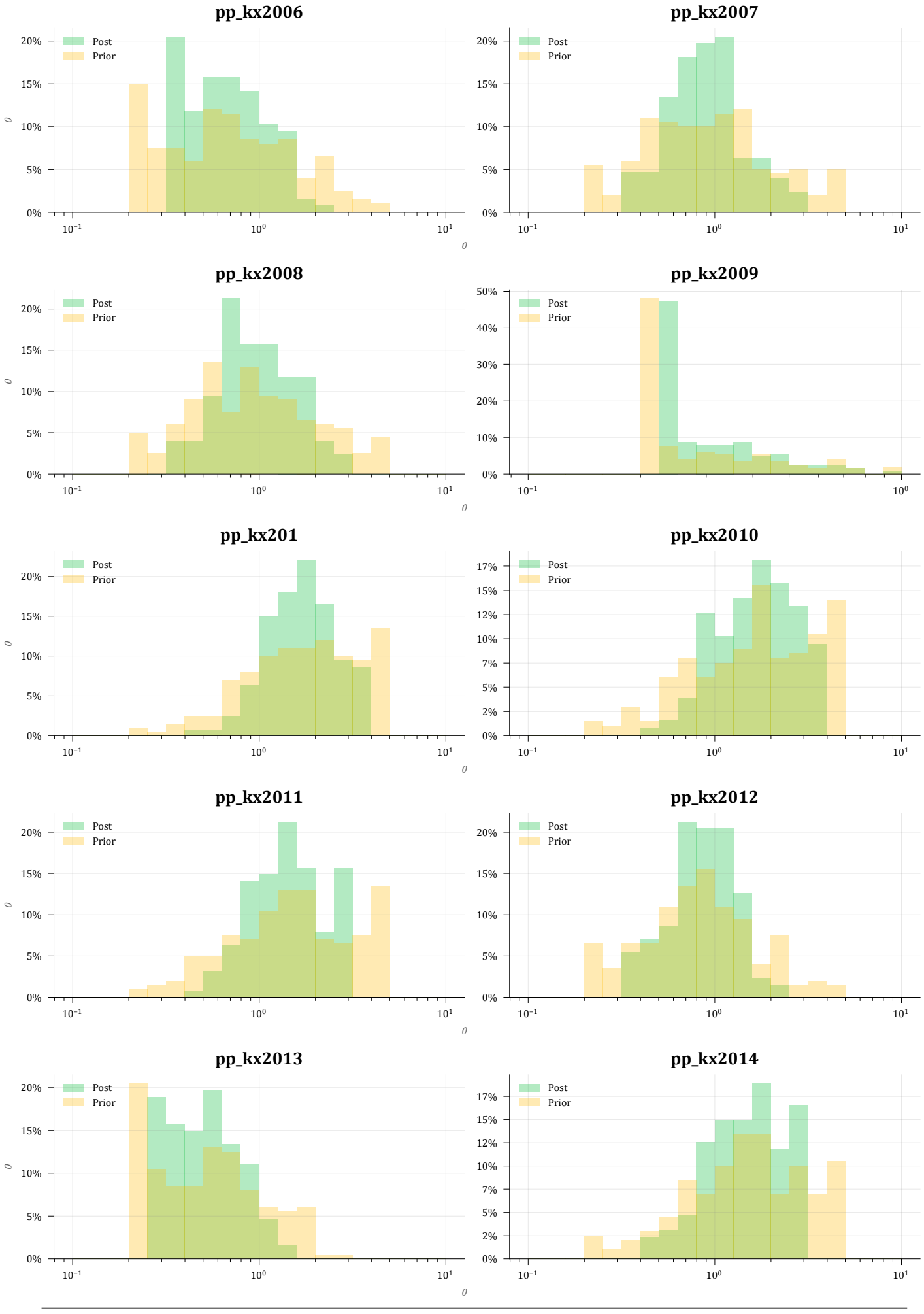

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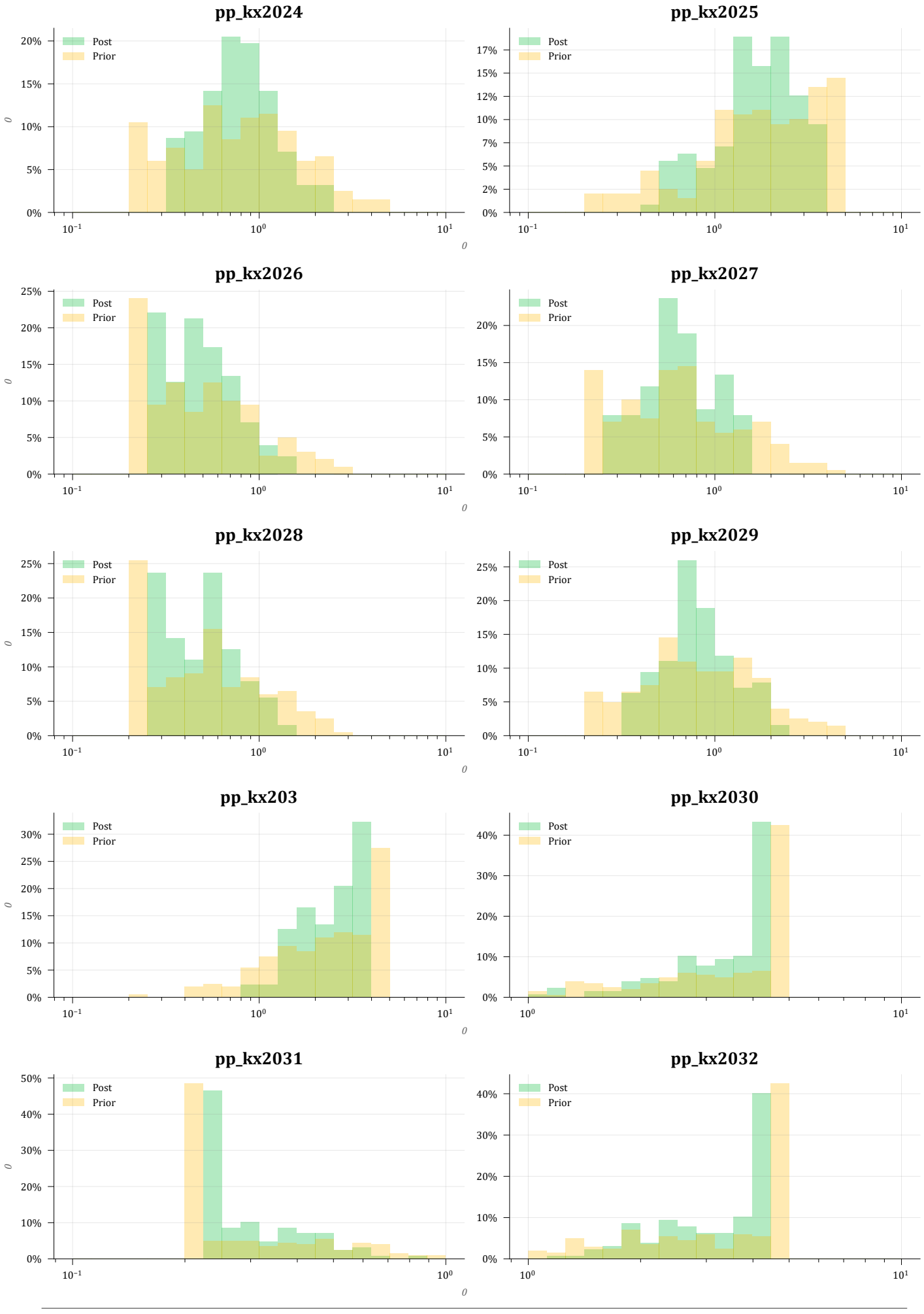

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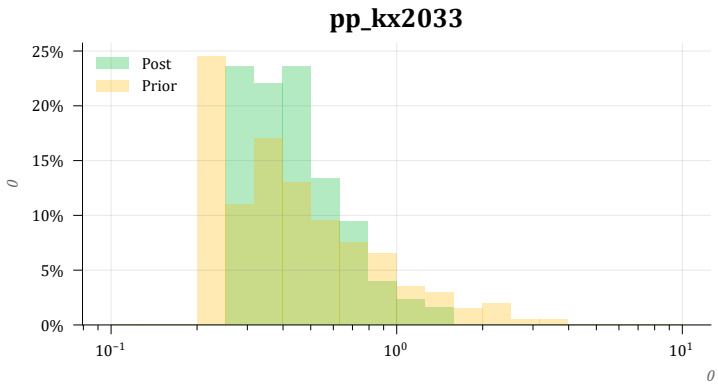

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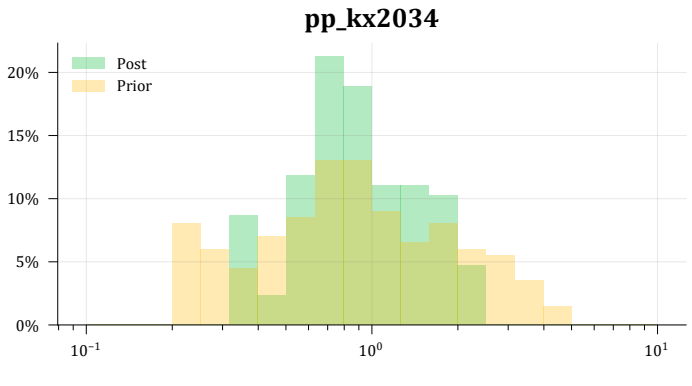
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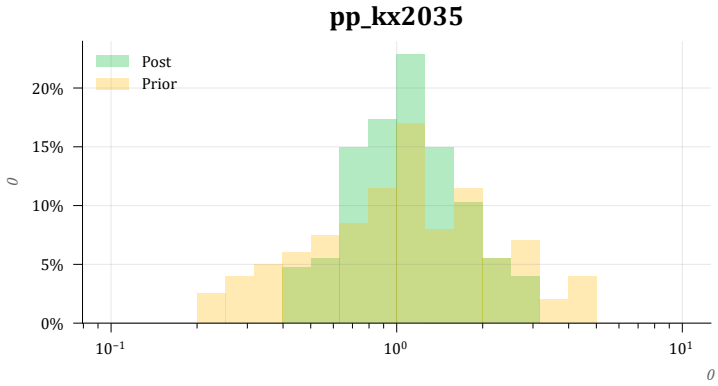

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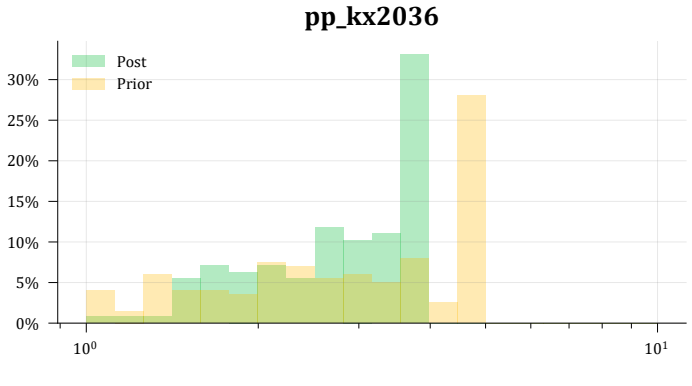

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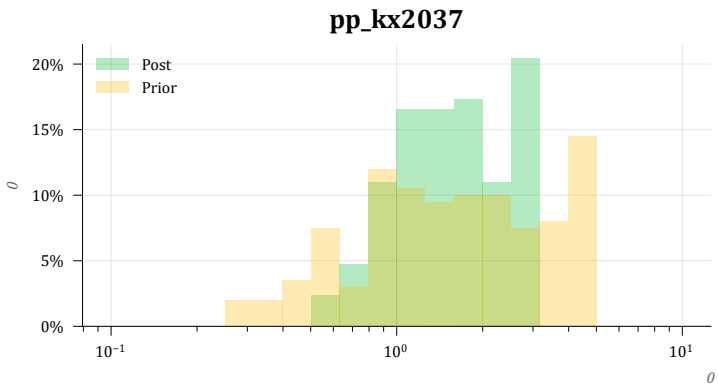

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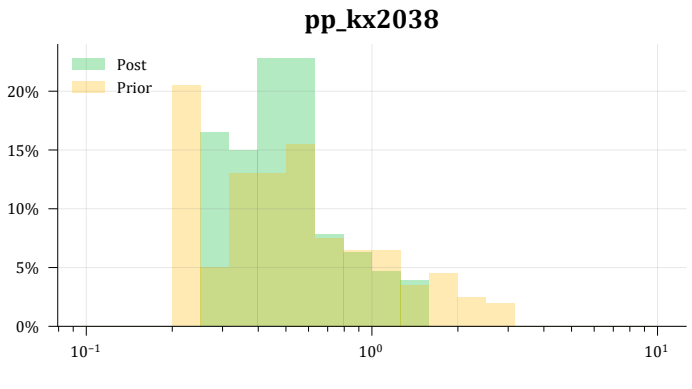

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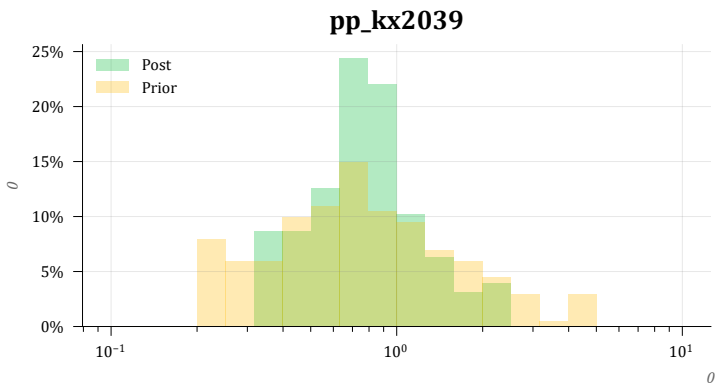

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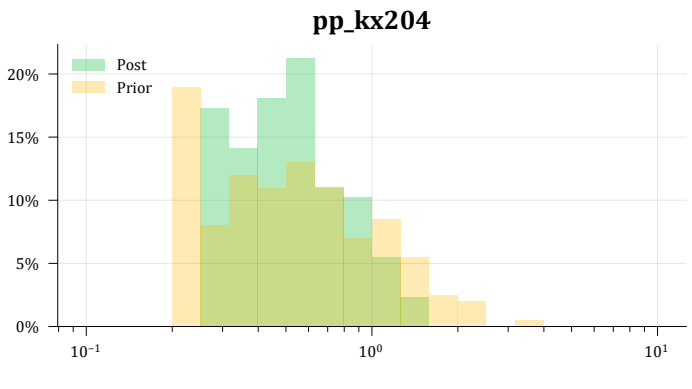

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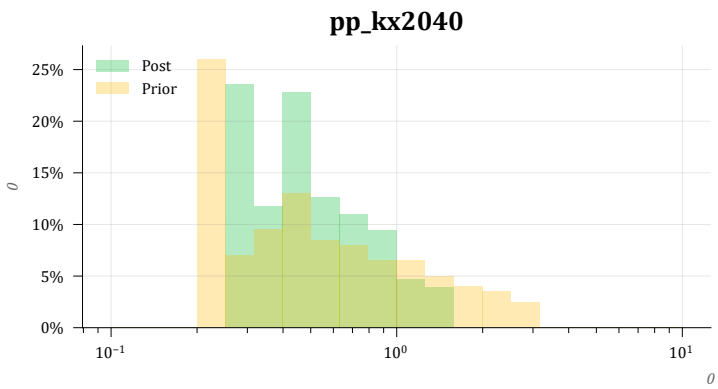

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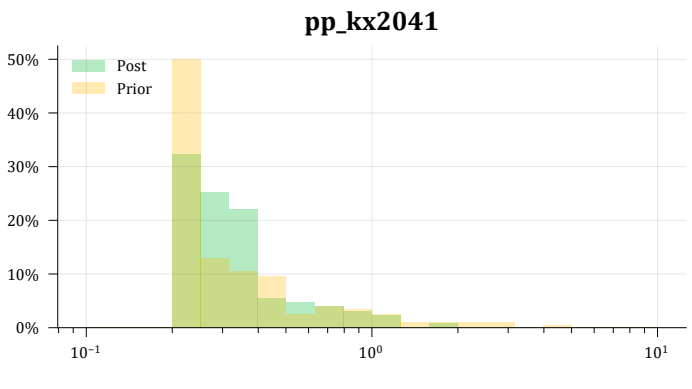

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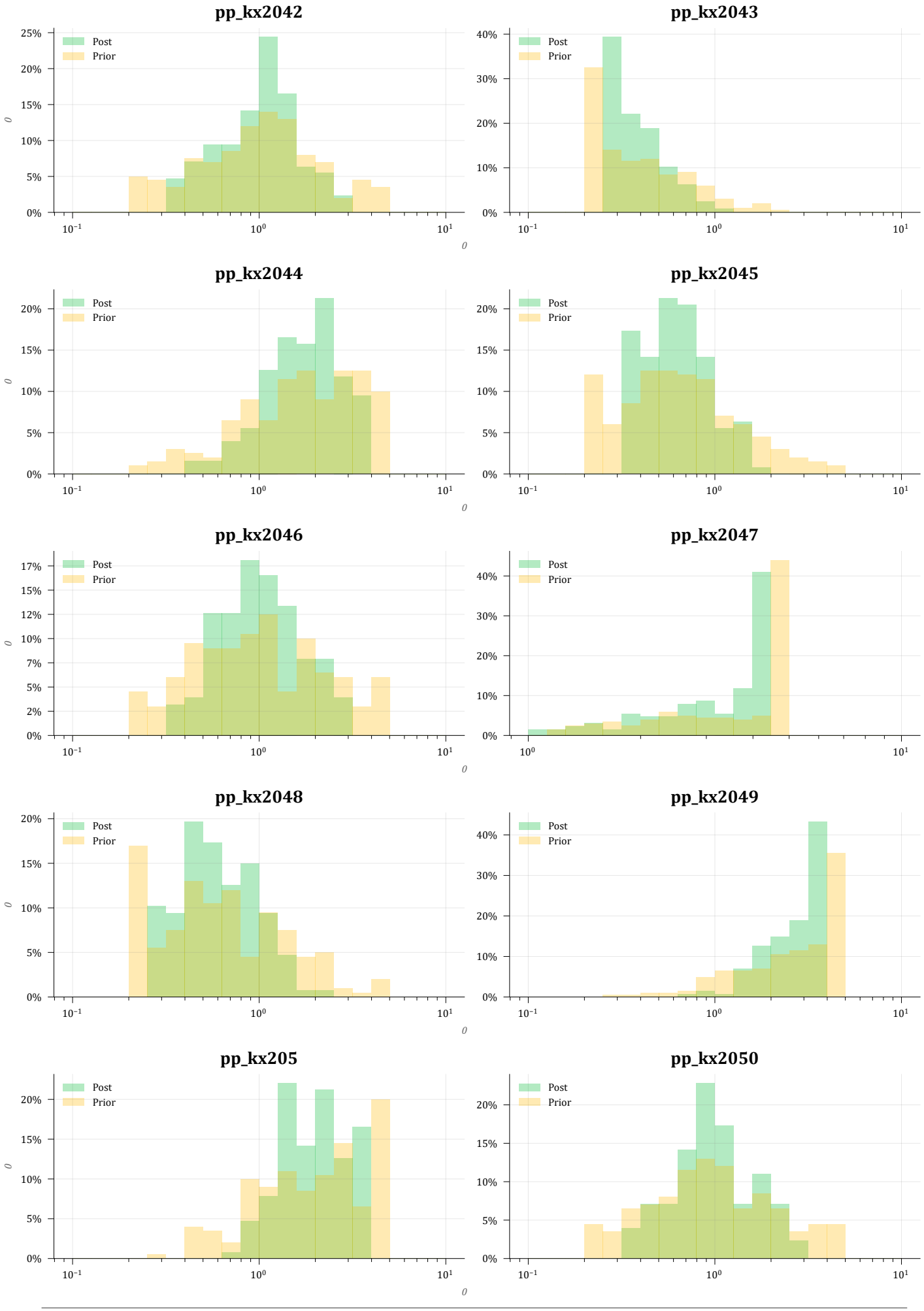

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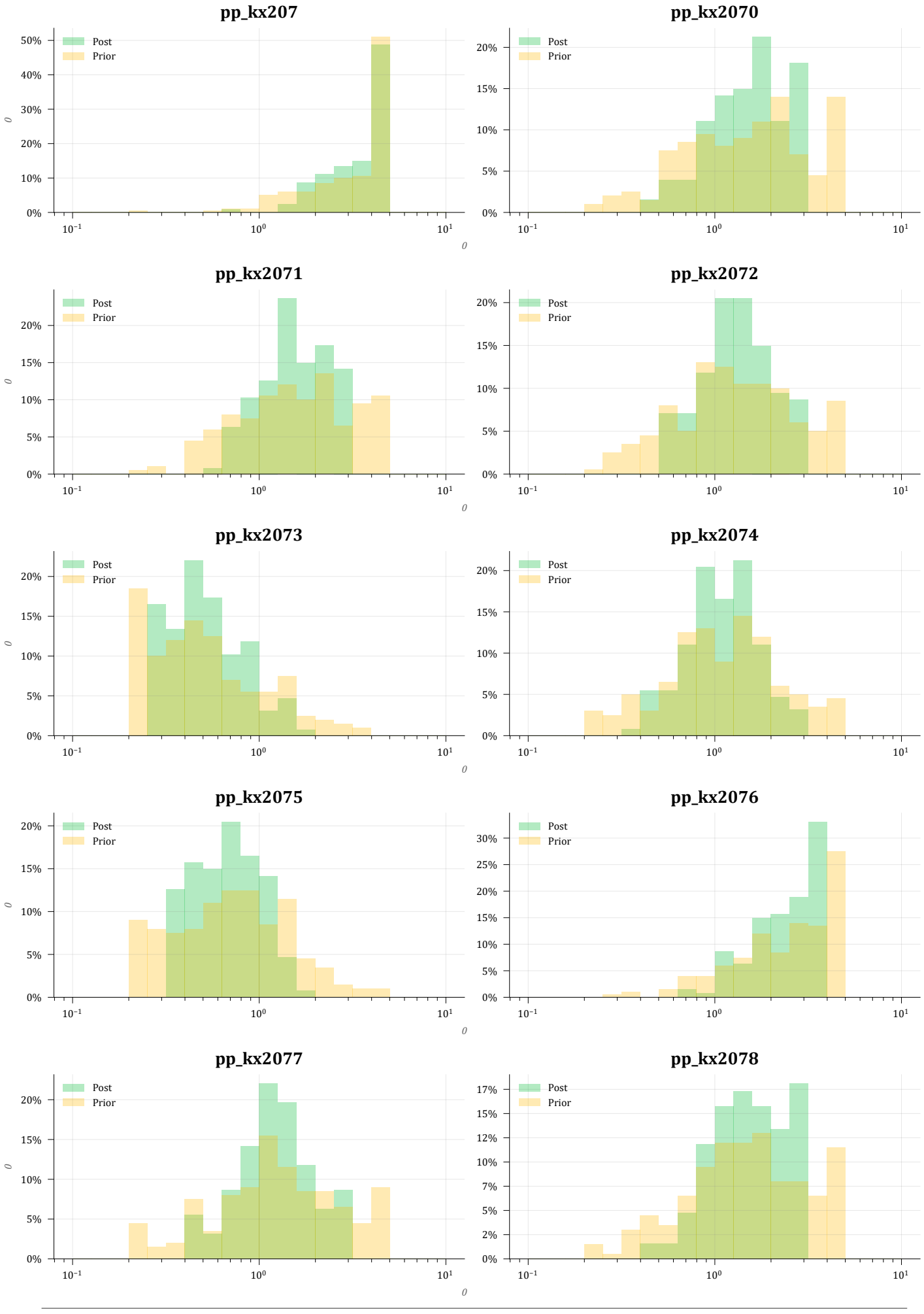

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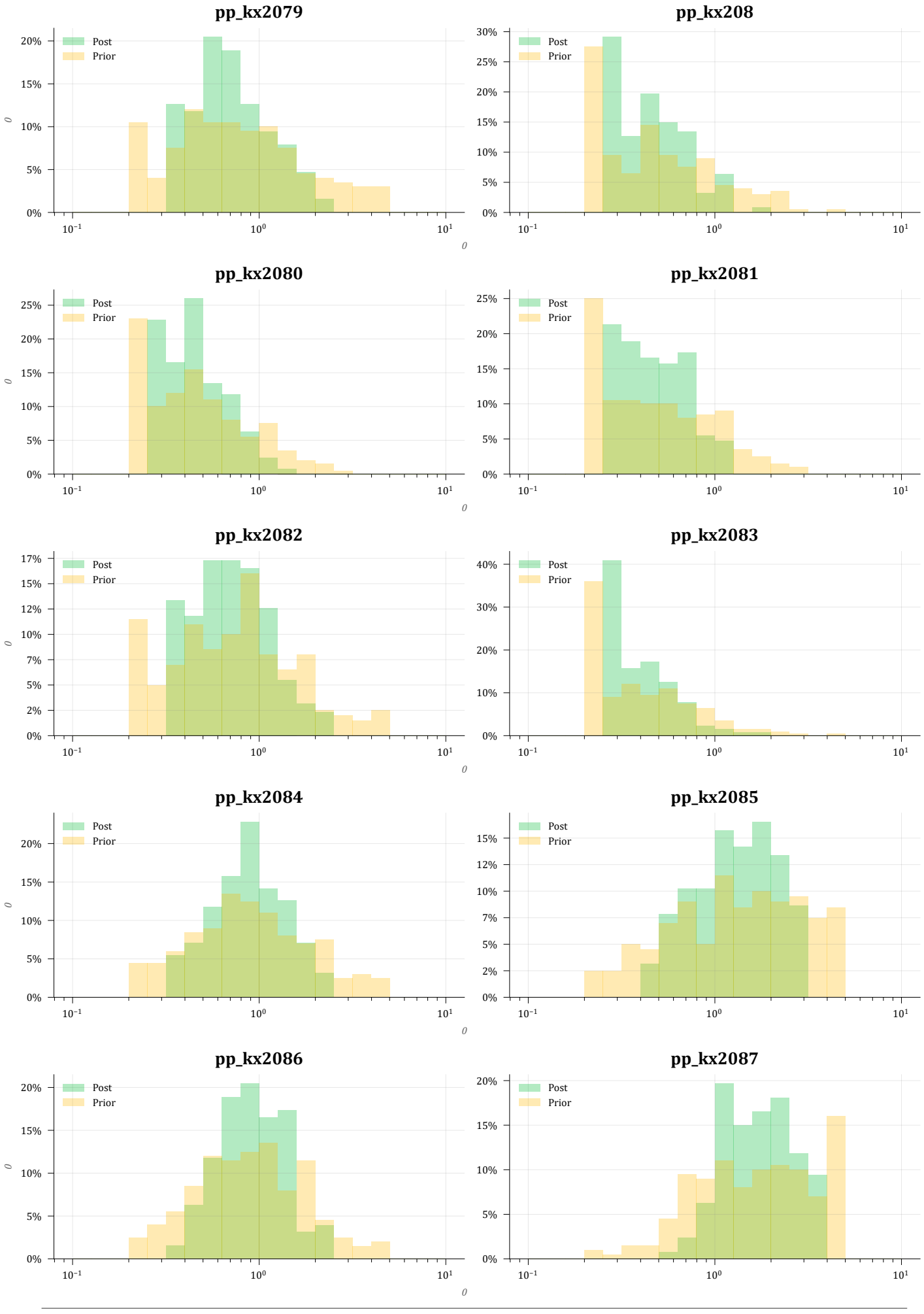
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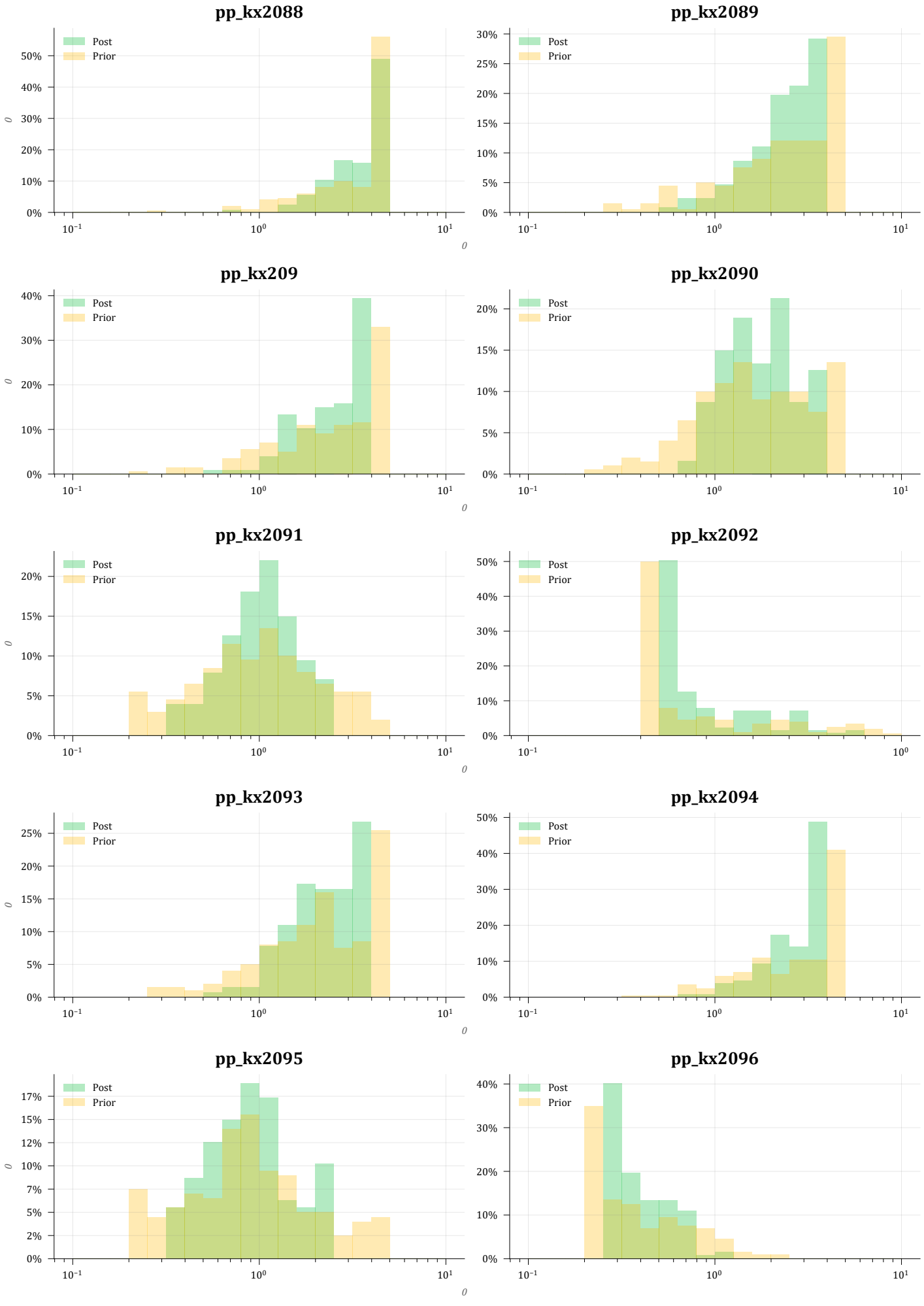

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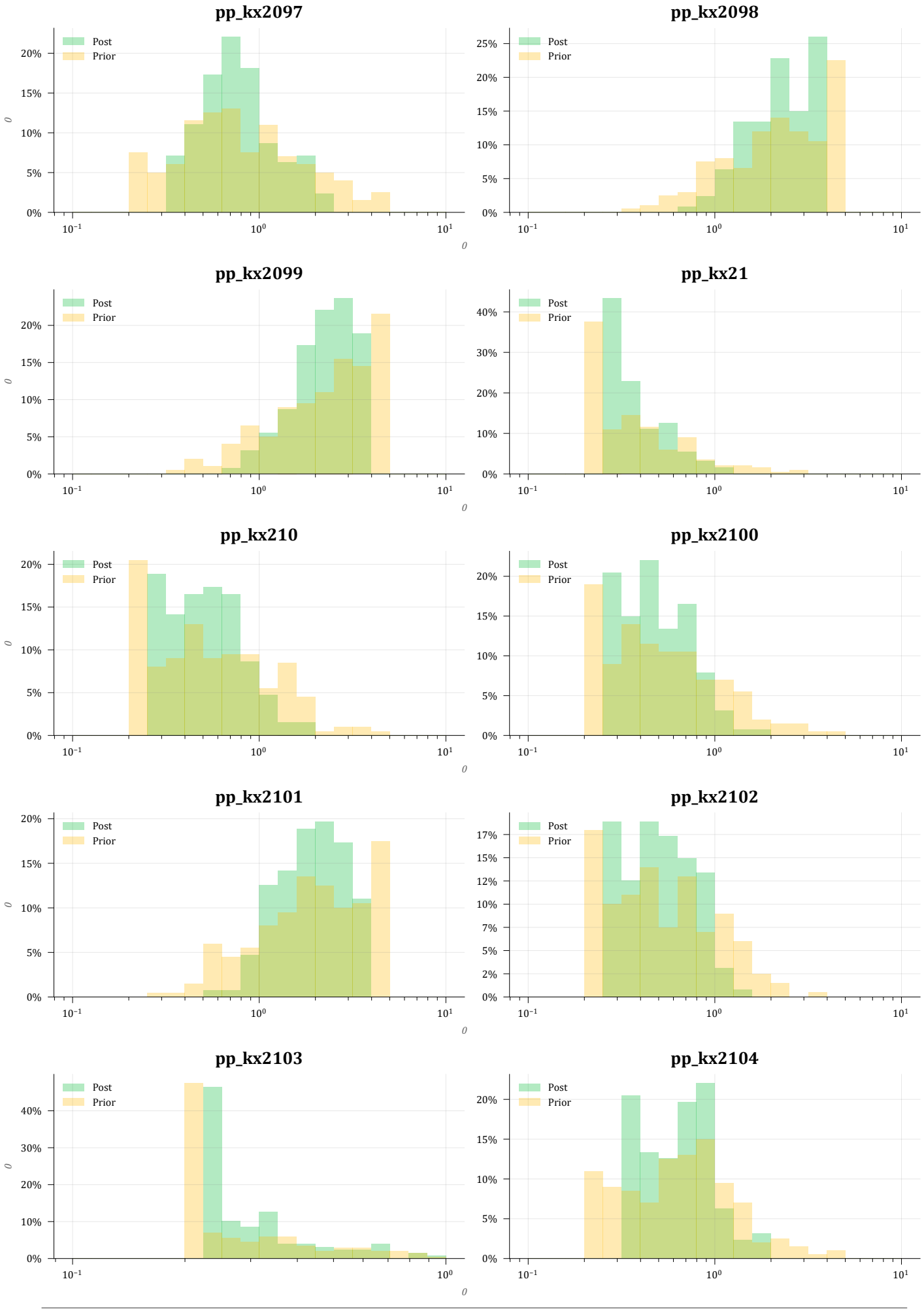

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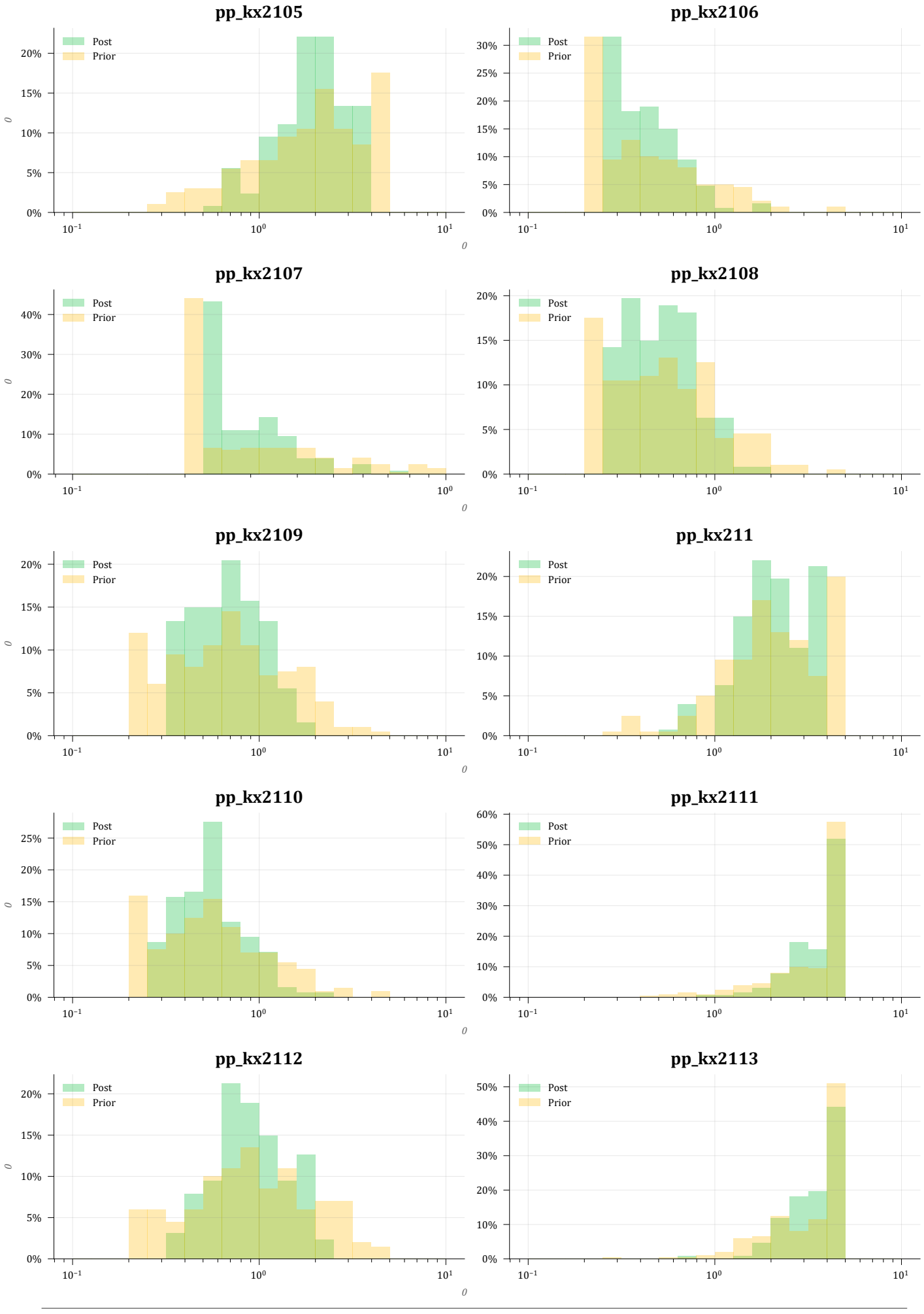

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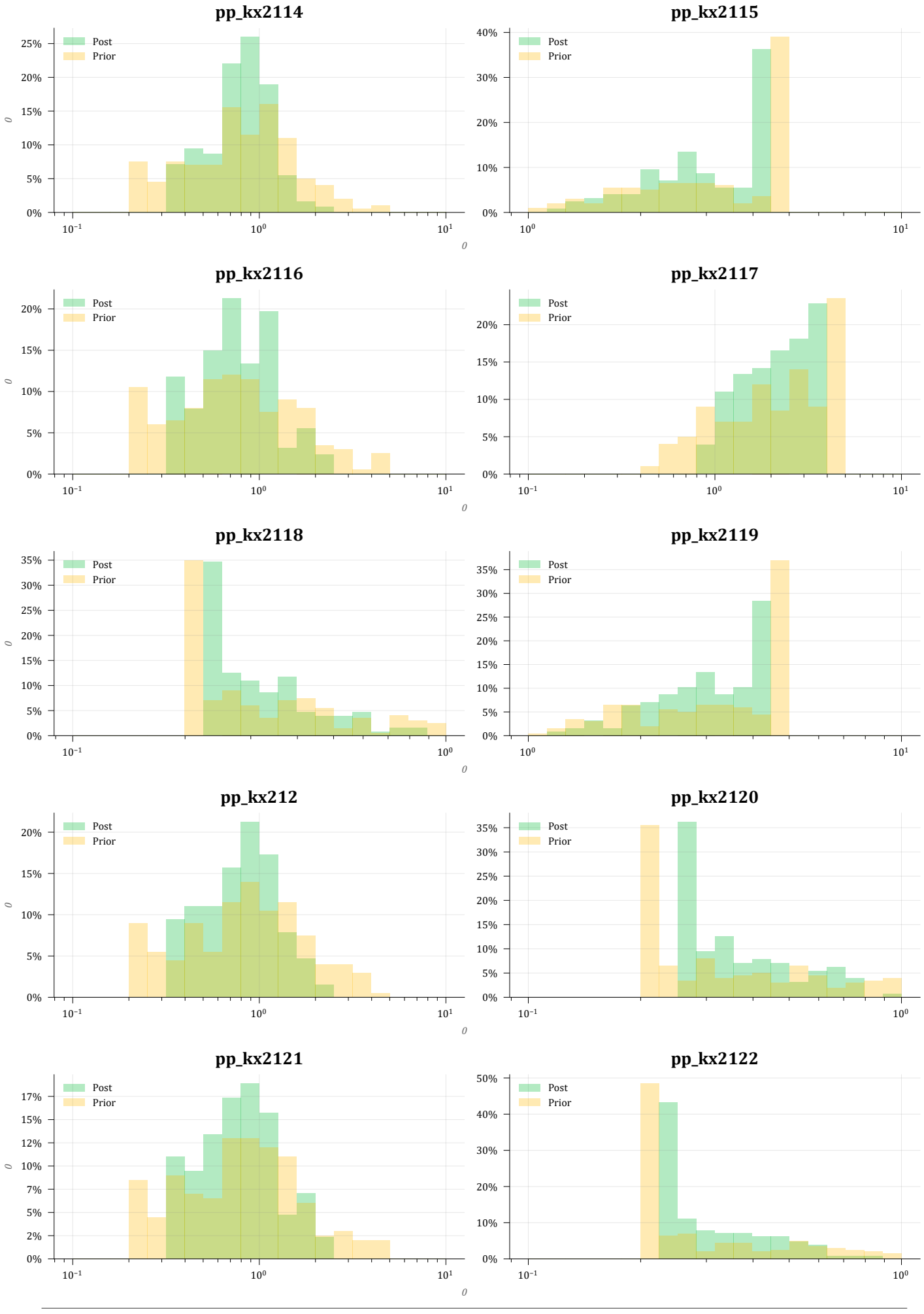

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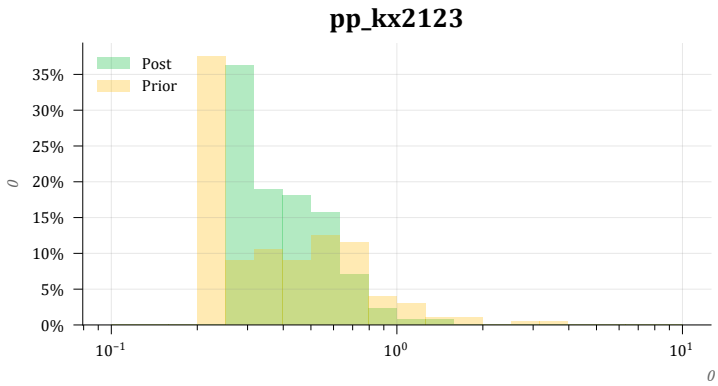

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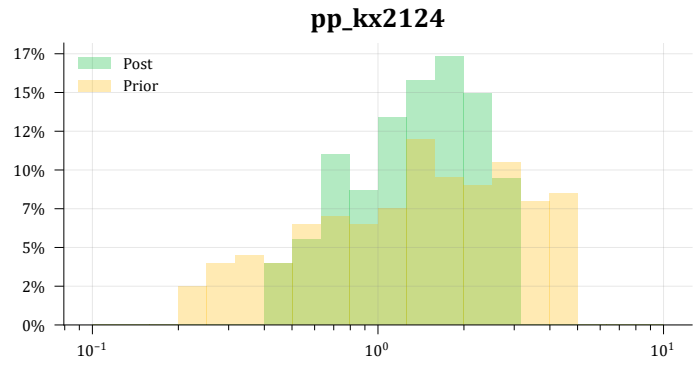

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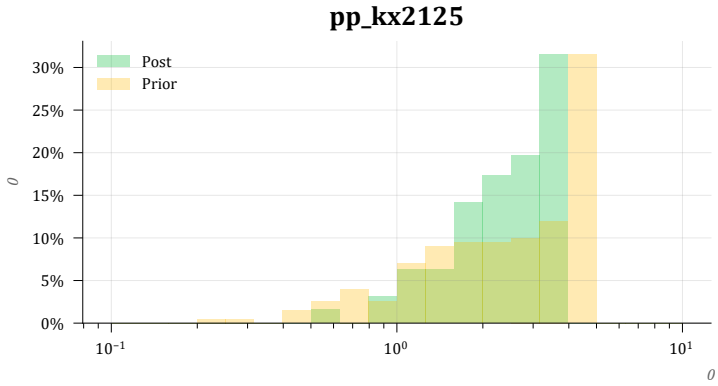

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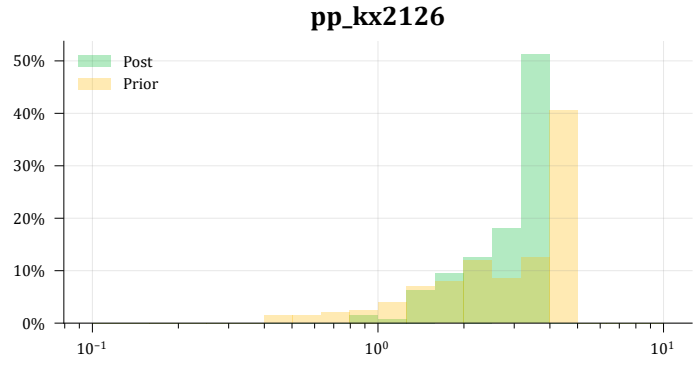

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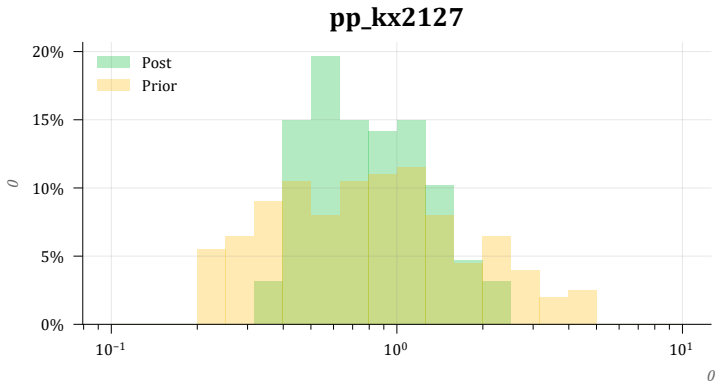

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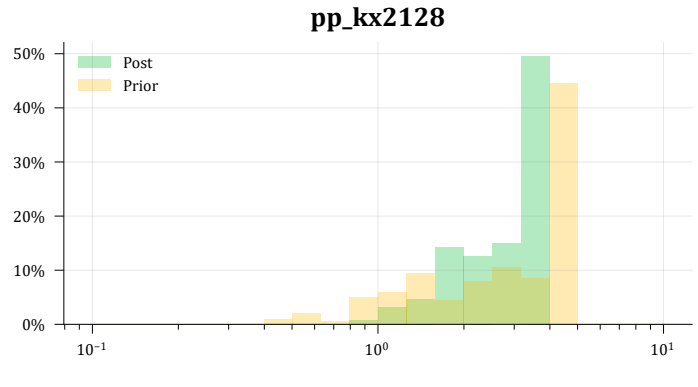

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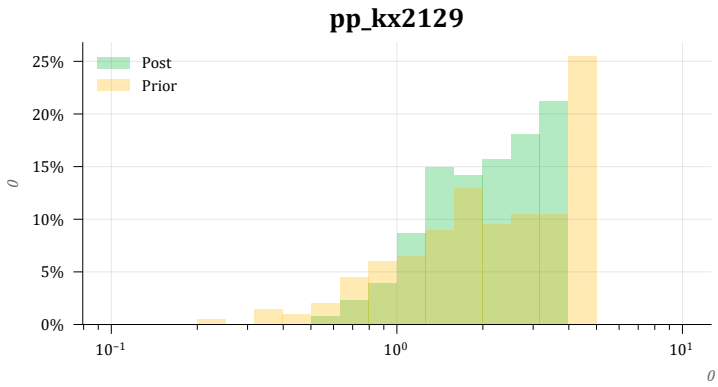

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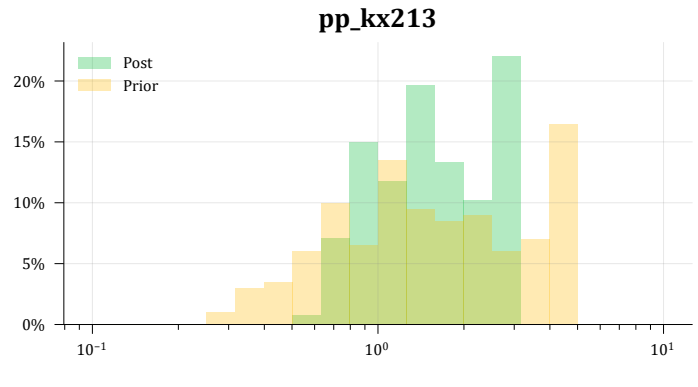

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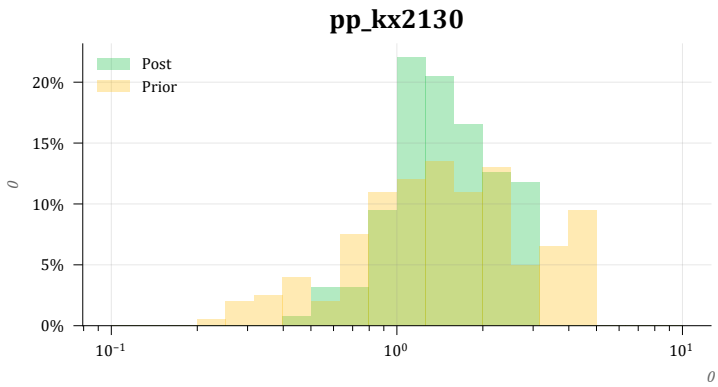

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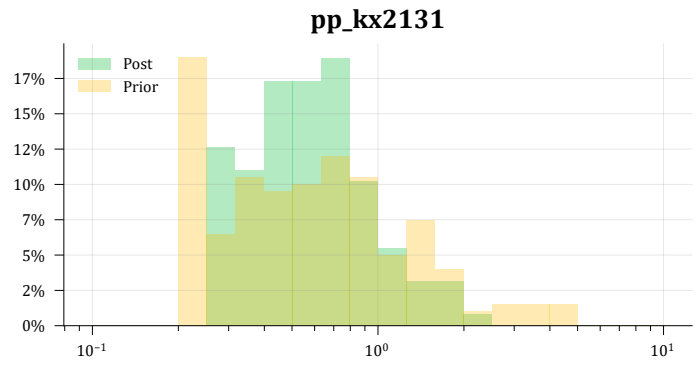

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pp_kx2128
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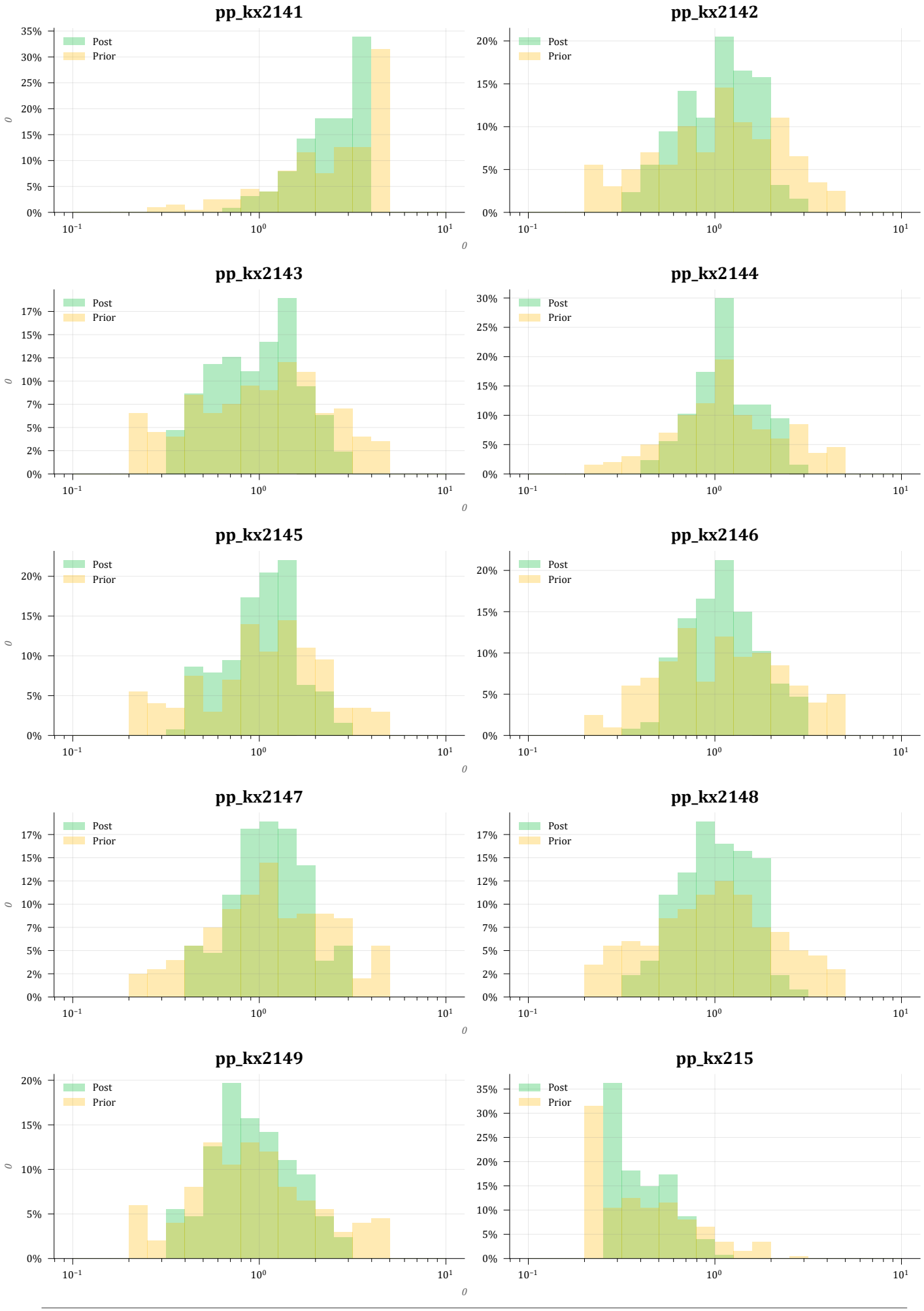

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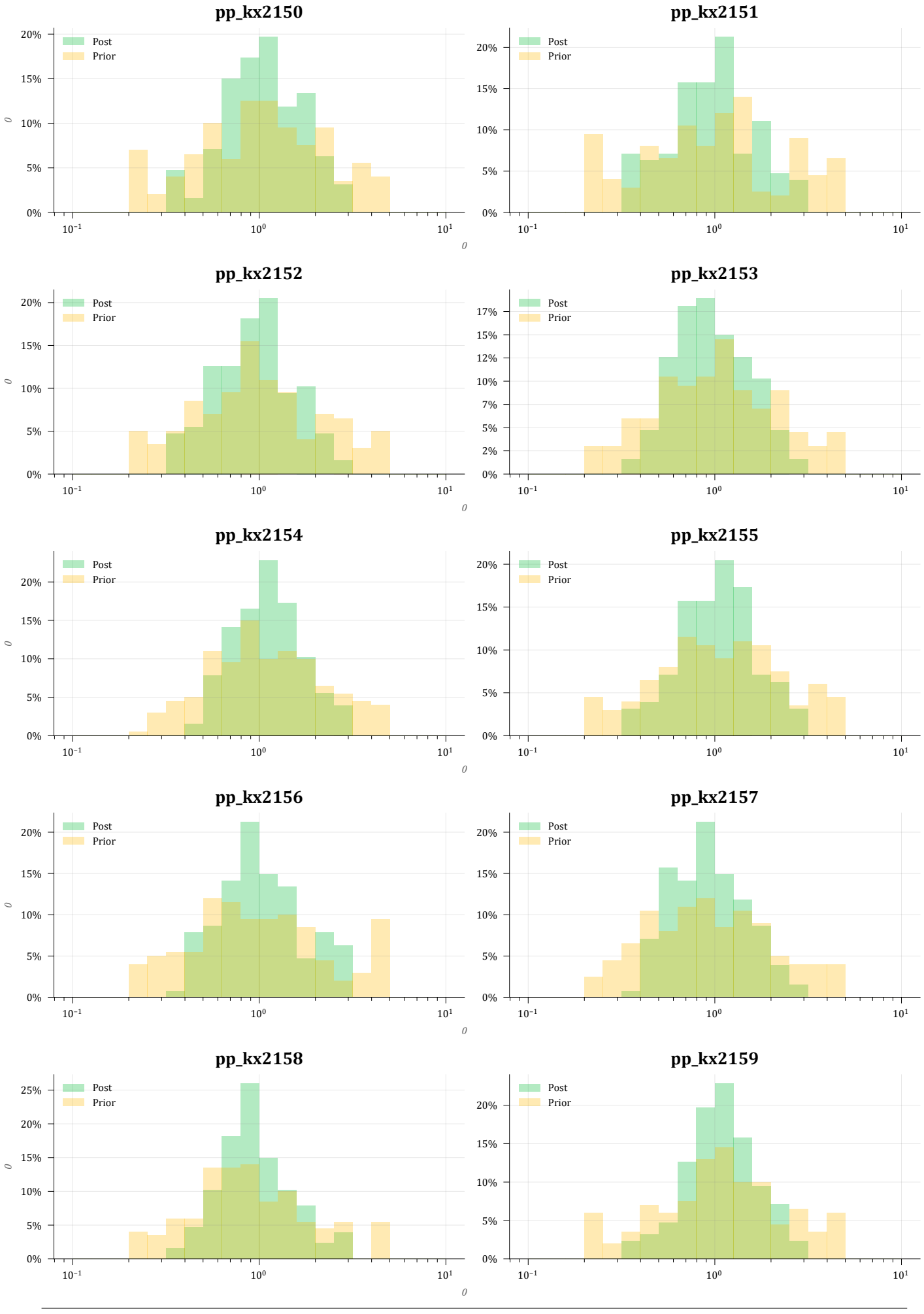

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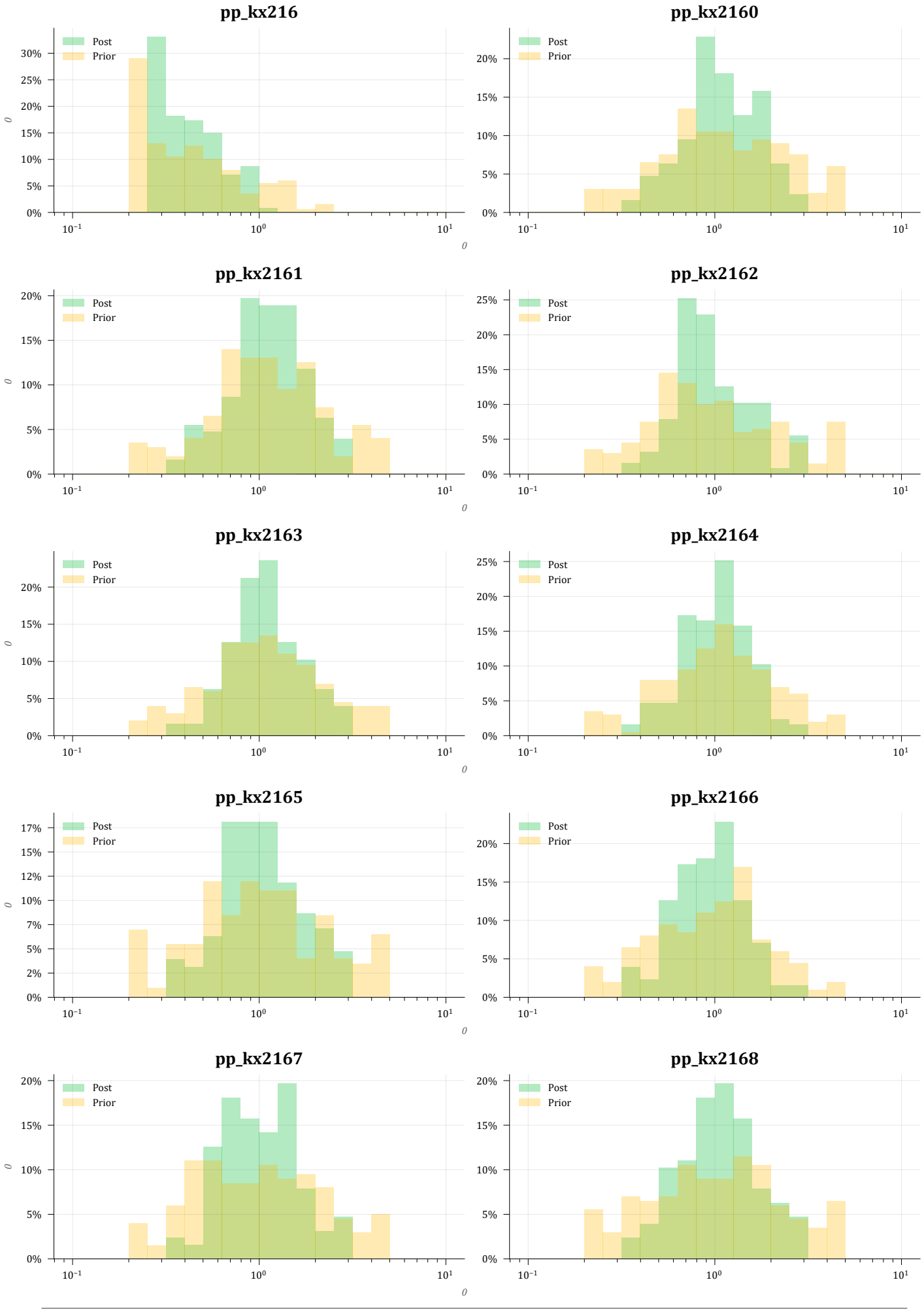

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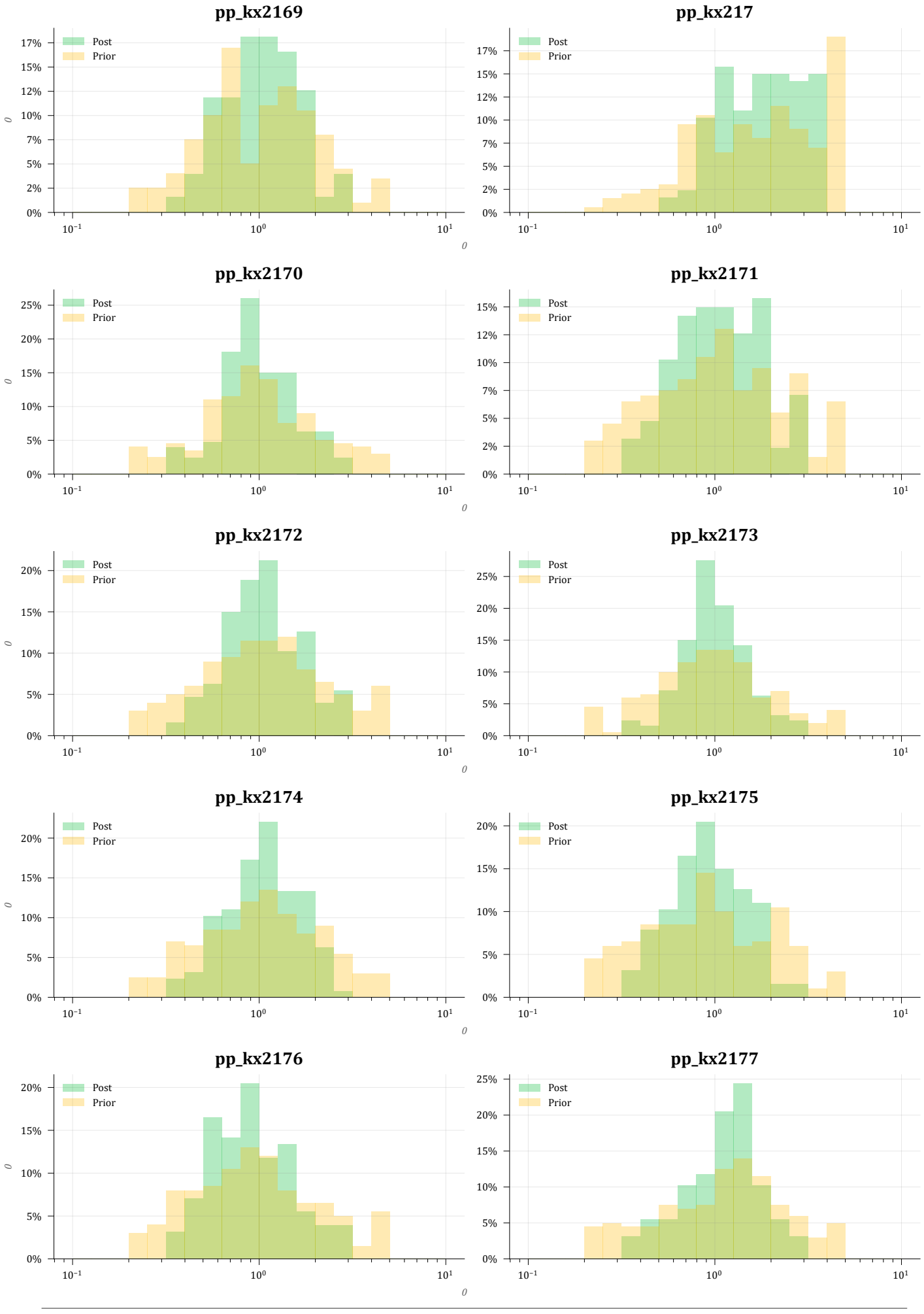

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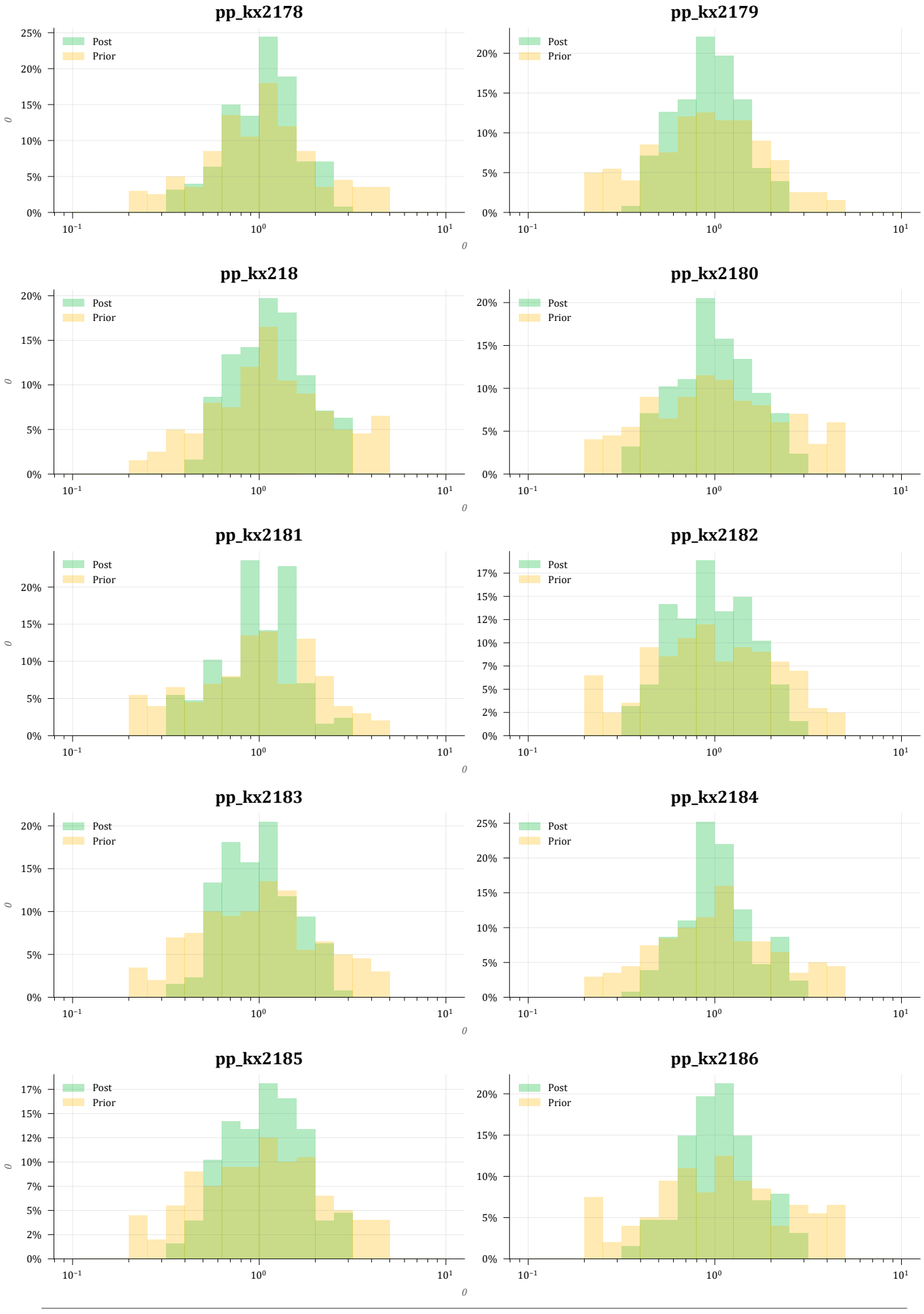

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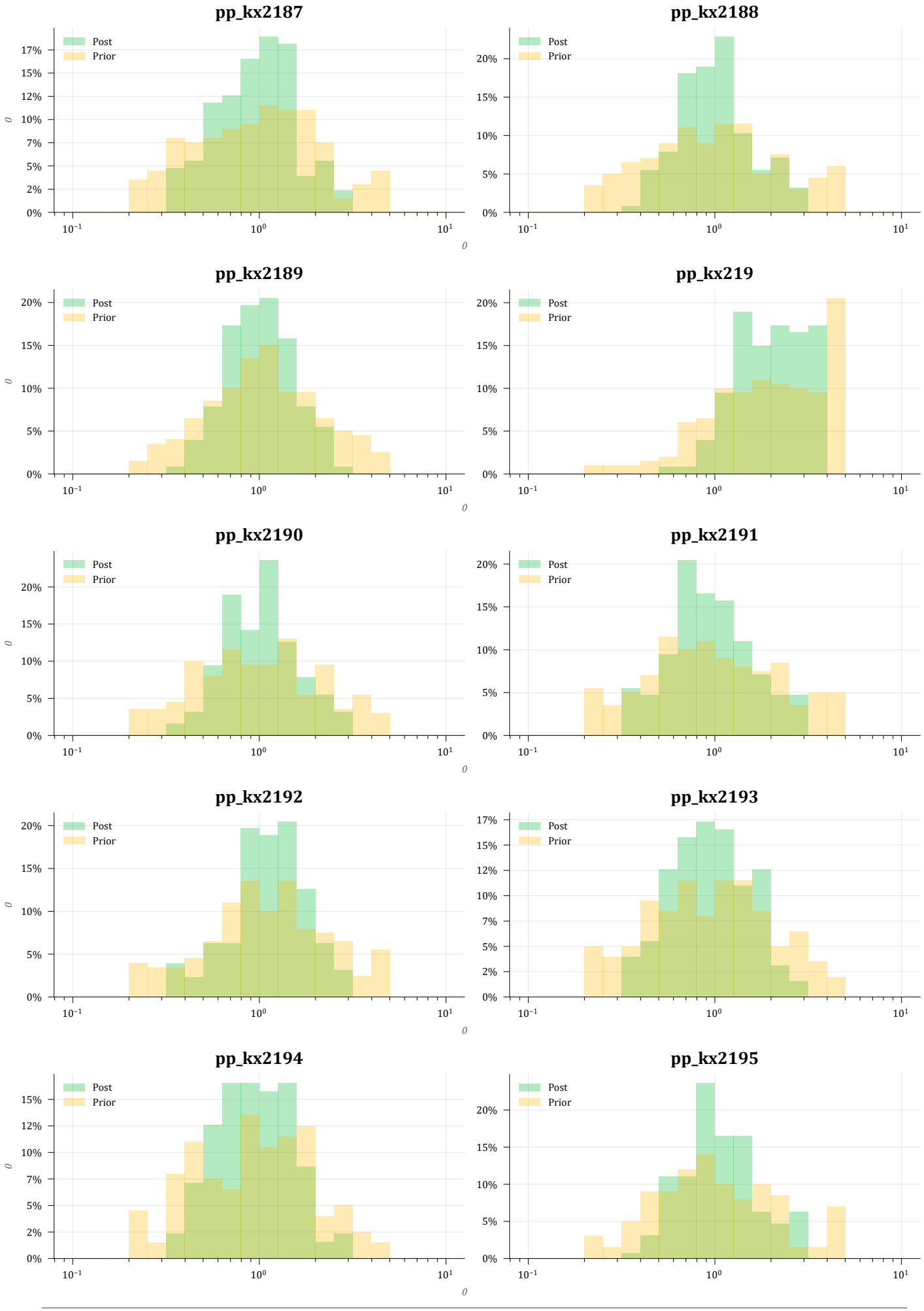

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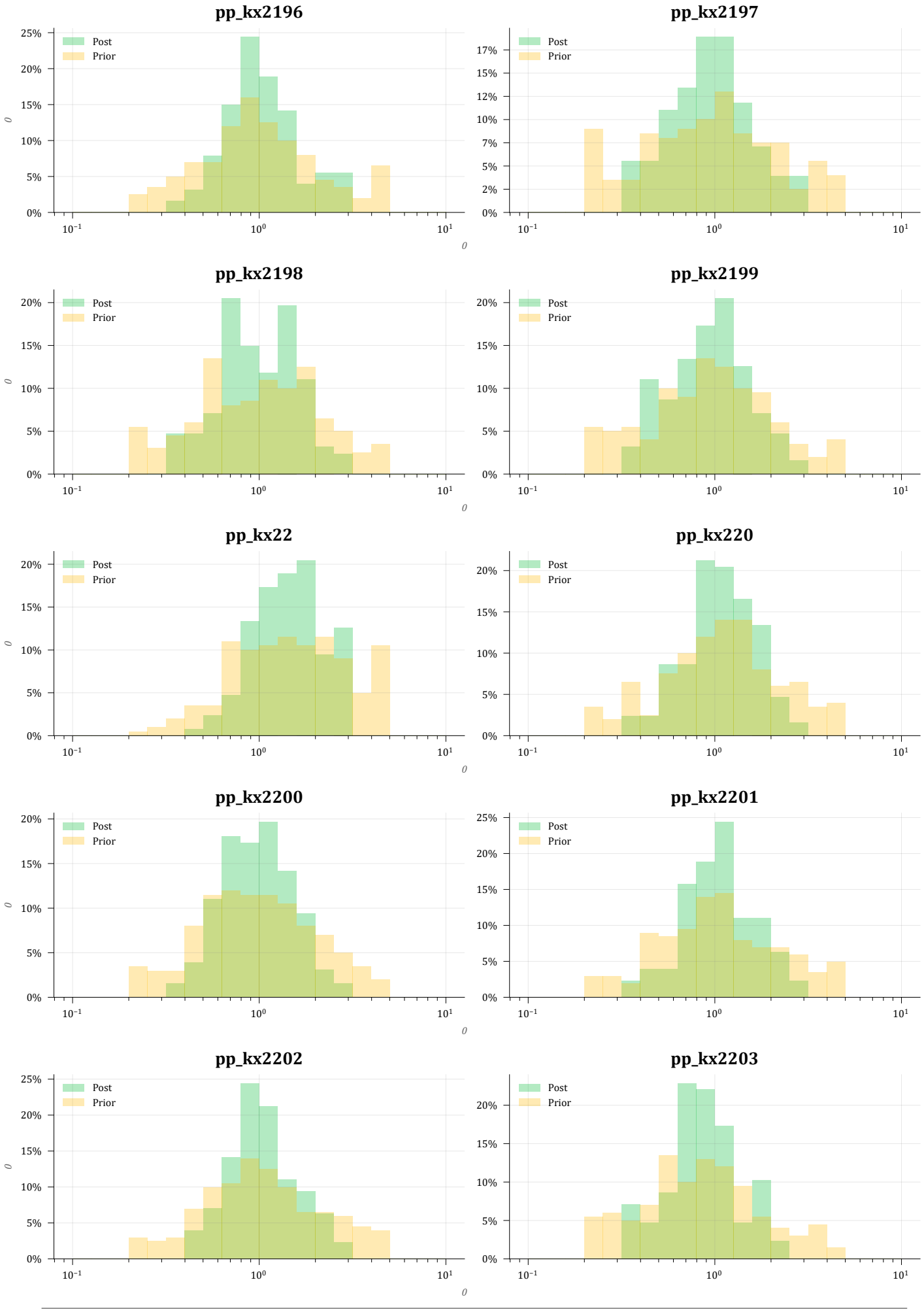

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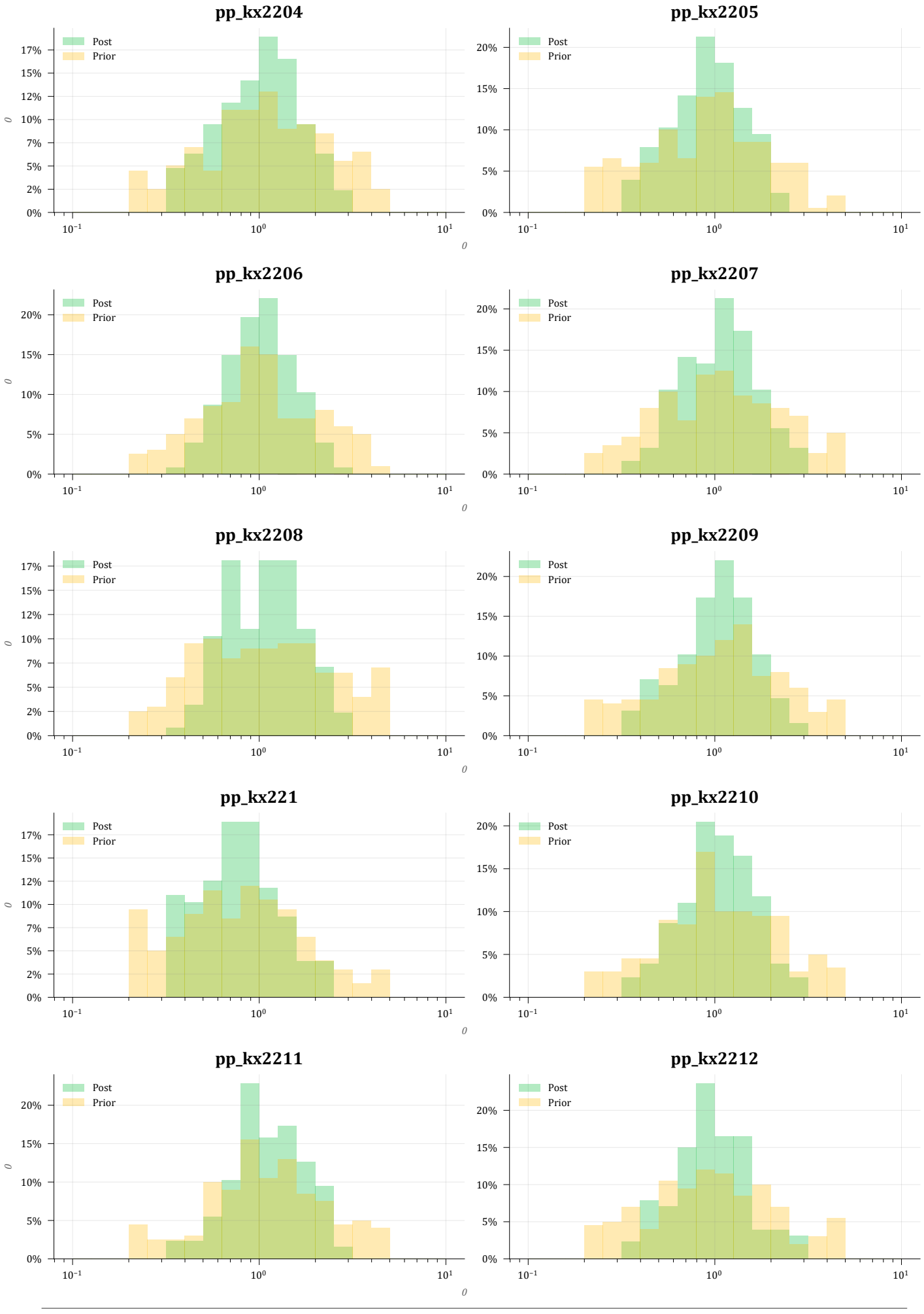

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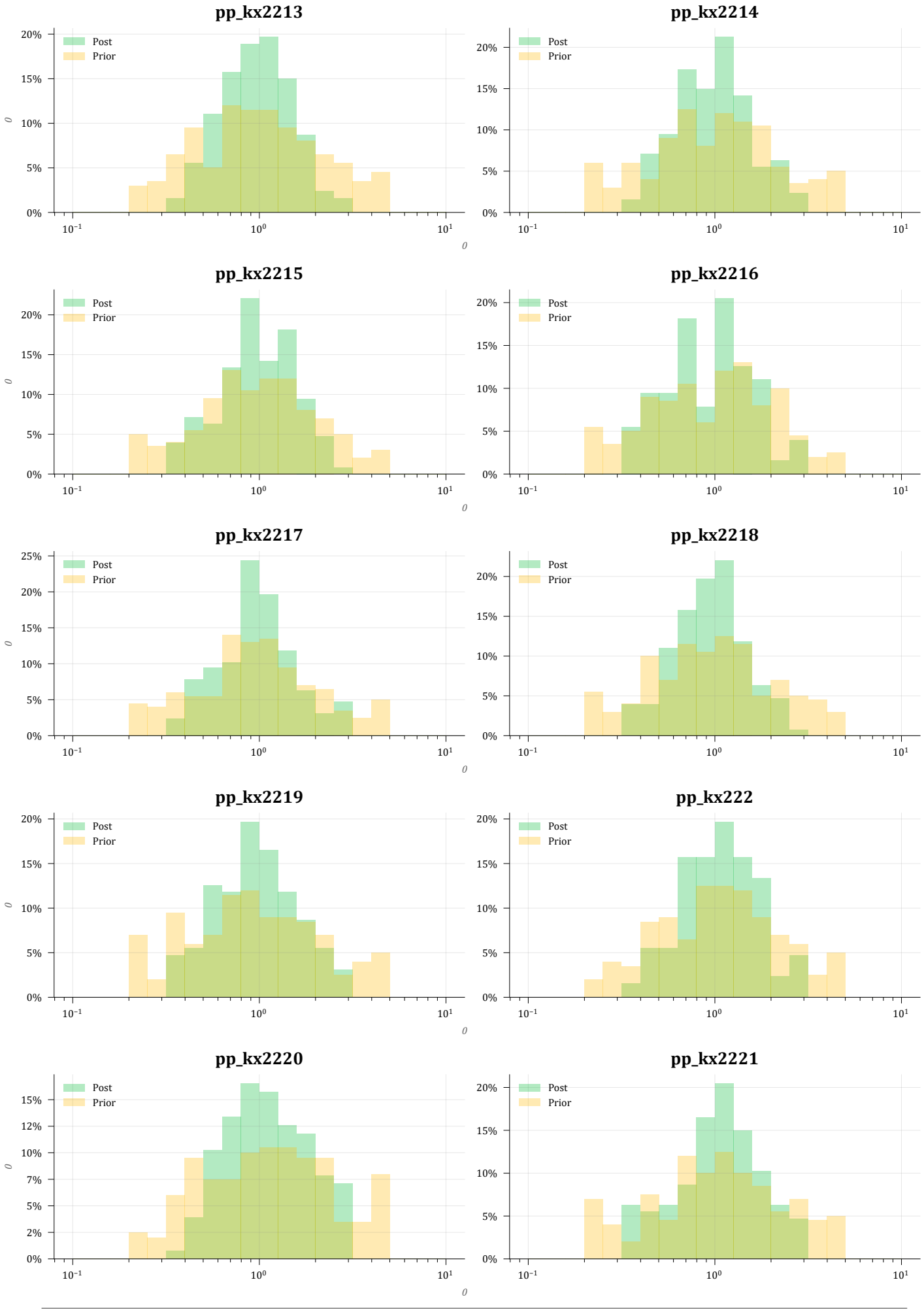

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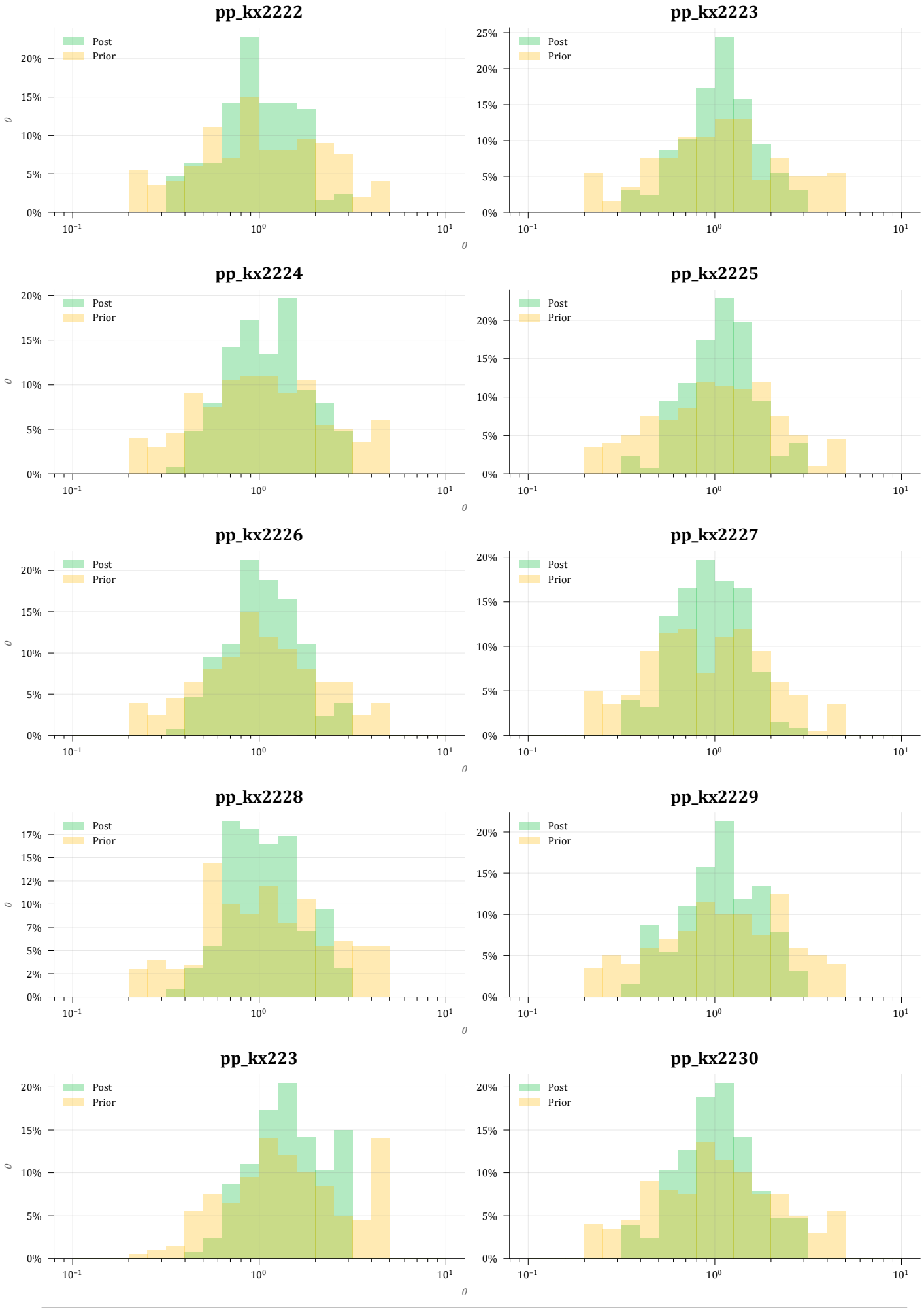

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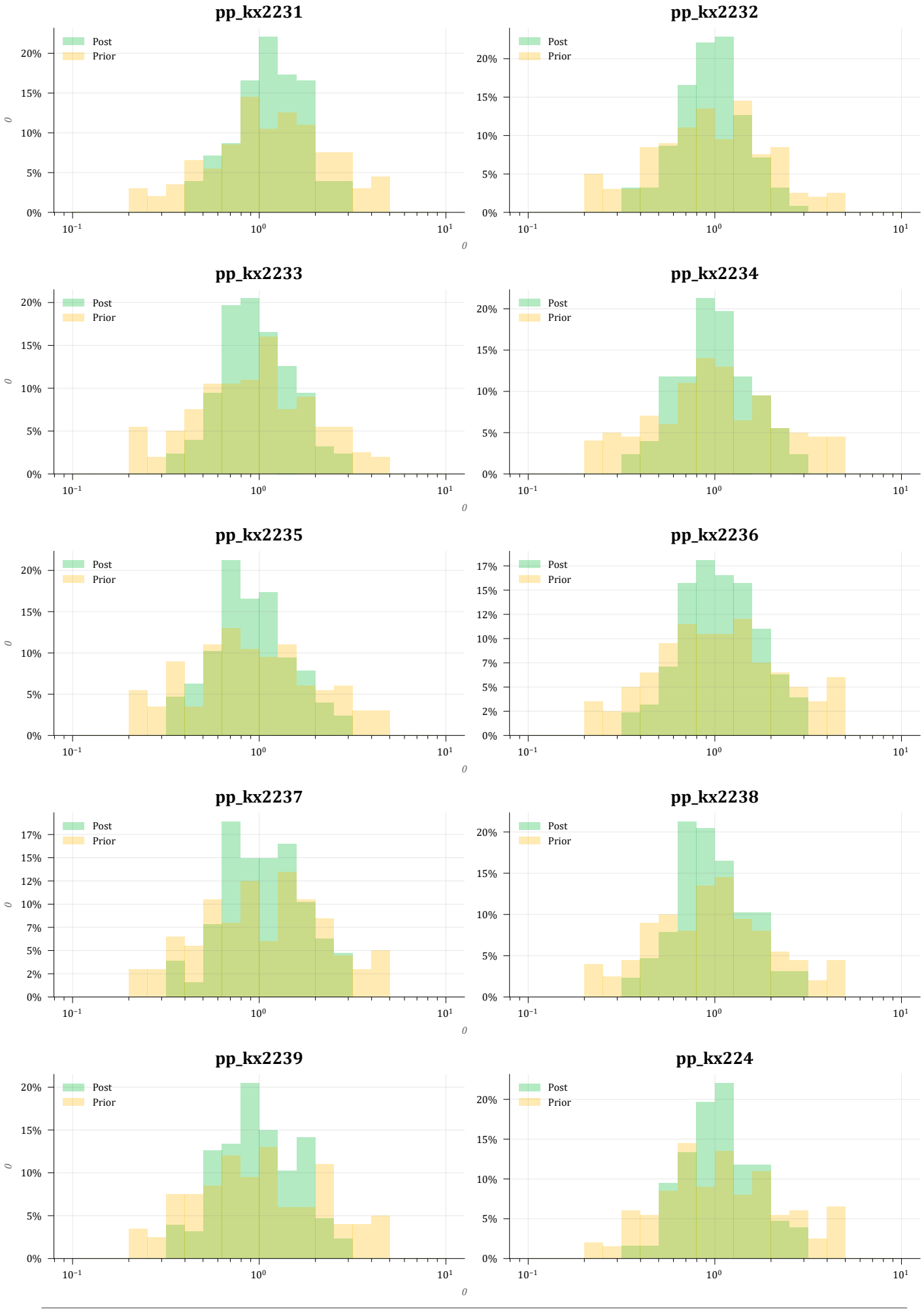

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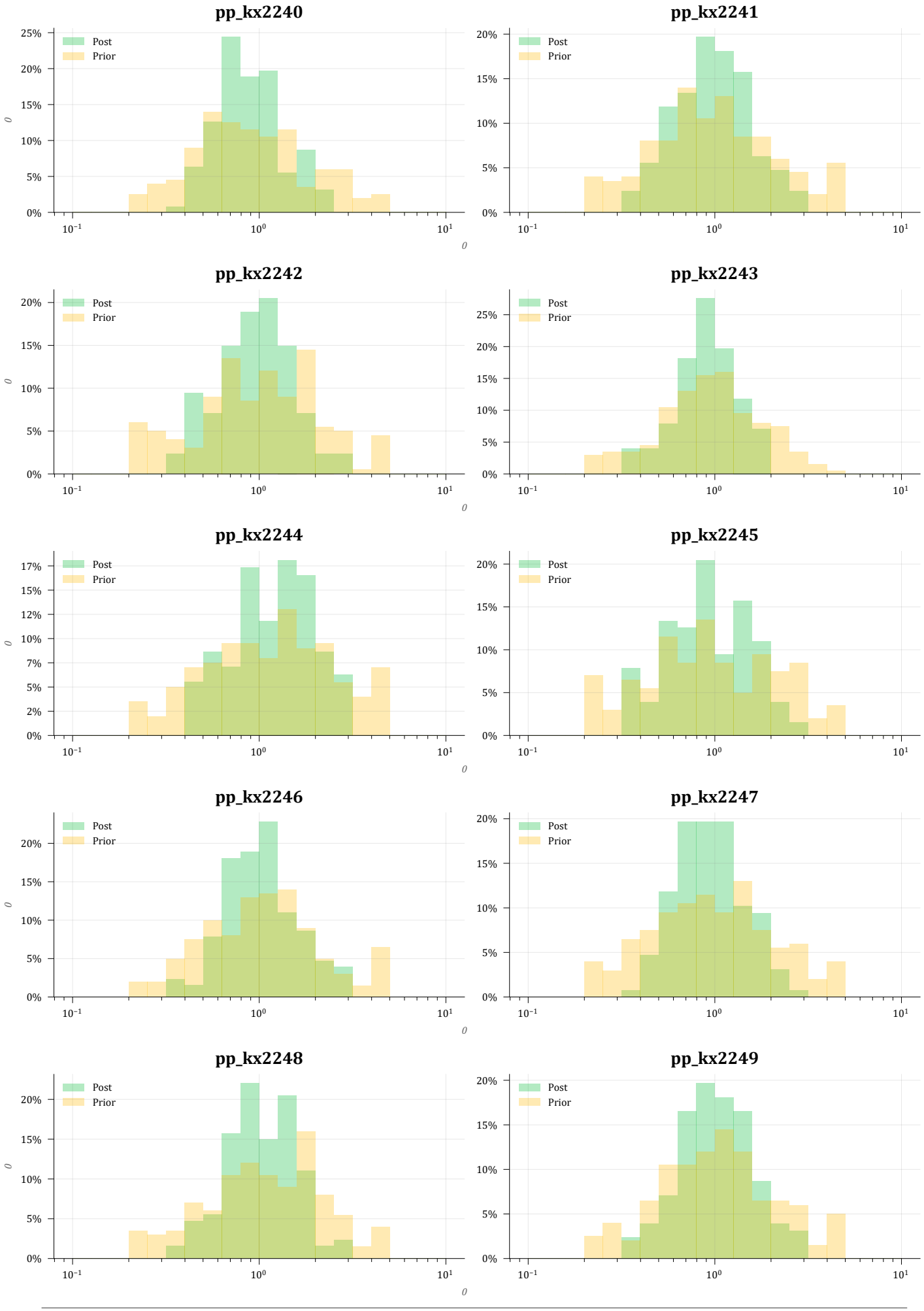

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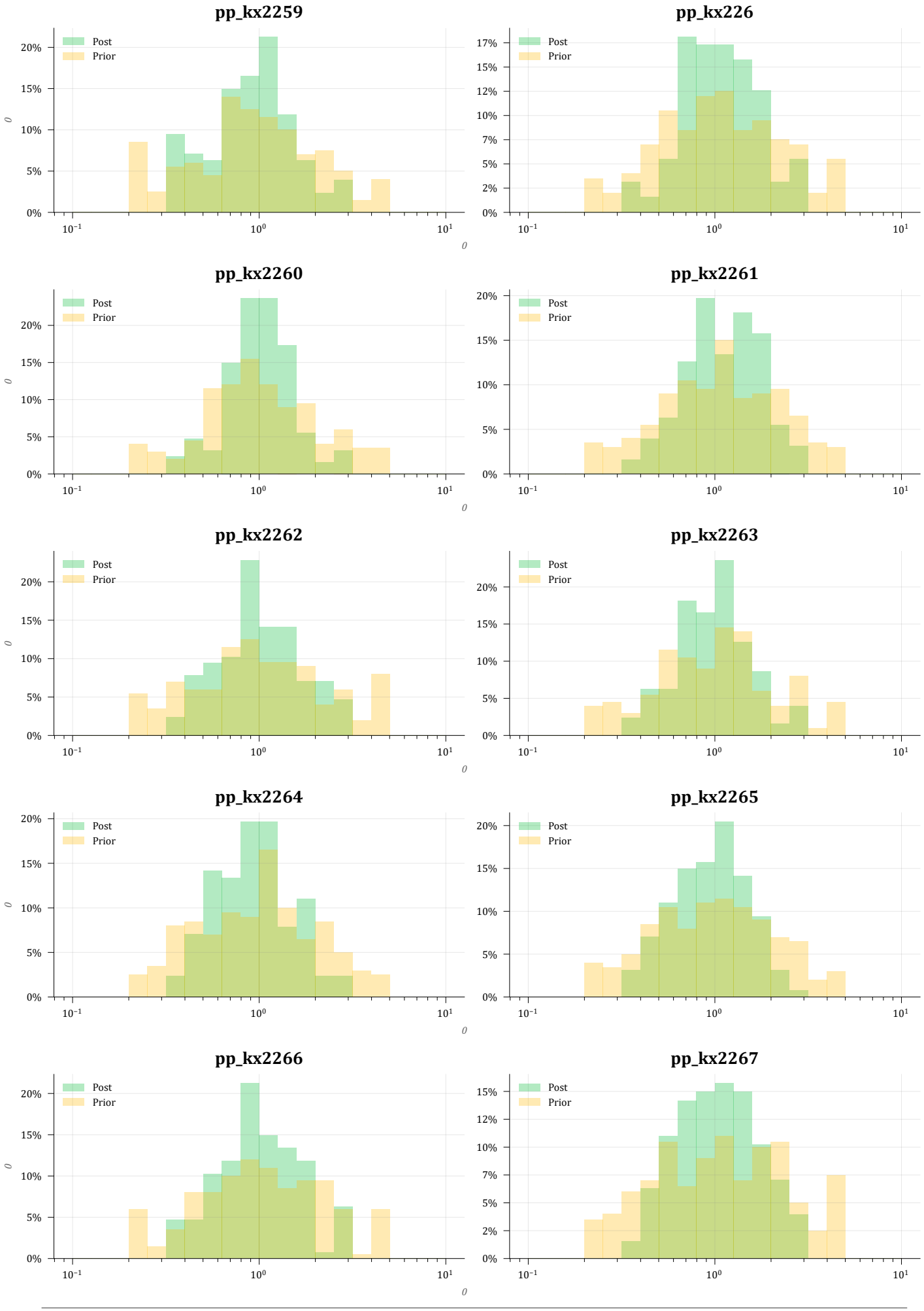

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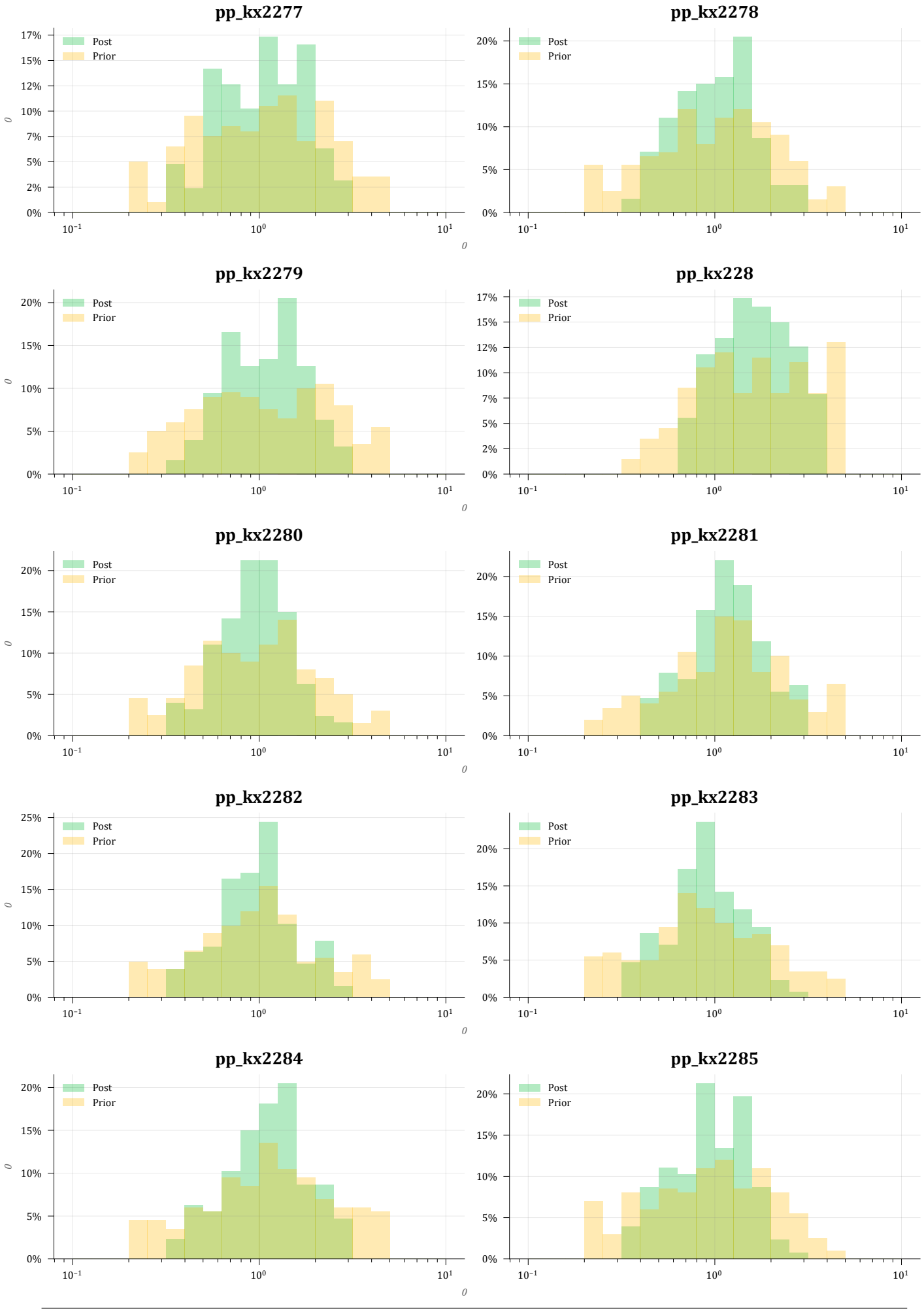

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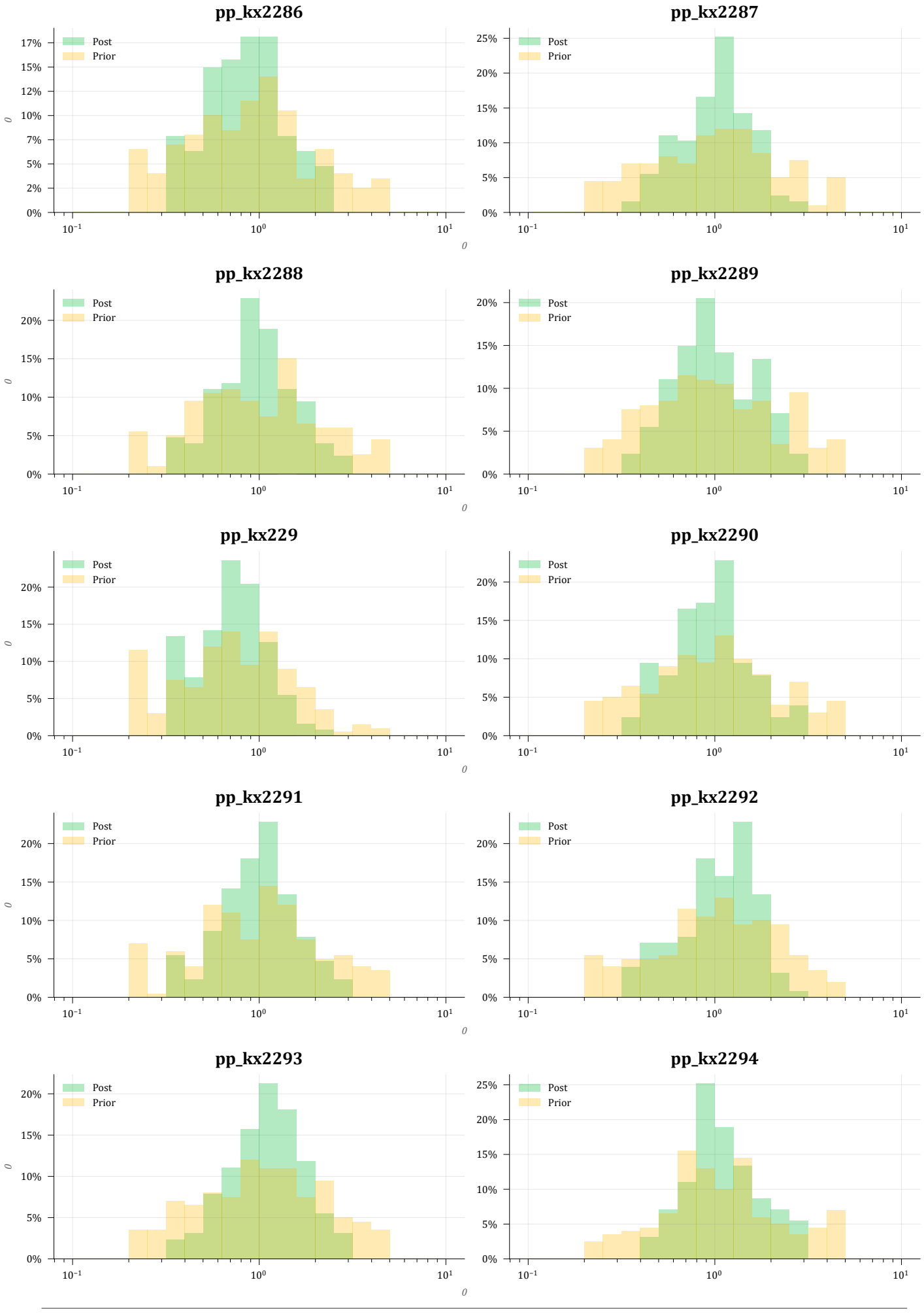

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Post
Prior
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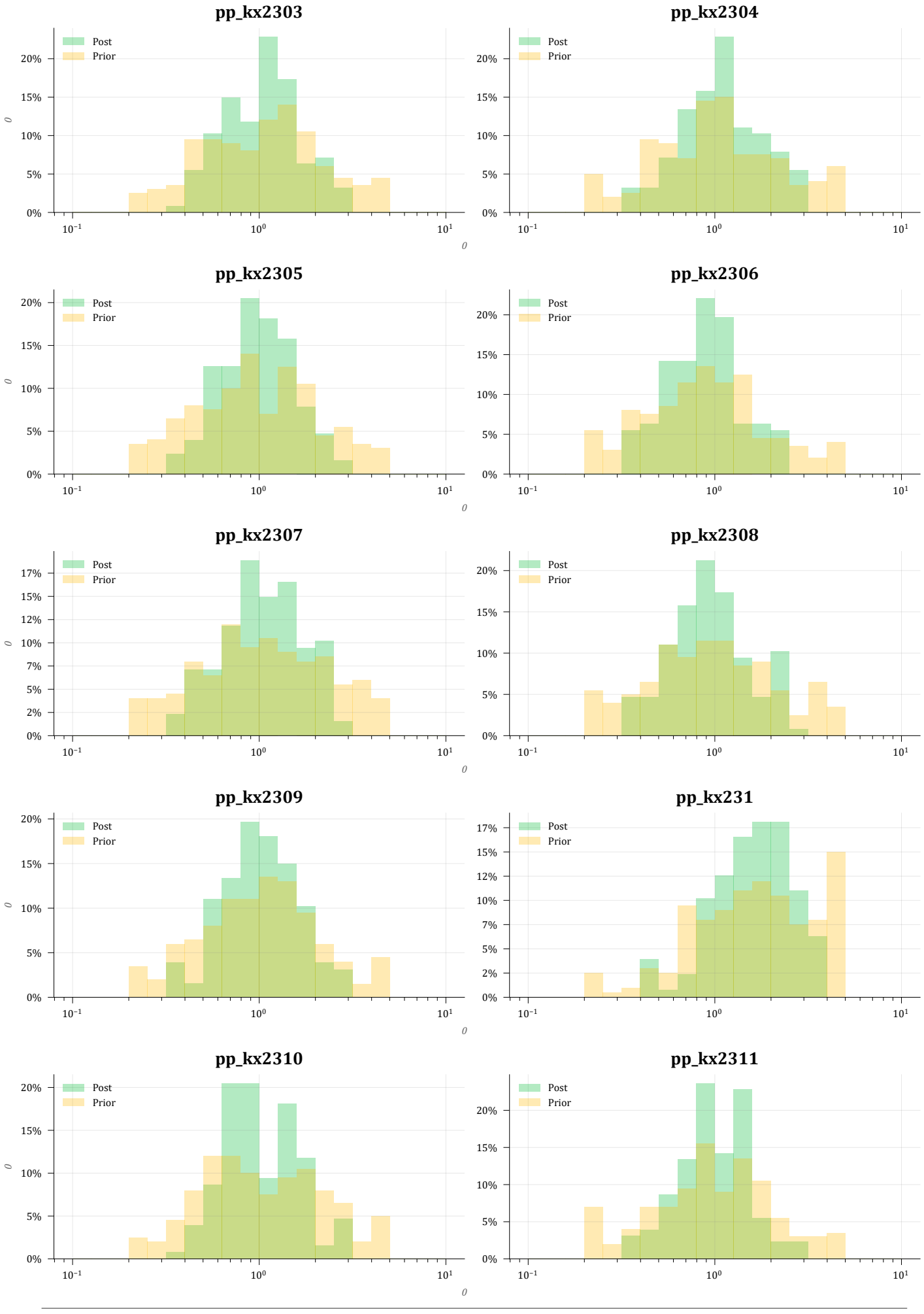

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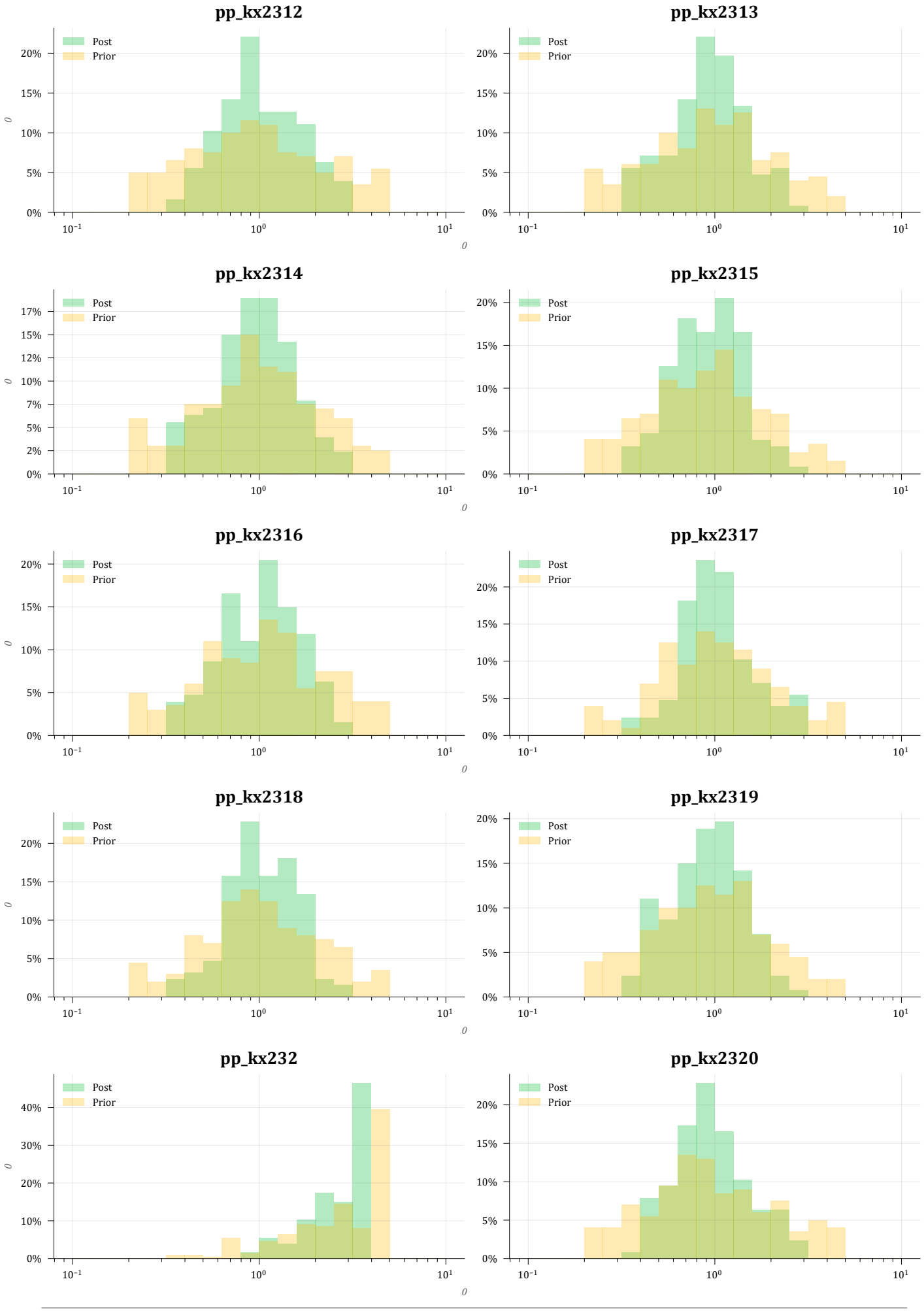

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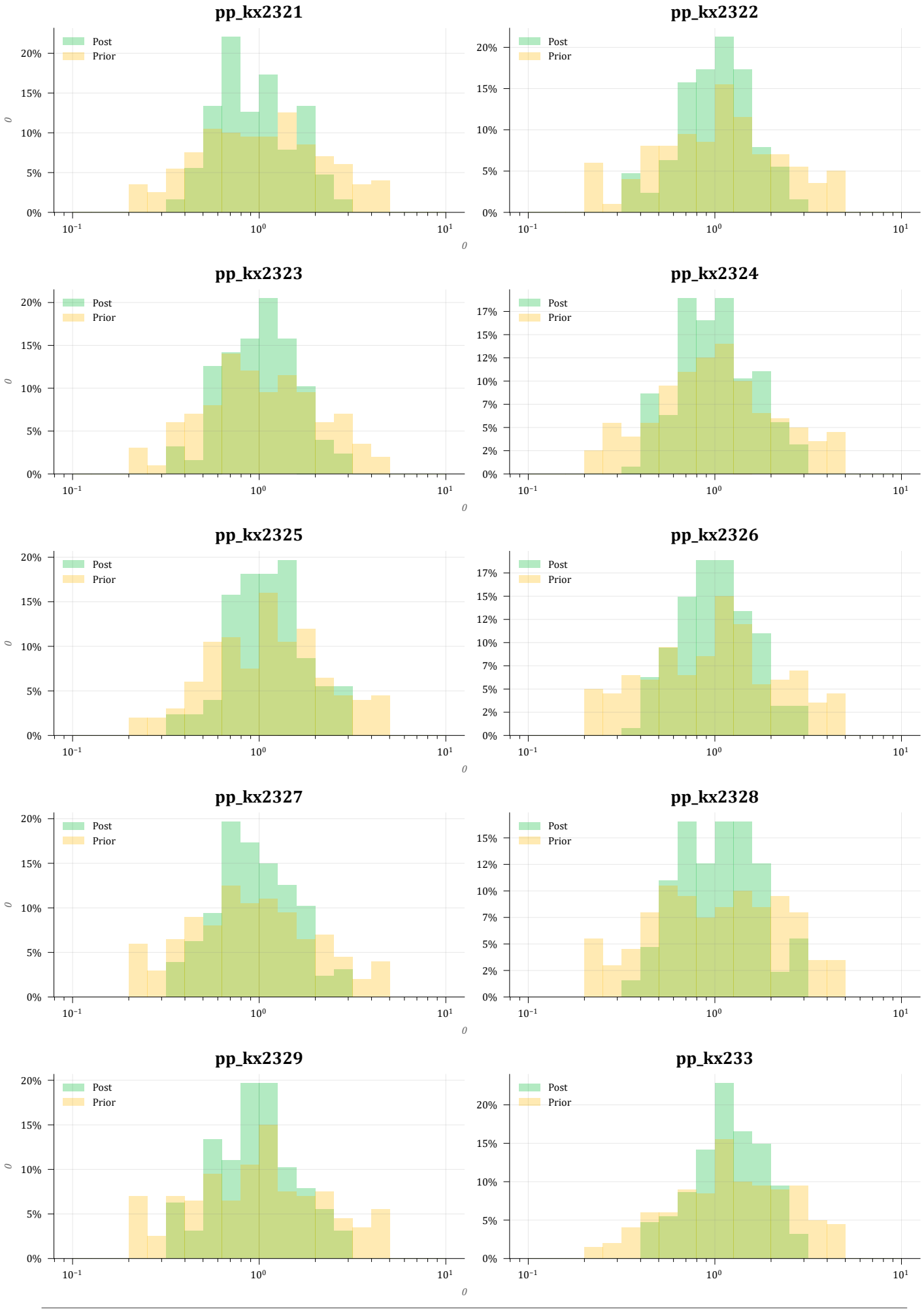

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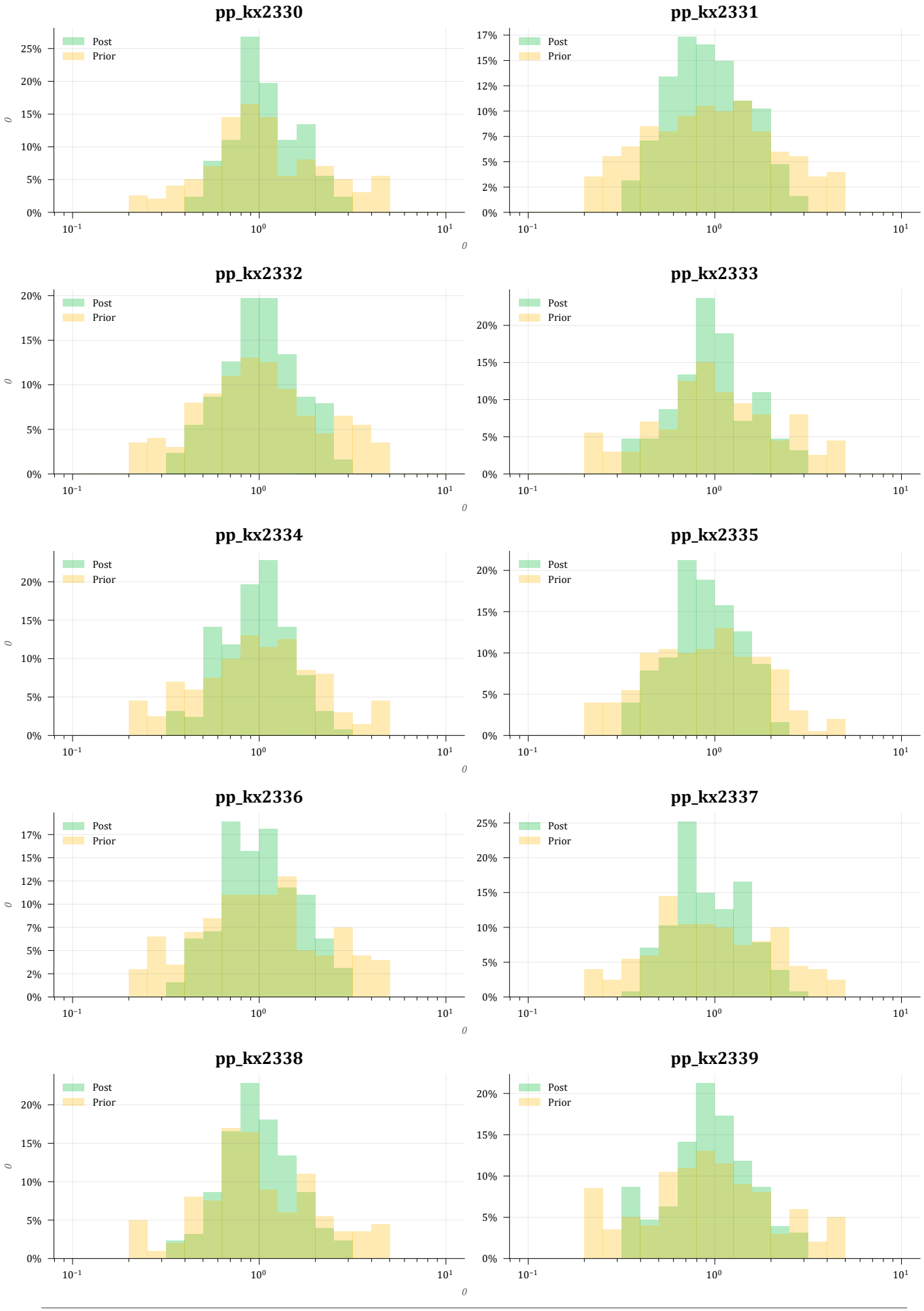

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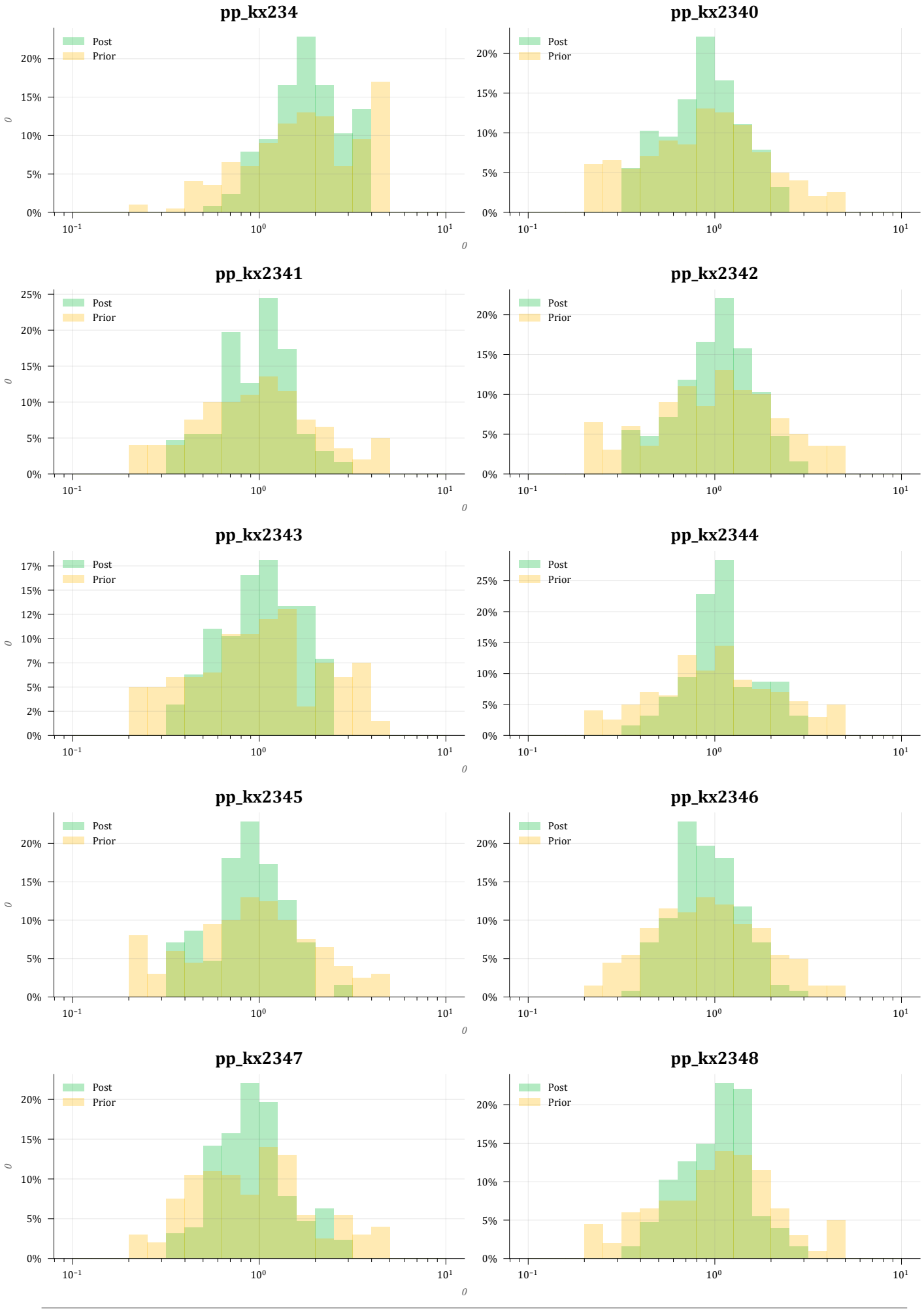

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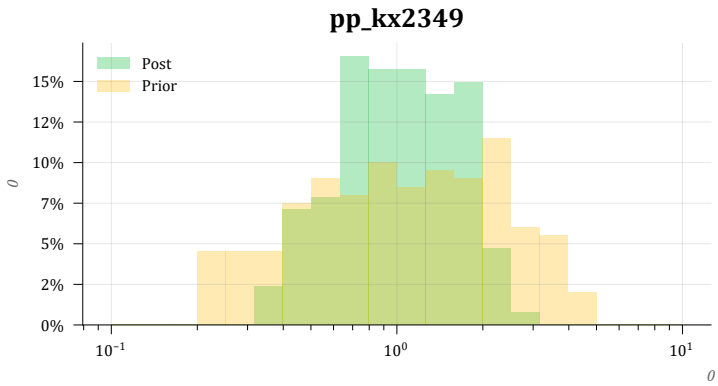

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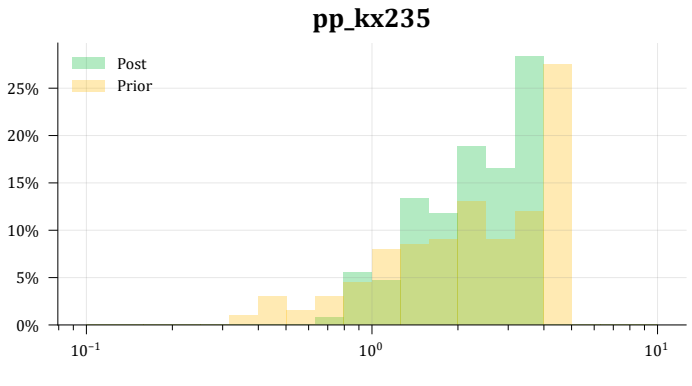

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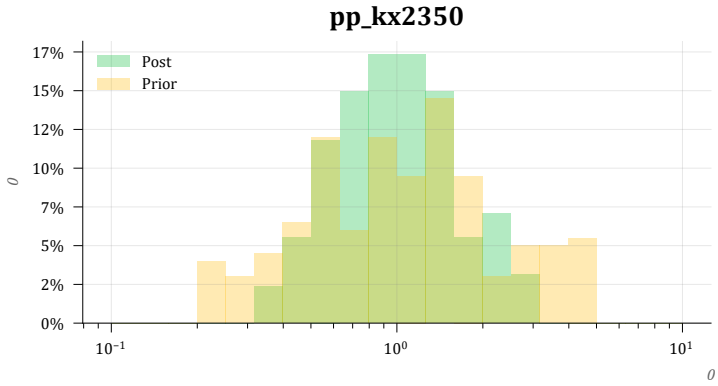

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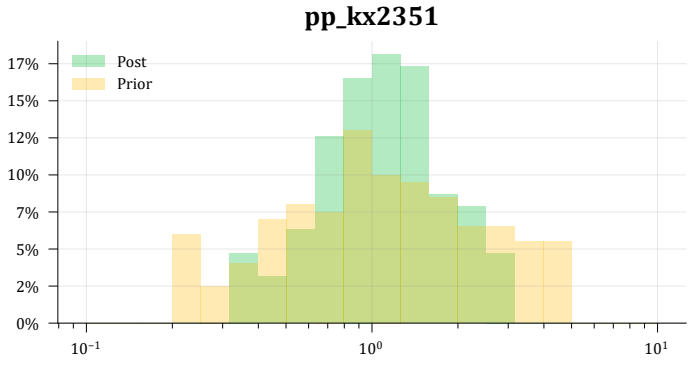

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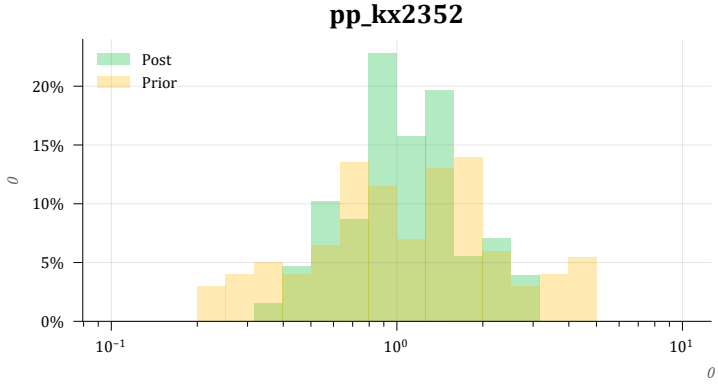

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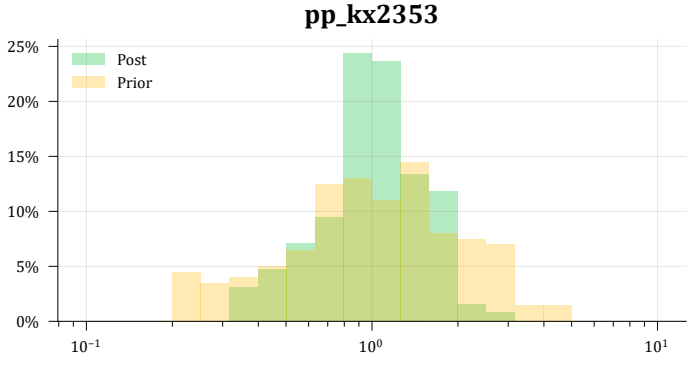

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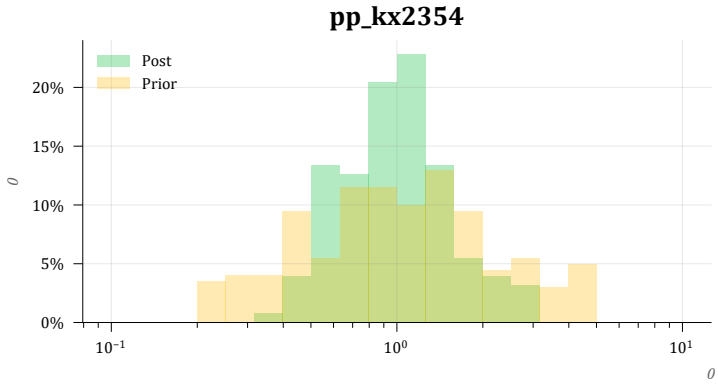

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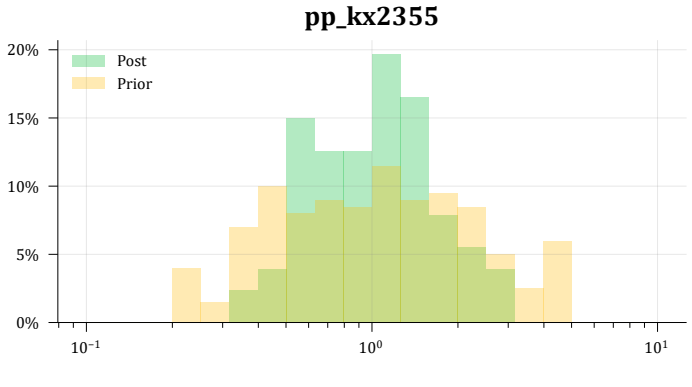

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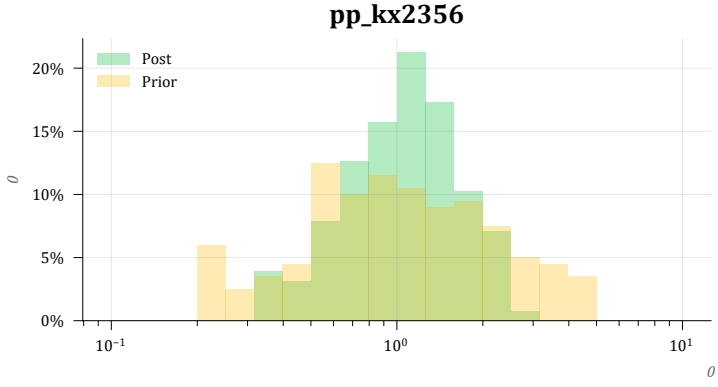

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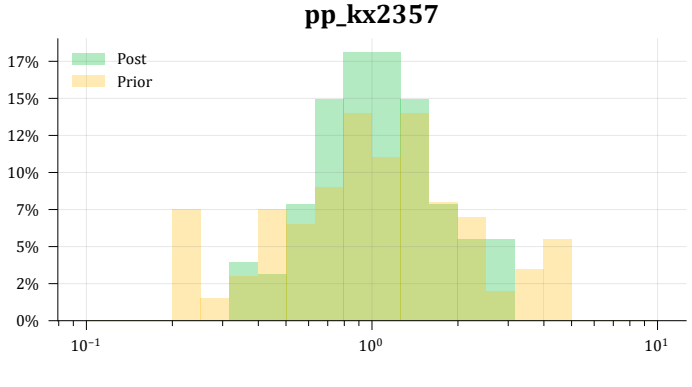

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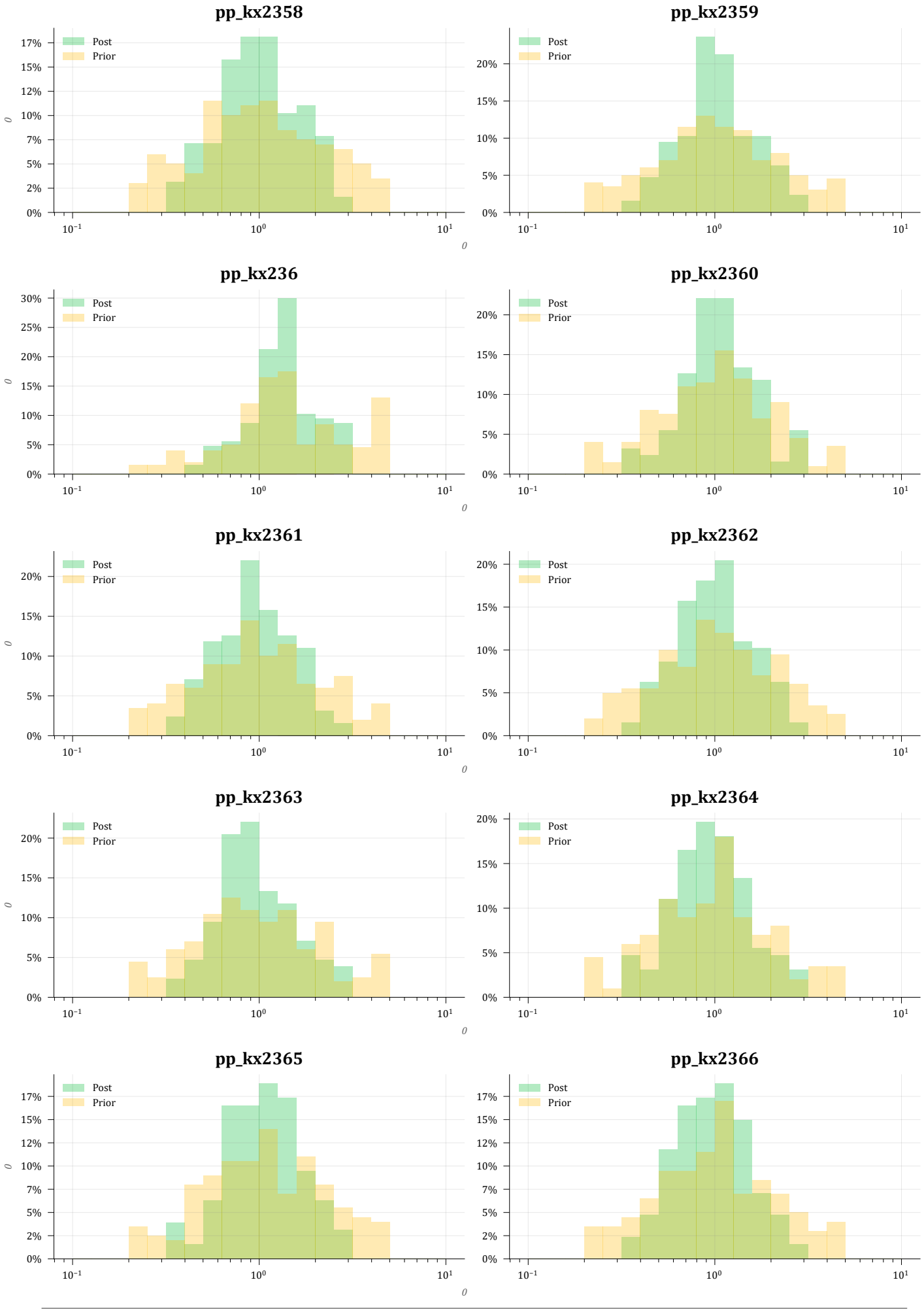

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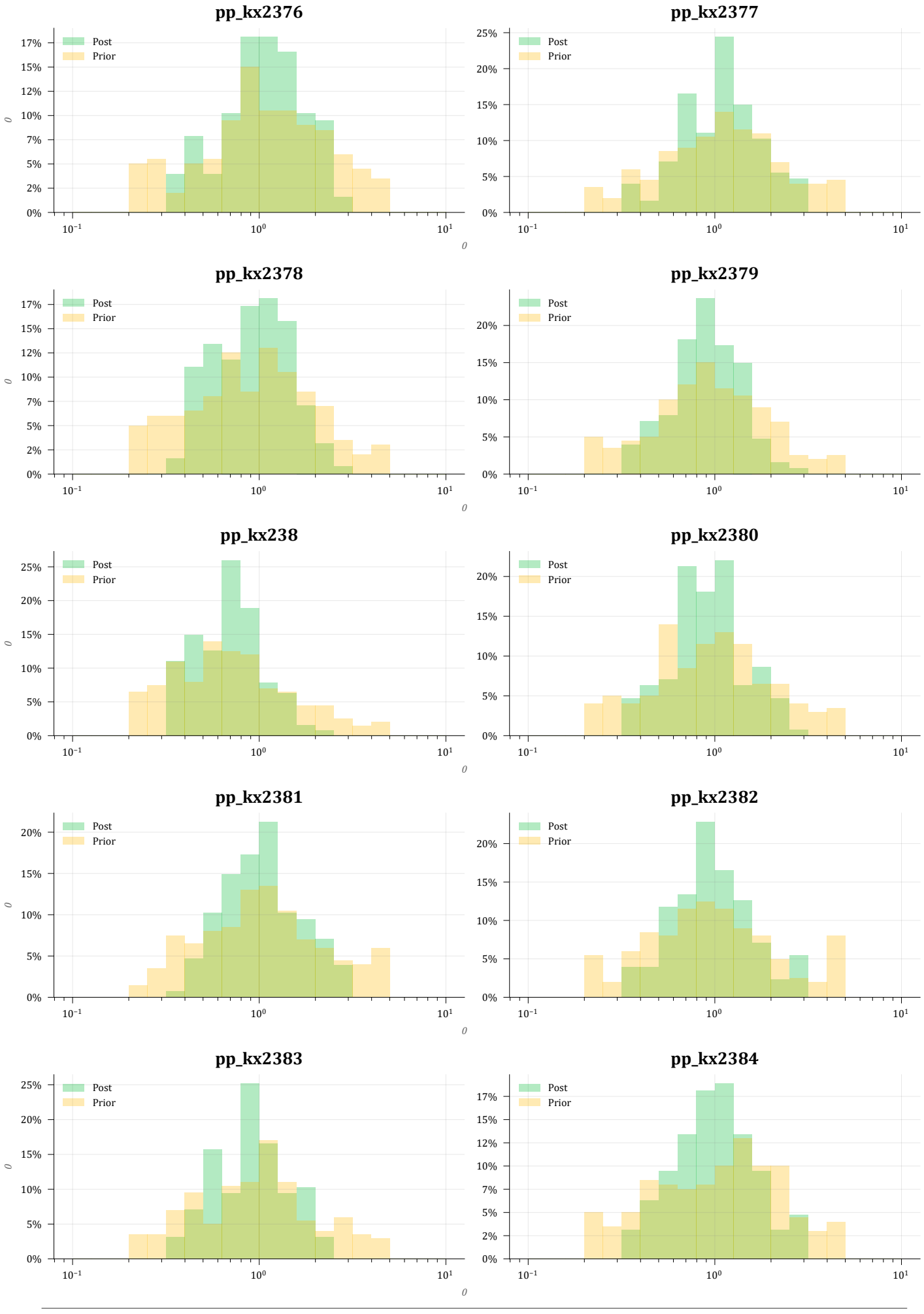

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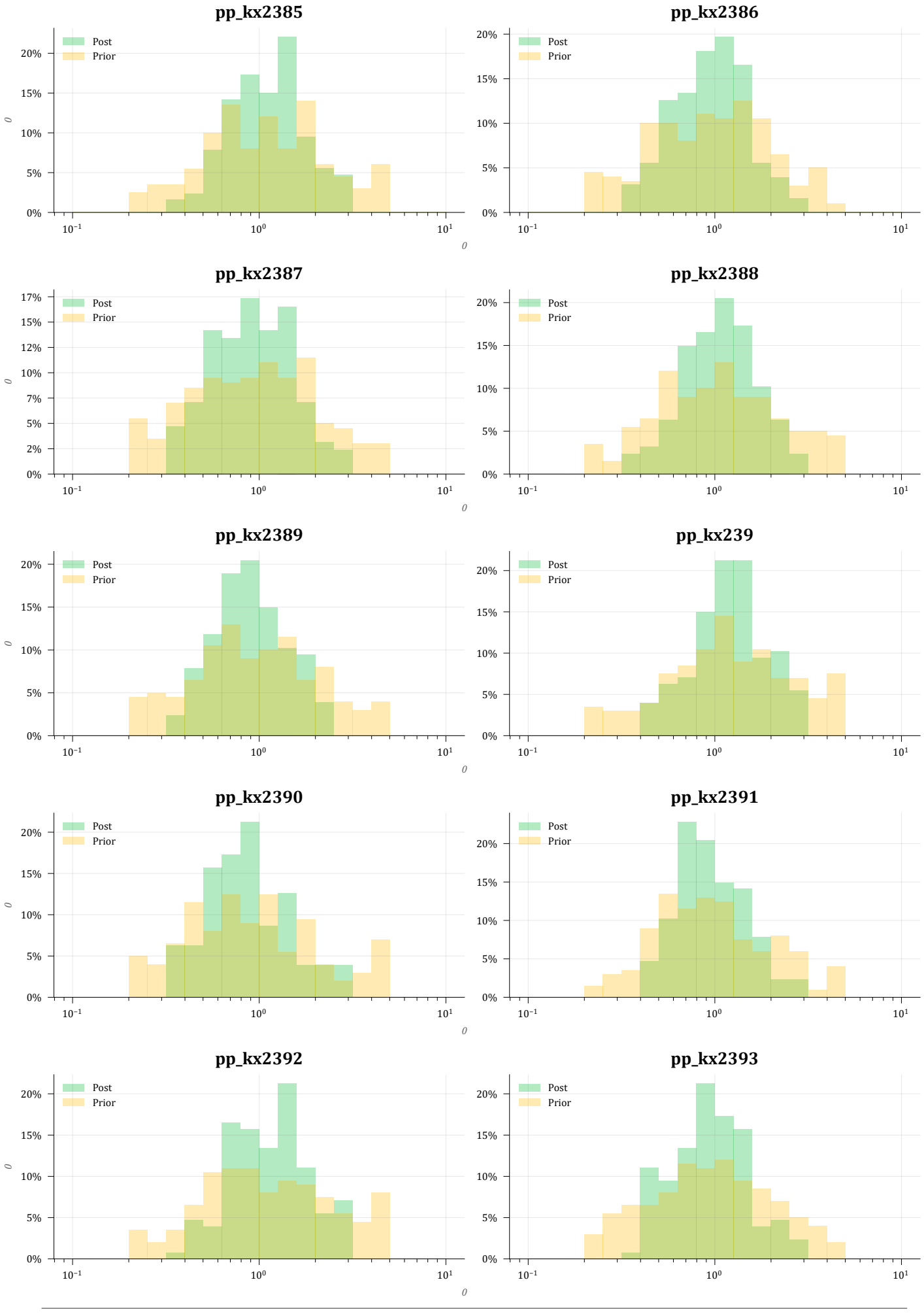

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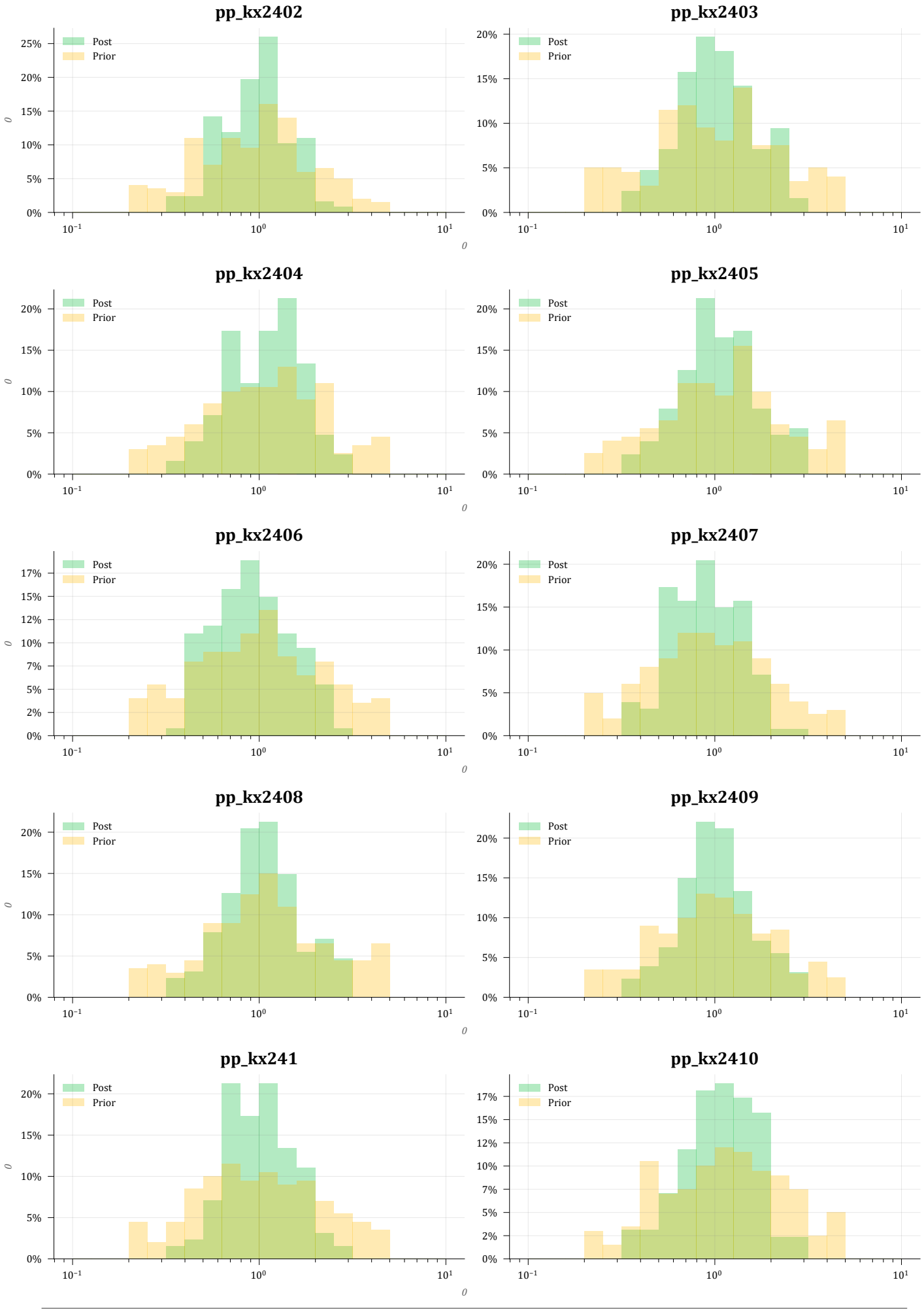

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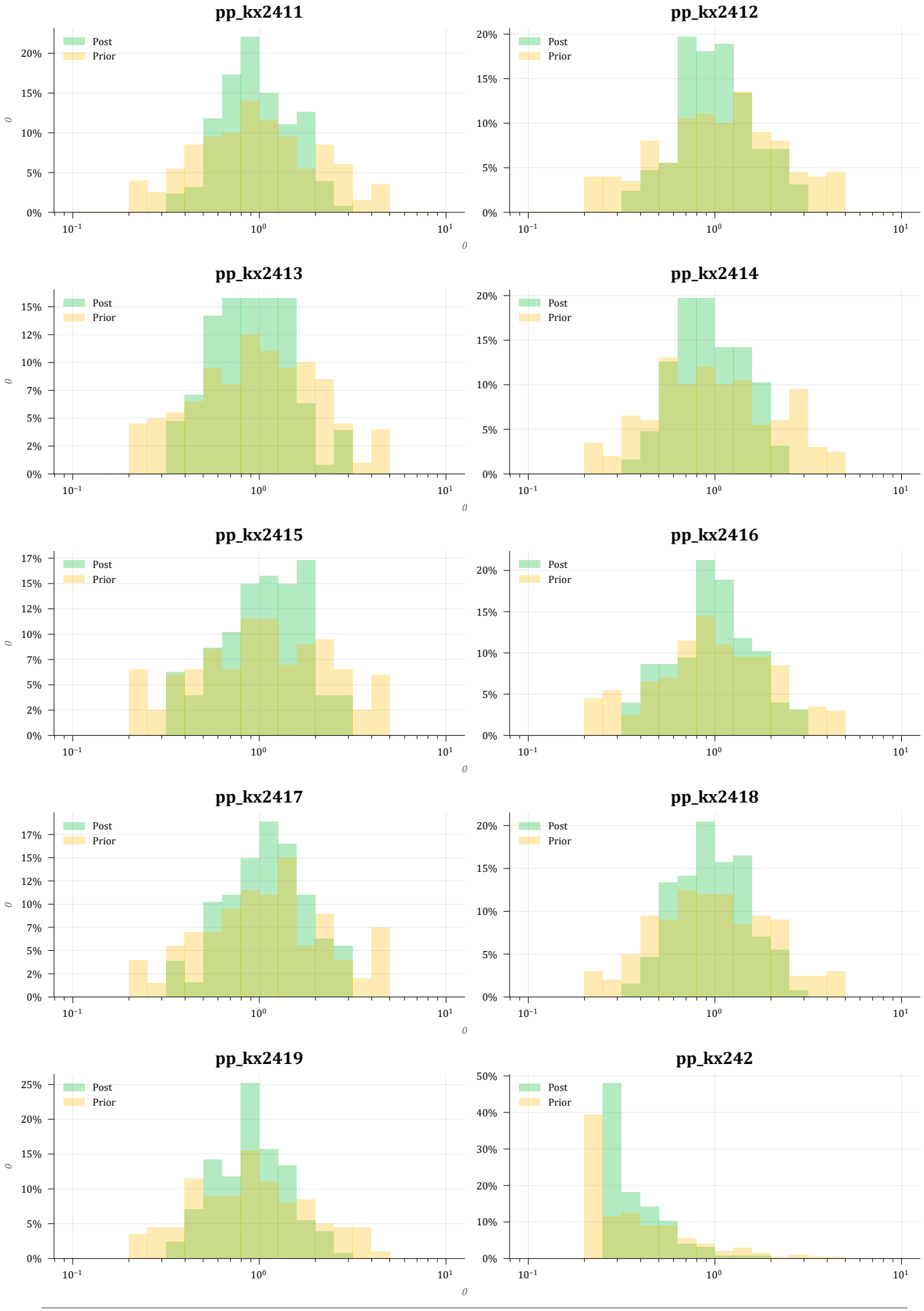

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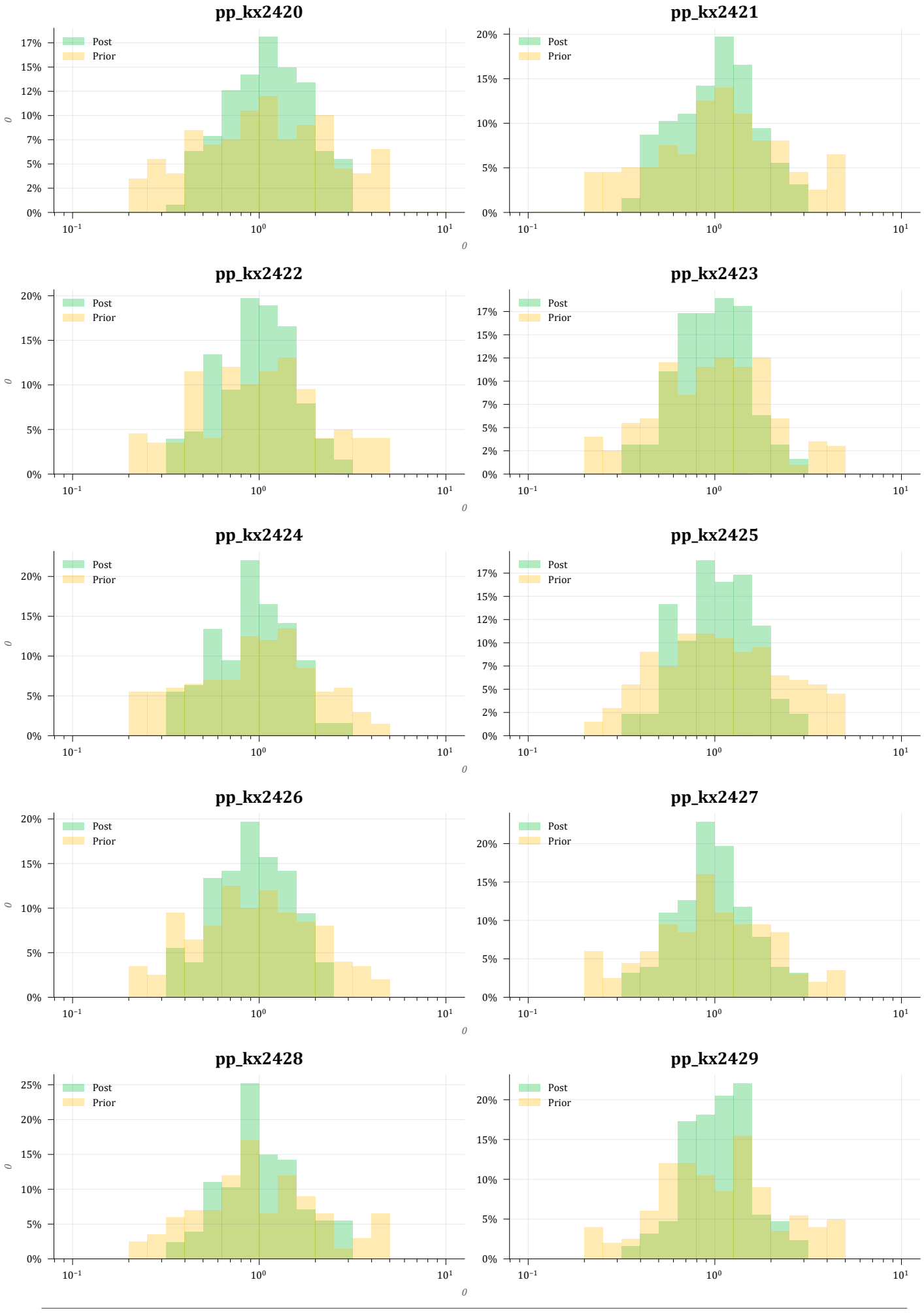

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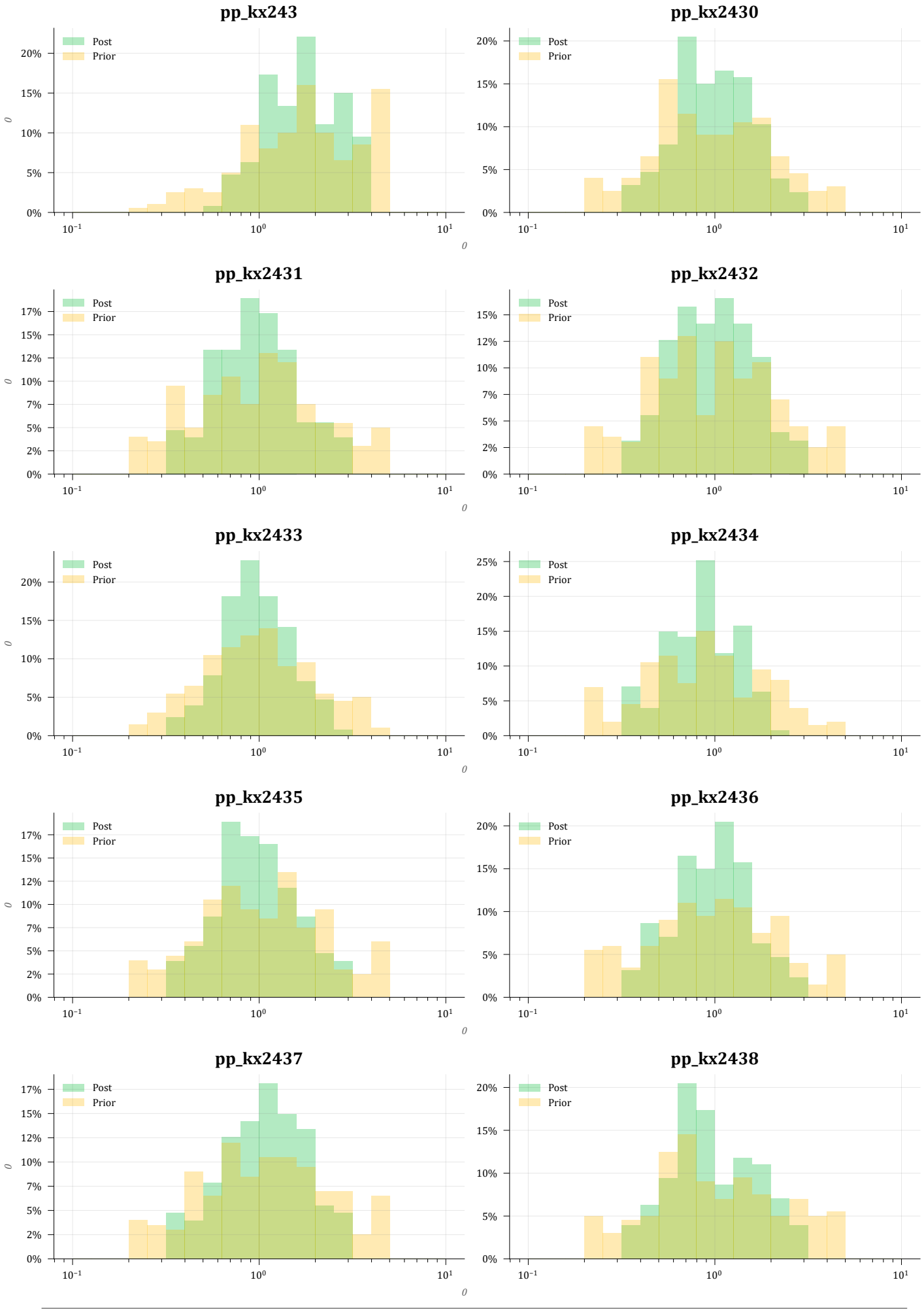

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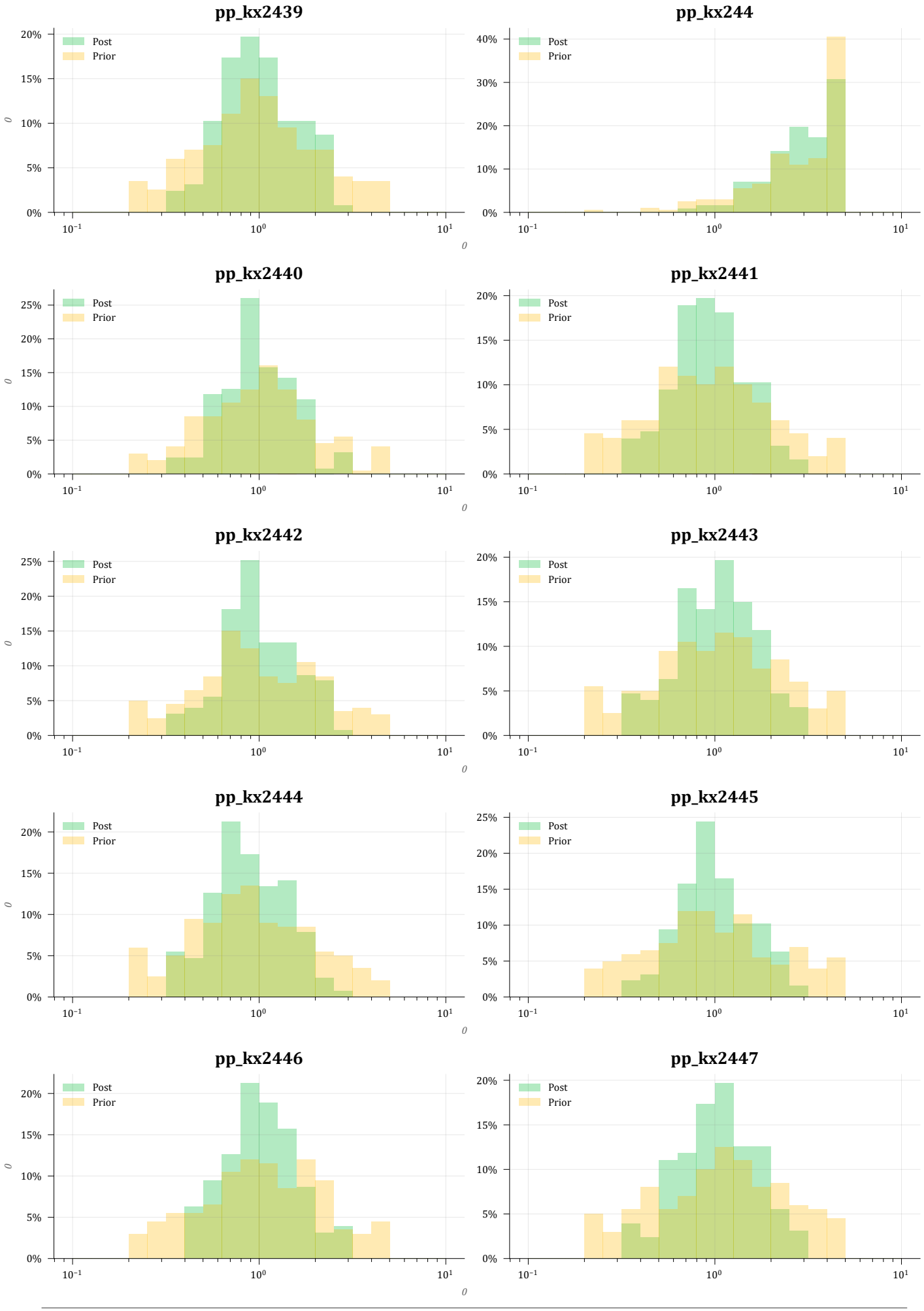

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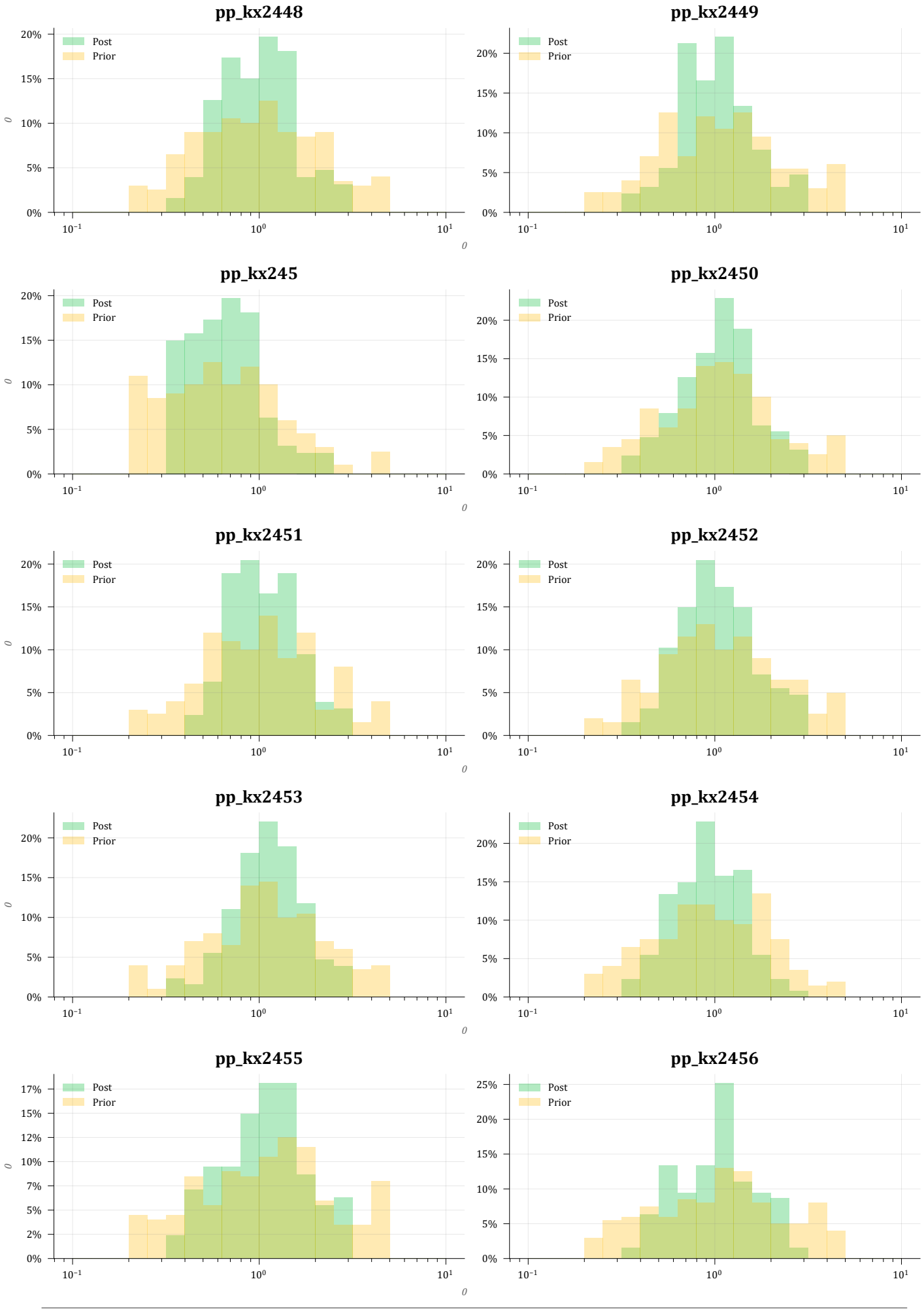

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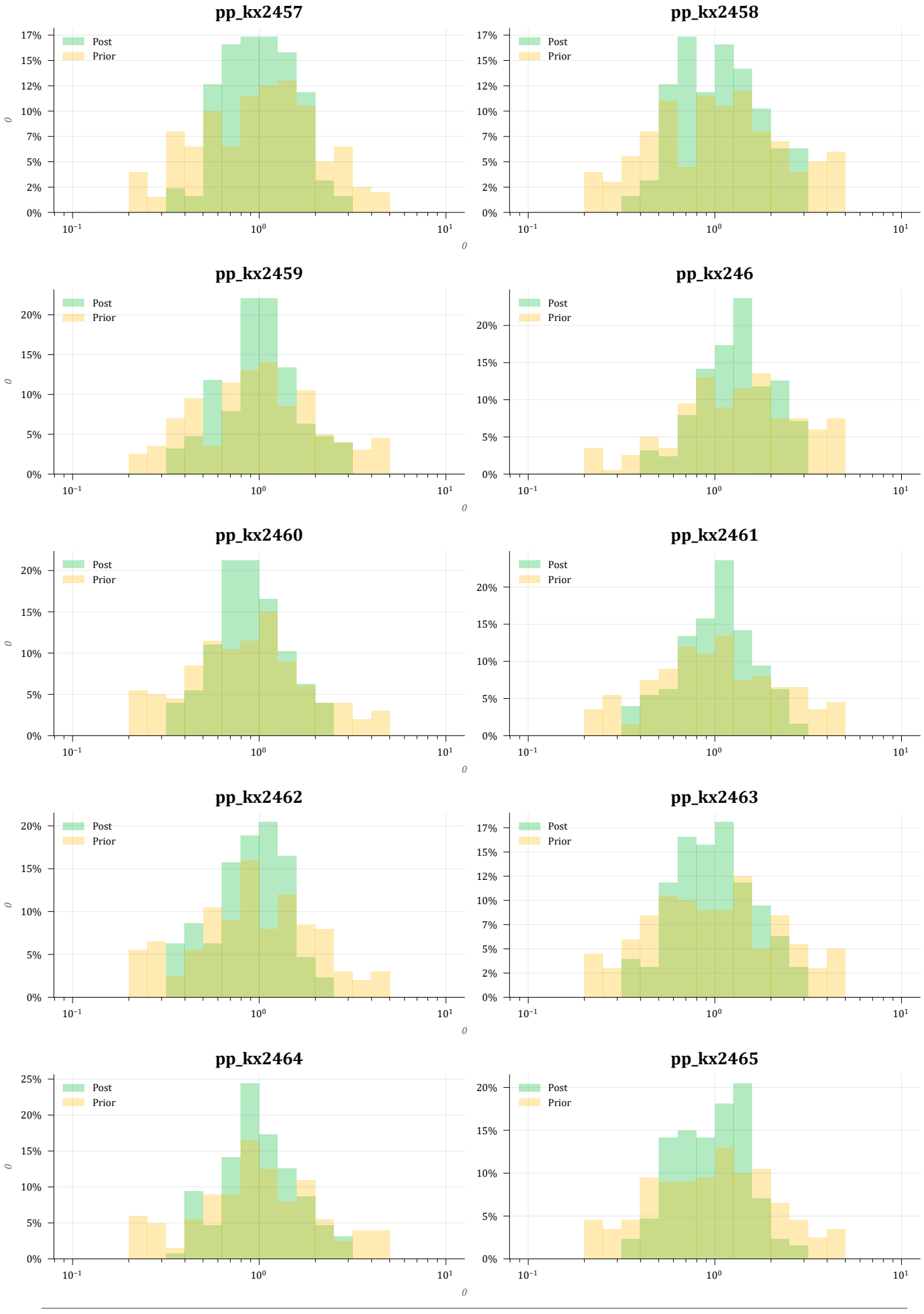

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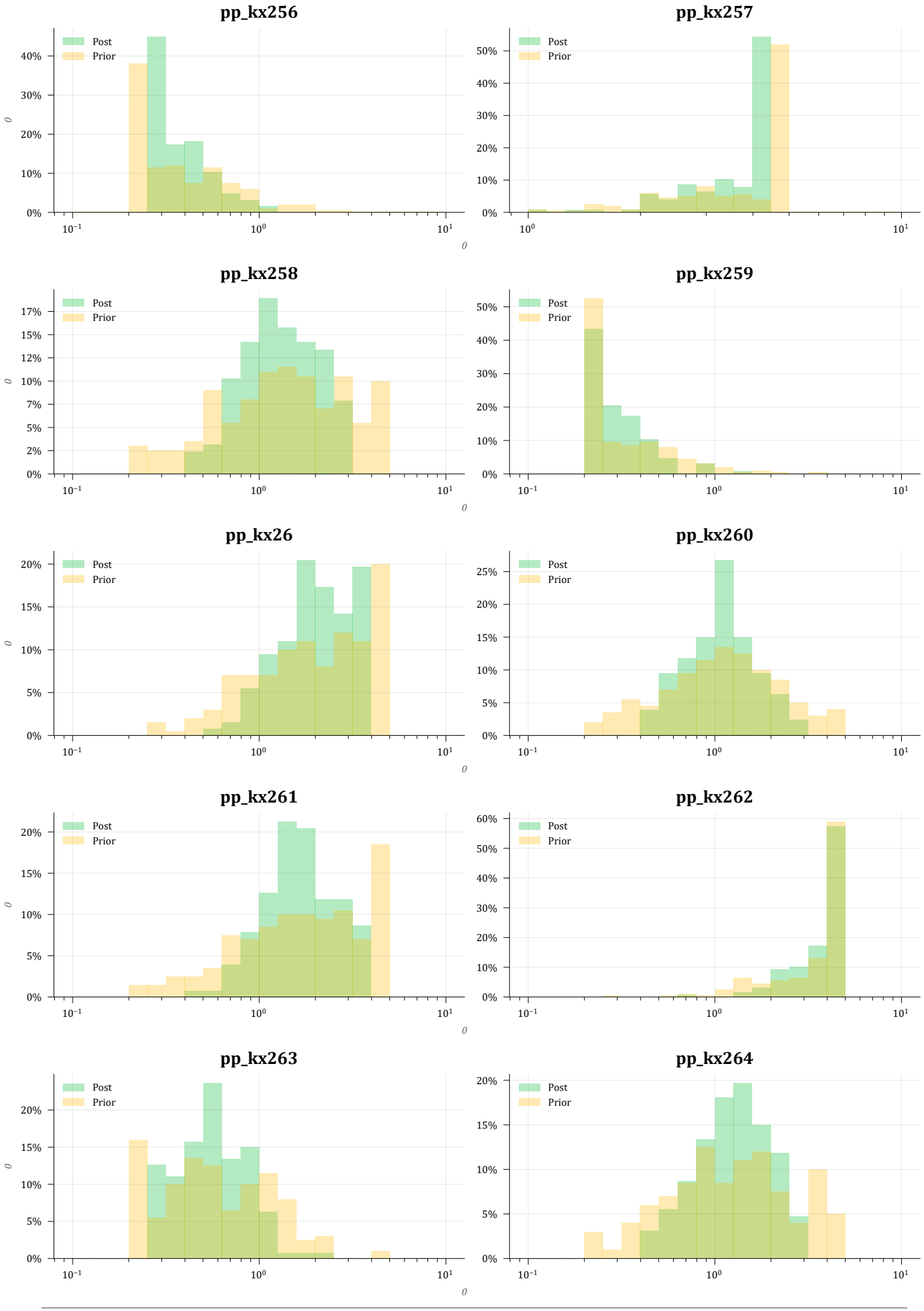

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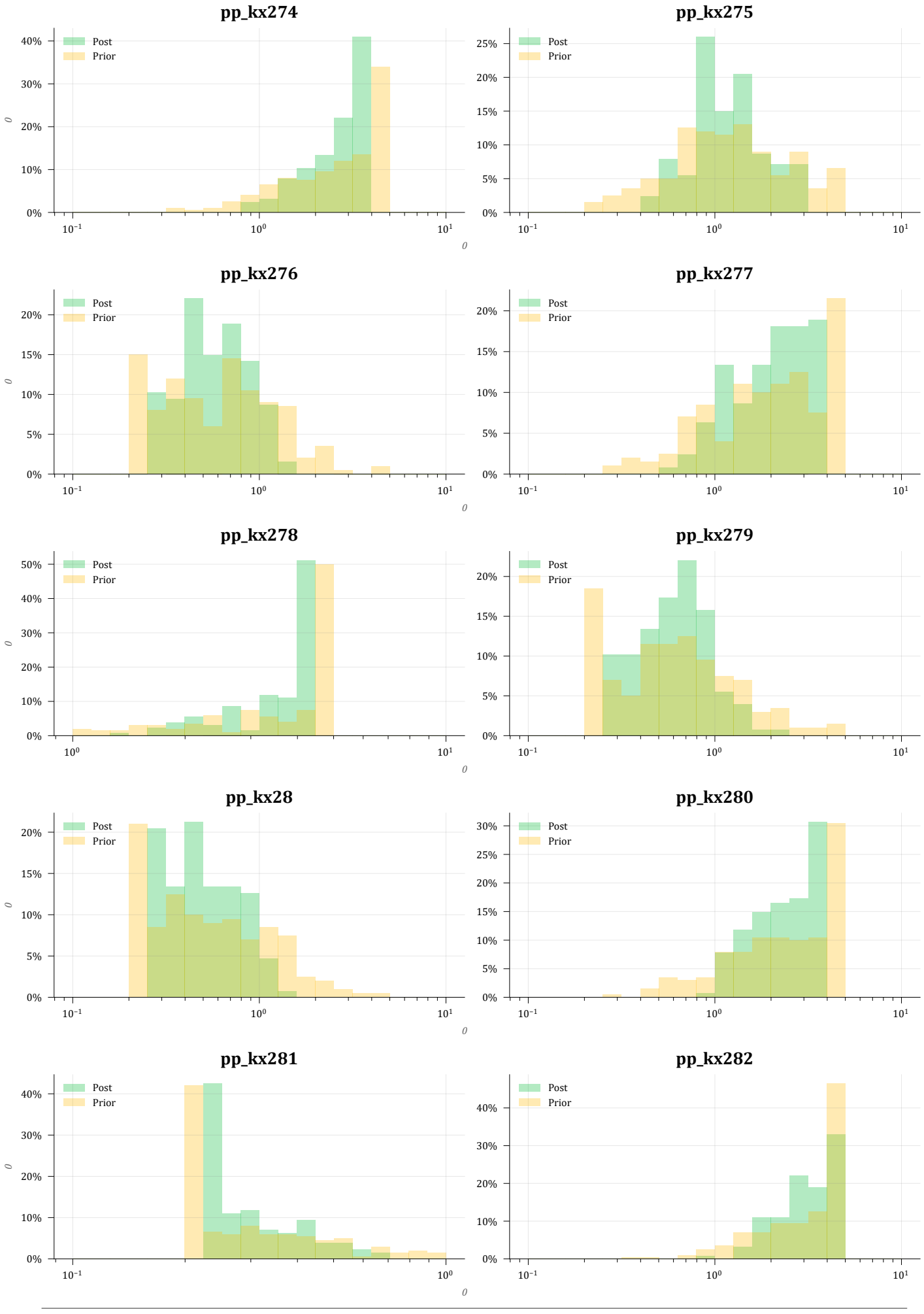

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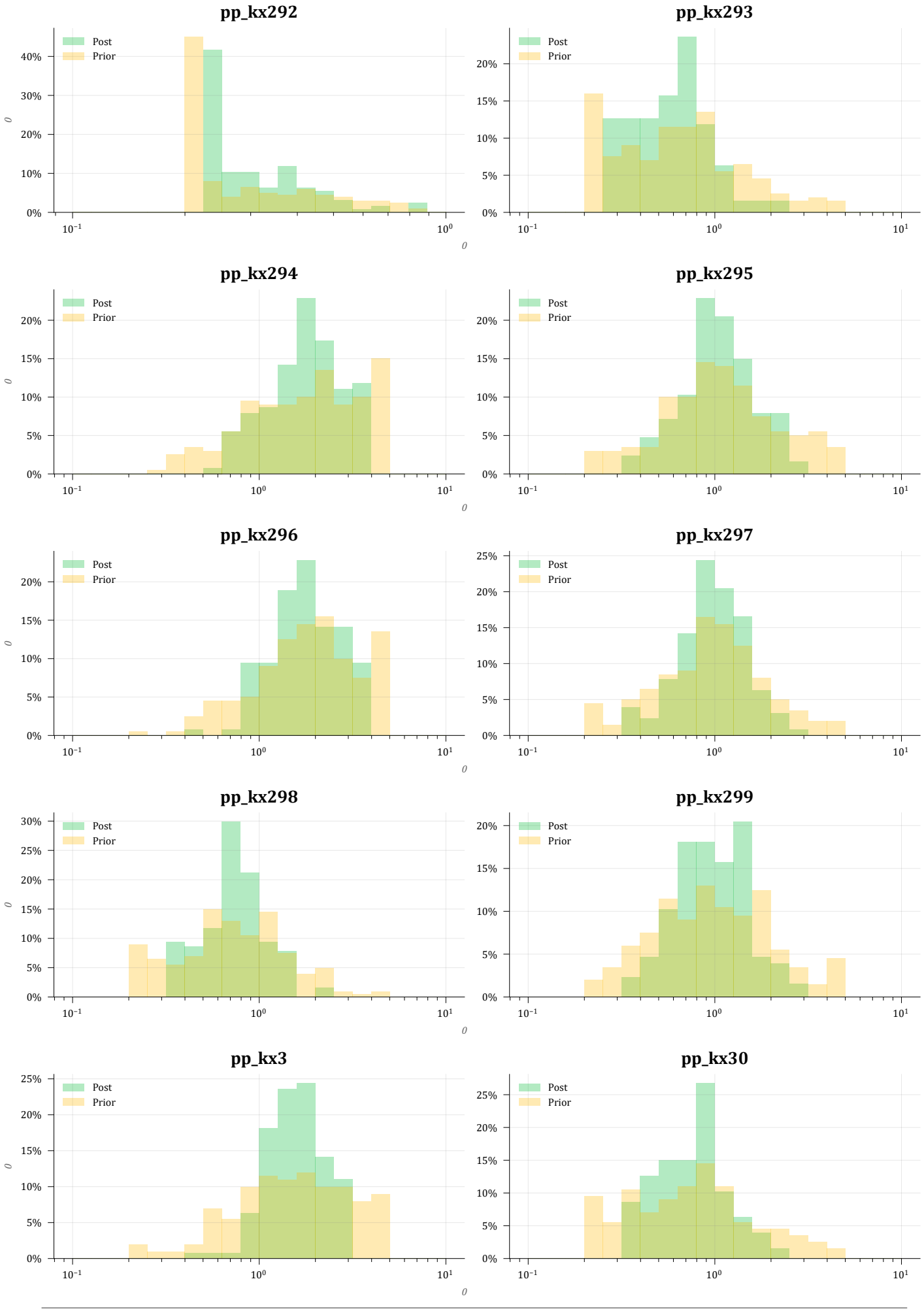

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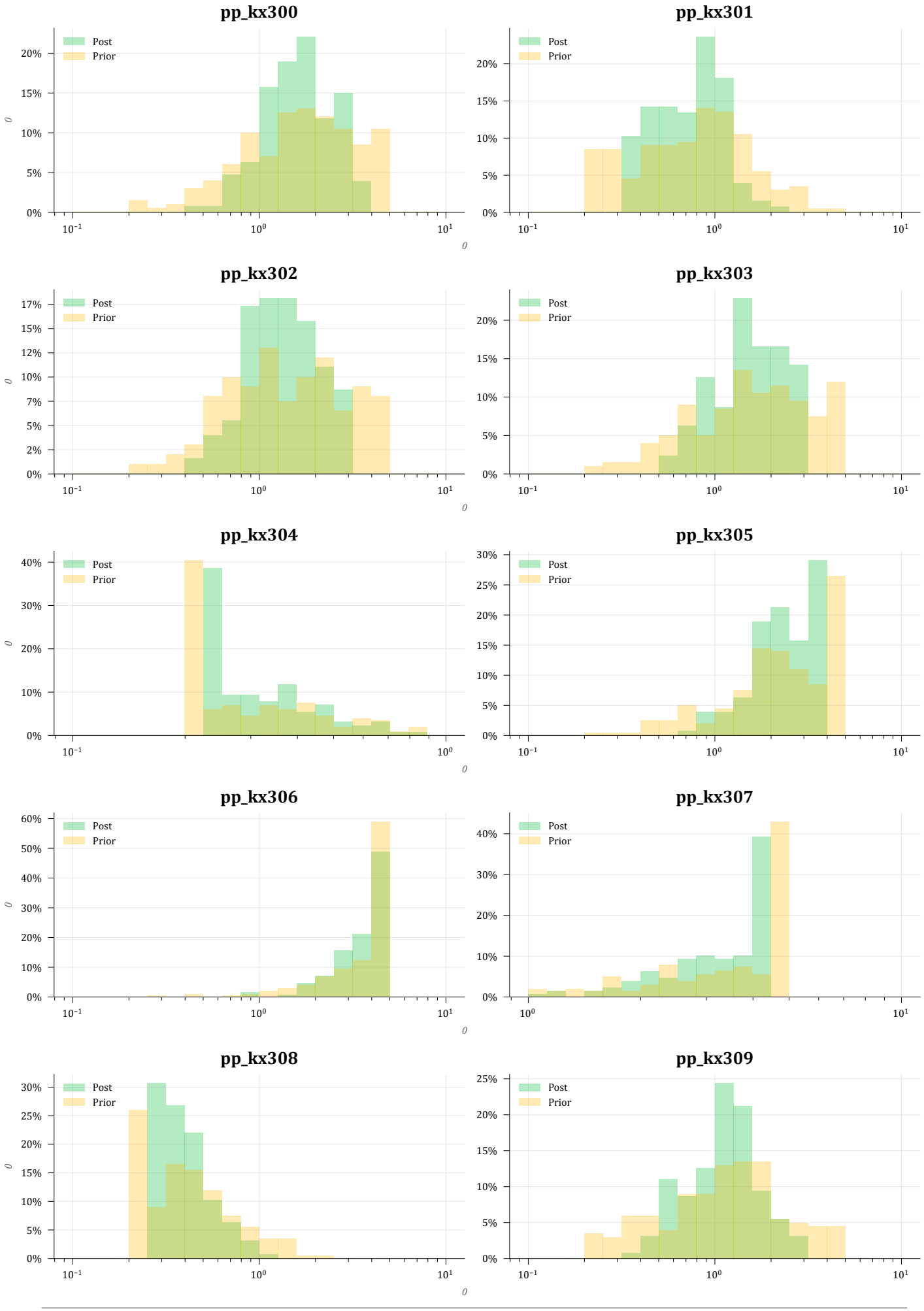

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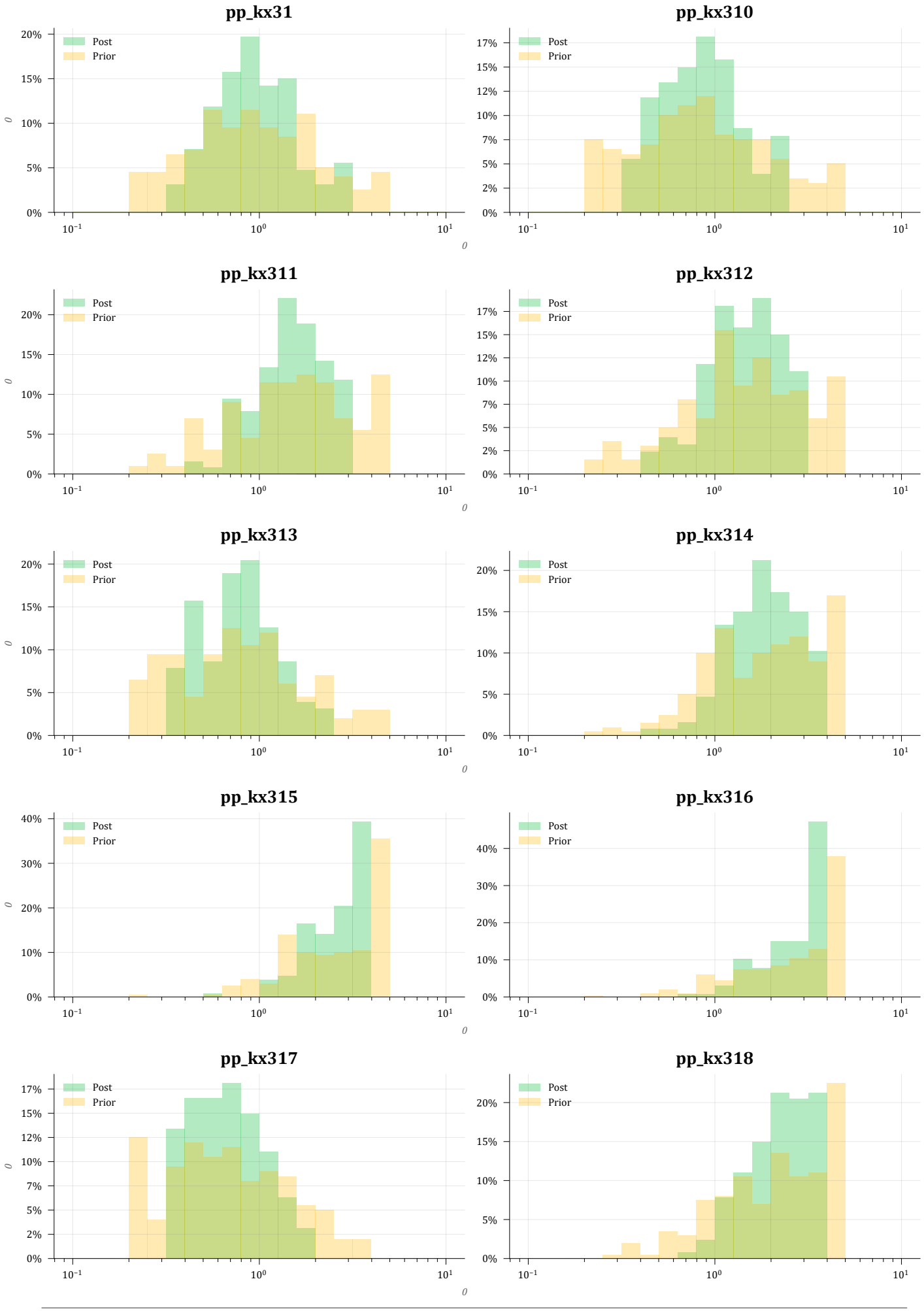

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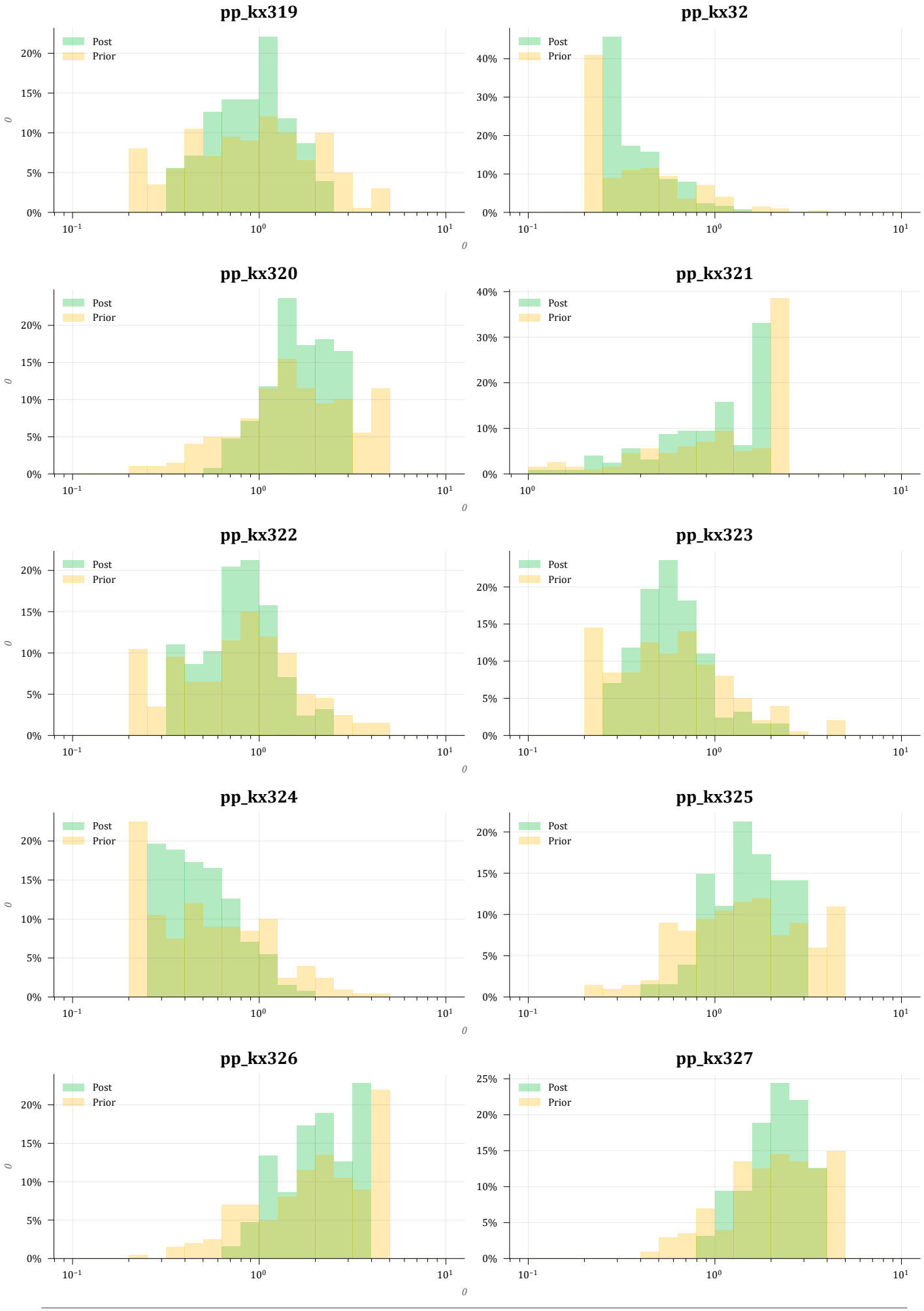

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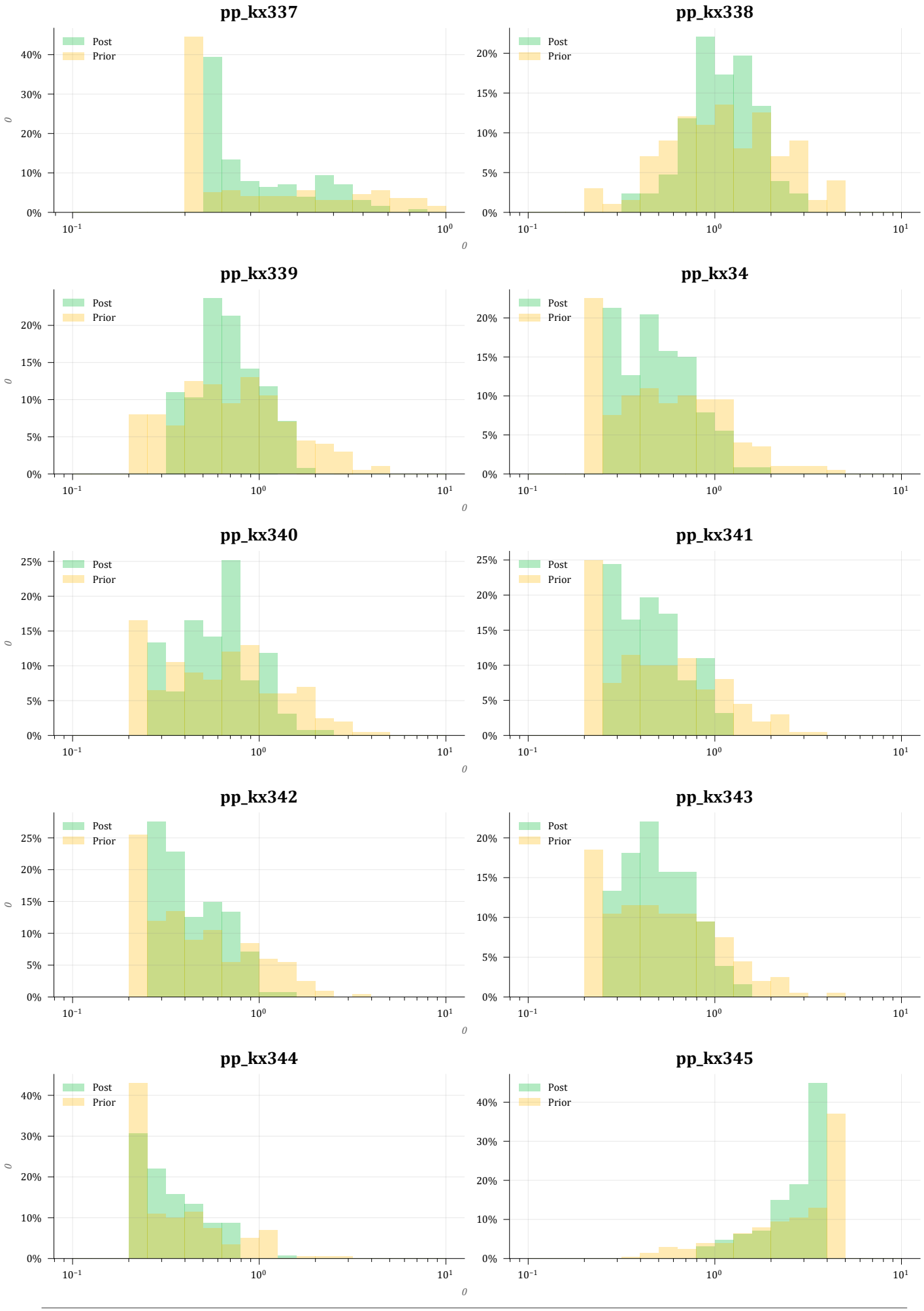

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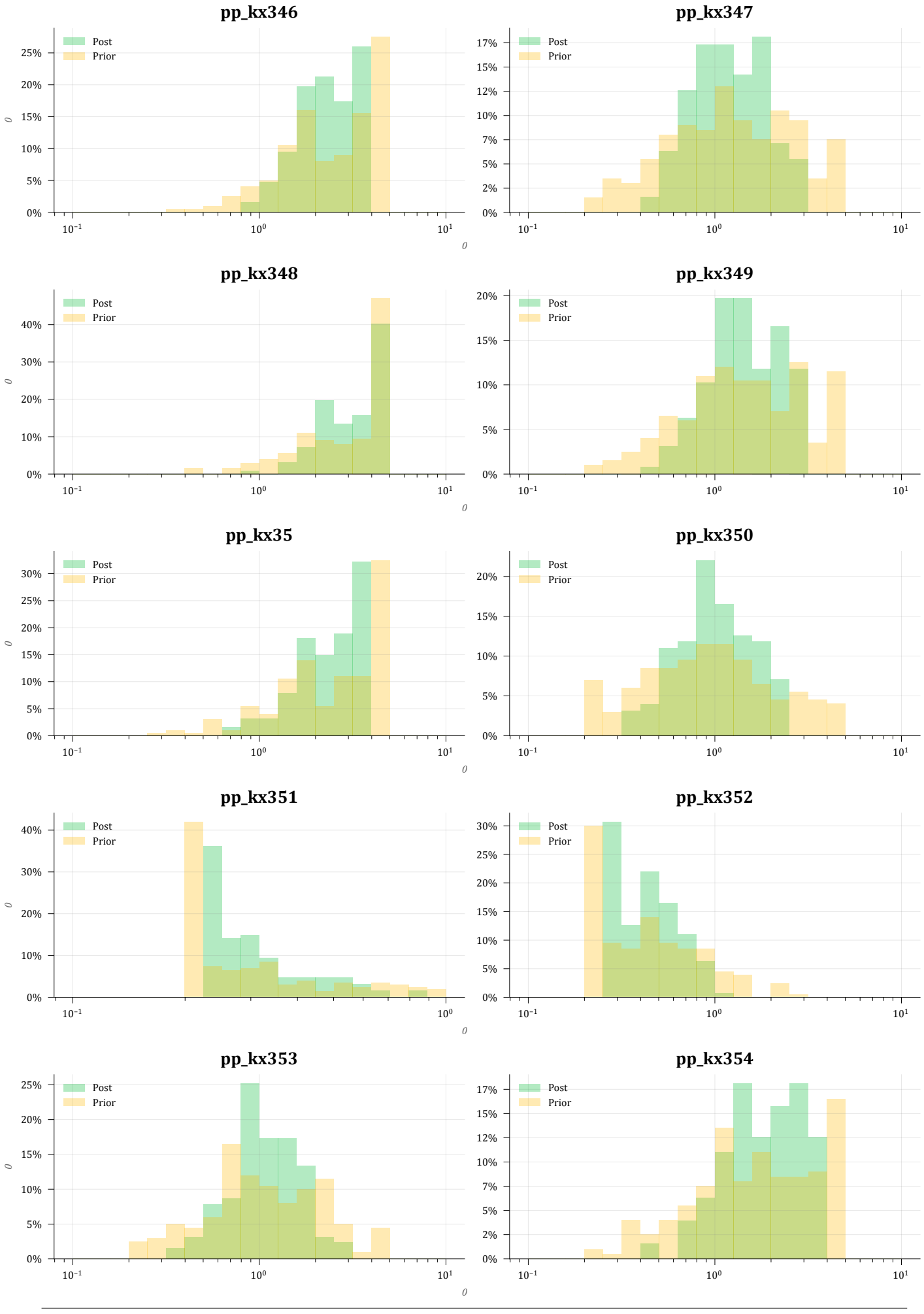

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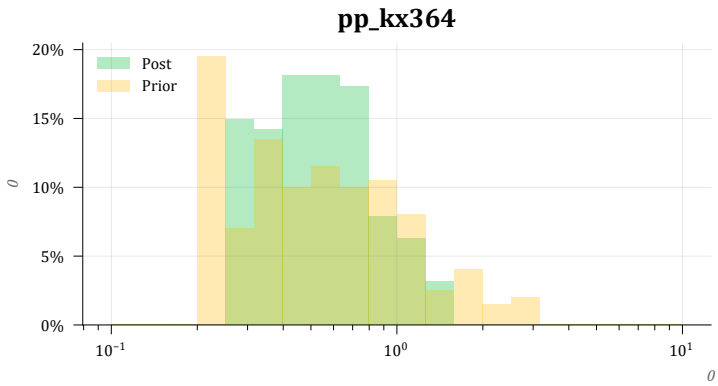

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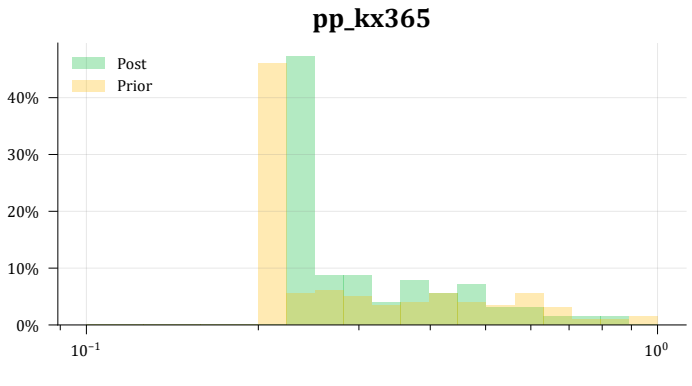

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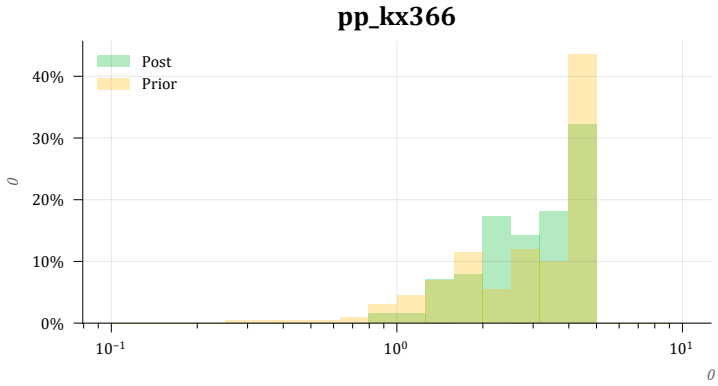

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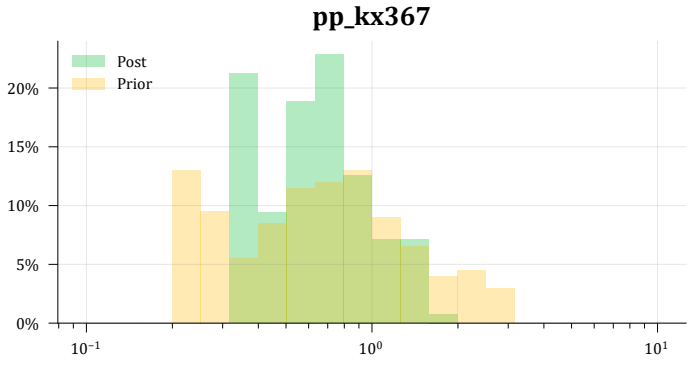

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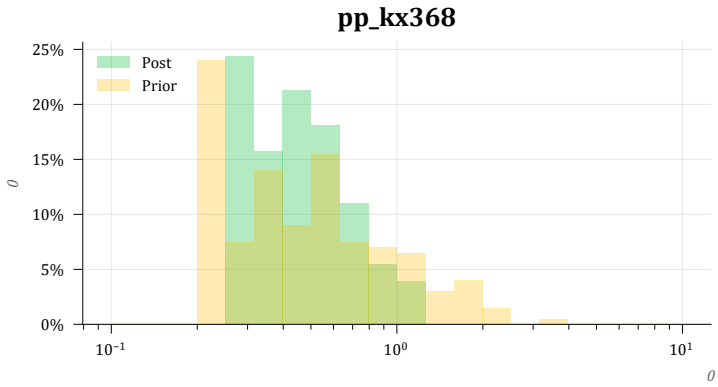

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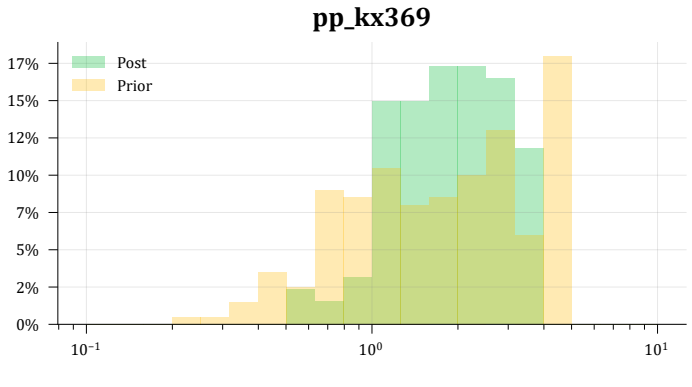

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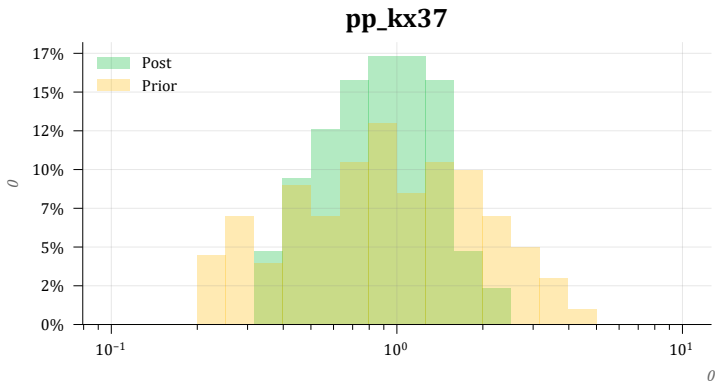

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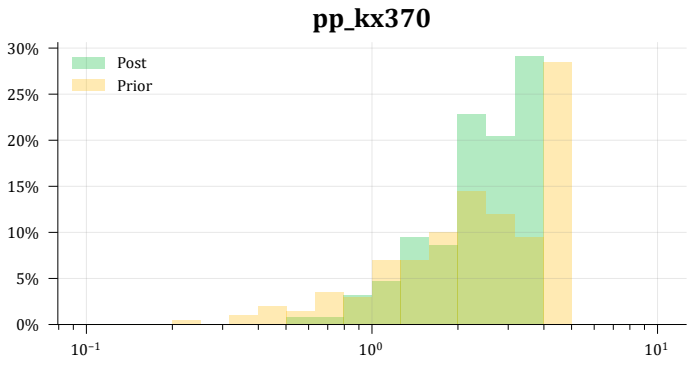

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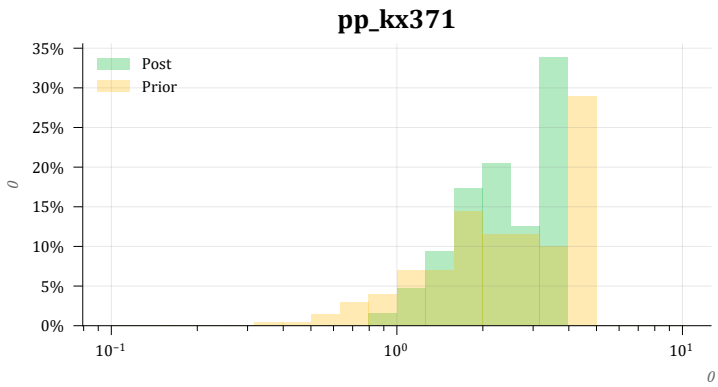

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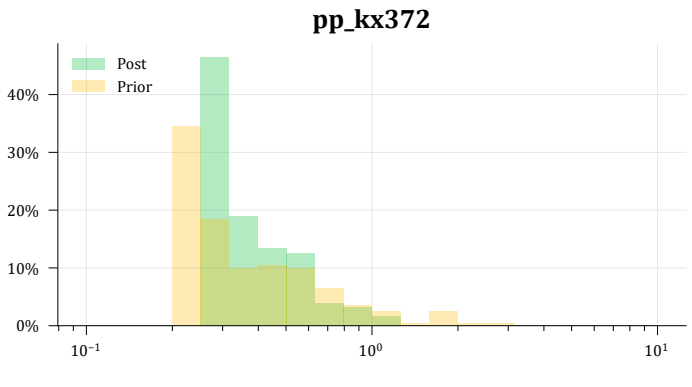

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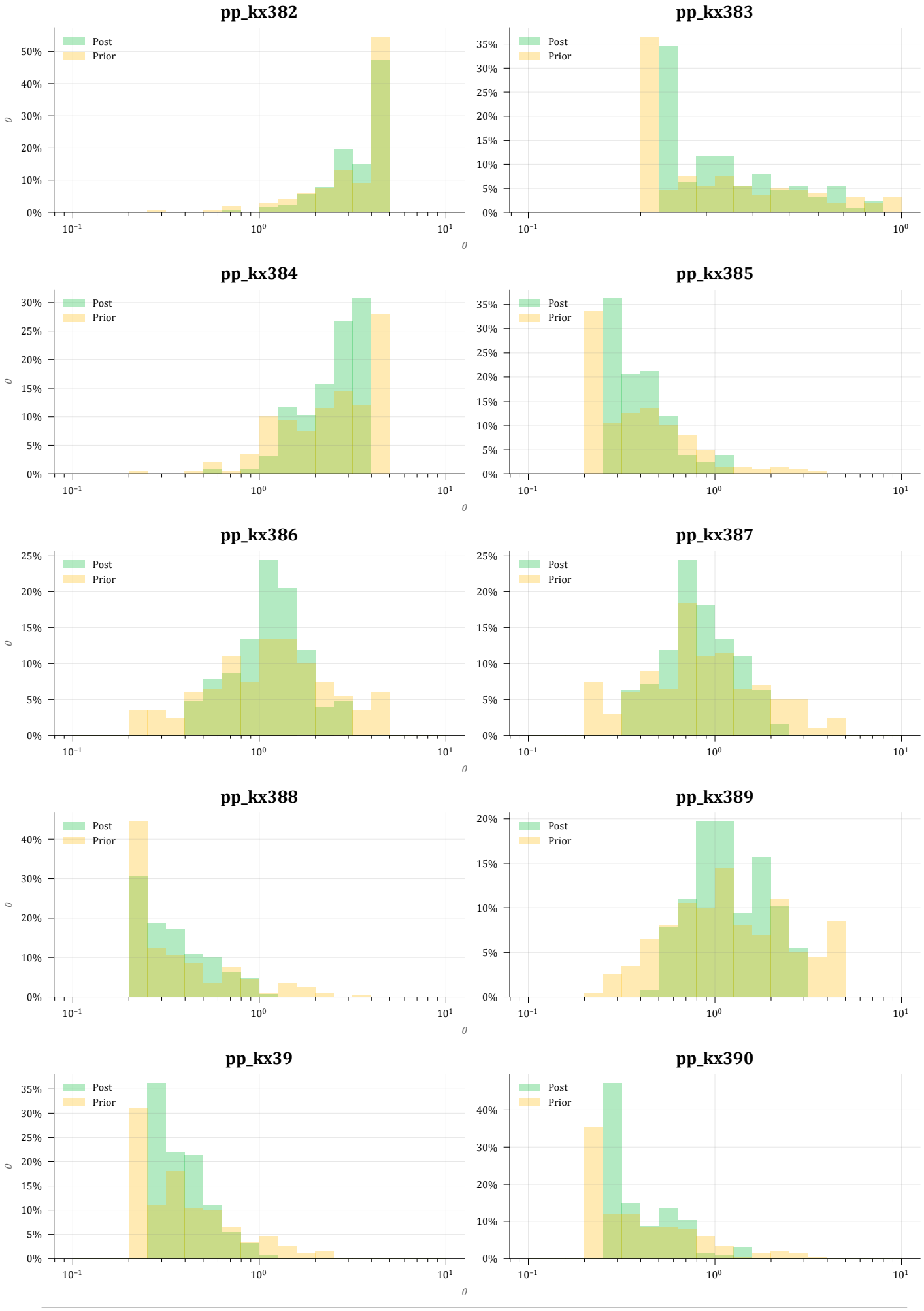

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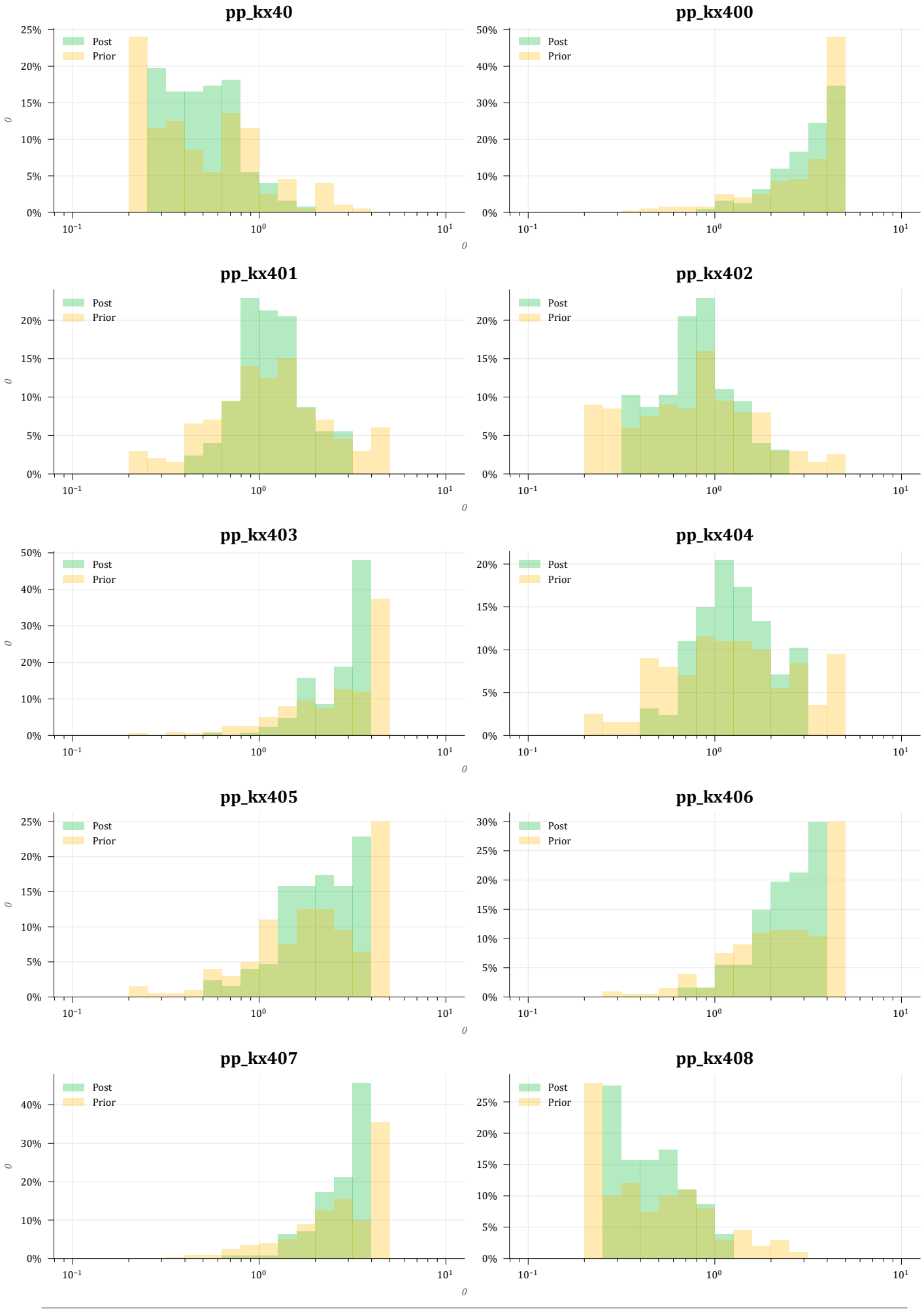

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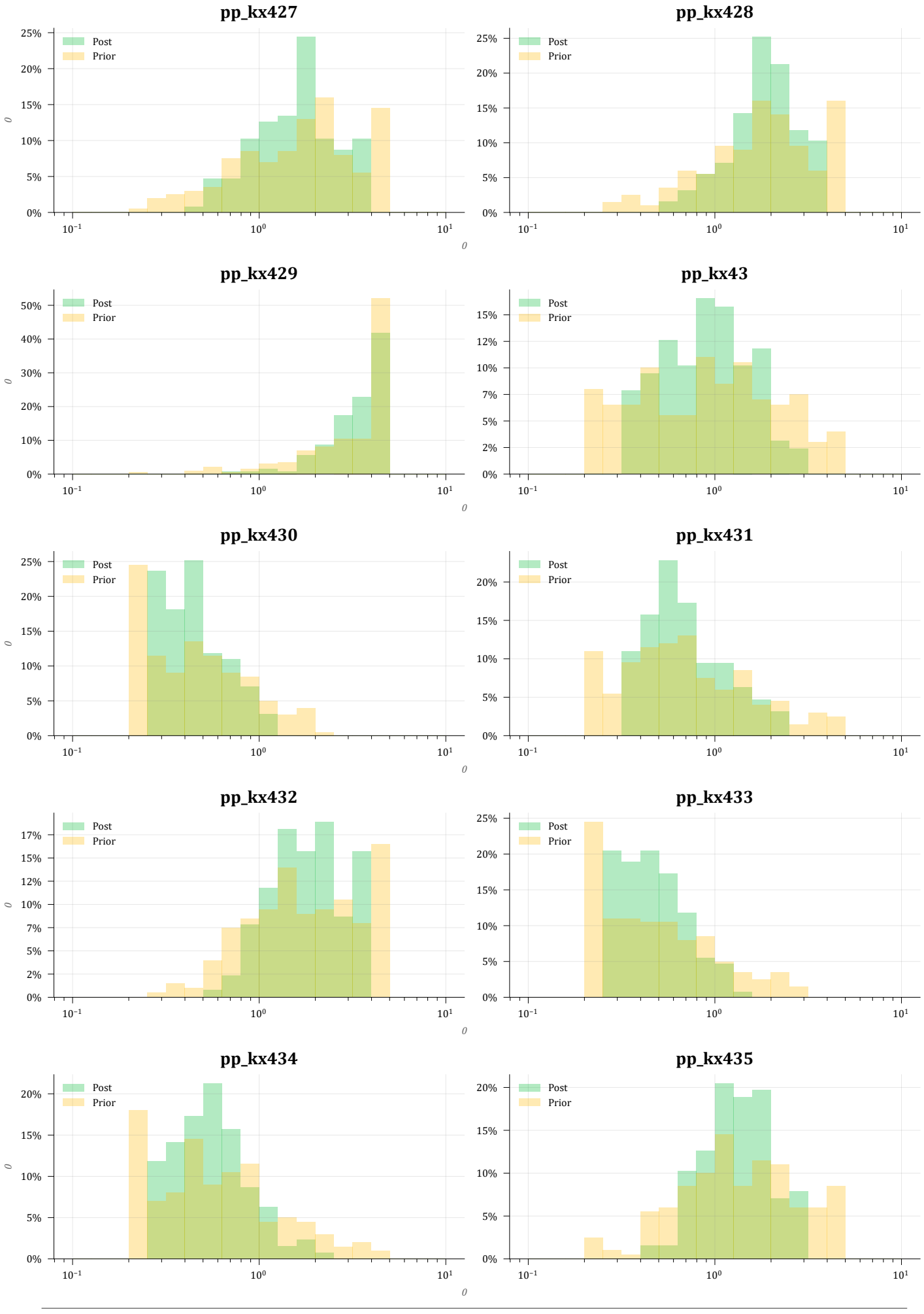

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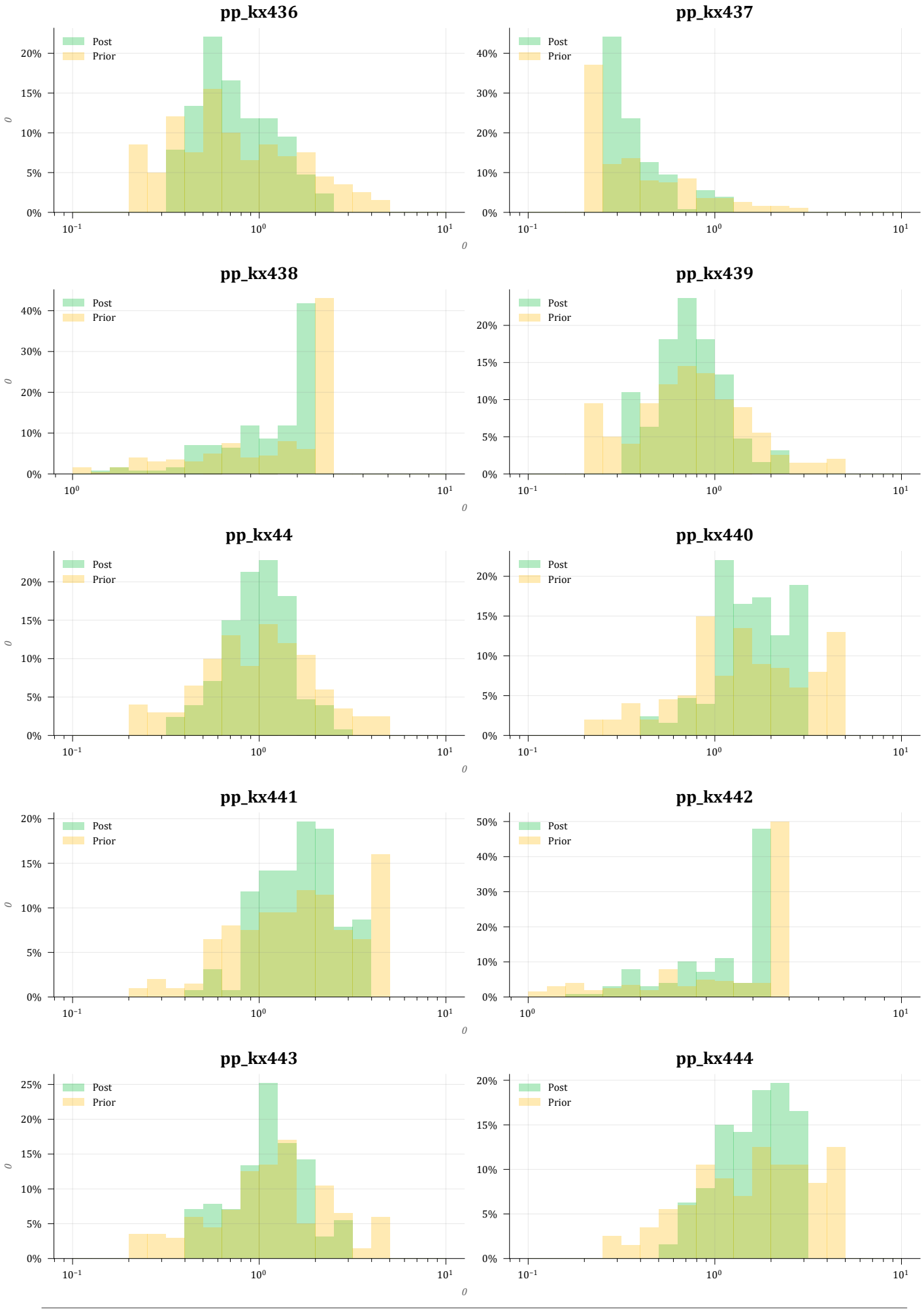

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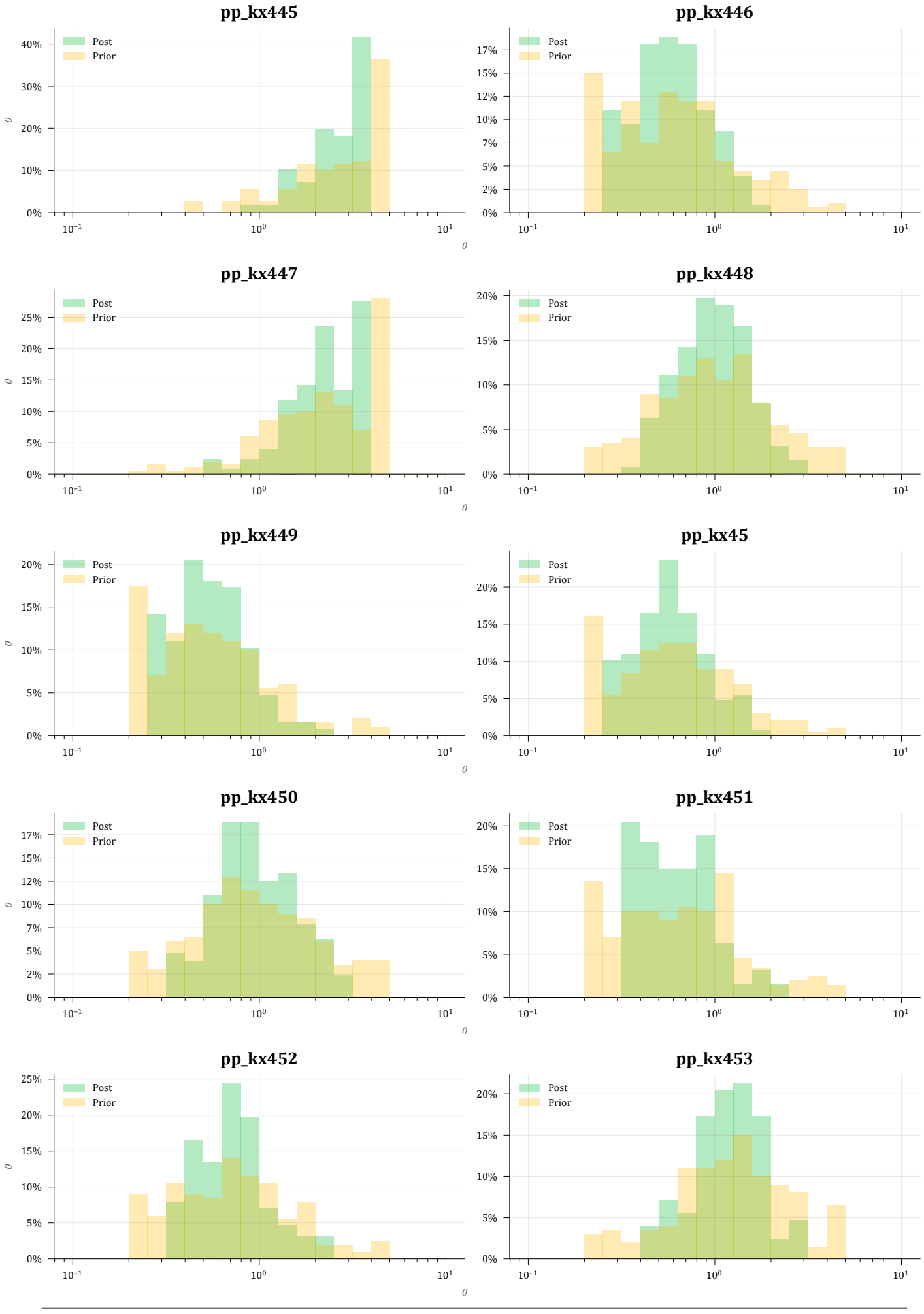

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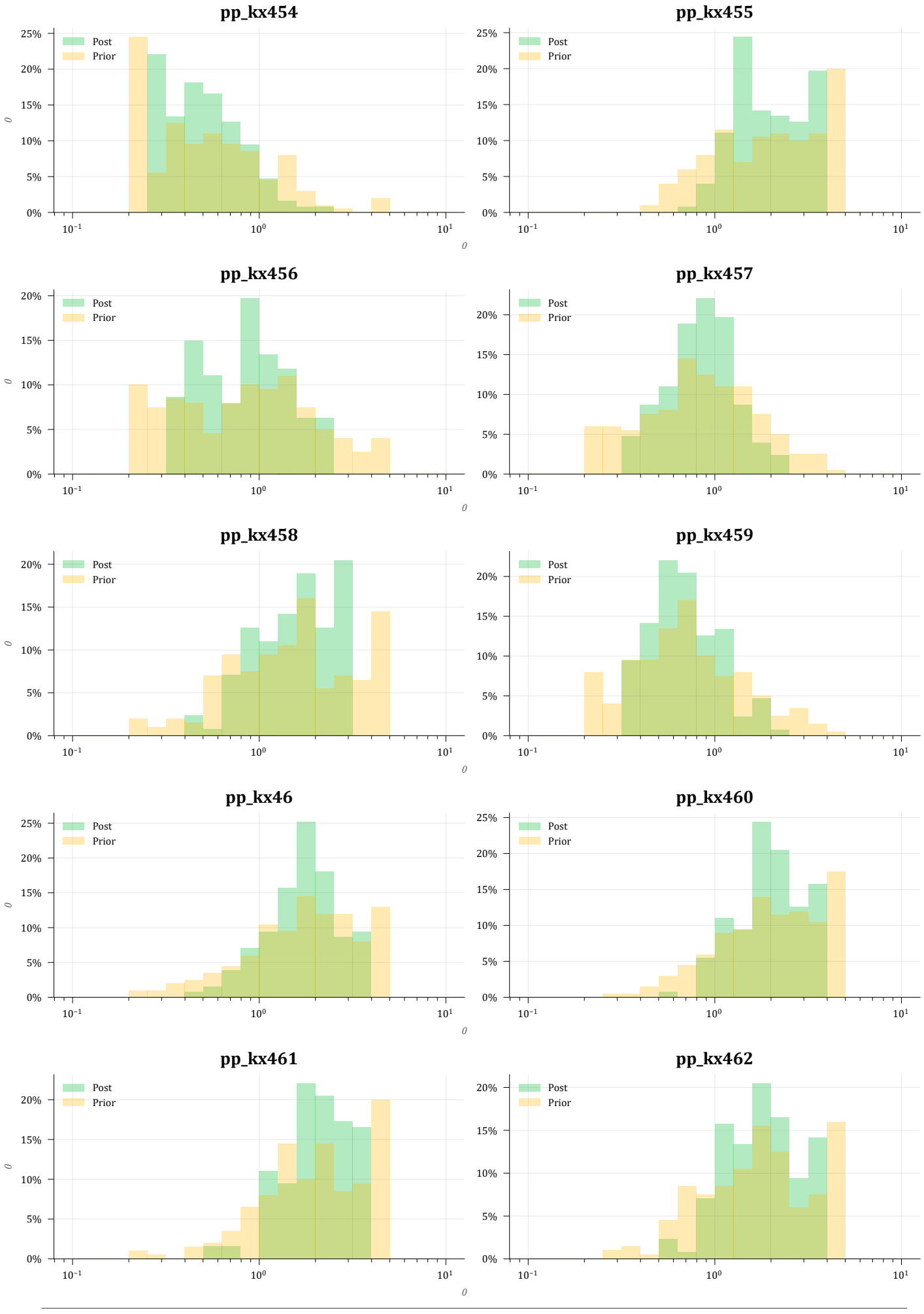

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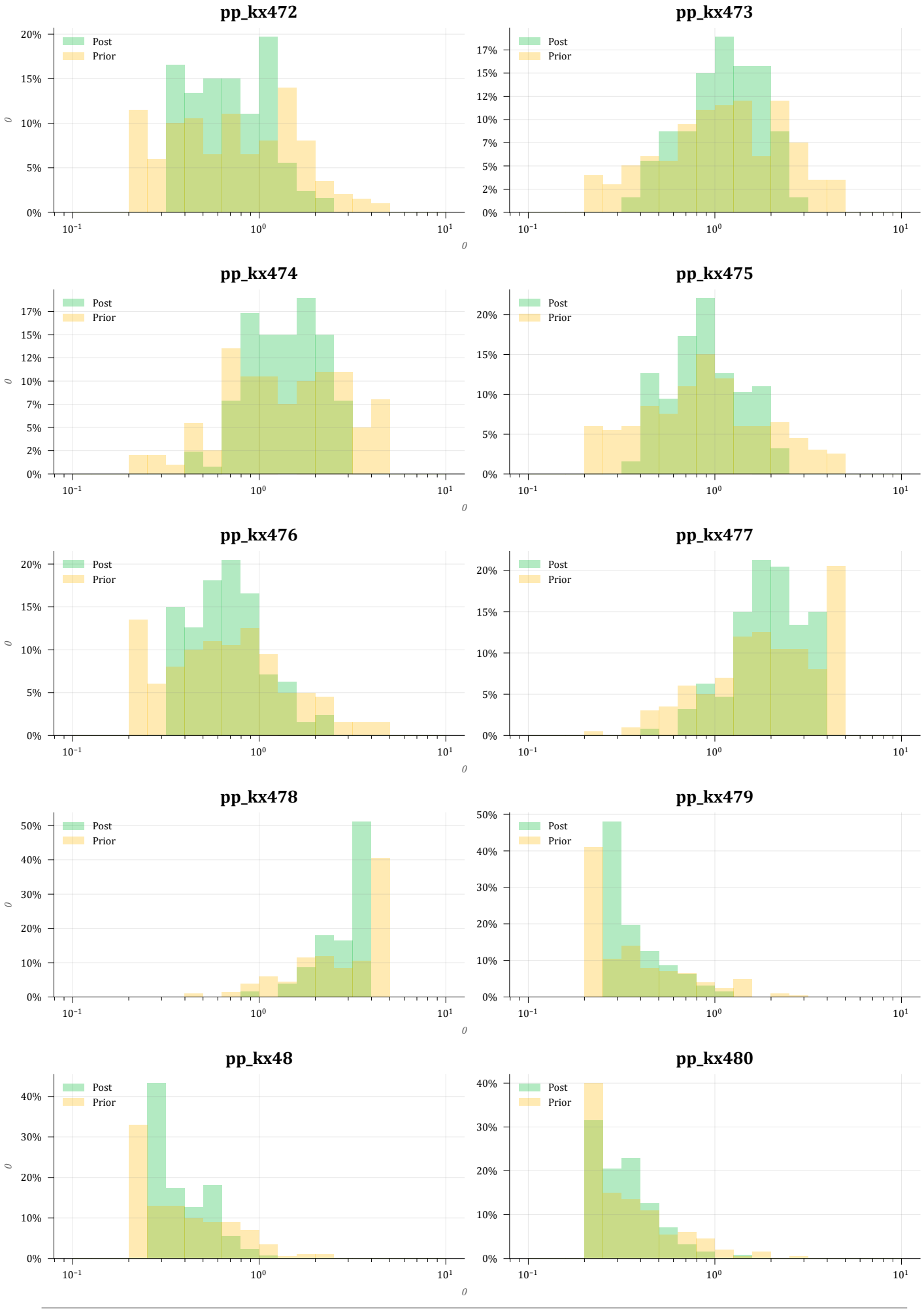

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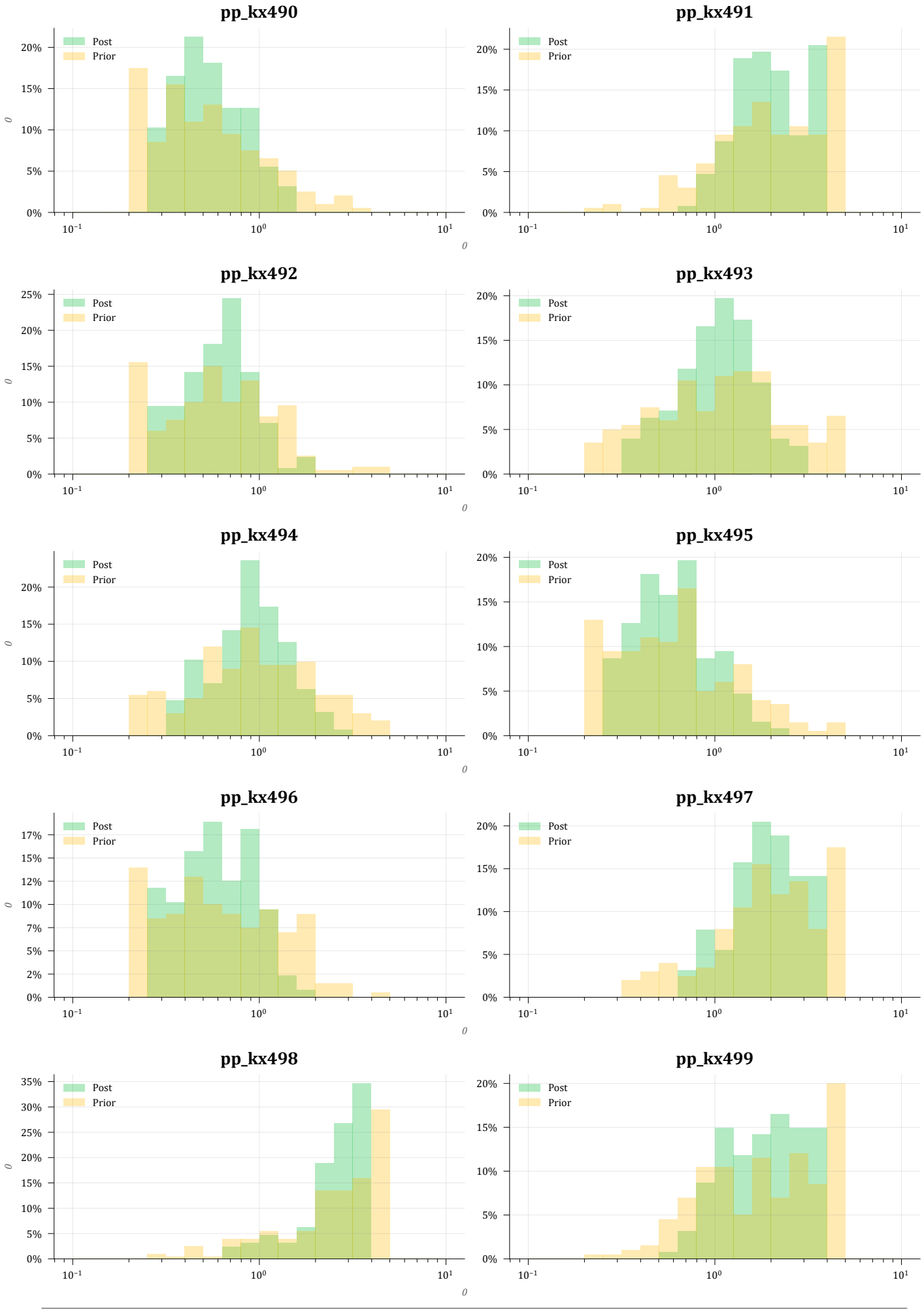

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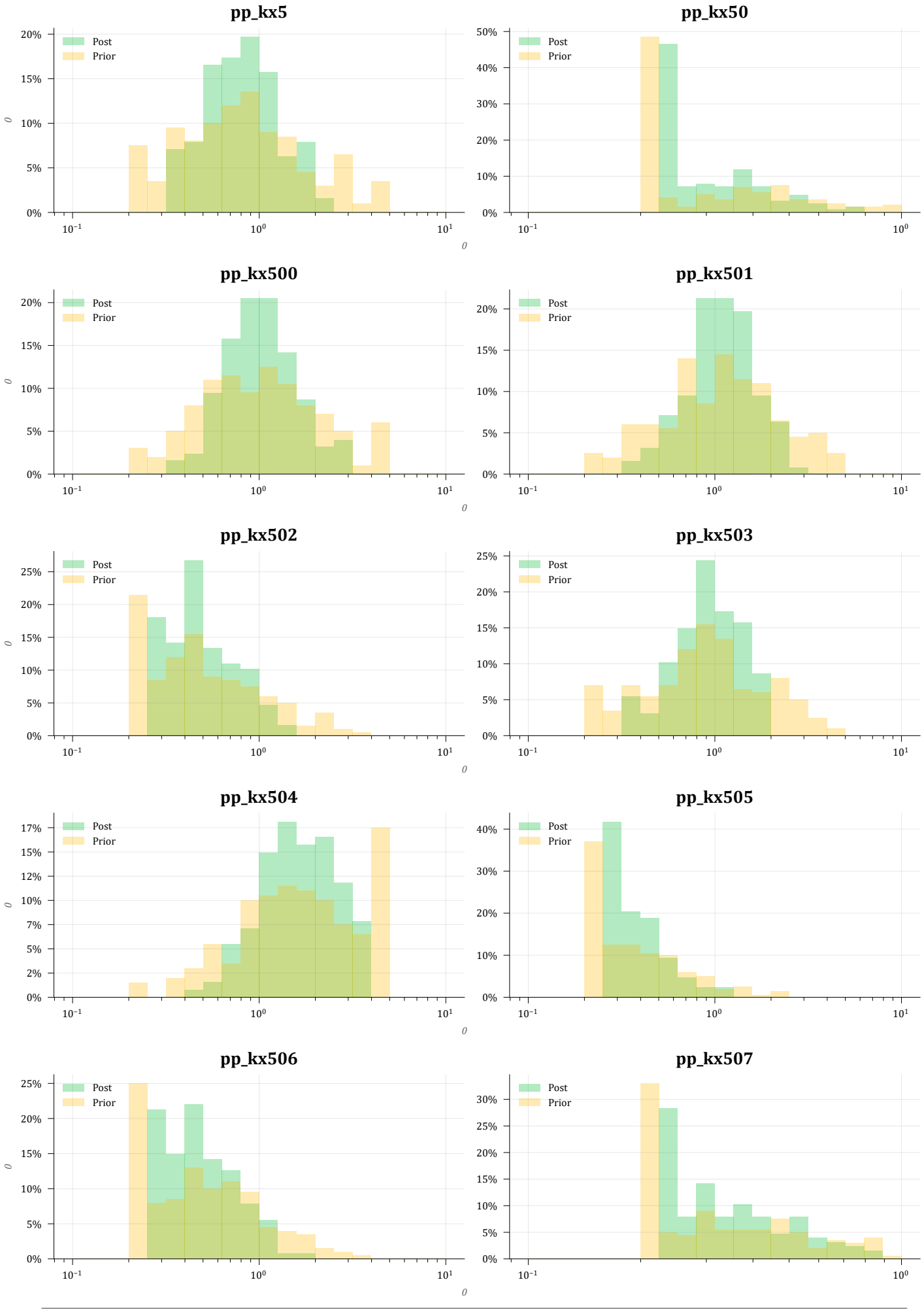

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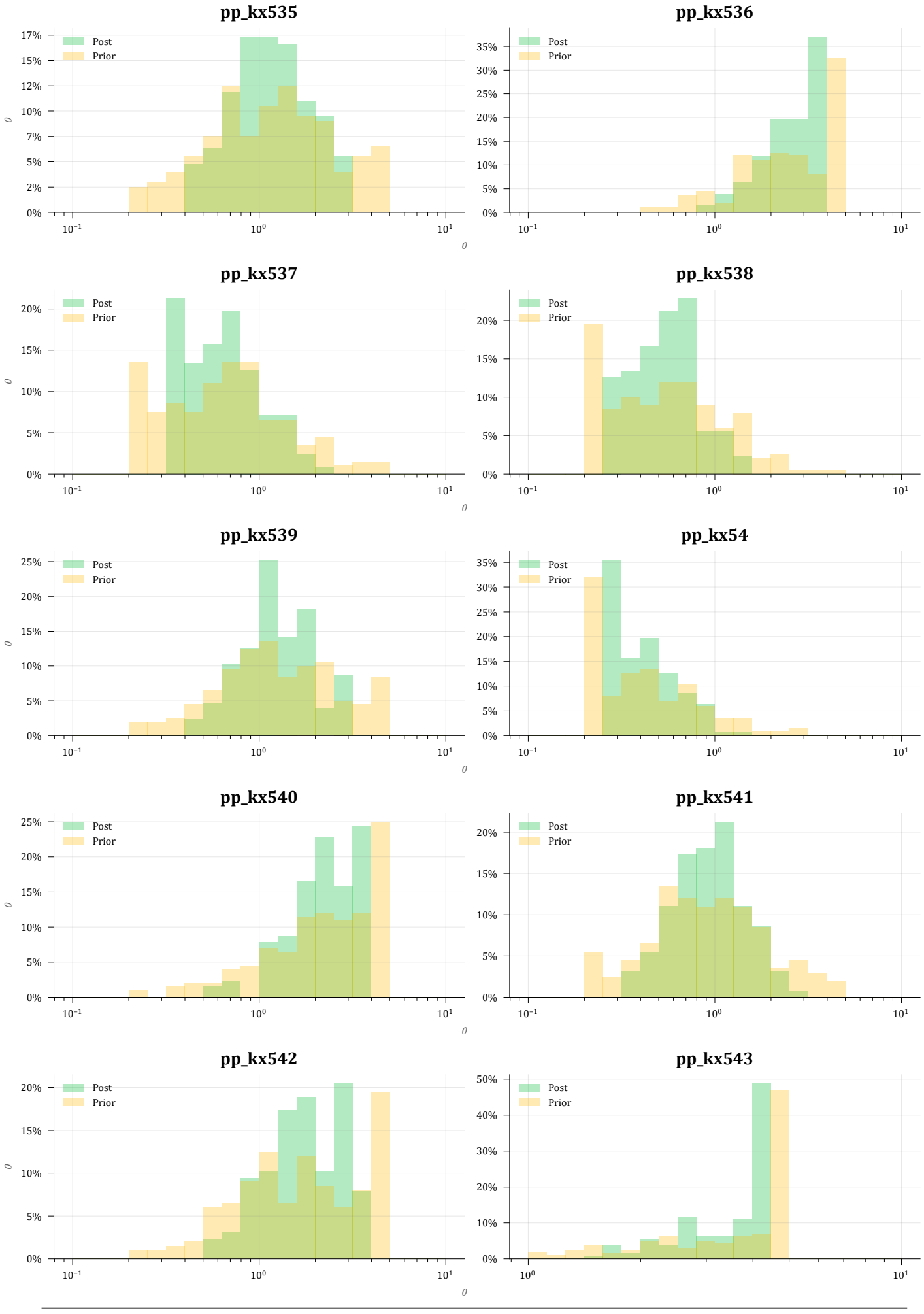

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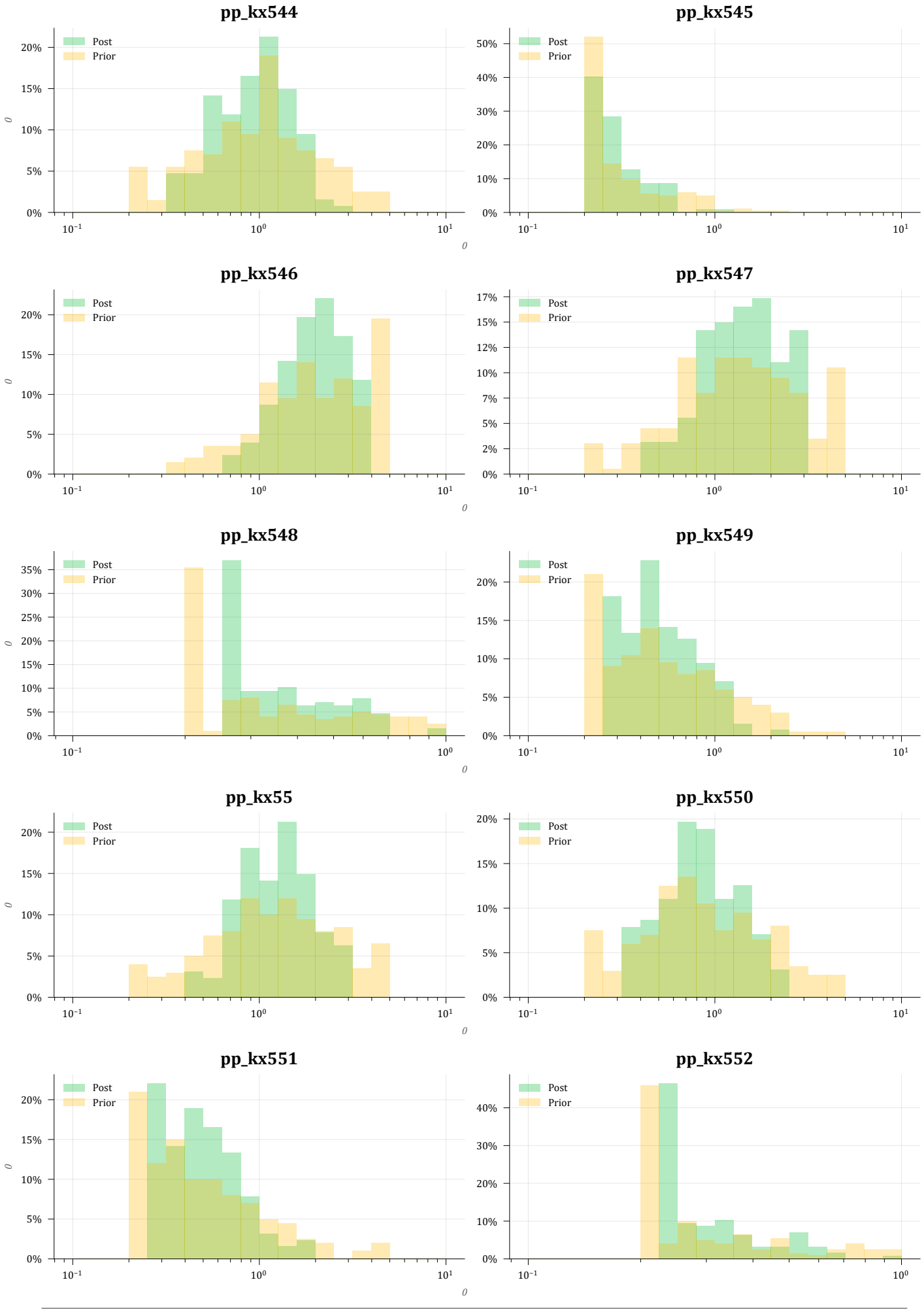

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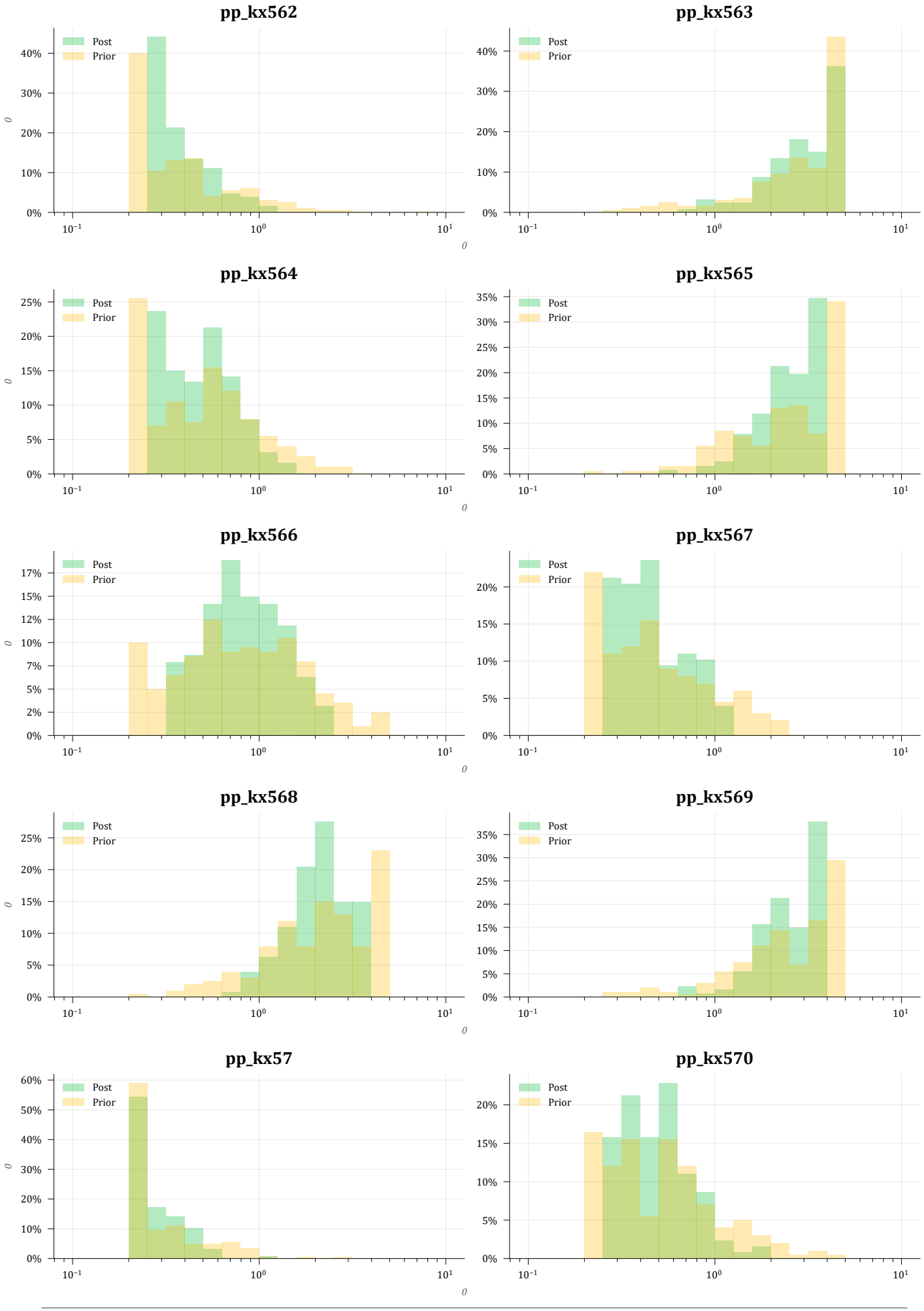

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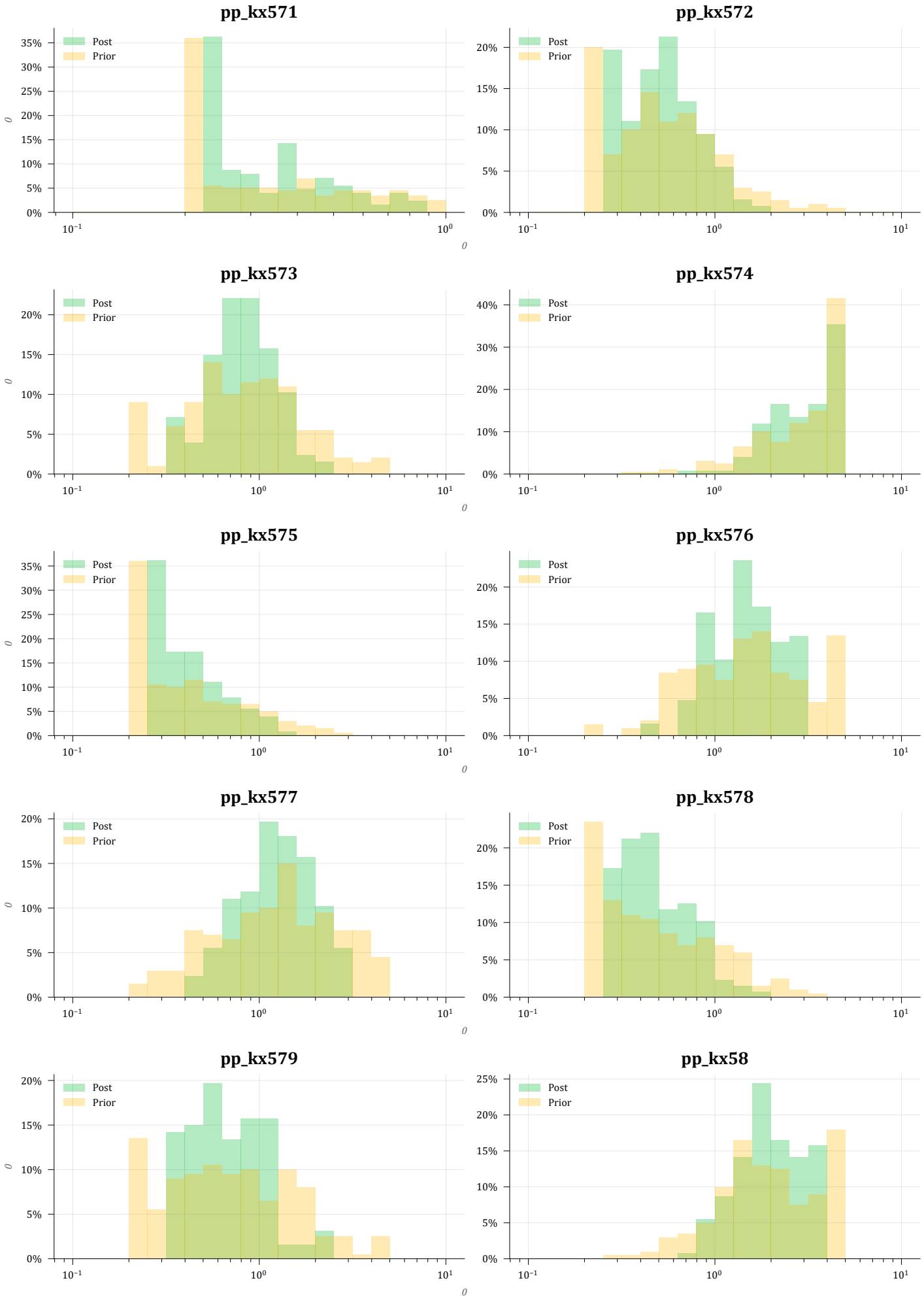

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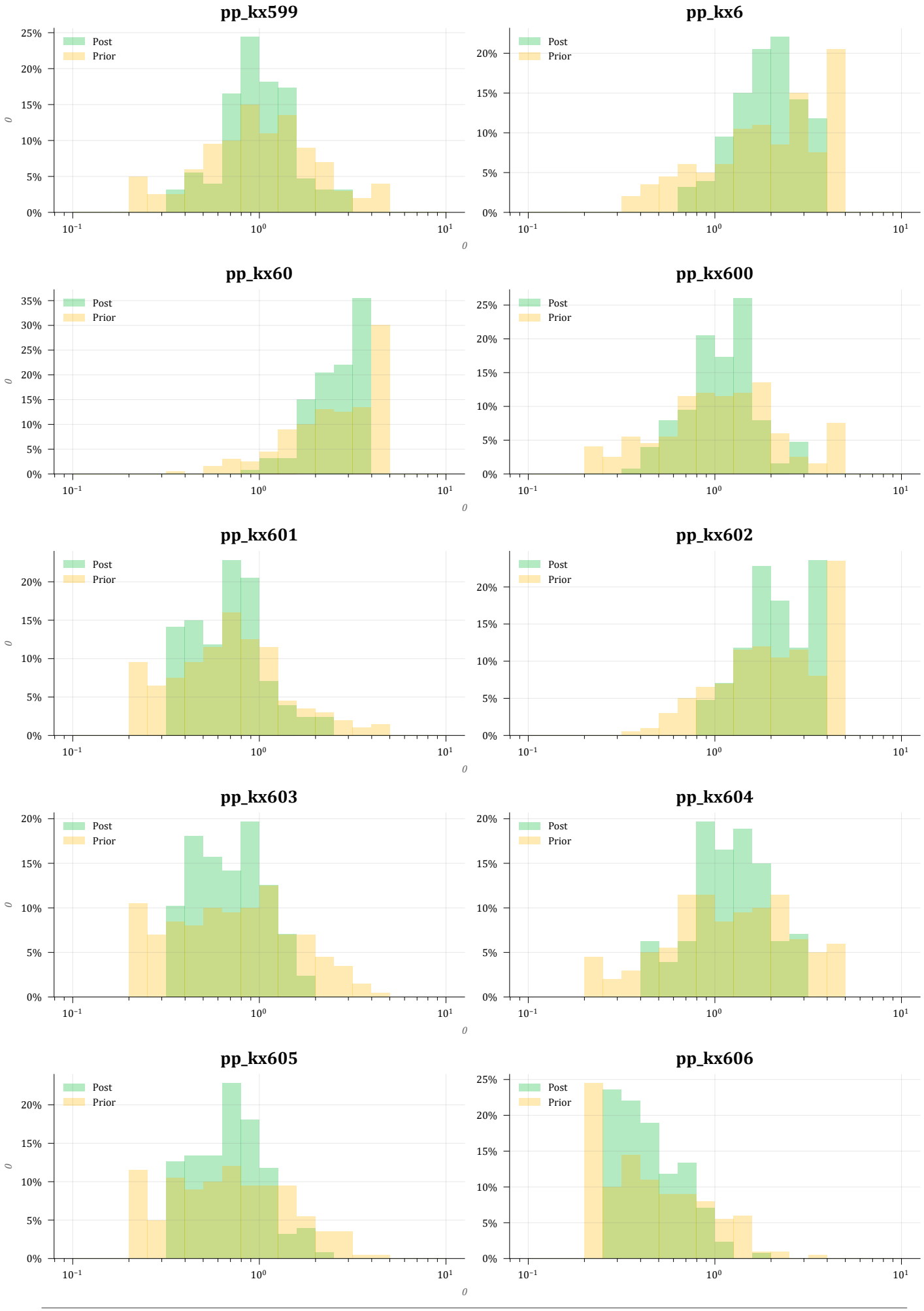

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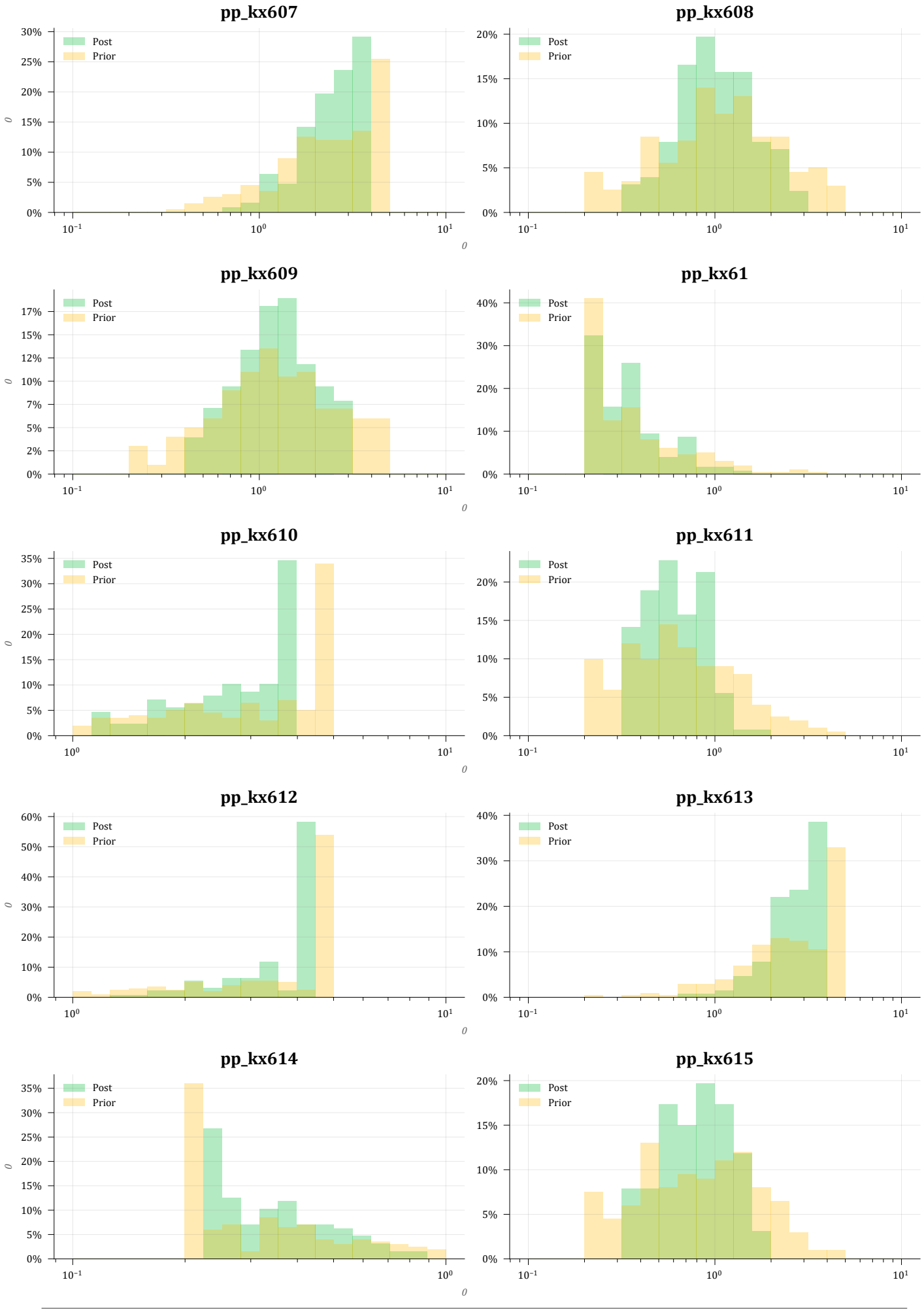

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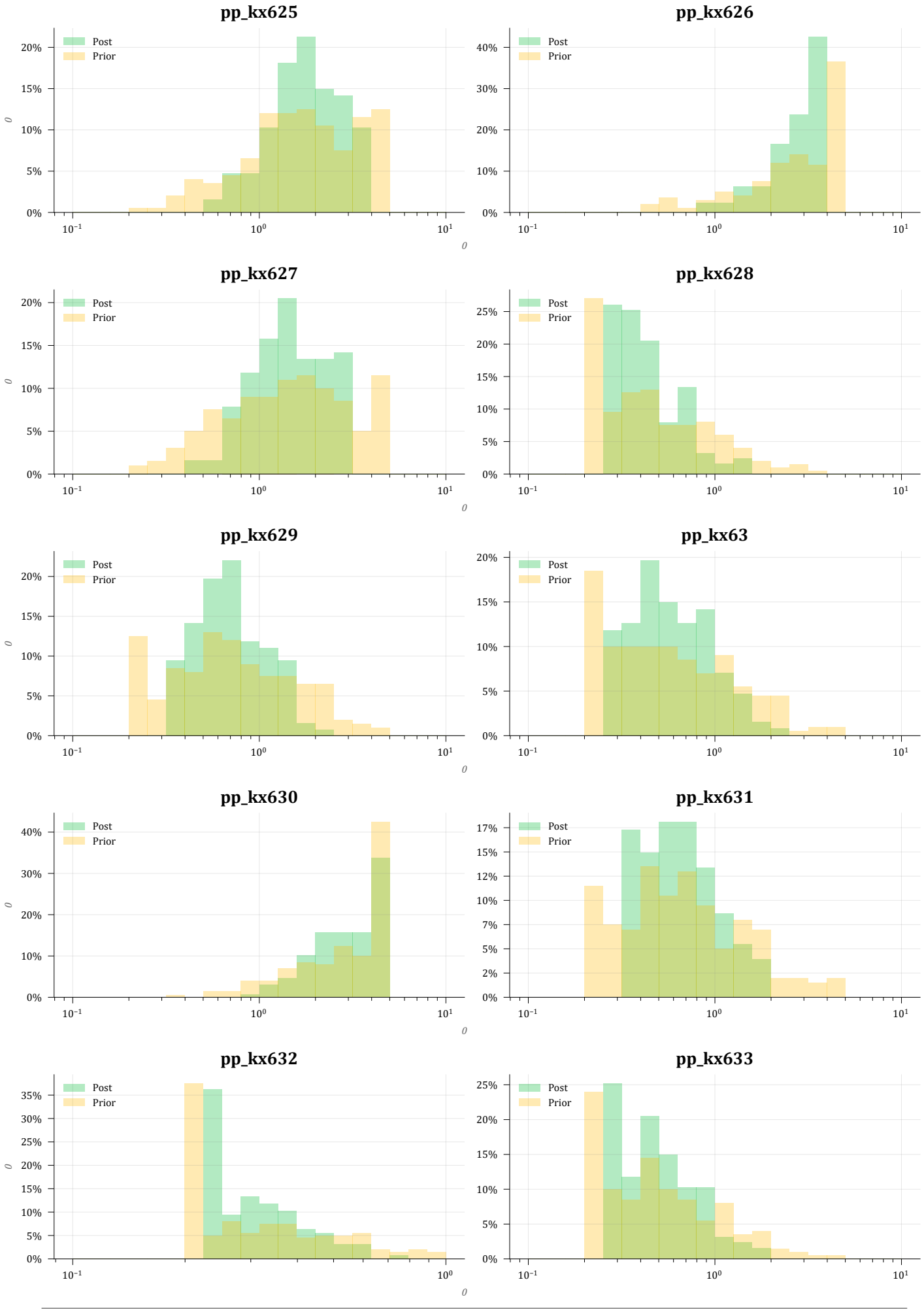

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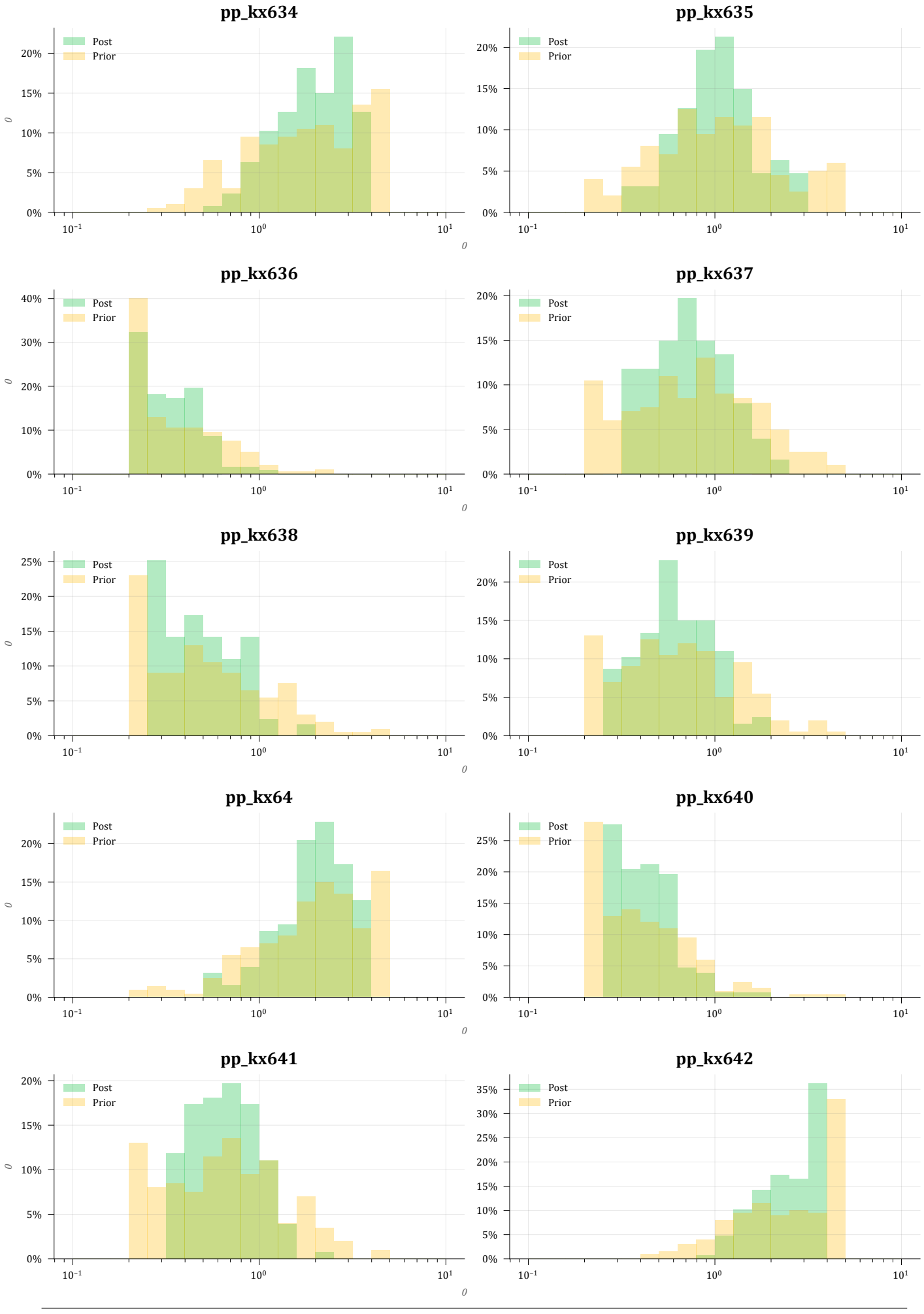

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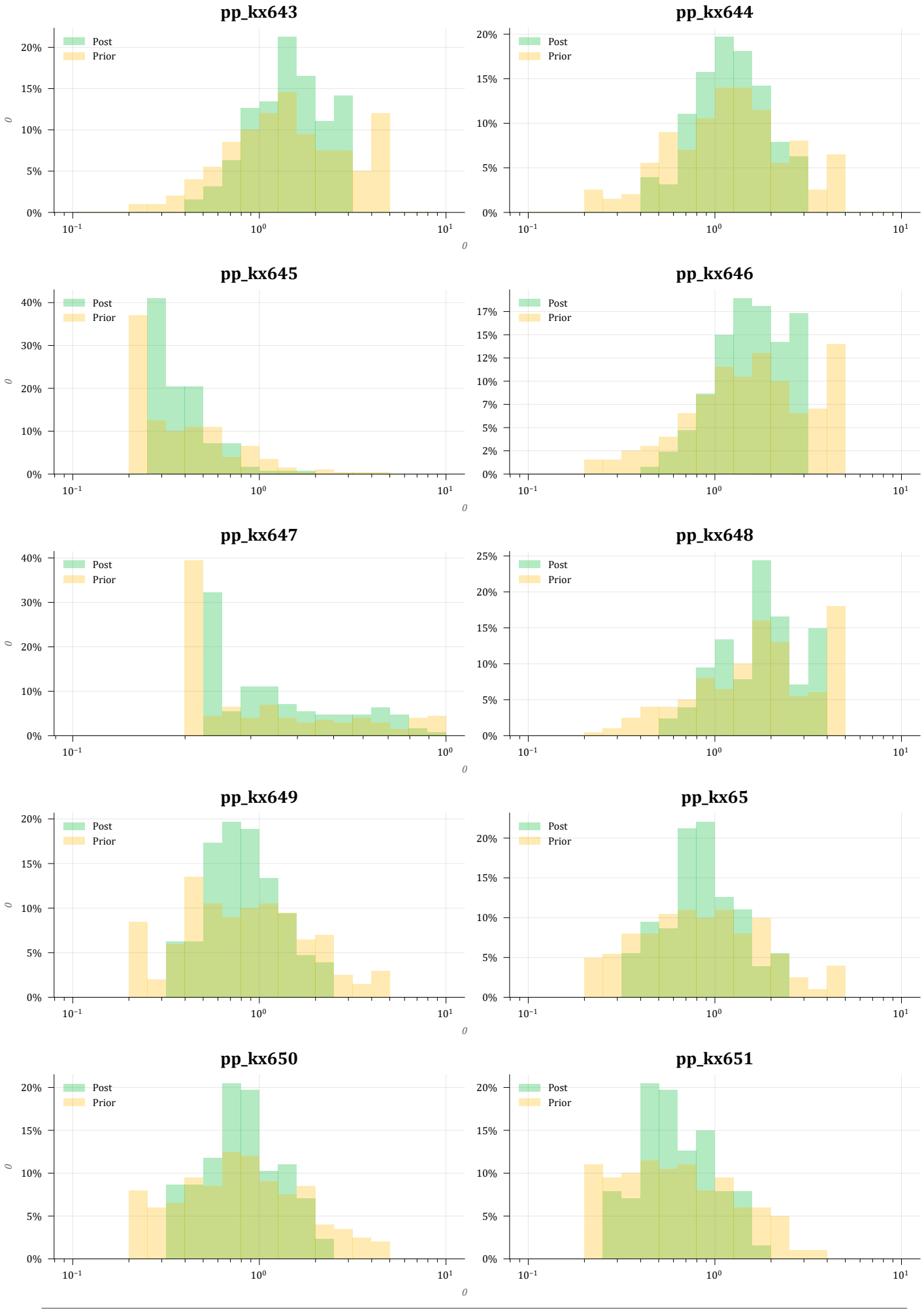

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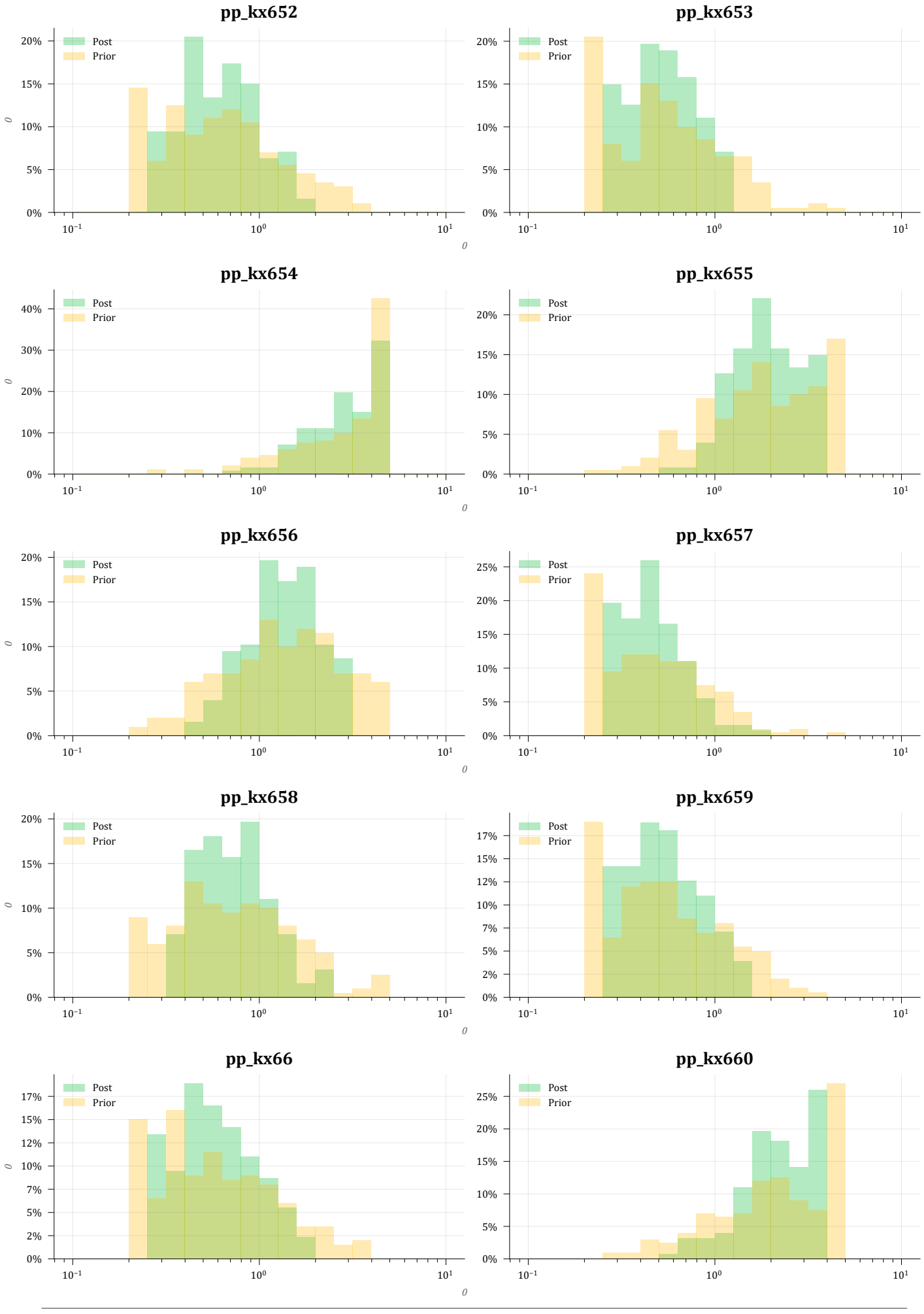

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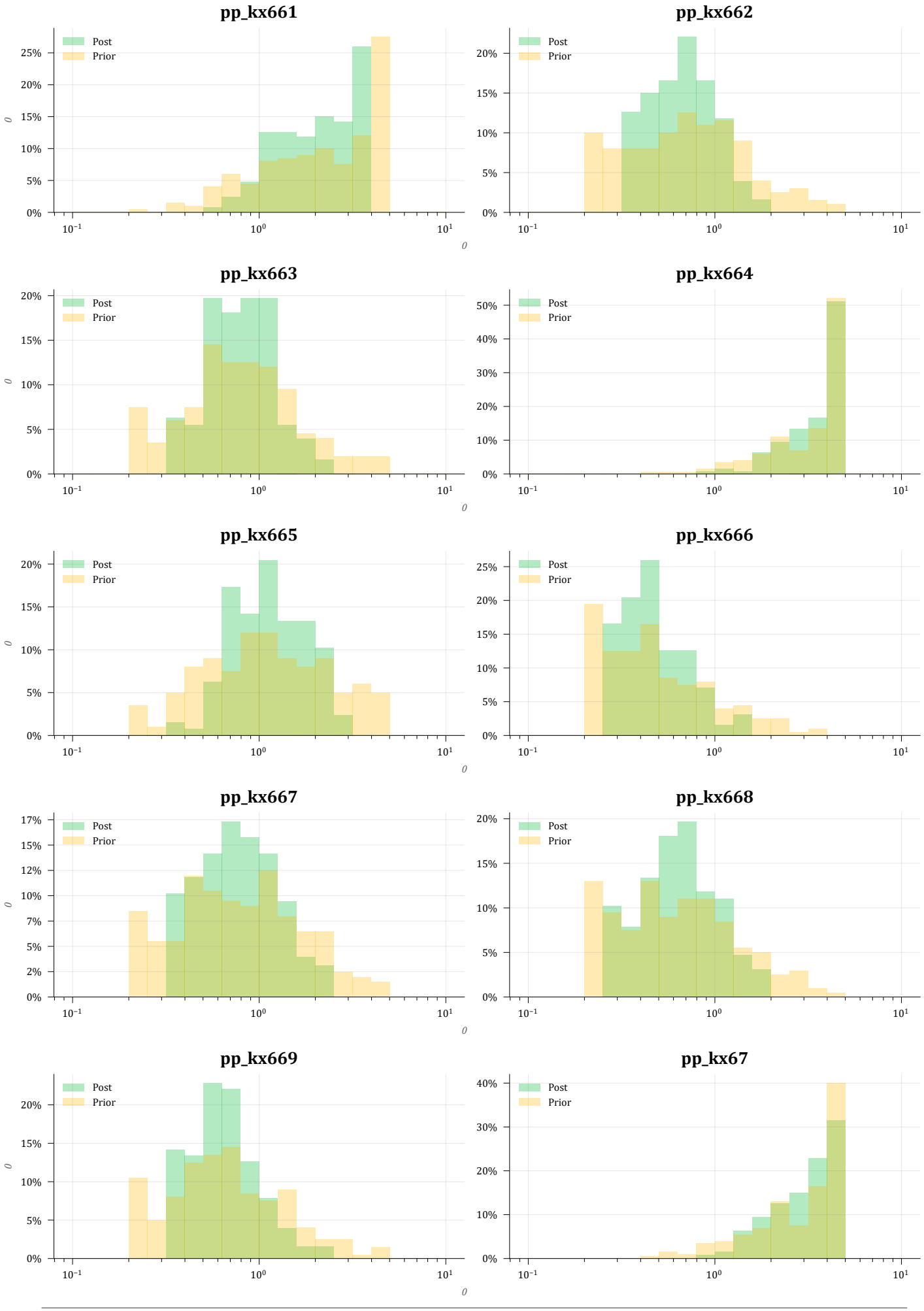

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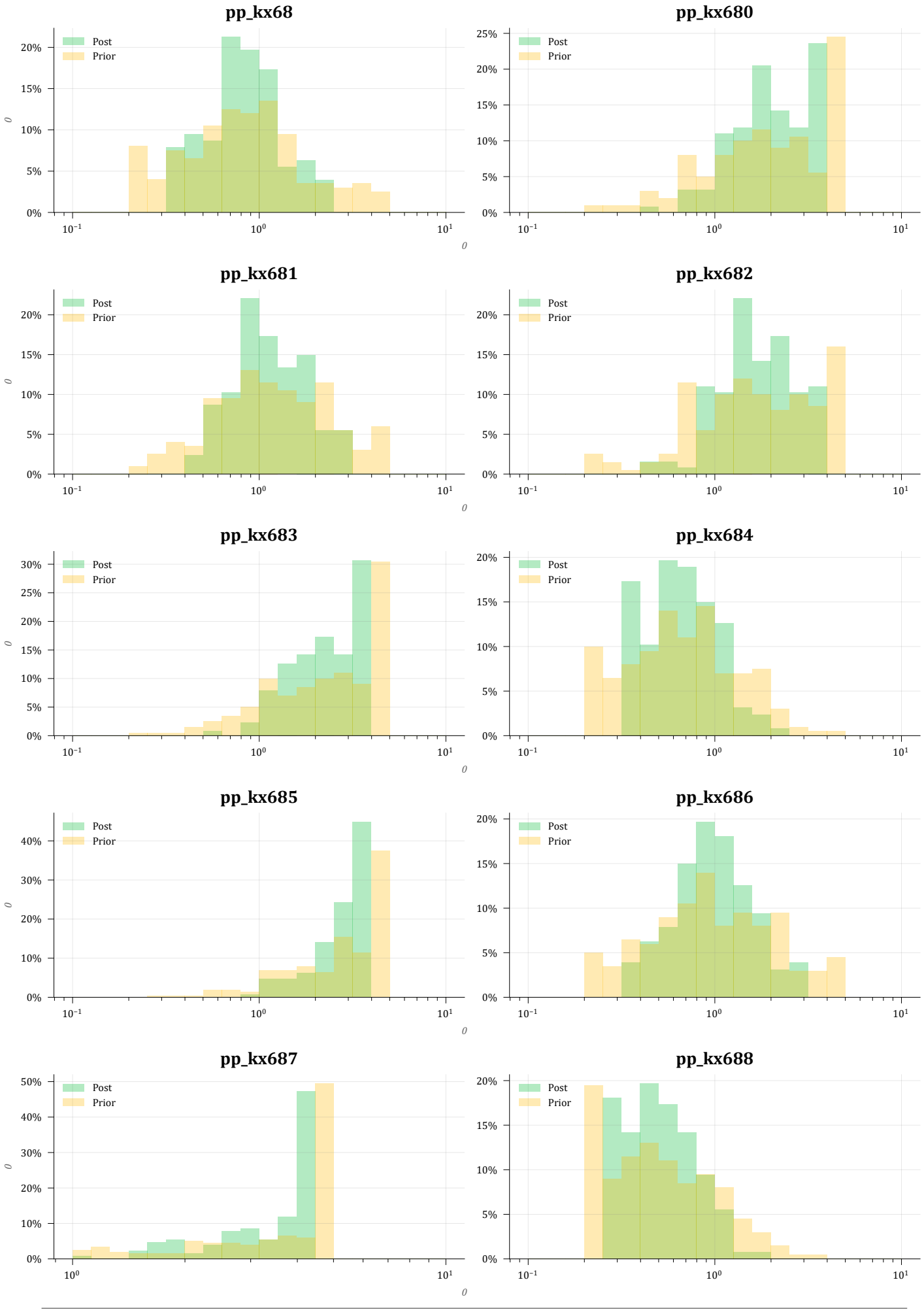

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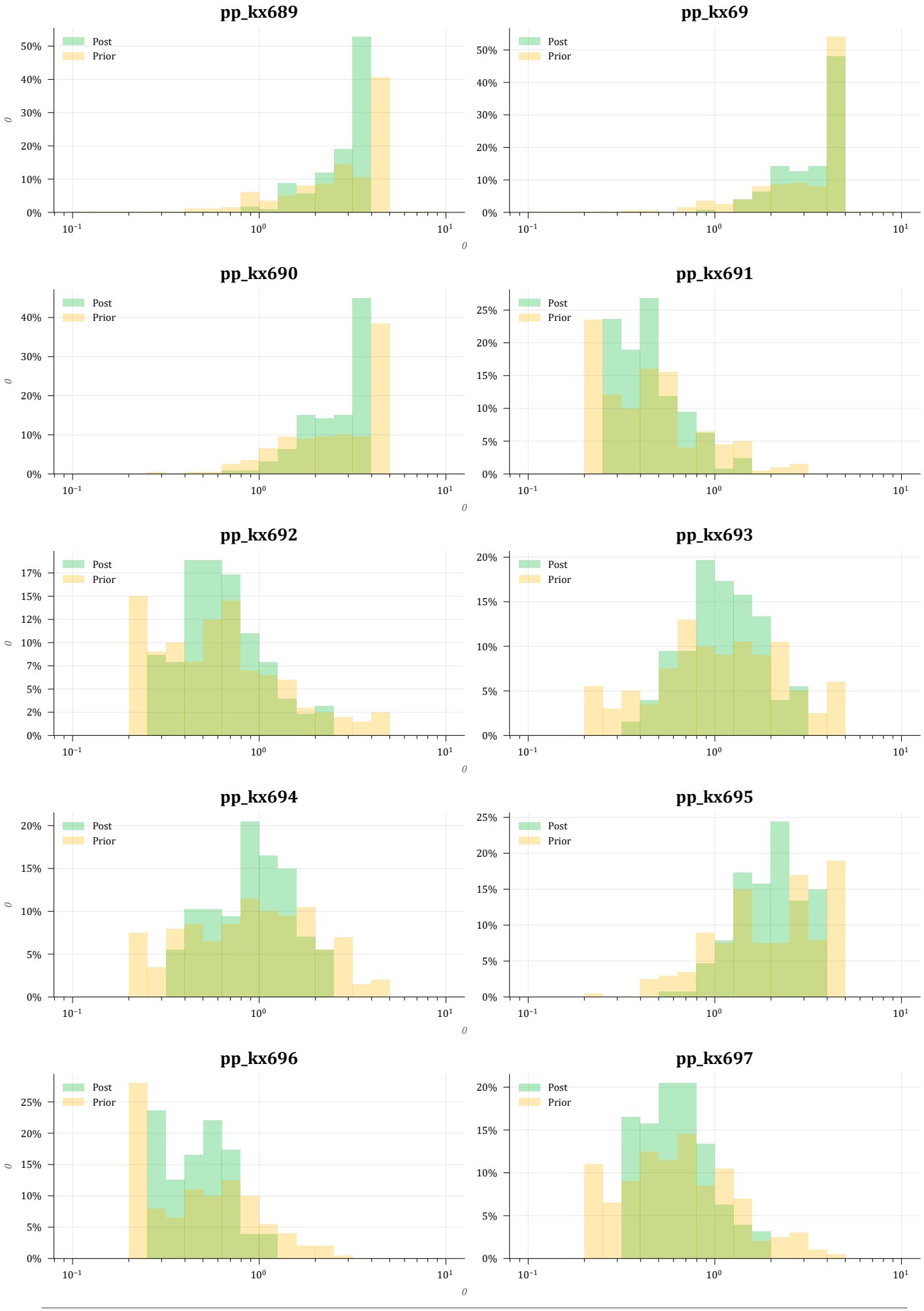

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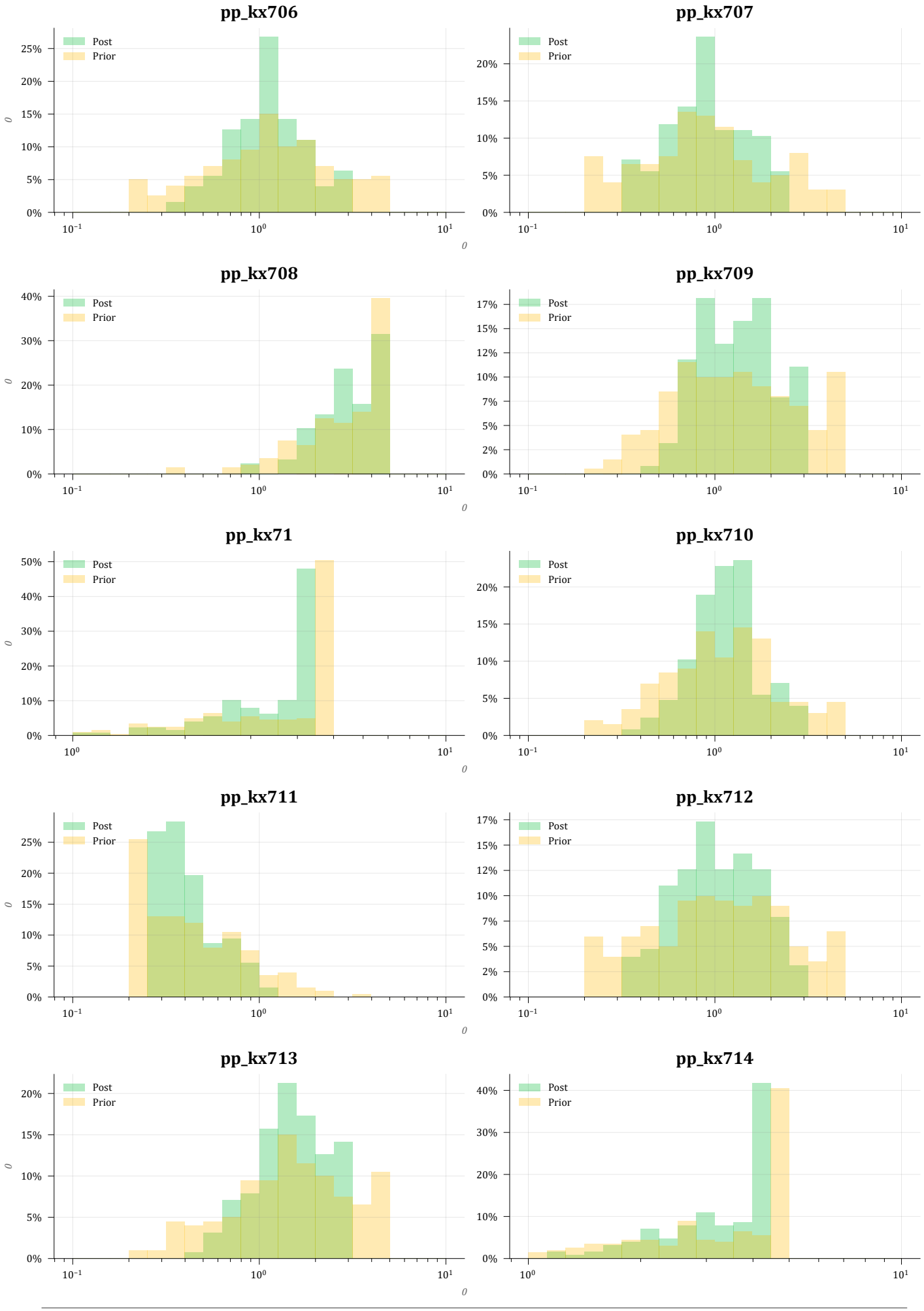

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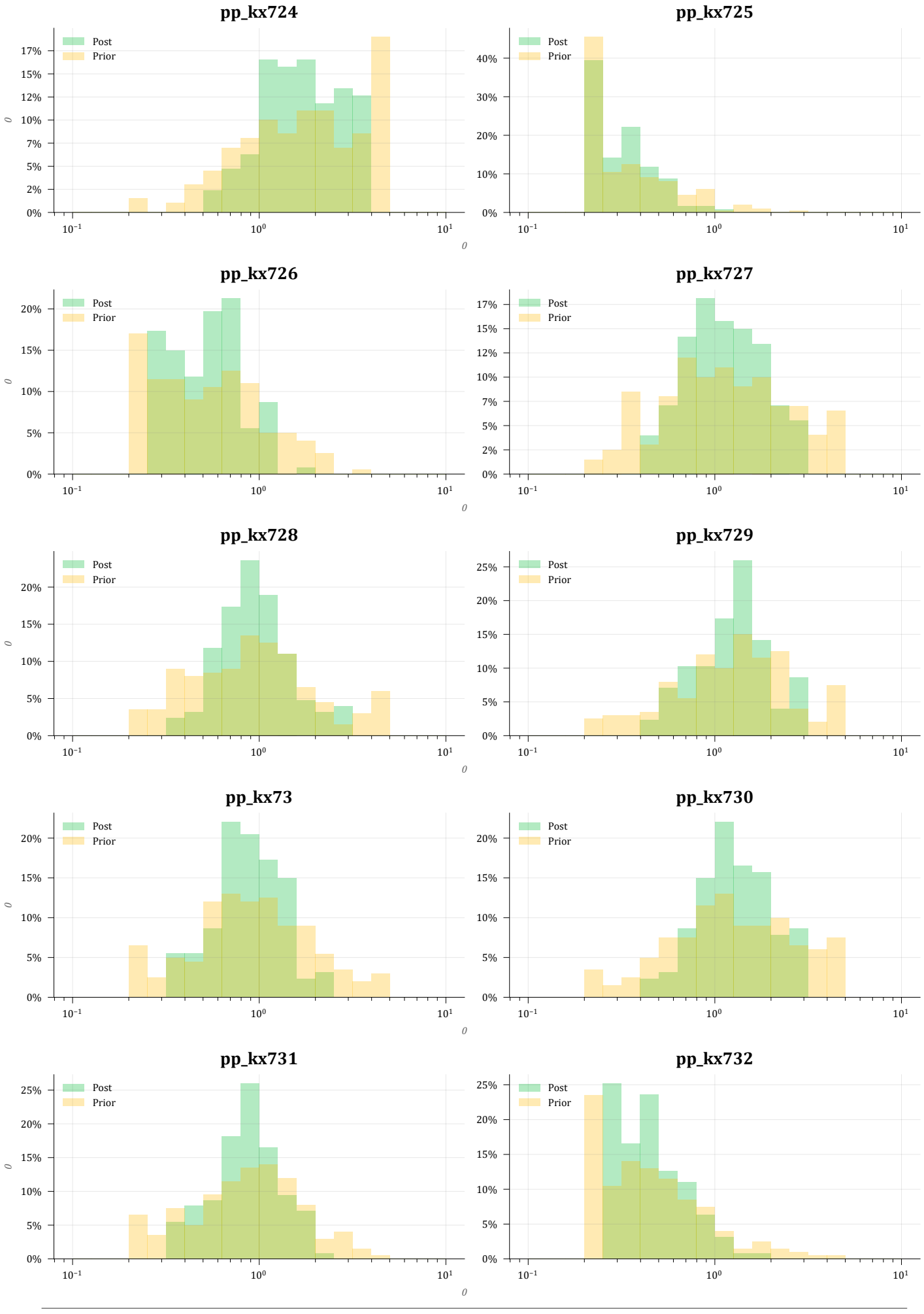

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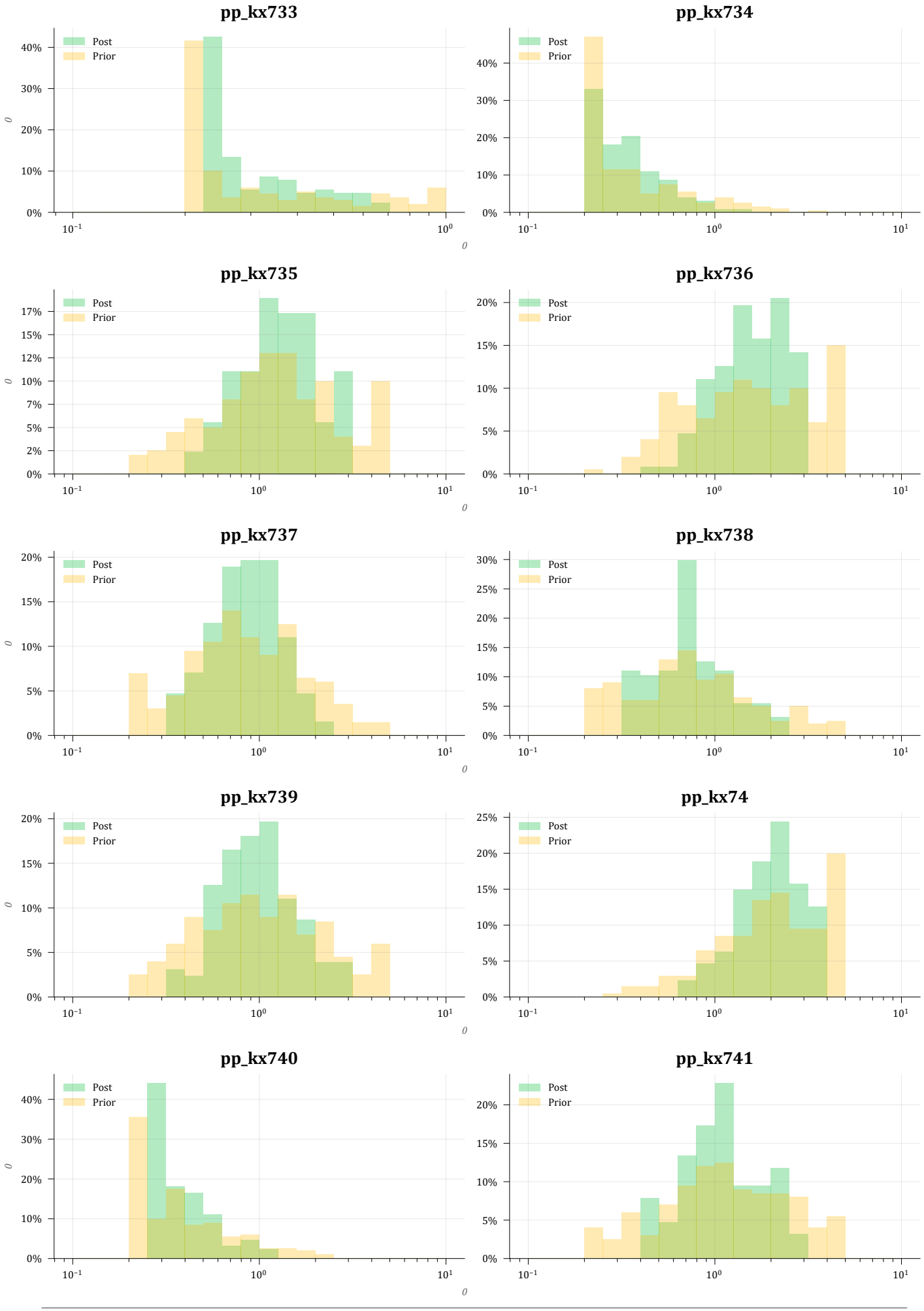

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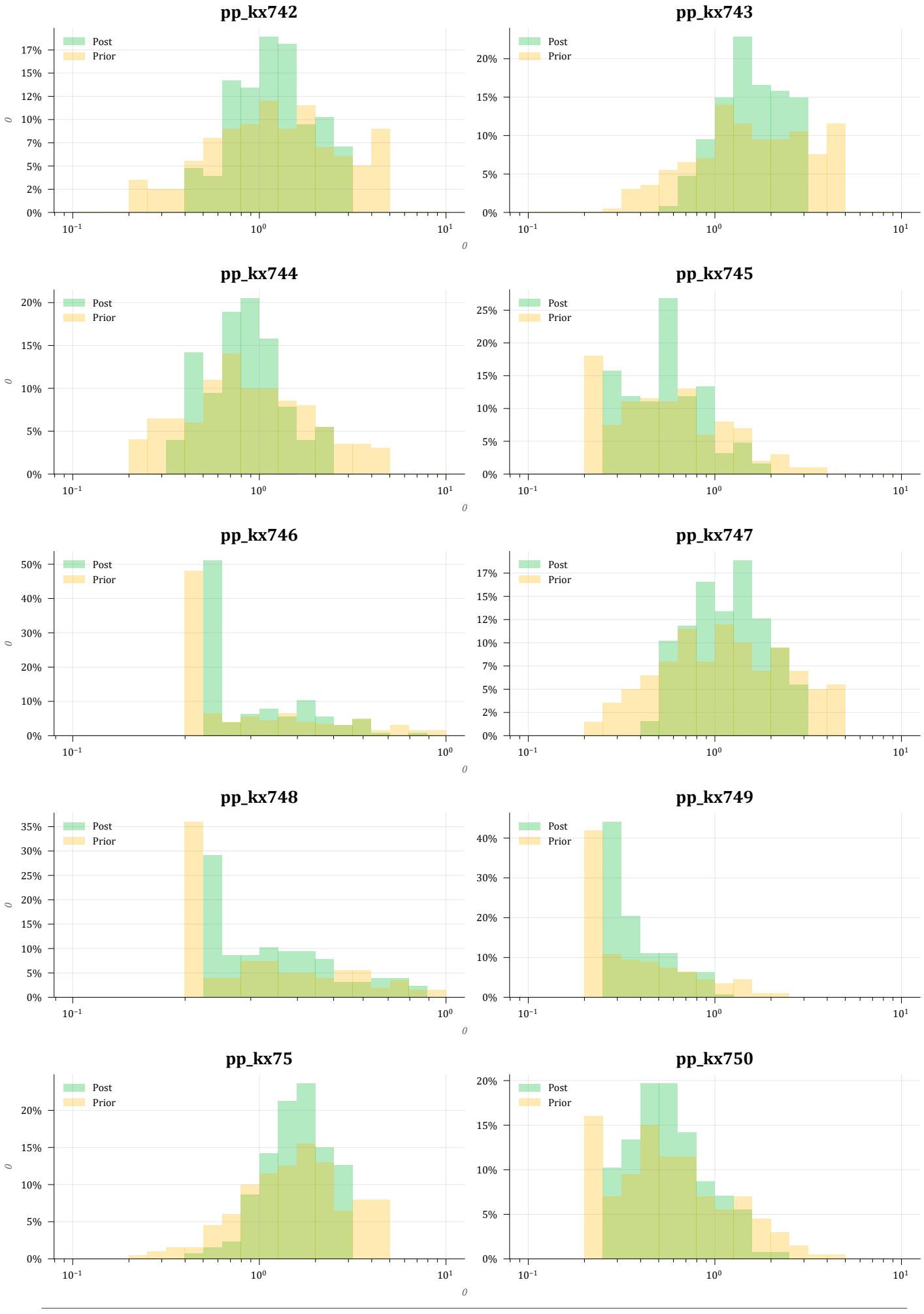

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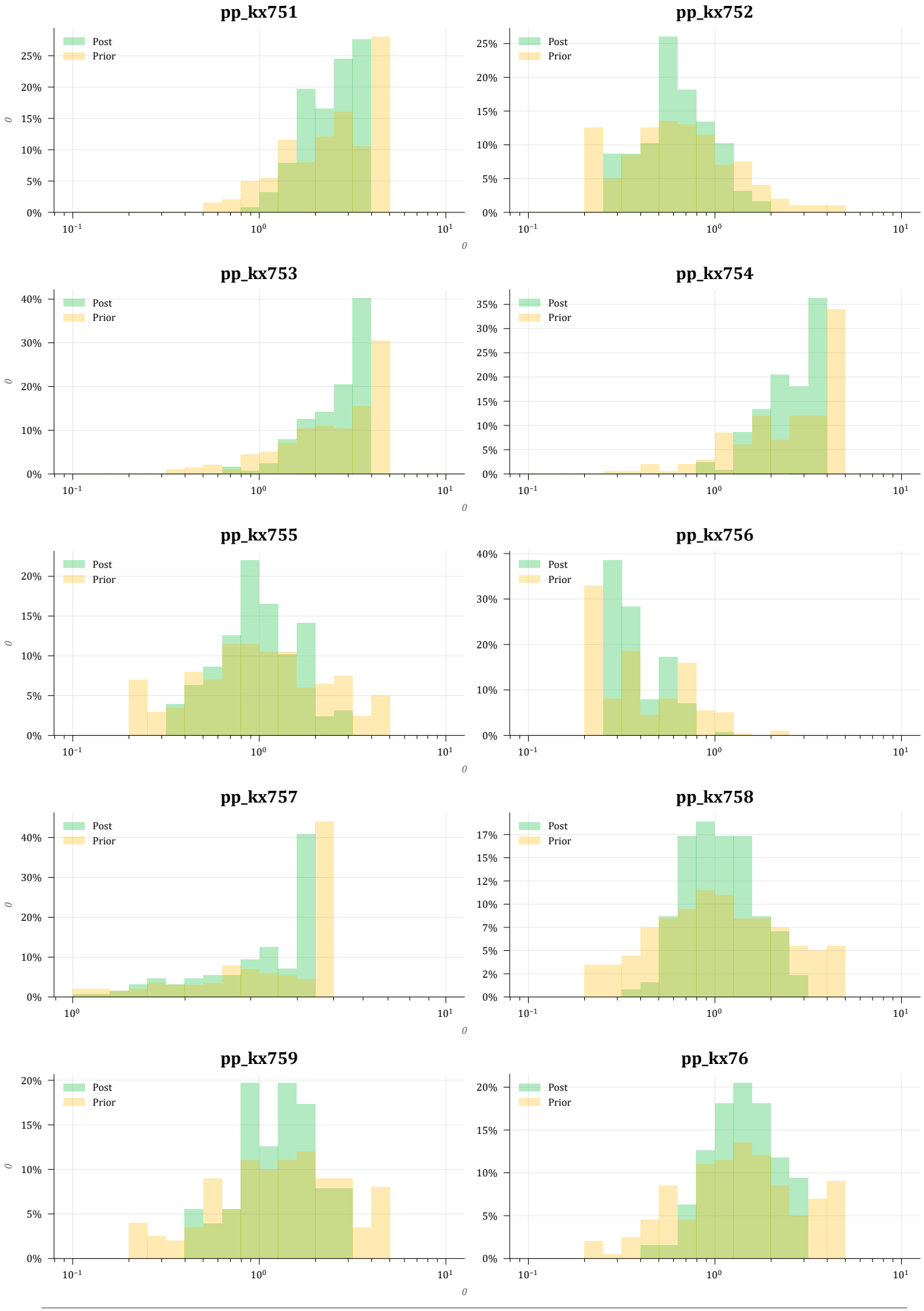

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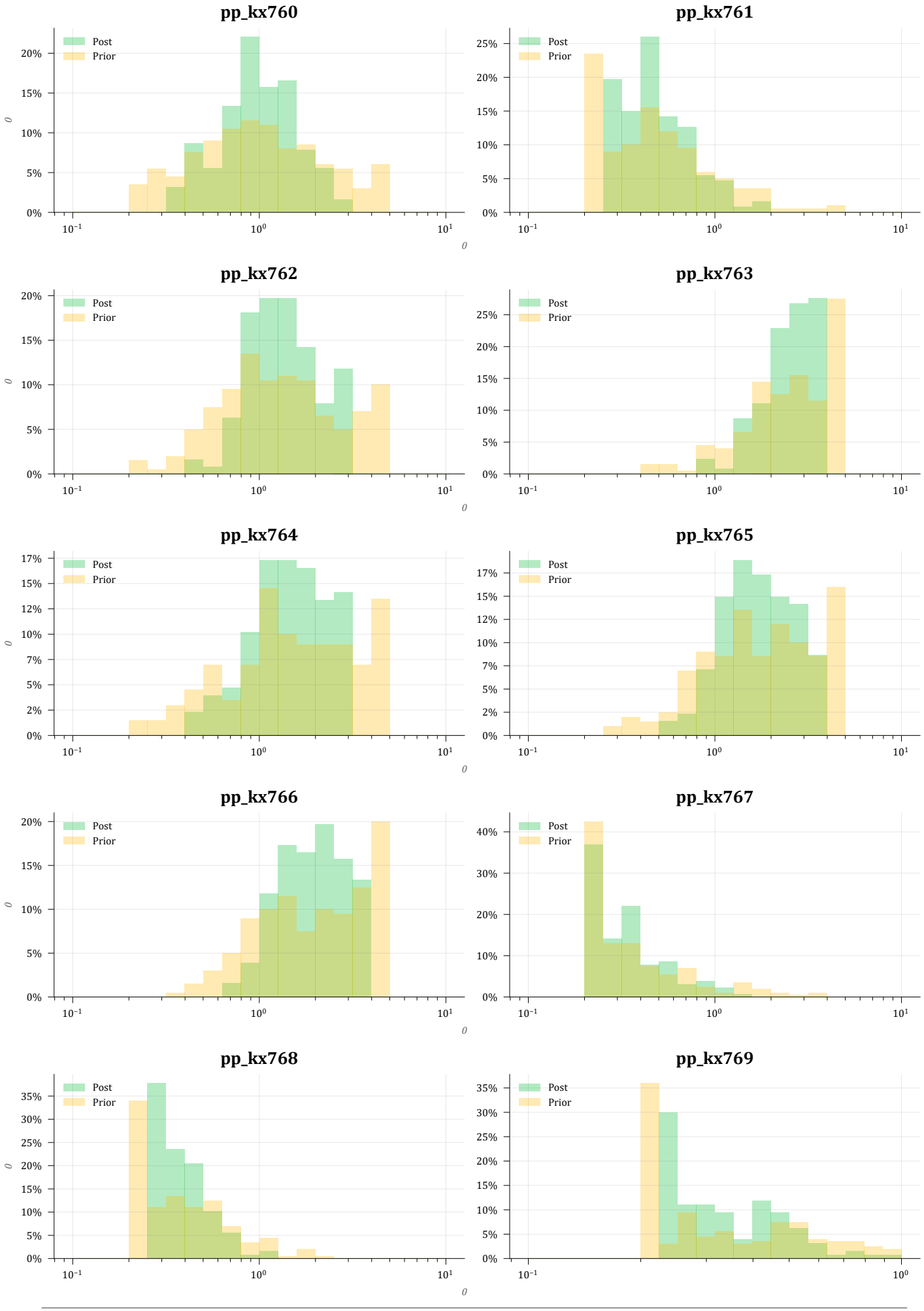

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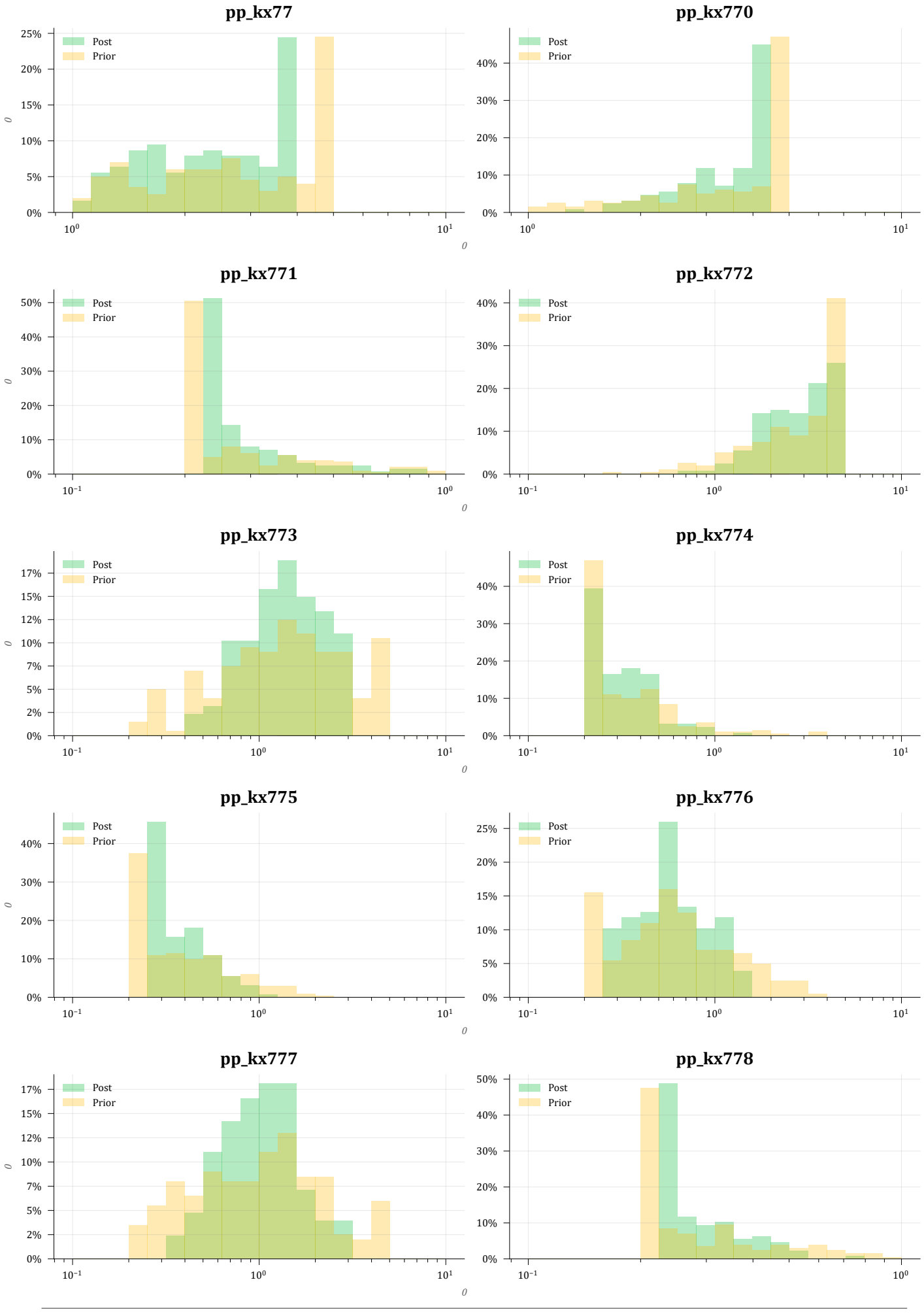

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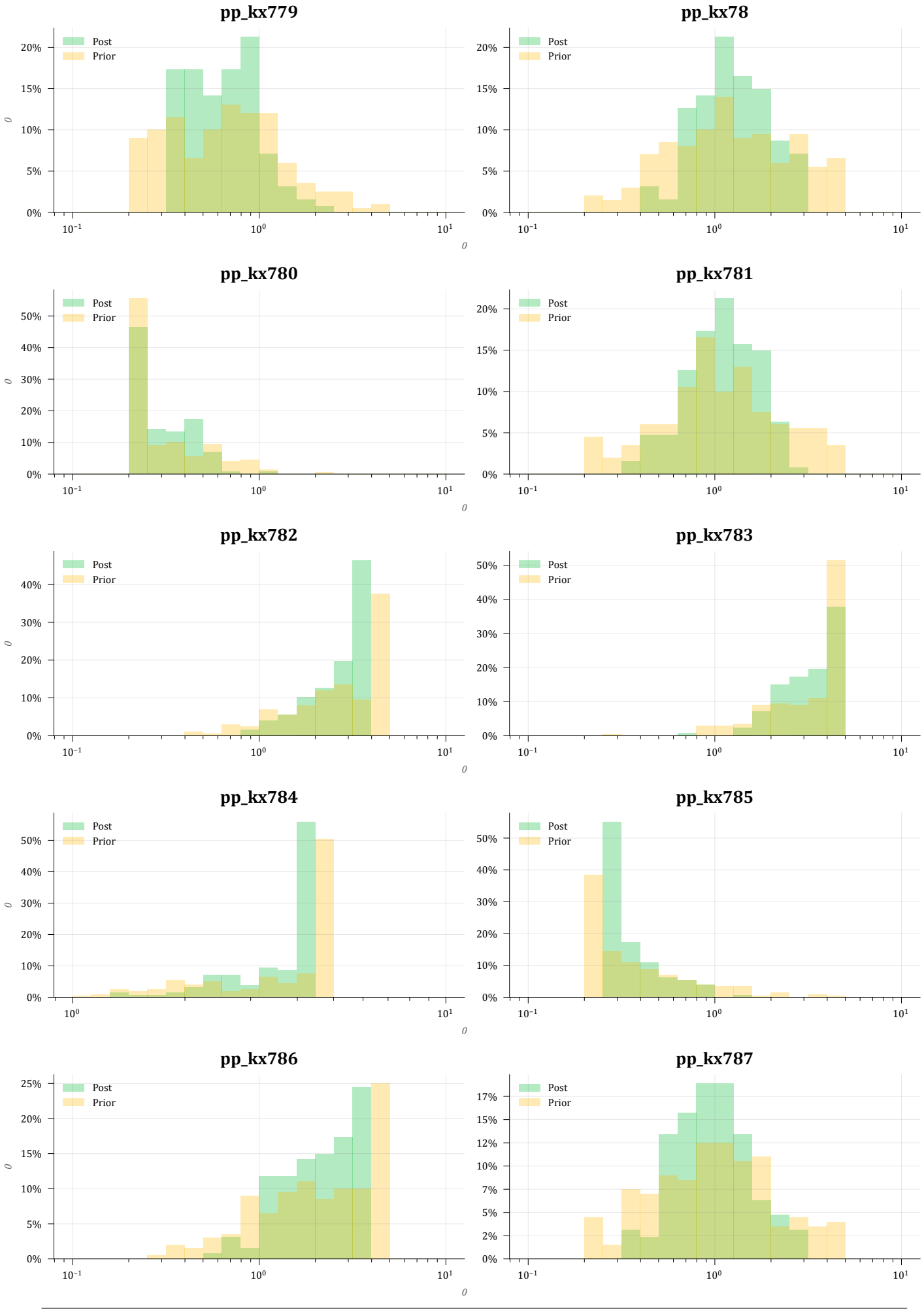

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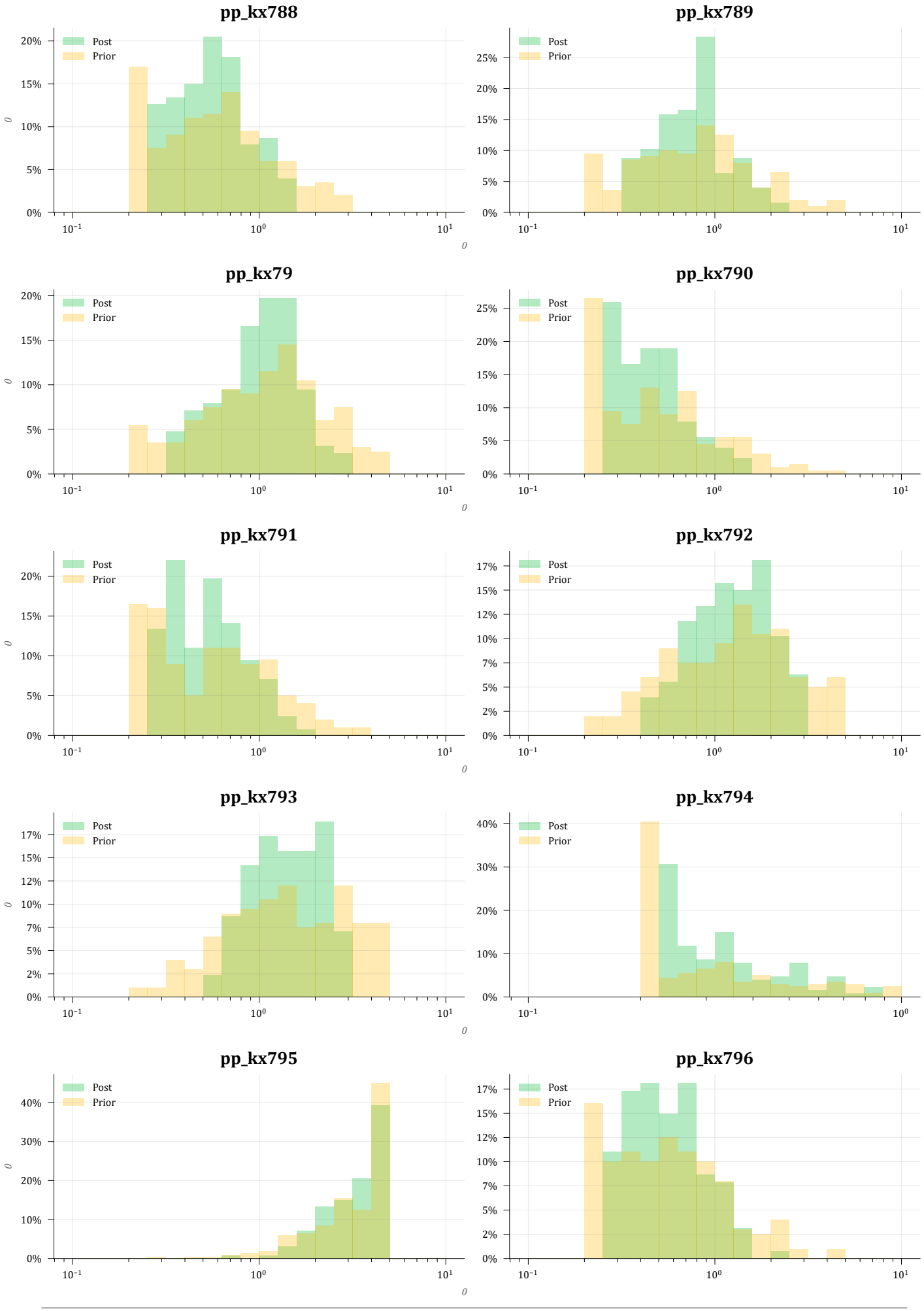

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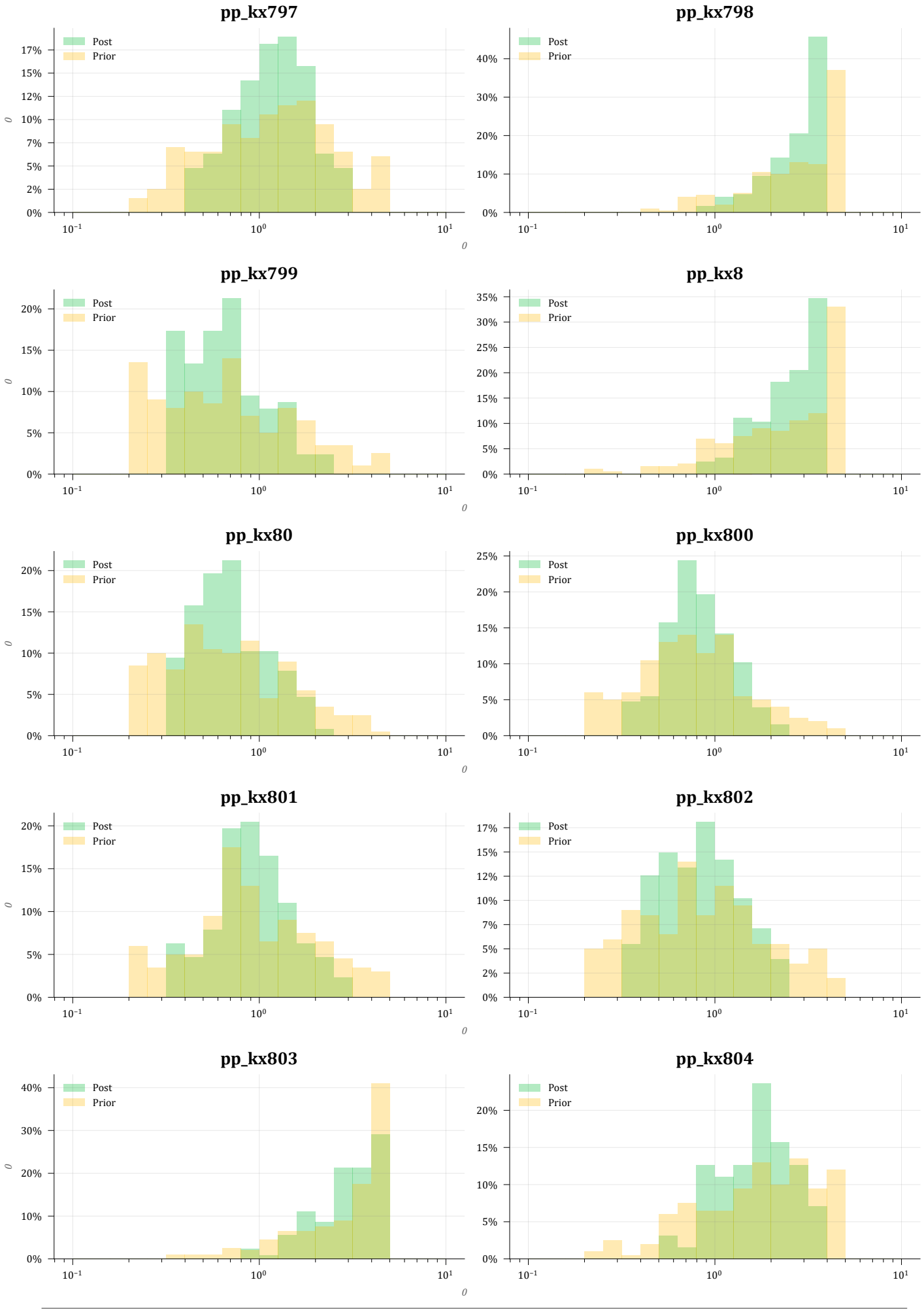

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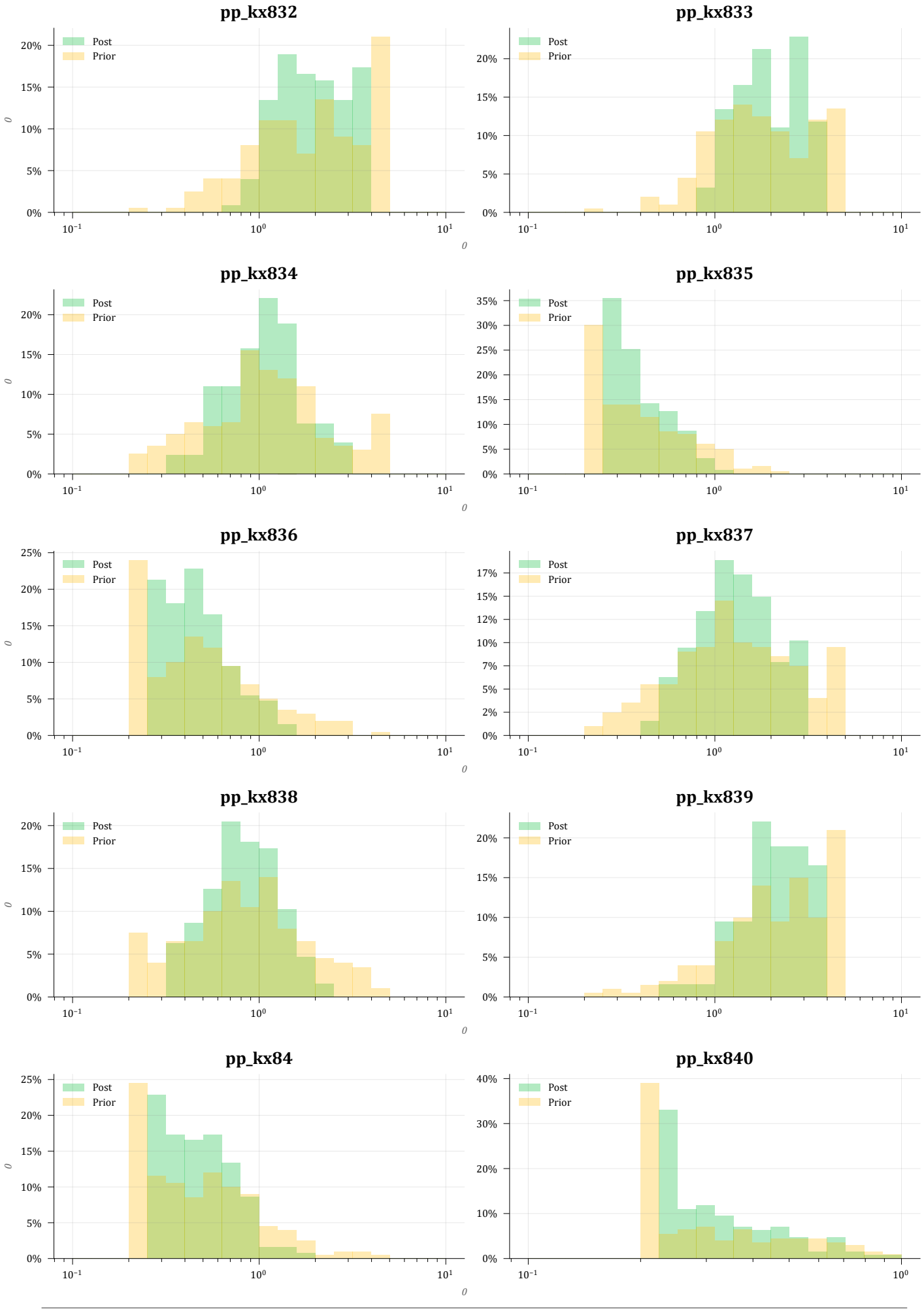

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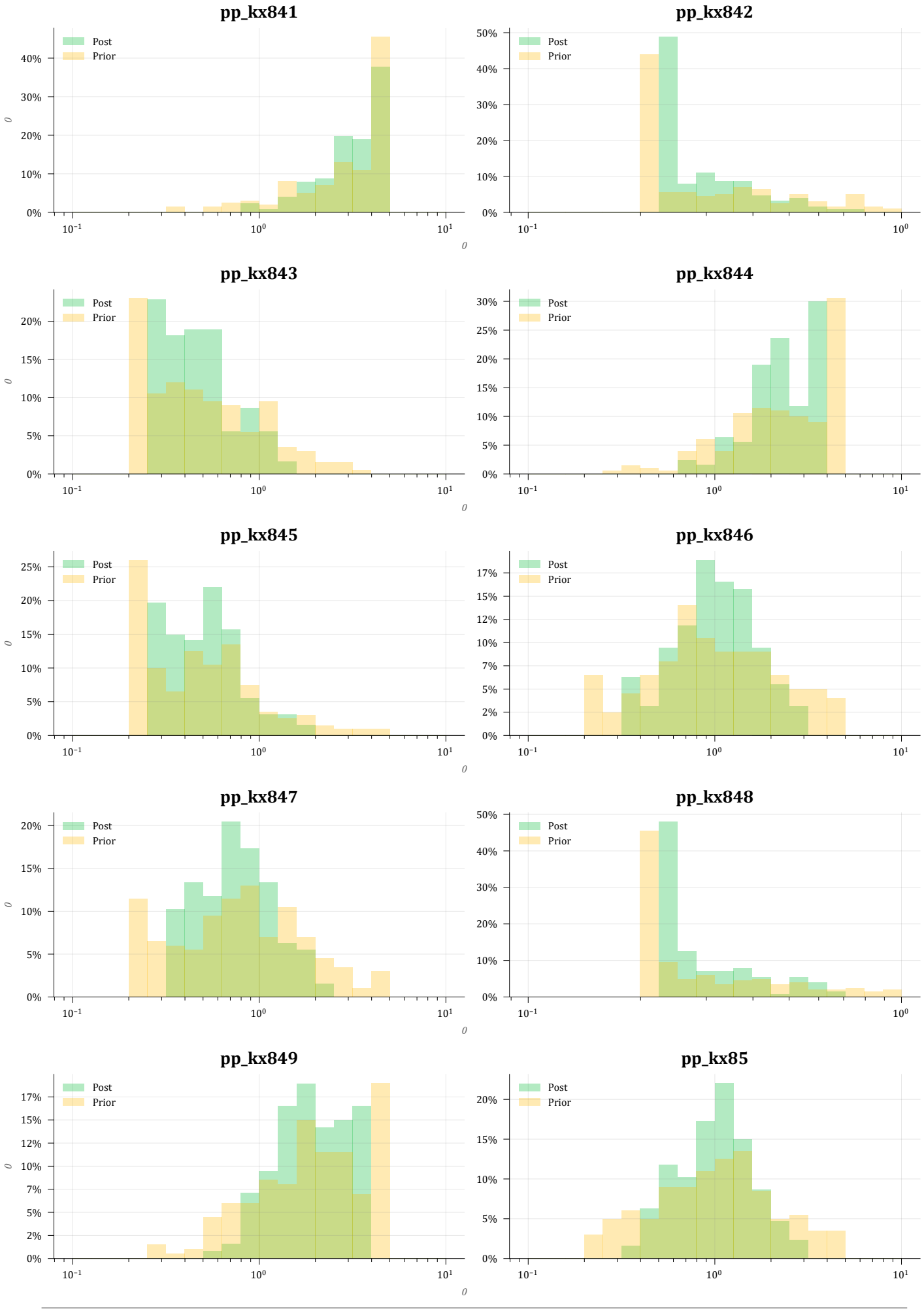

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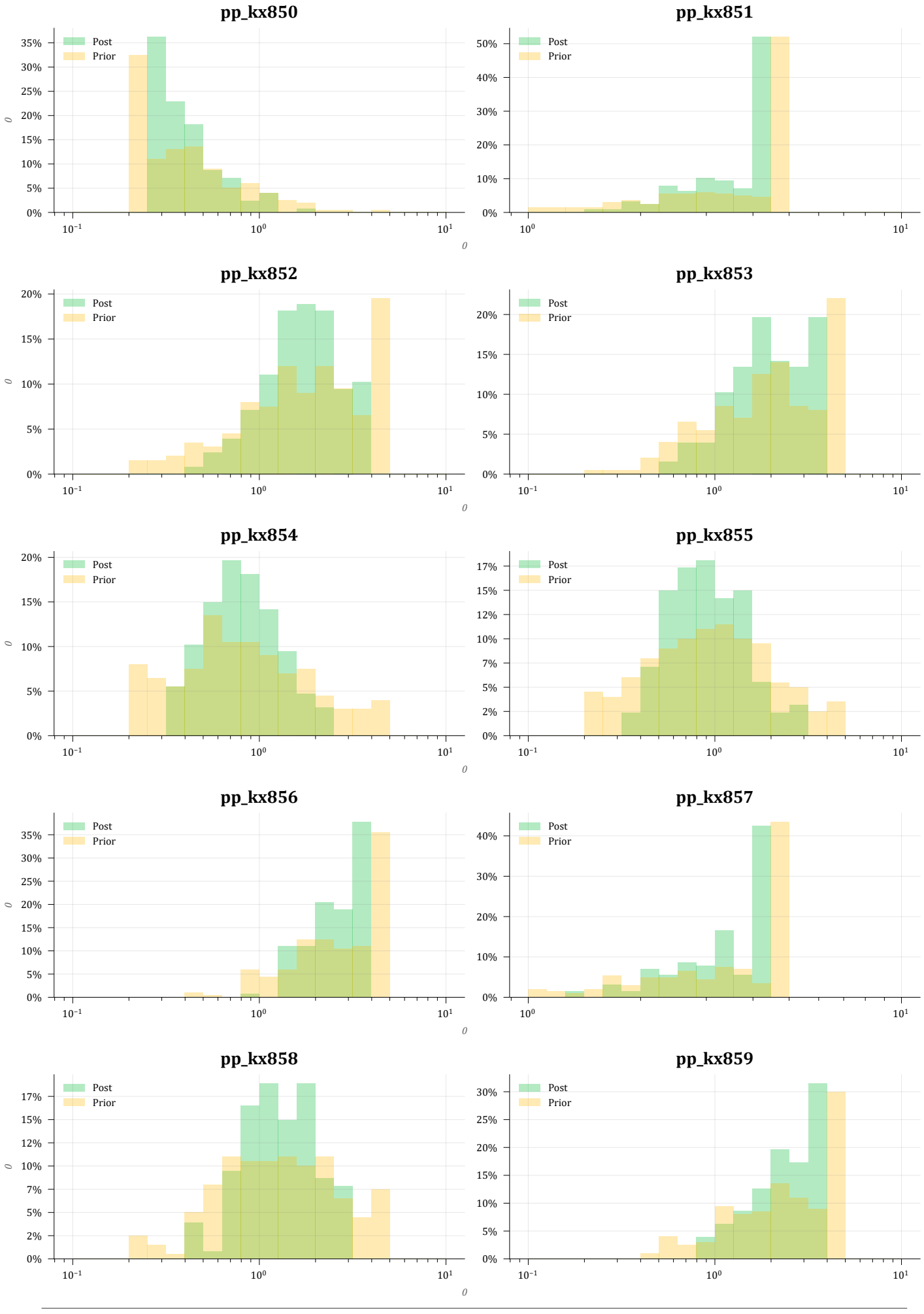

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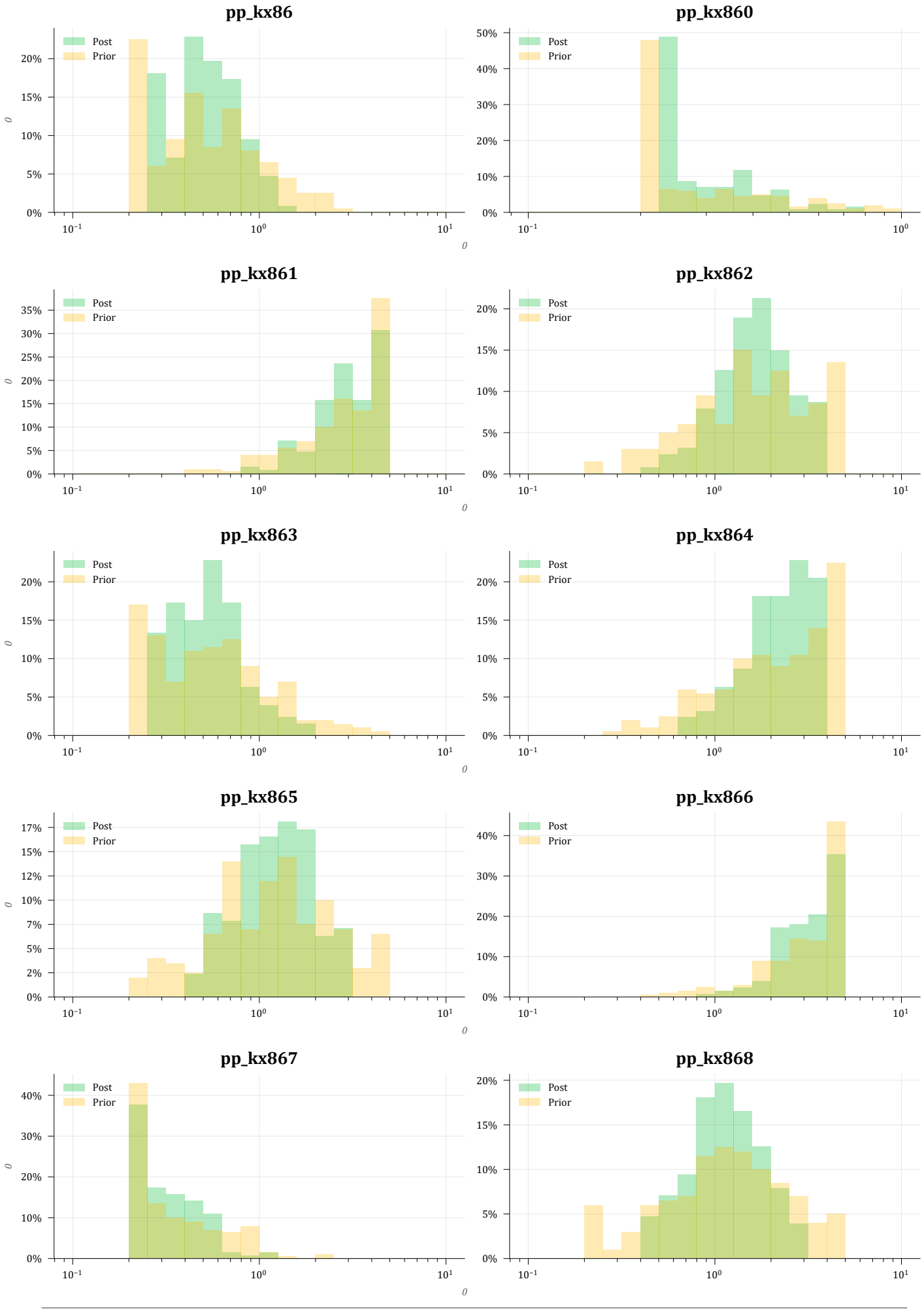

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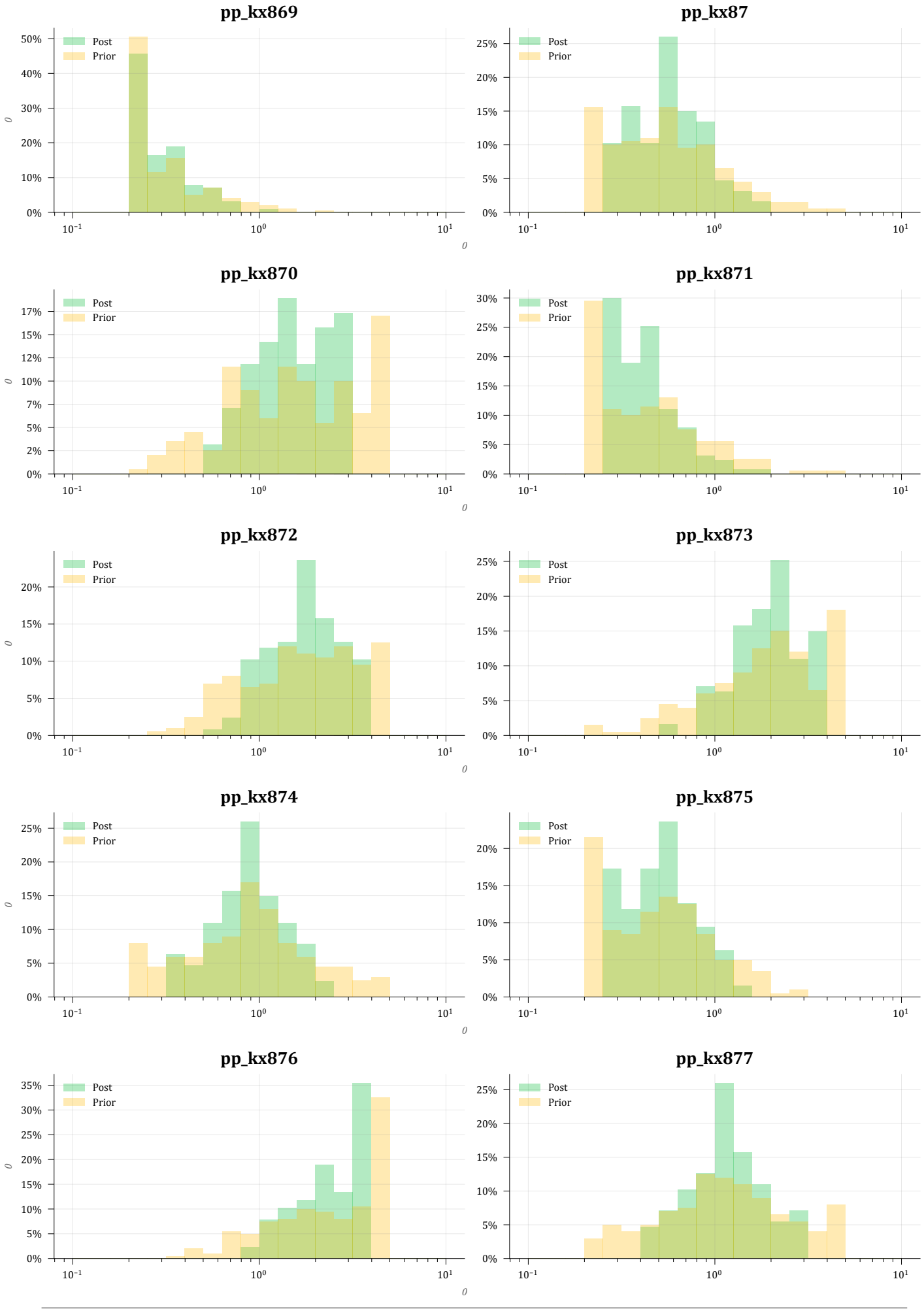

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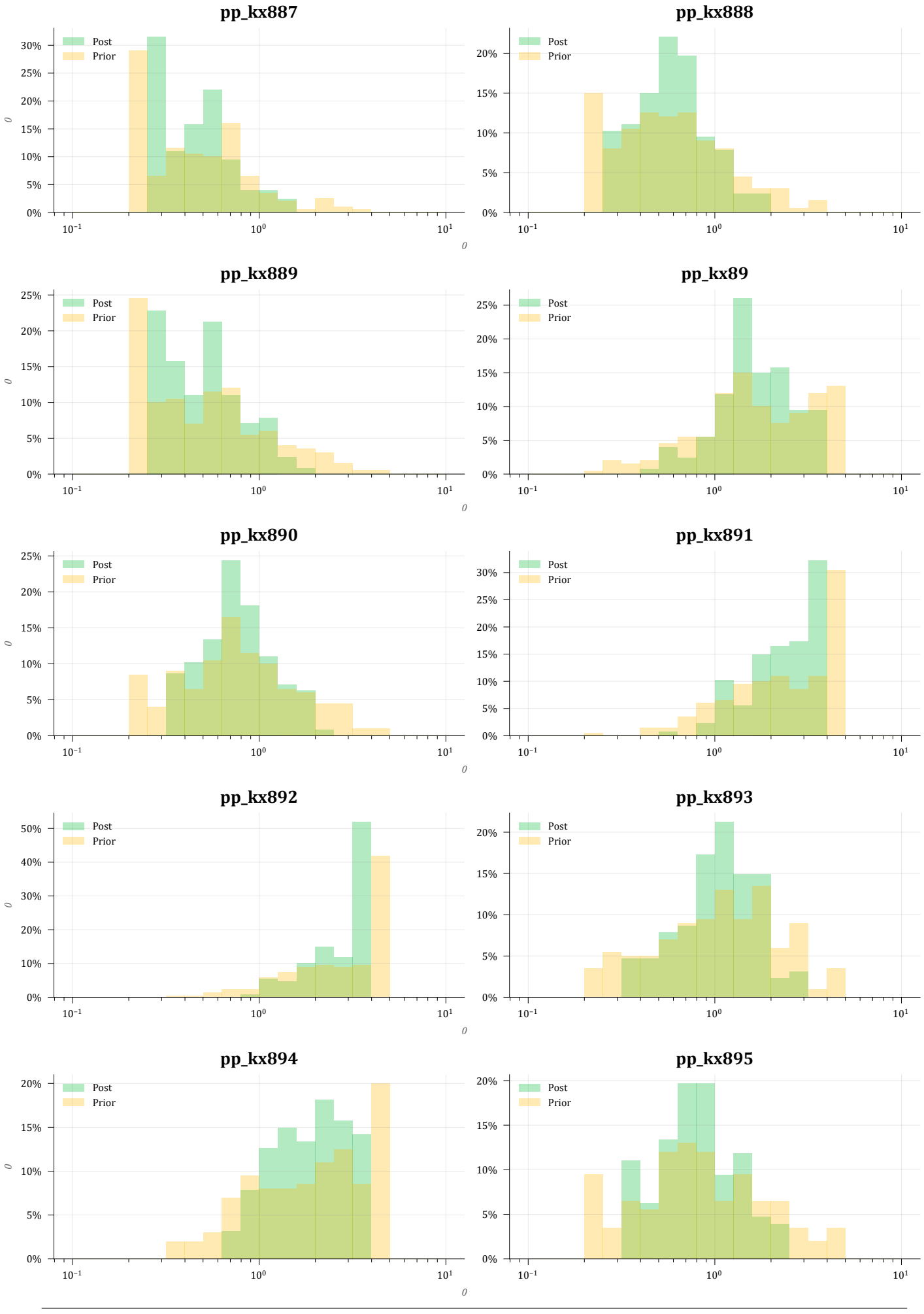

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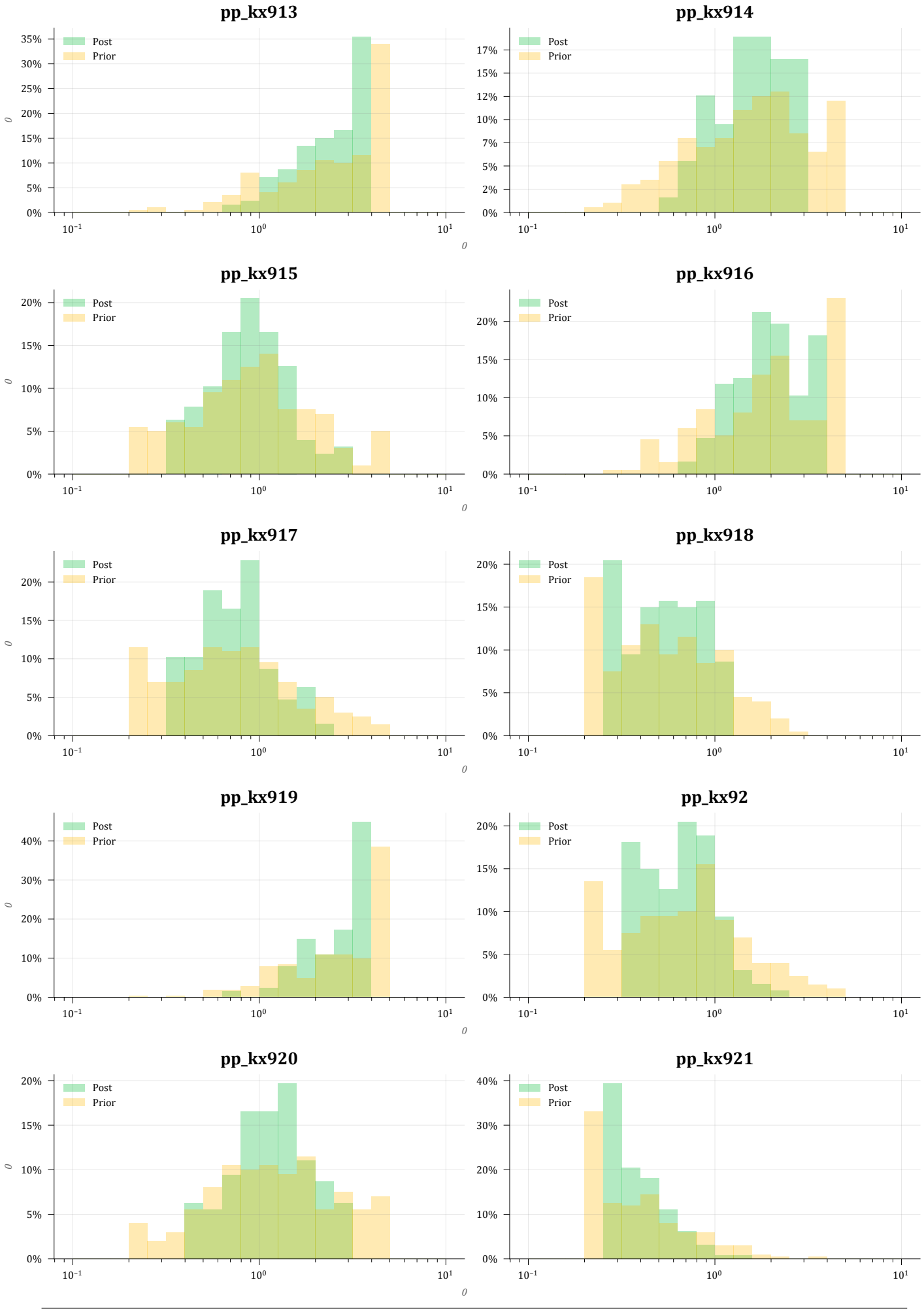

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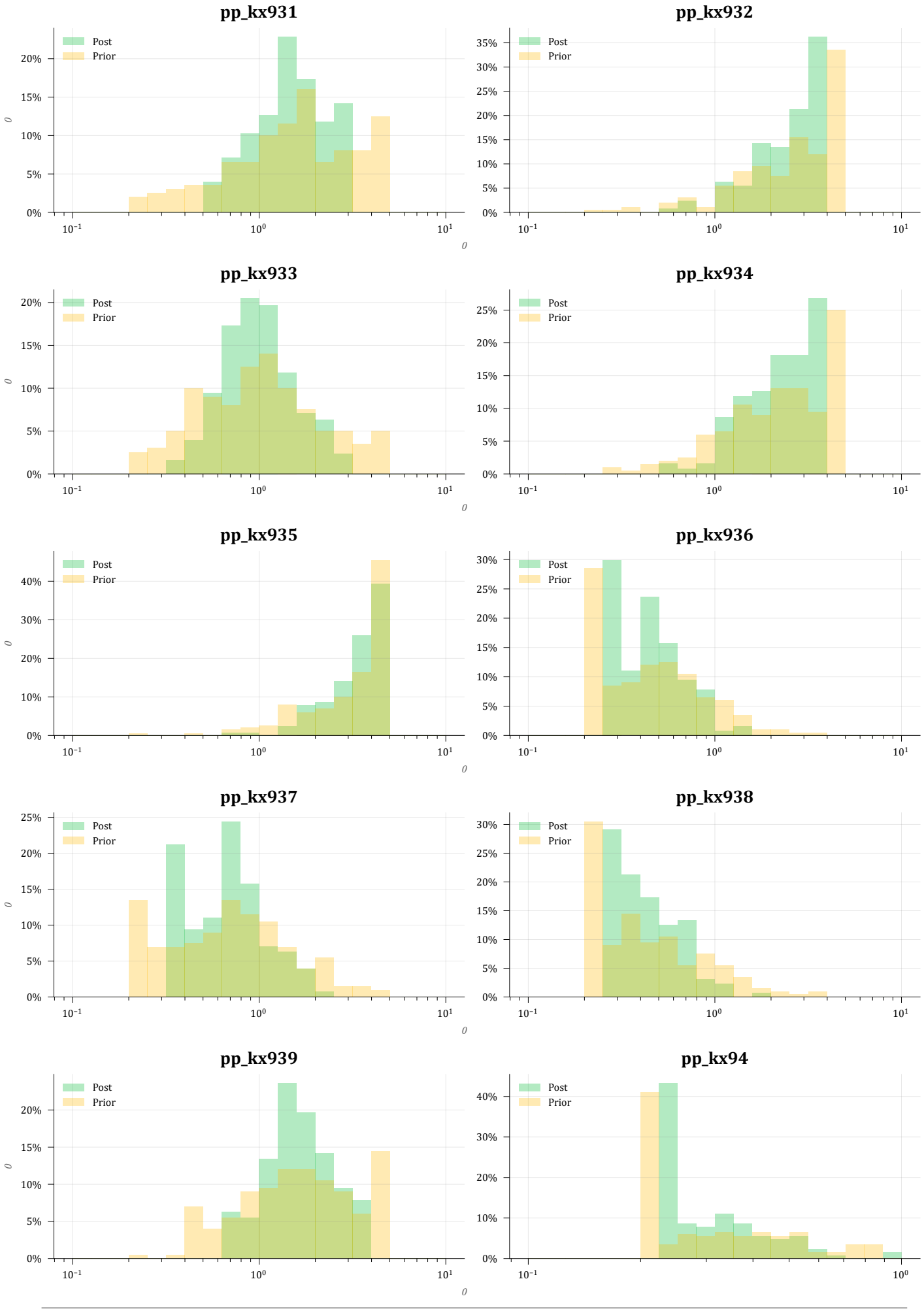

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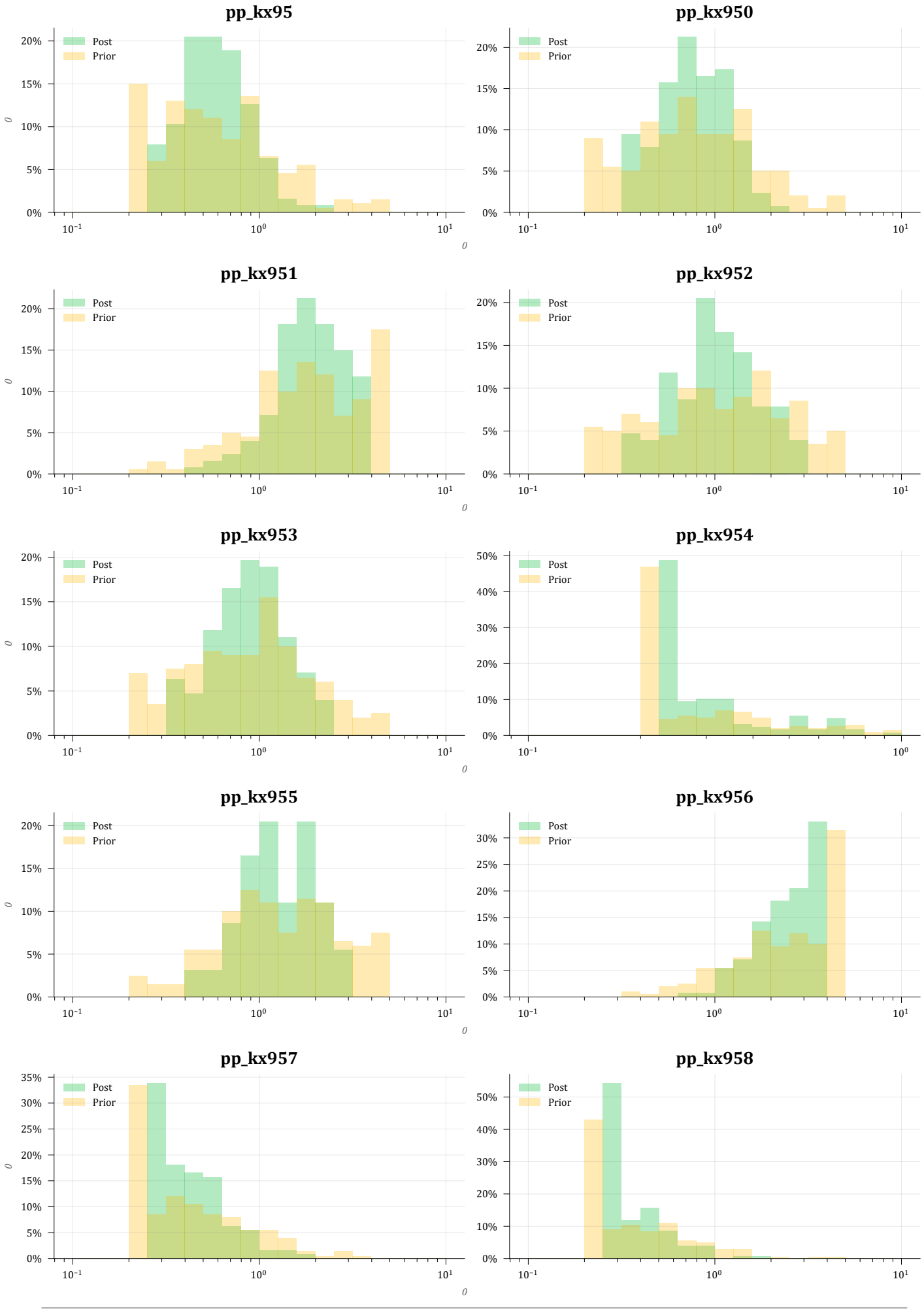

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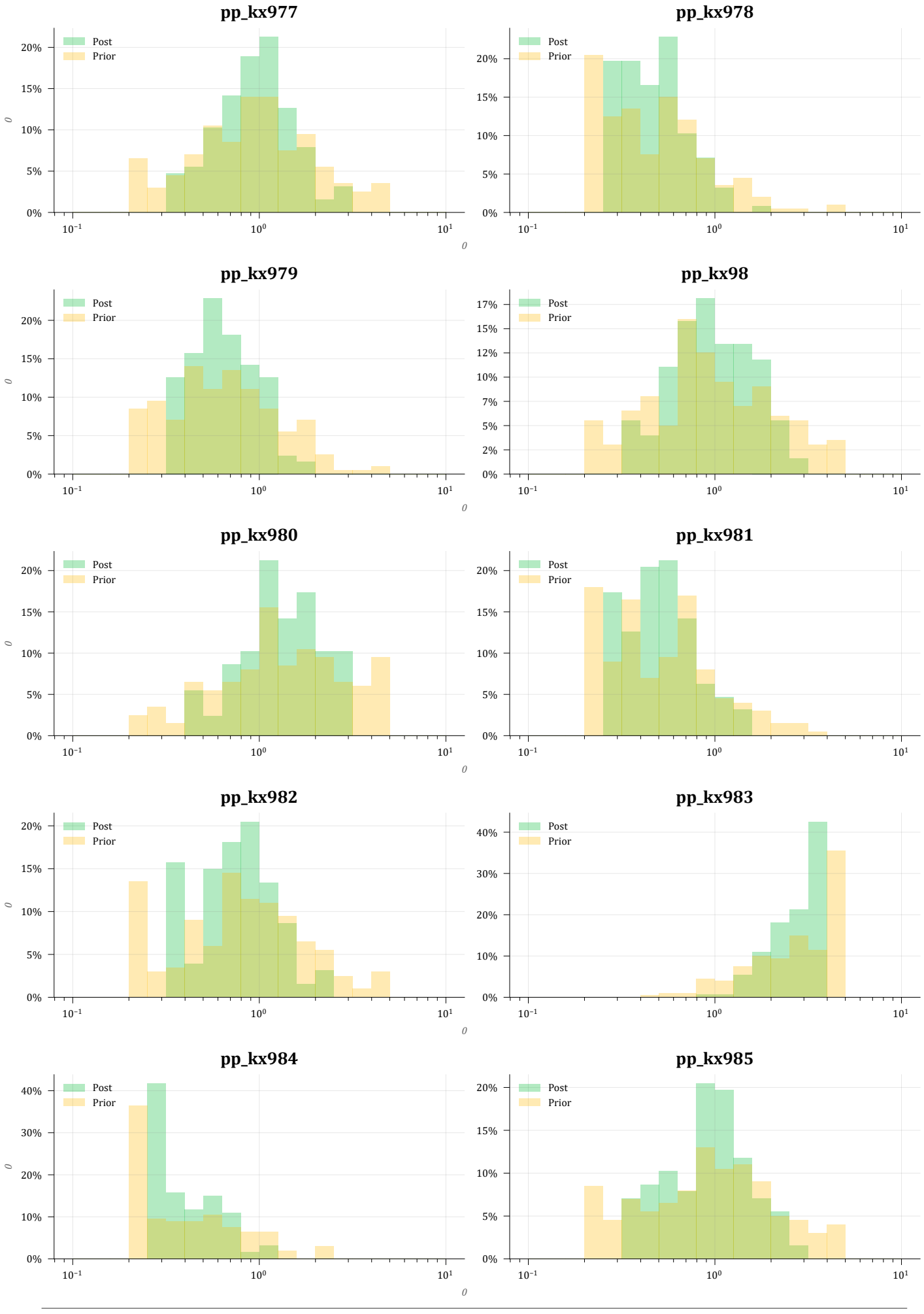

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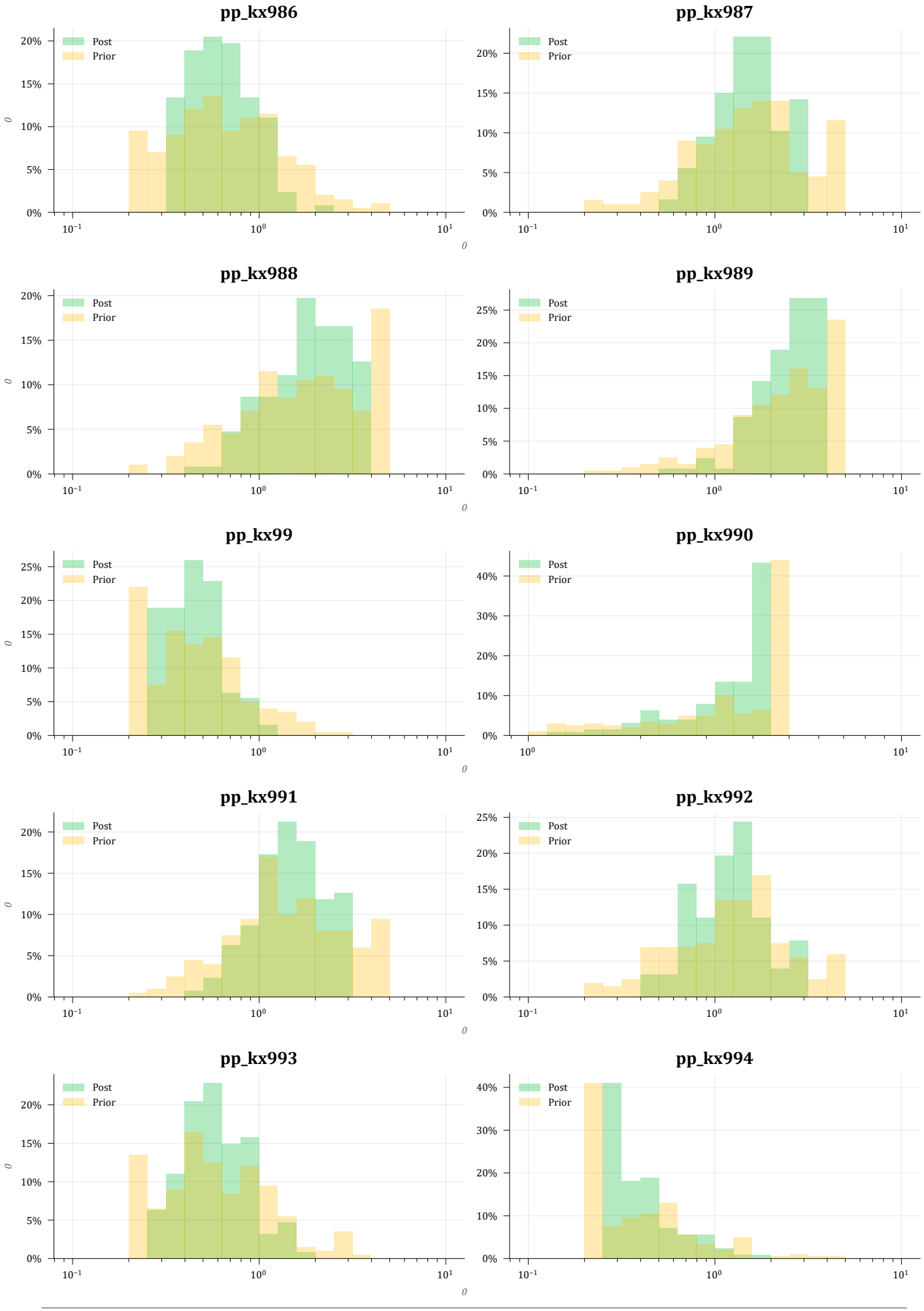

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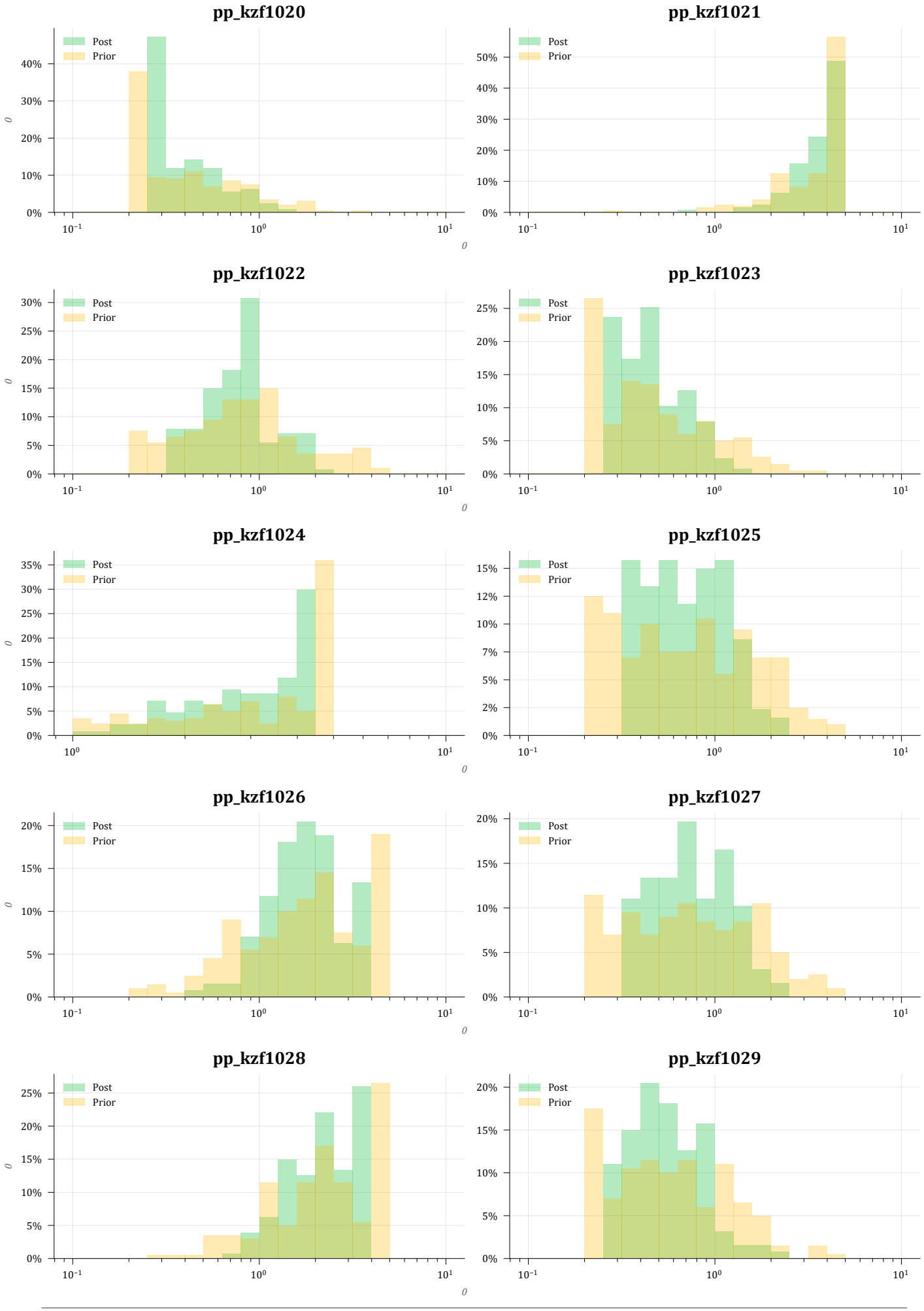

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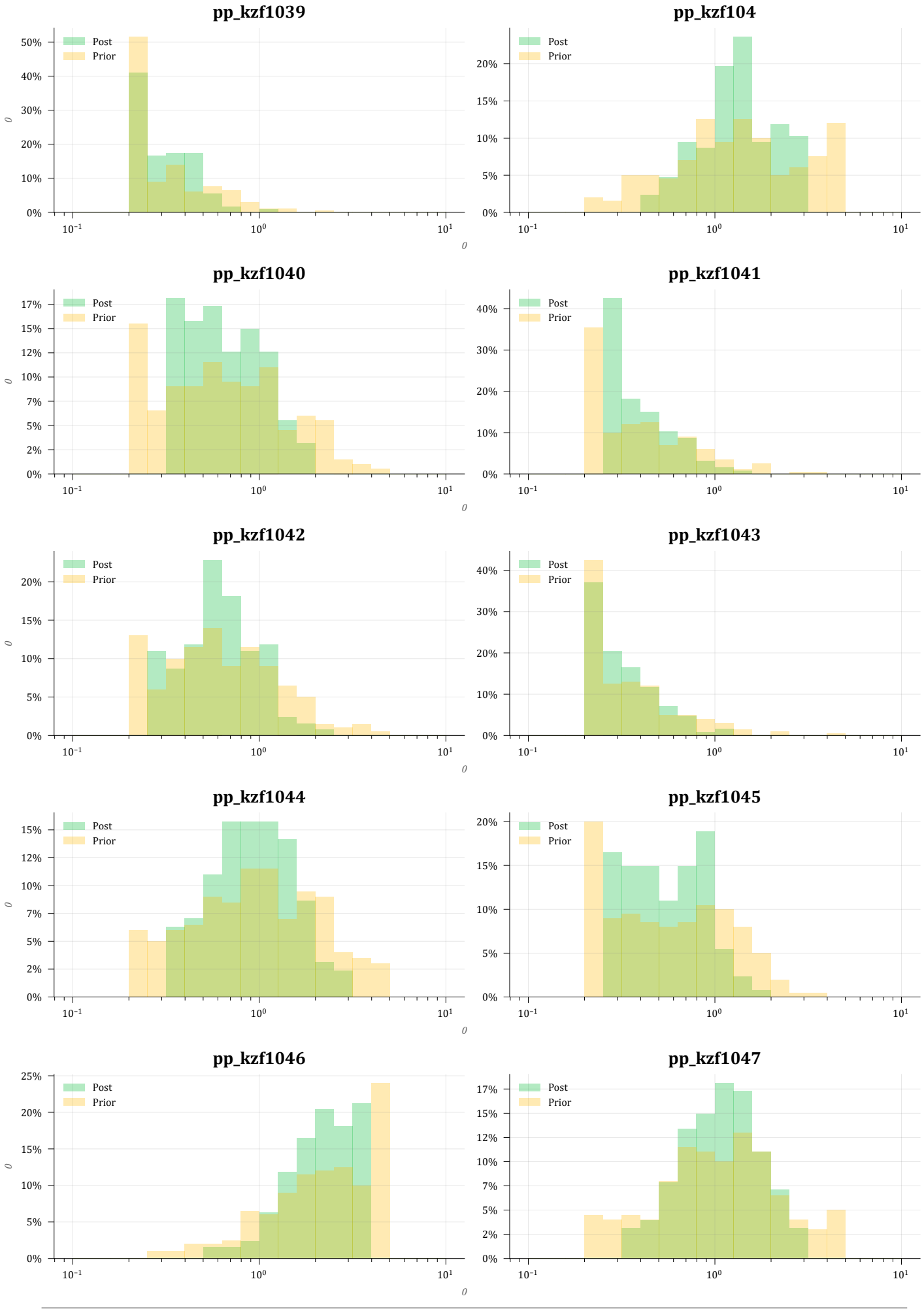

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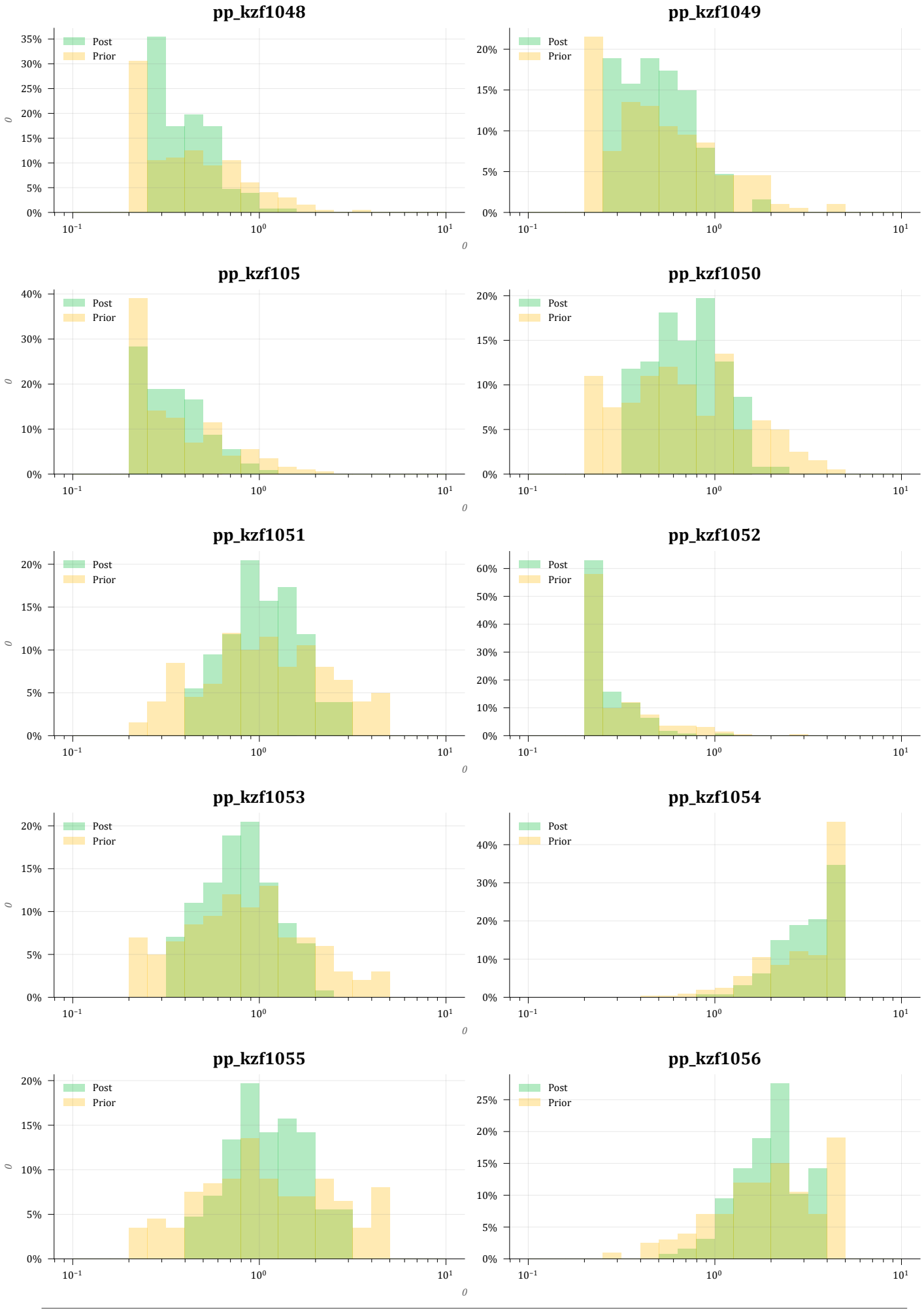

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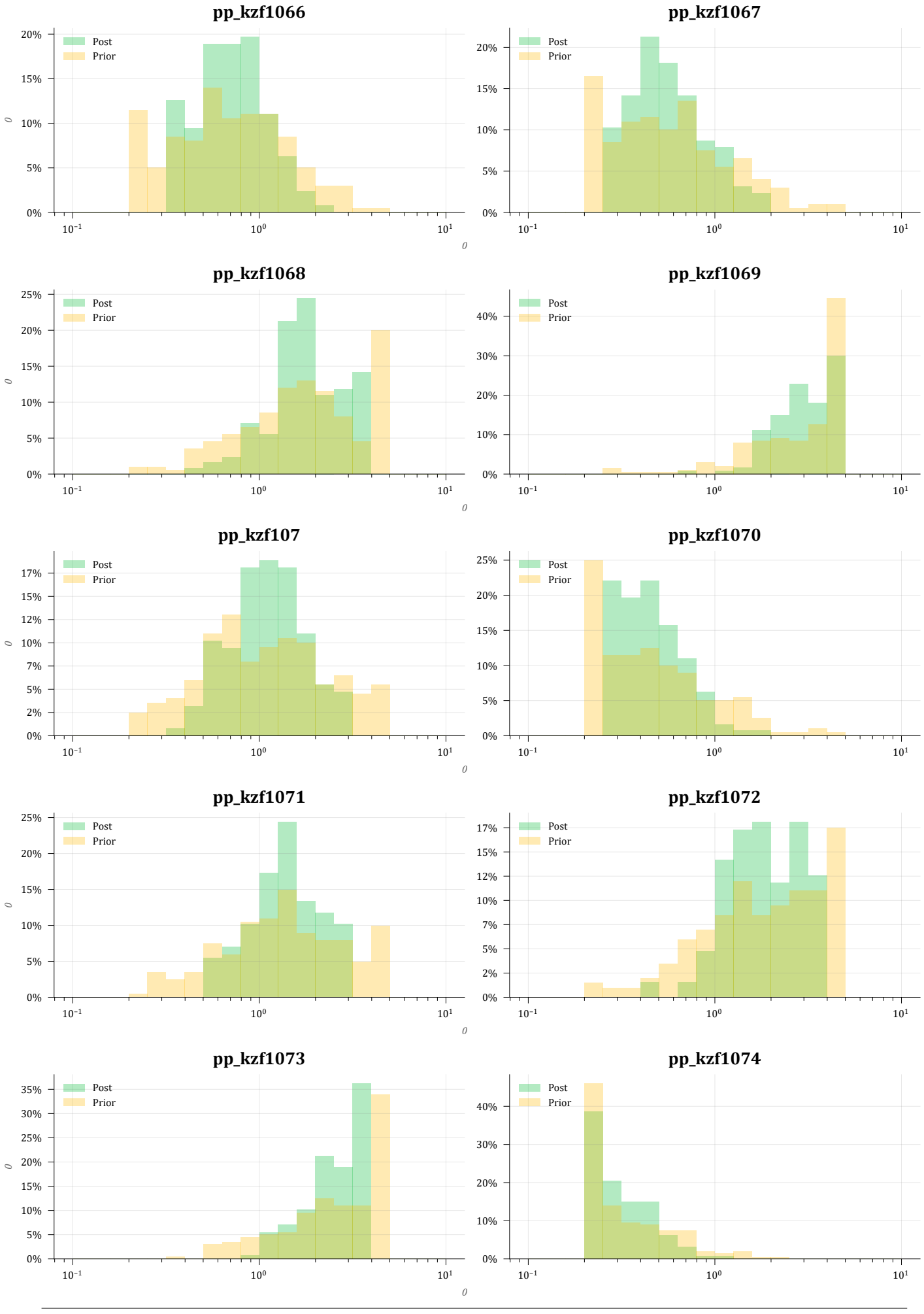

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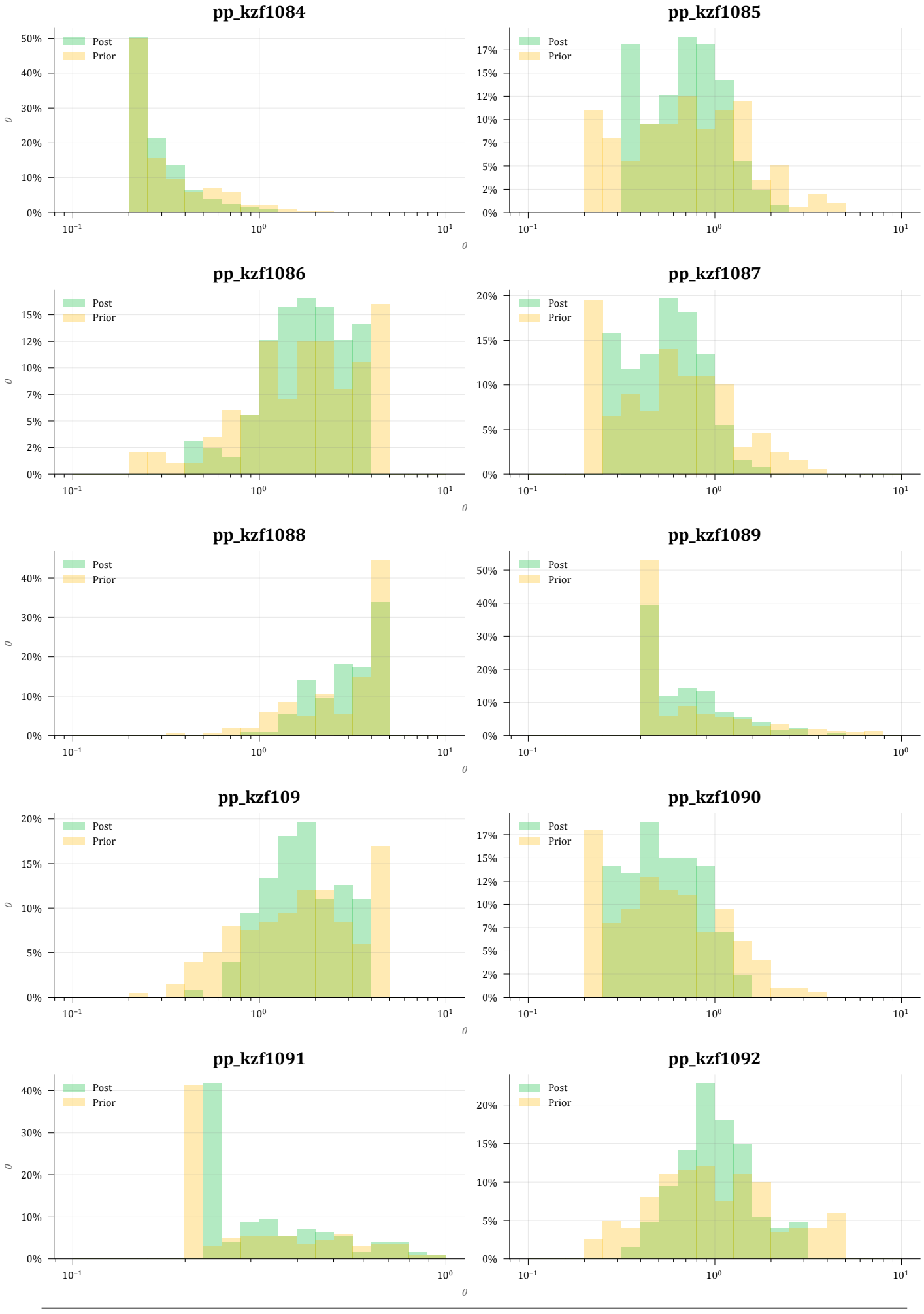

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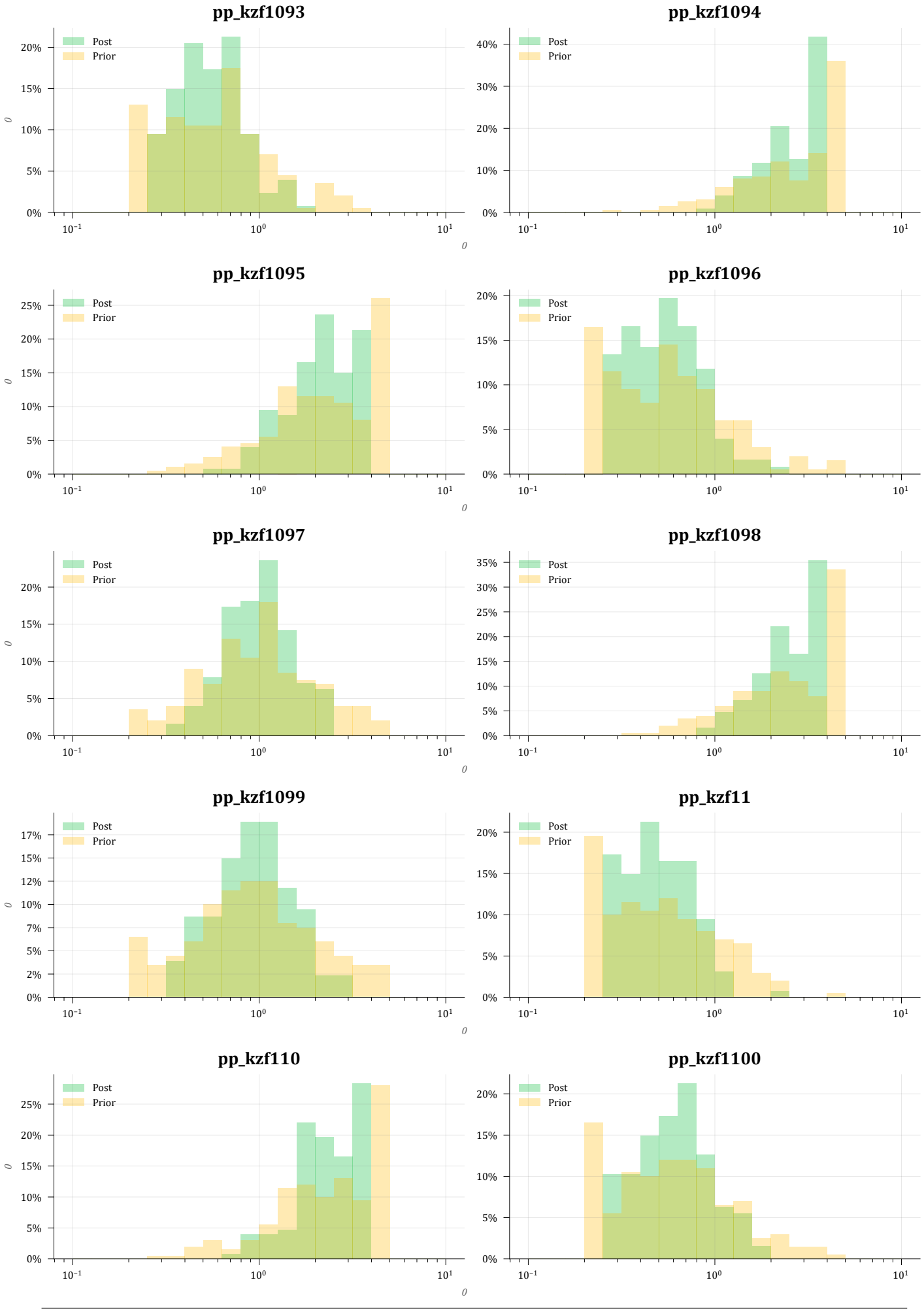

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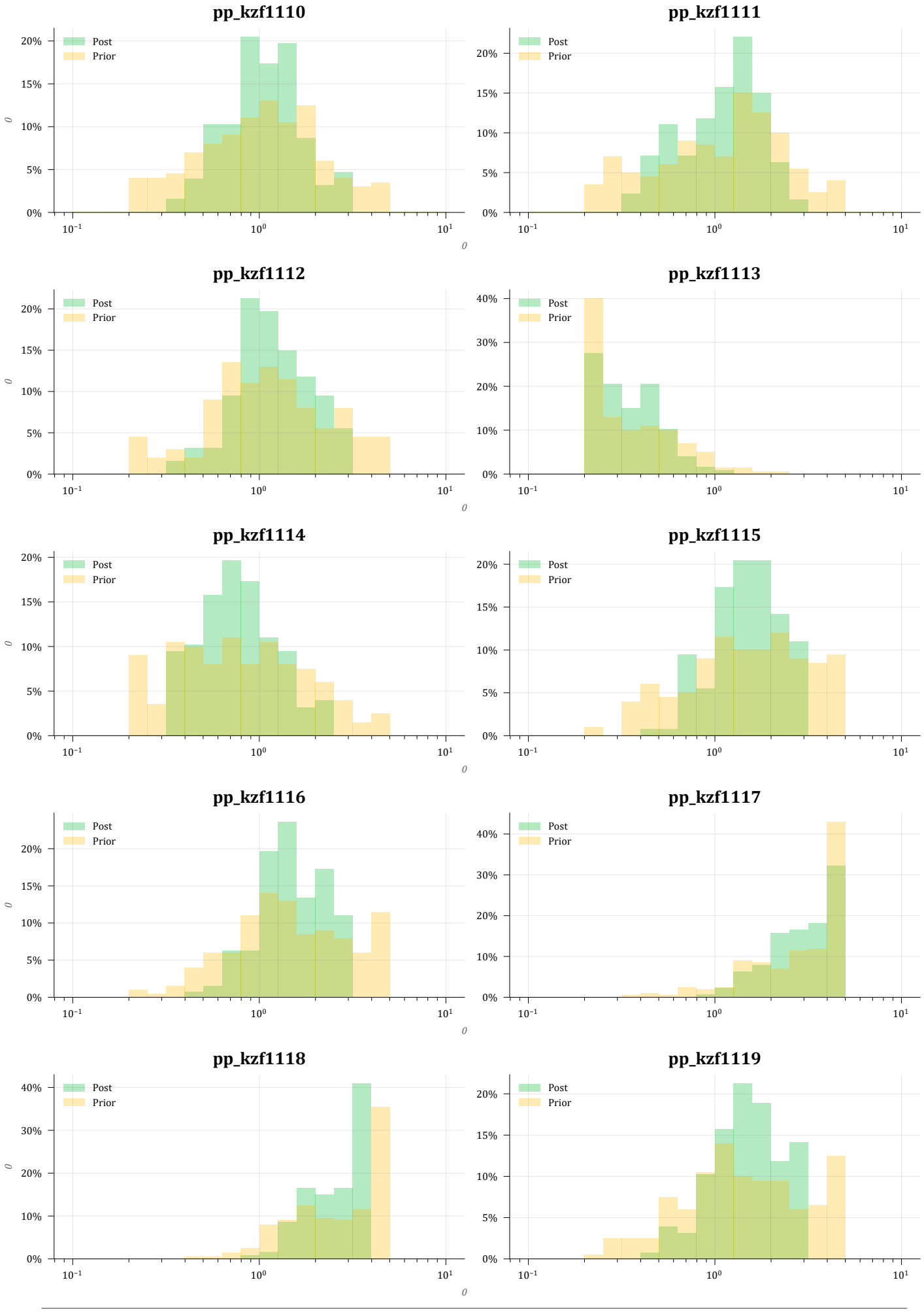

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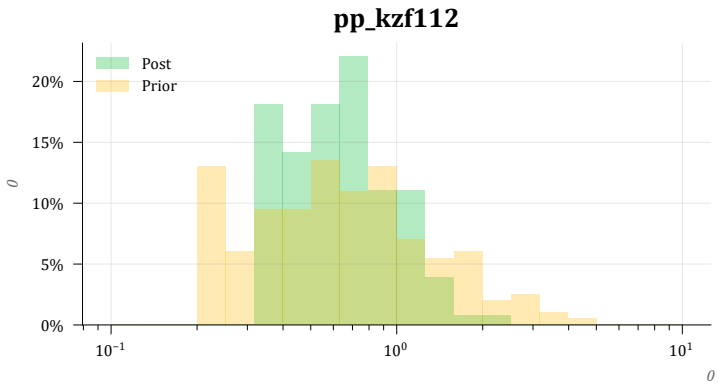

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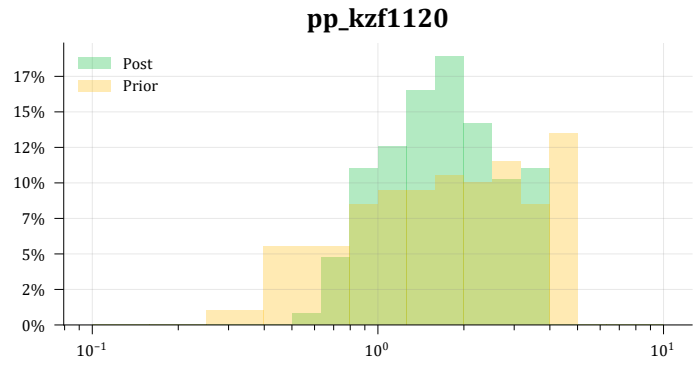

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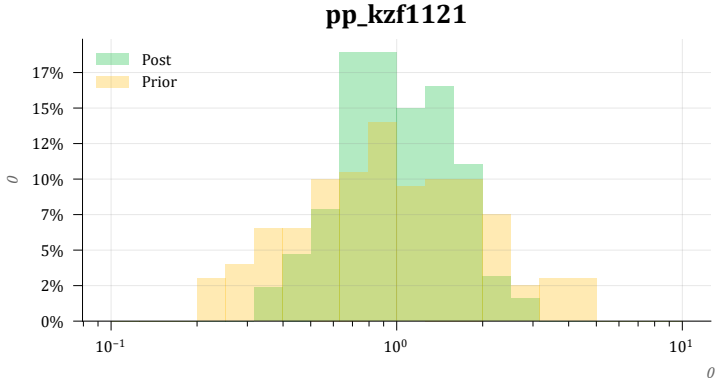

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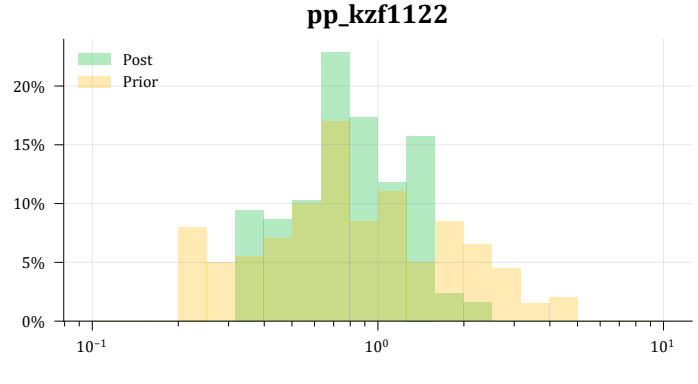

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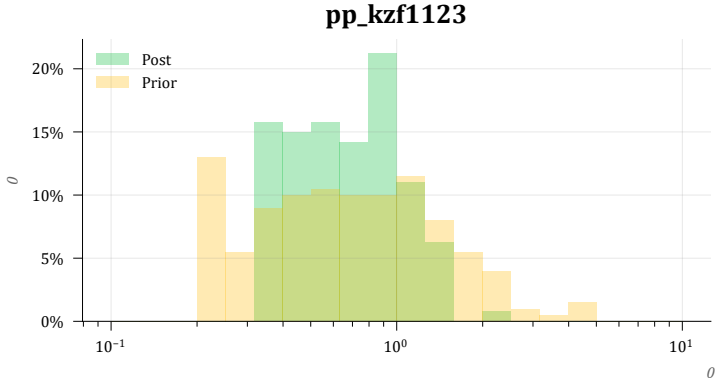

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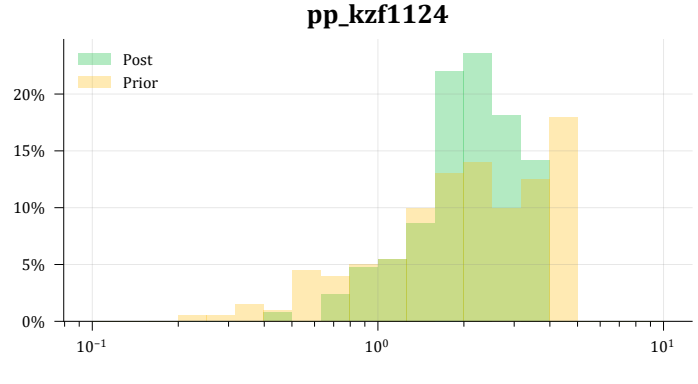

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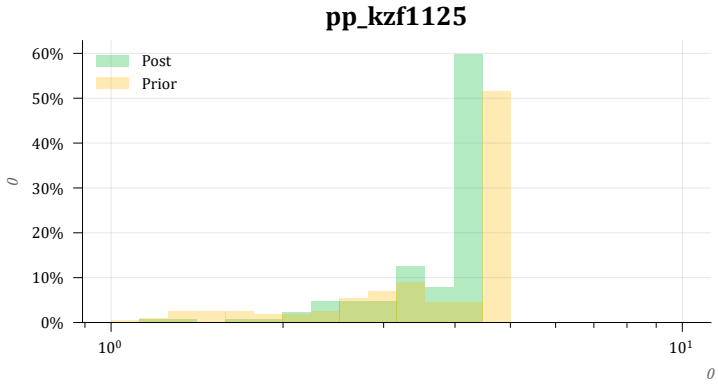

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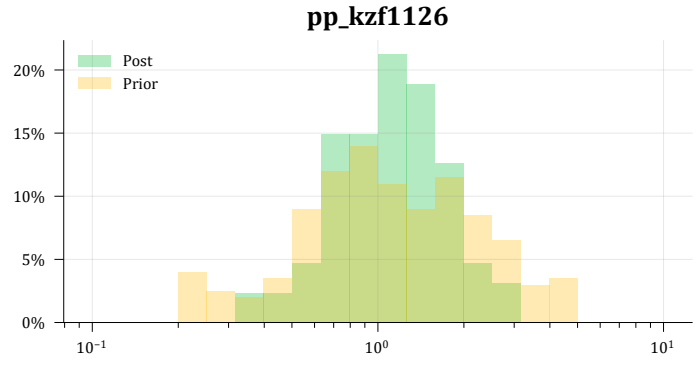

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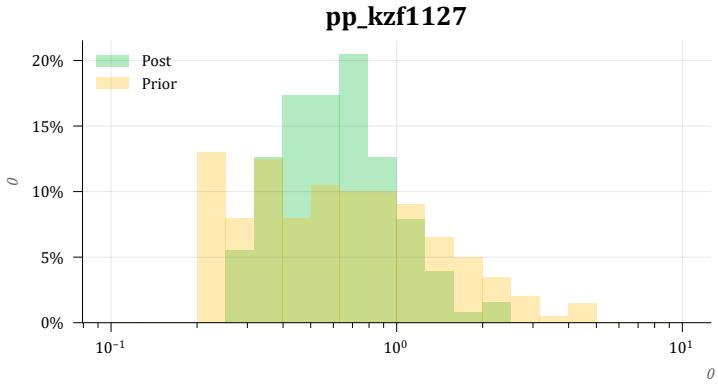

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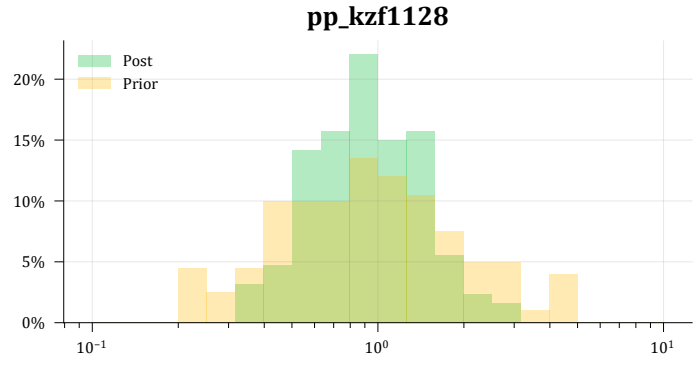

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pp_kzf1124
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10¹


pp_kzf1125
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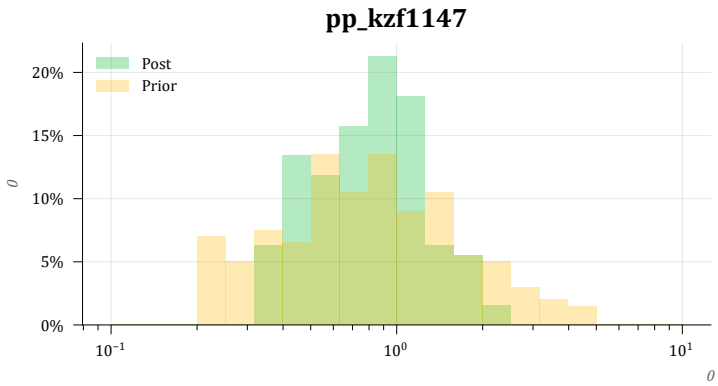

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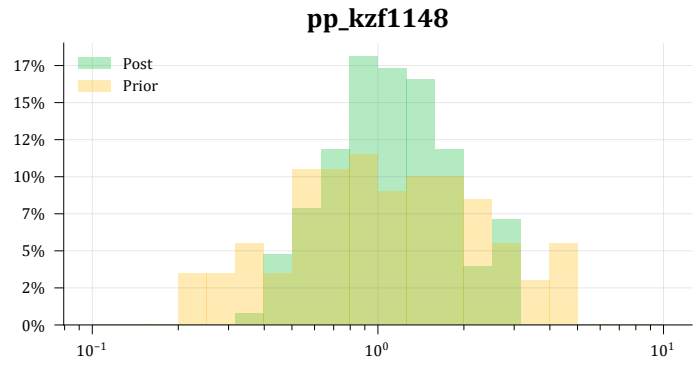

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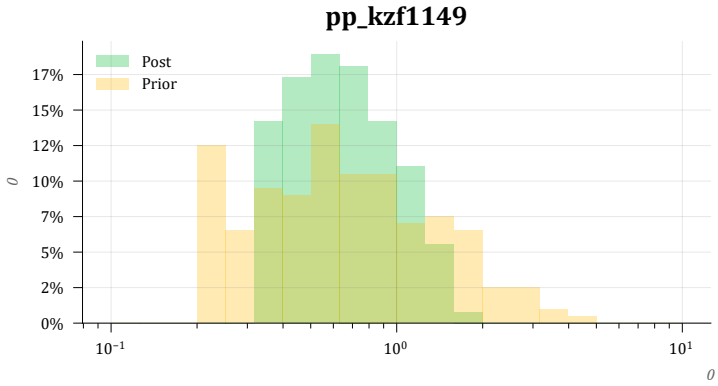

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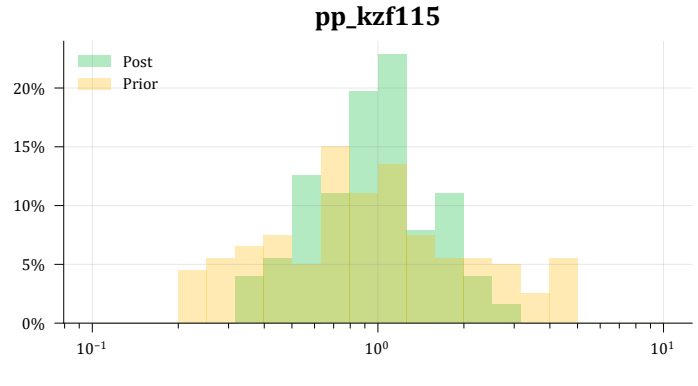

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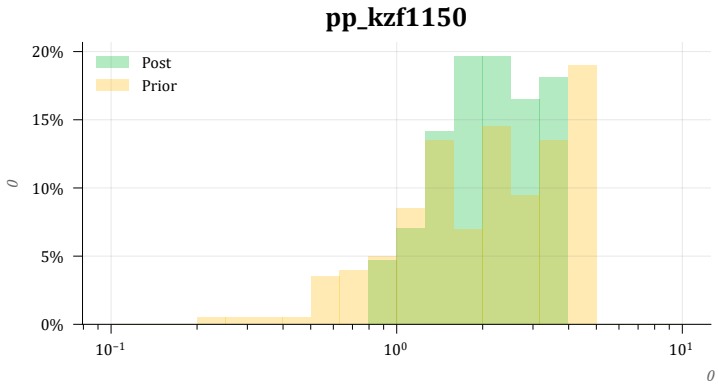

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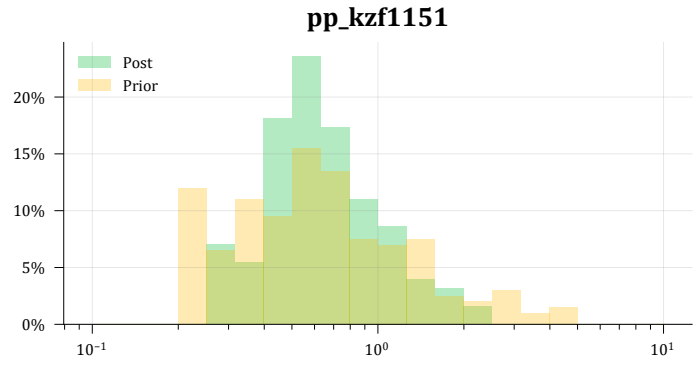

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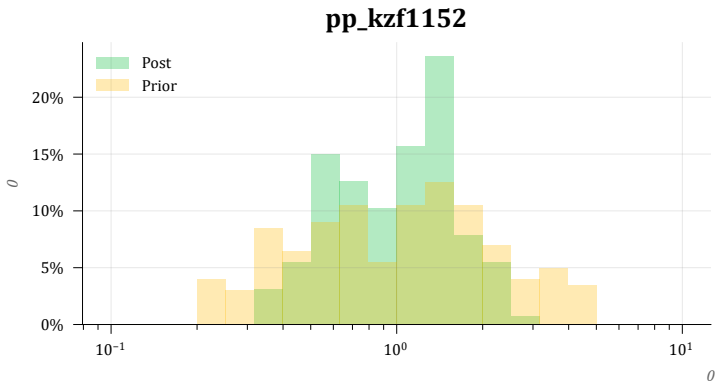

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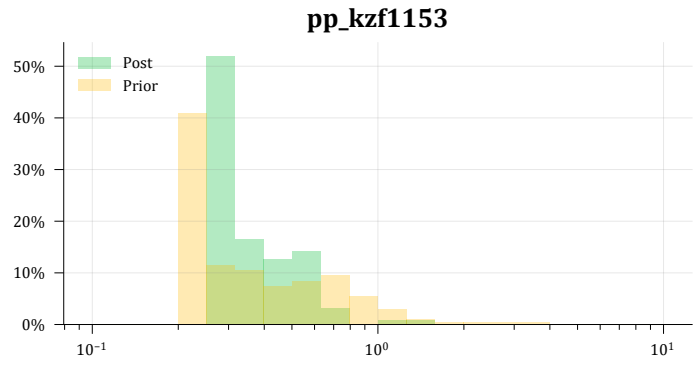

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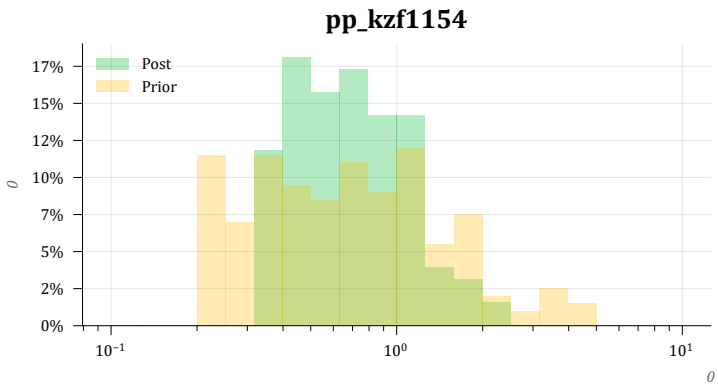

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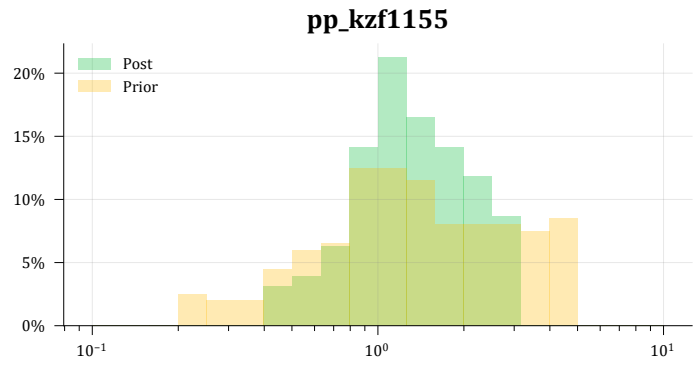

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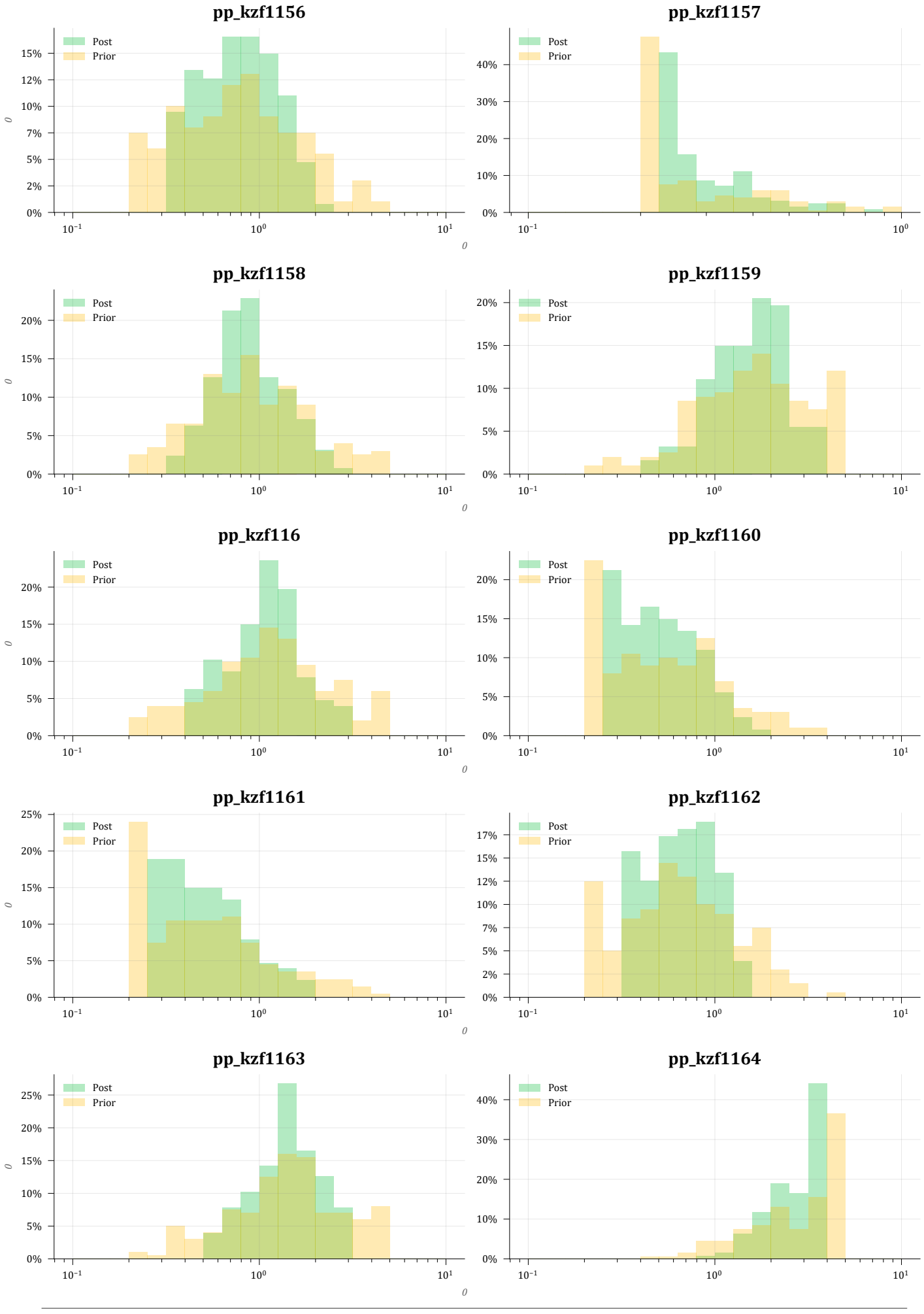

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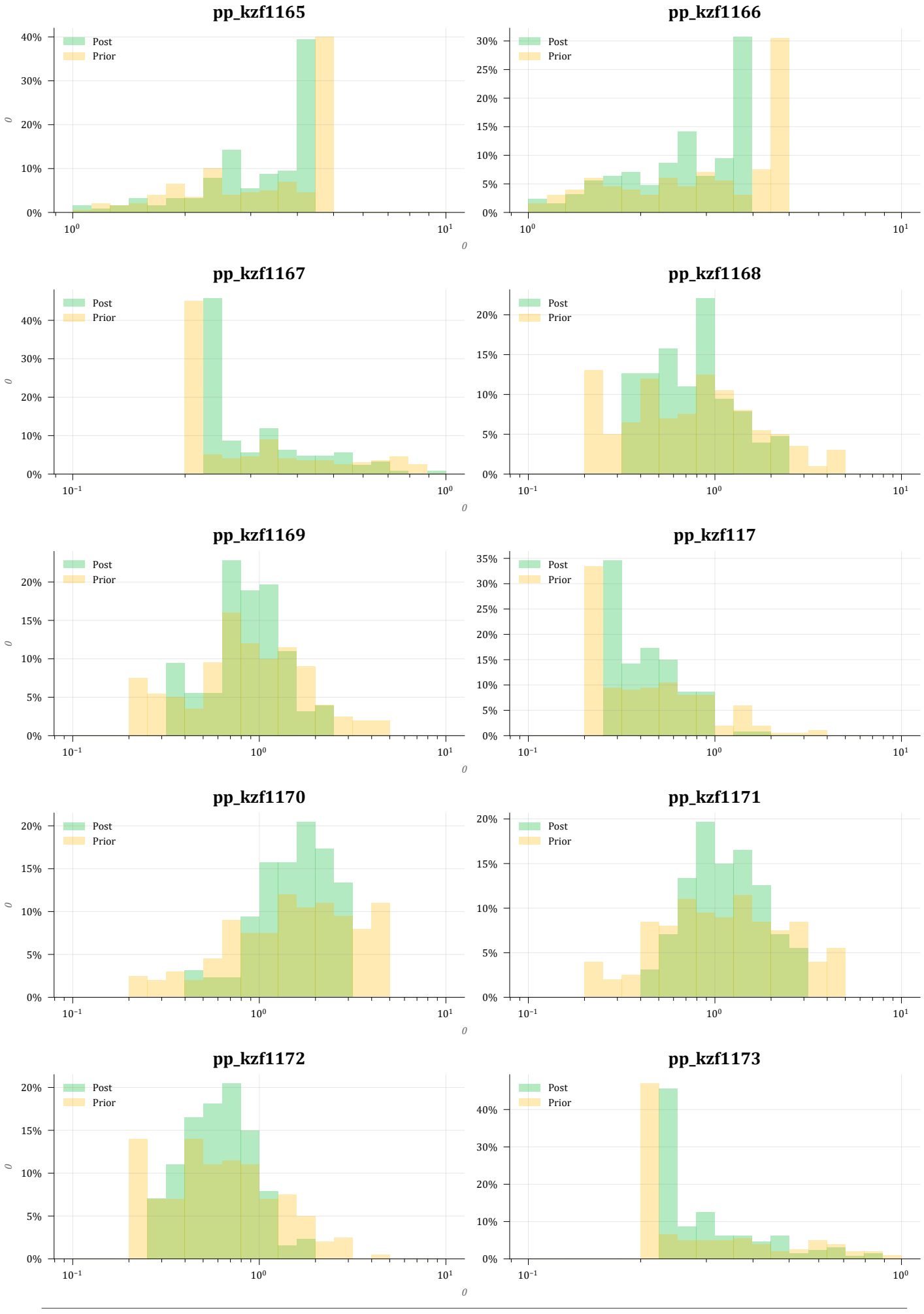

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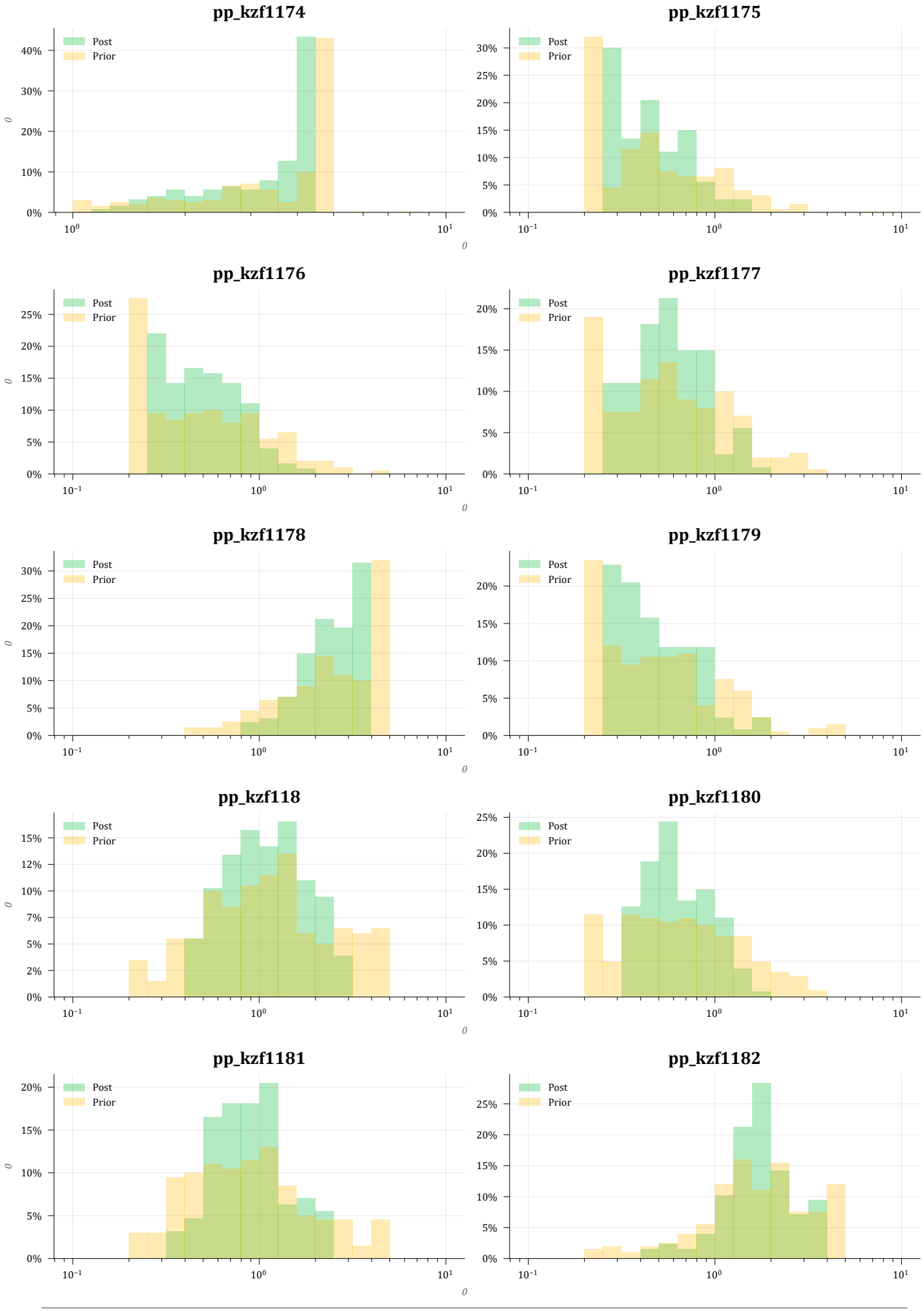

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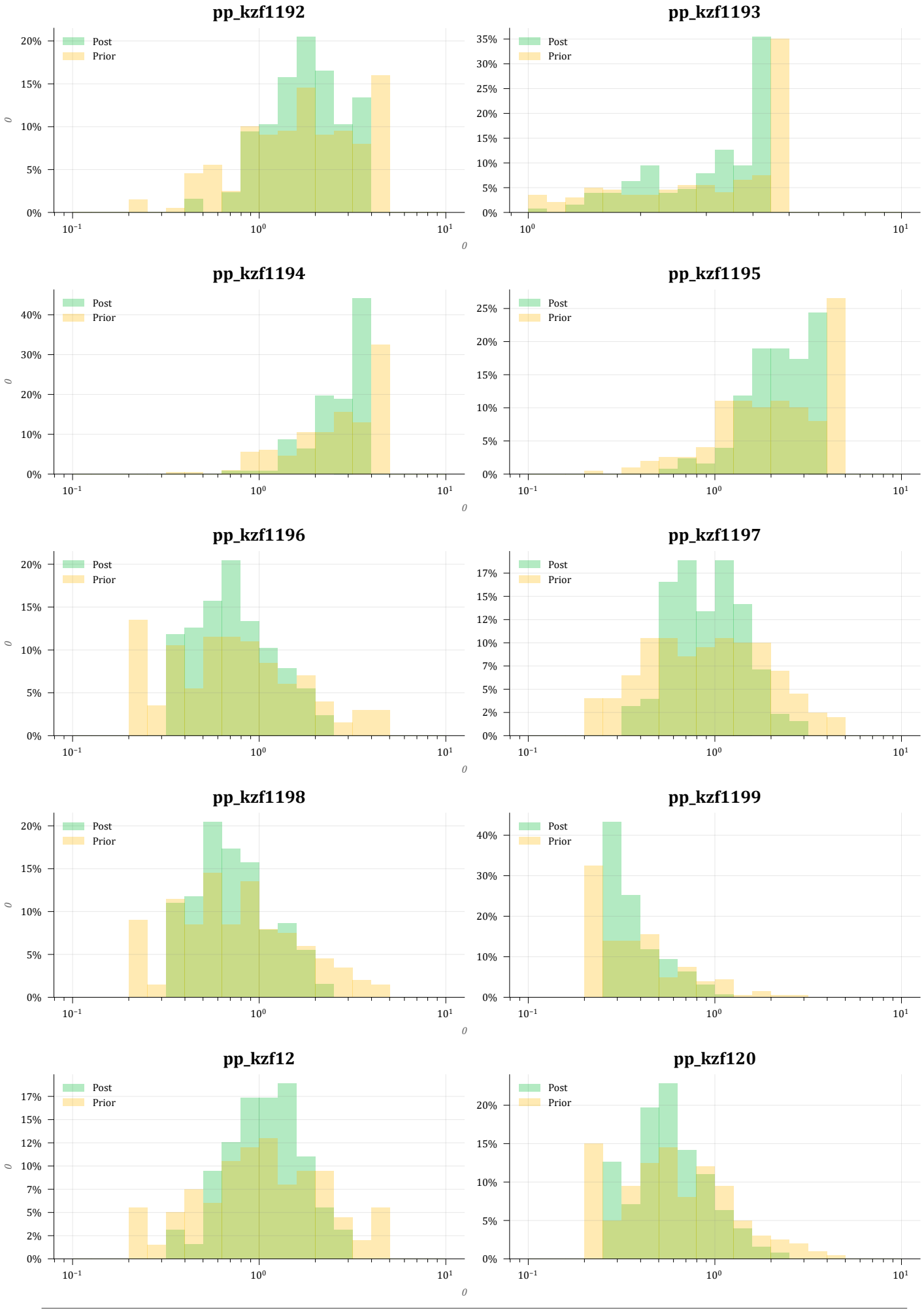

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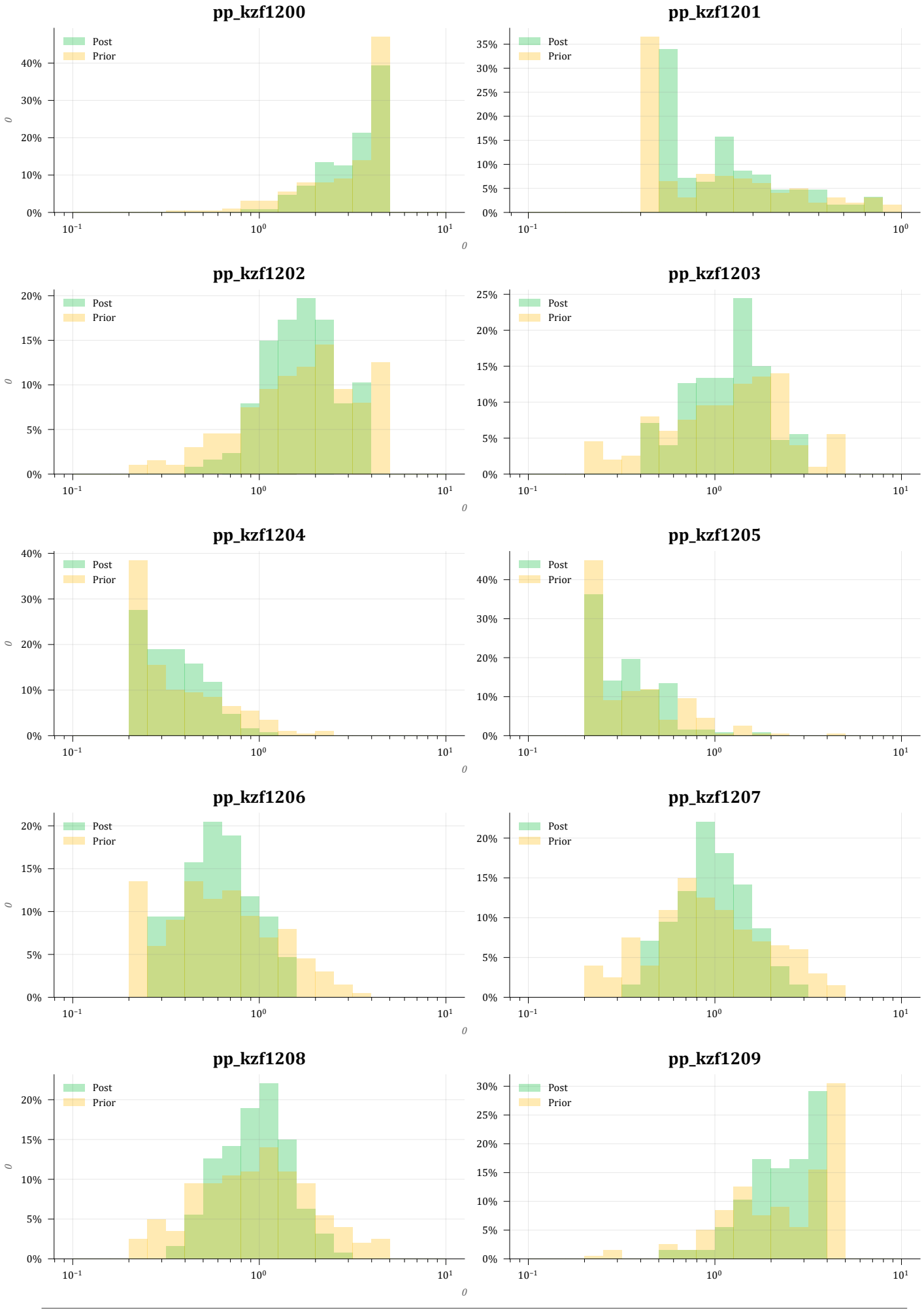

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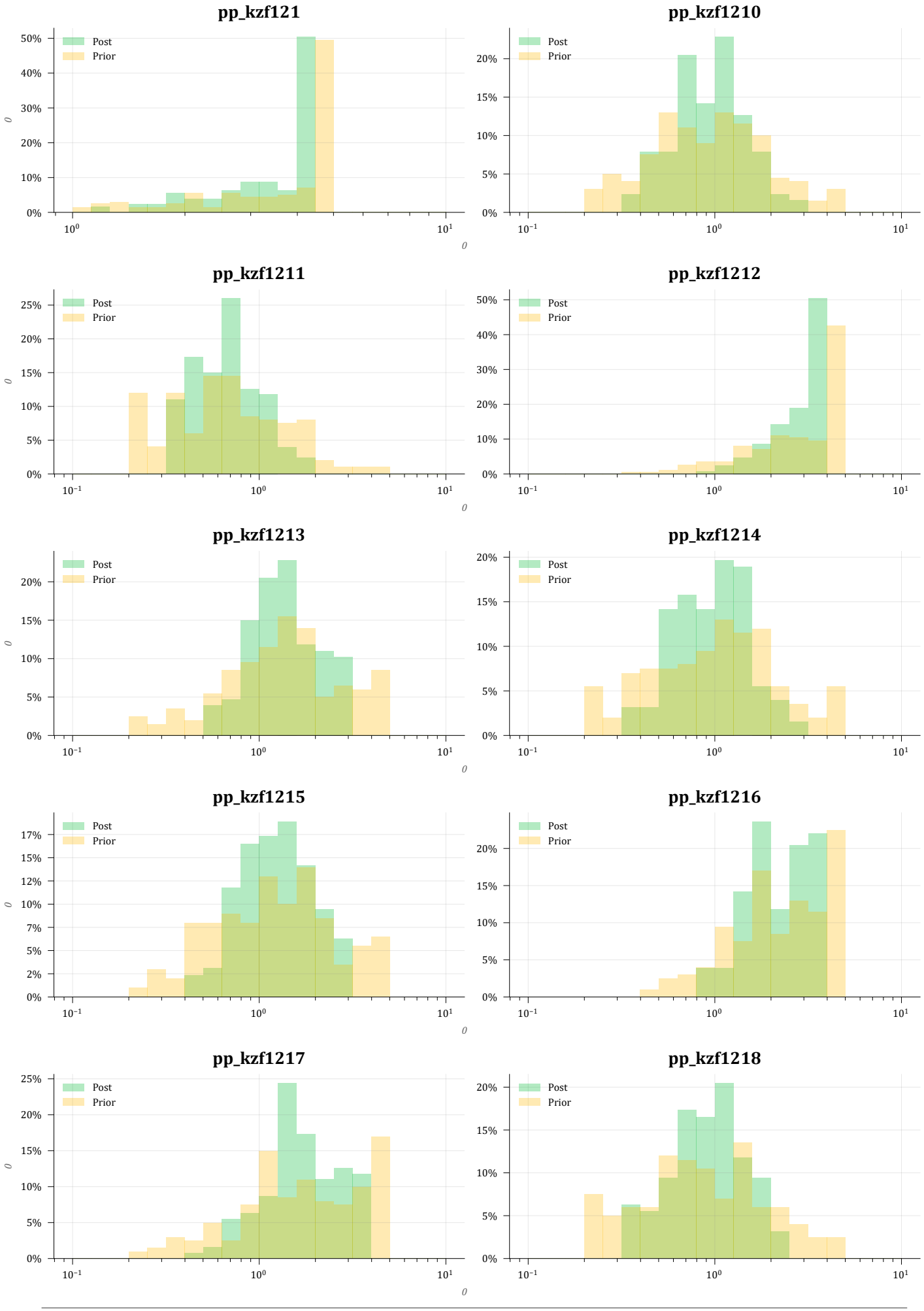

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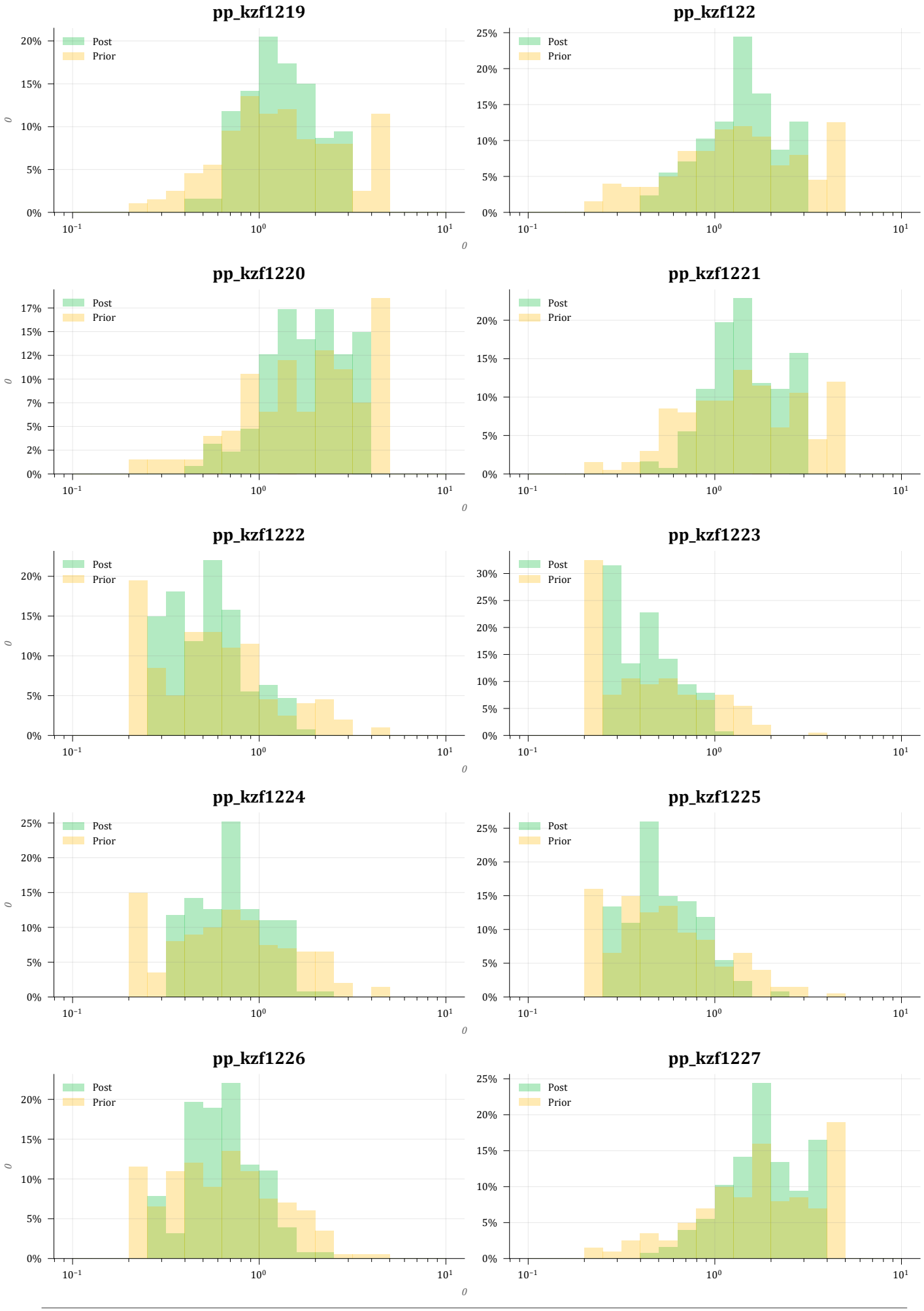

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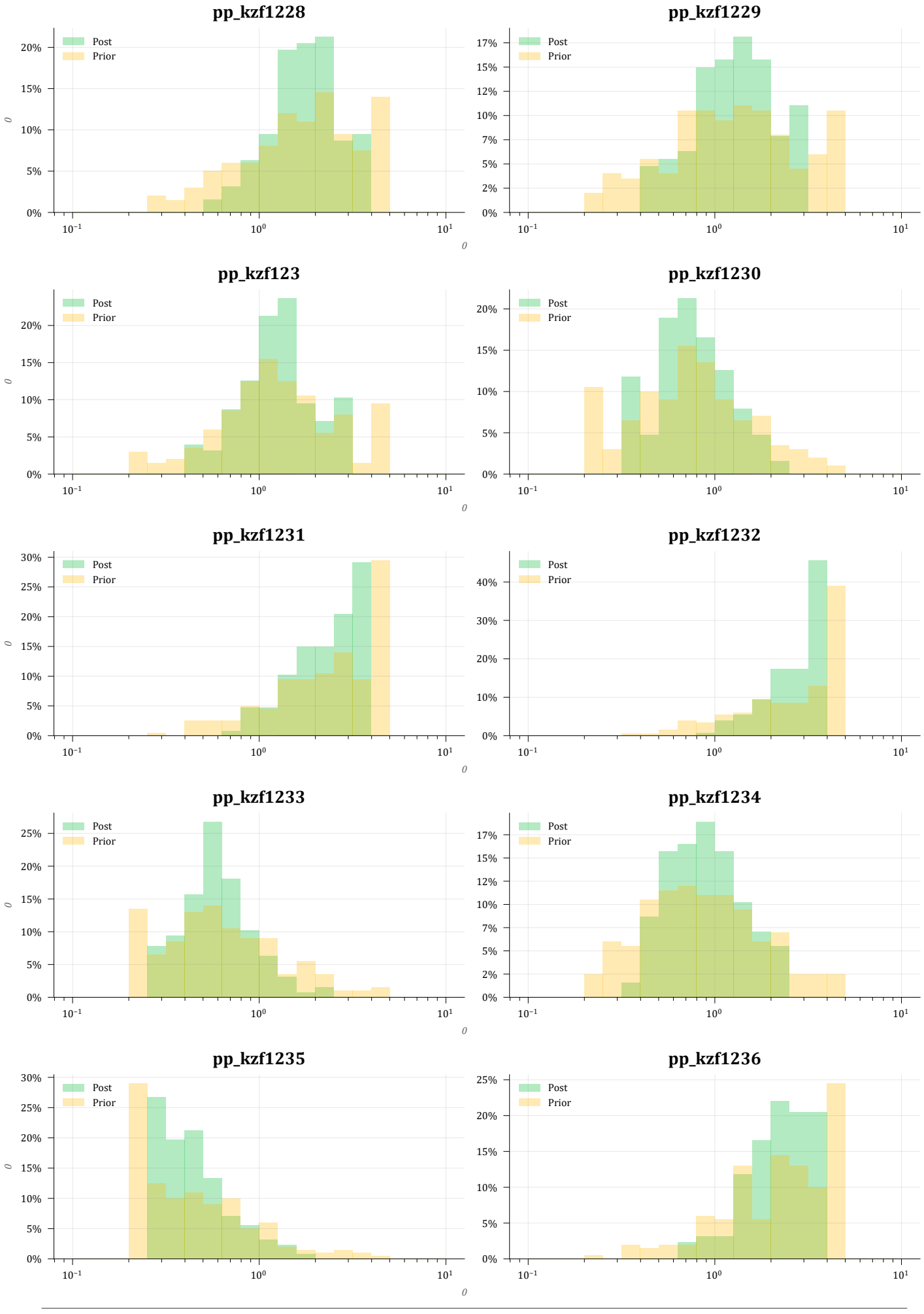

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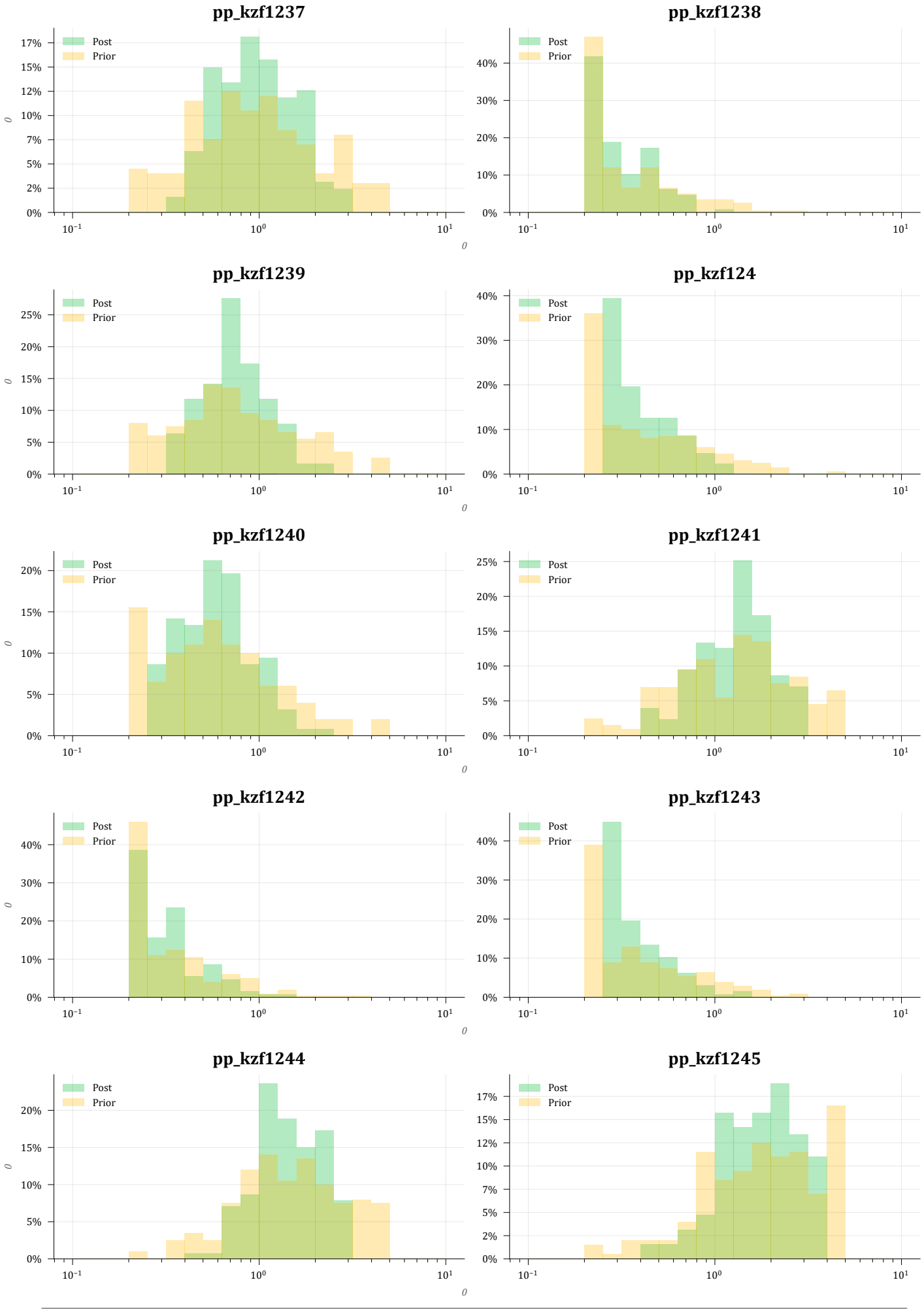

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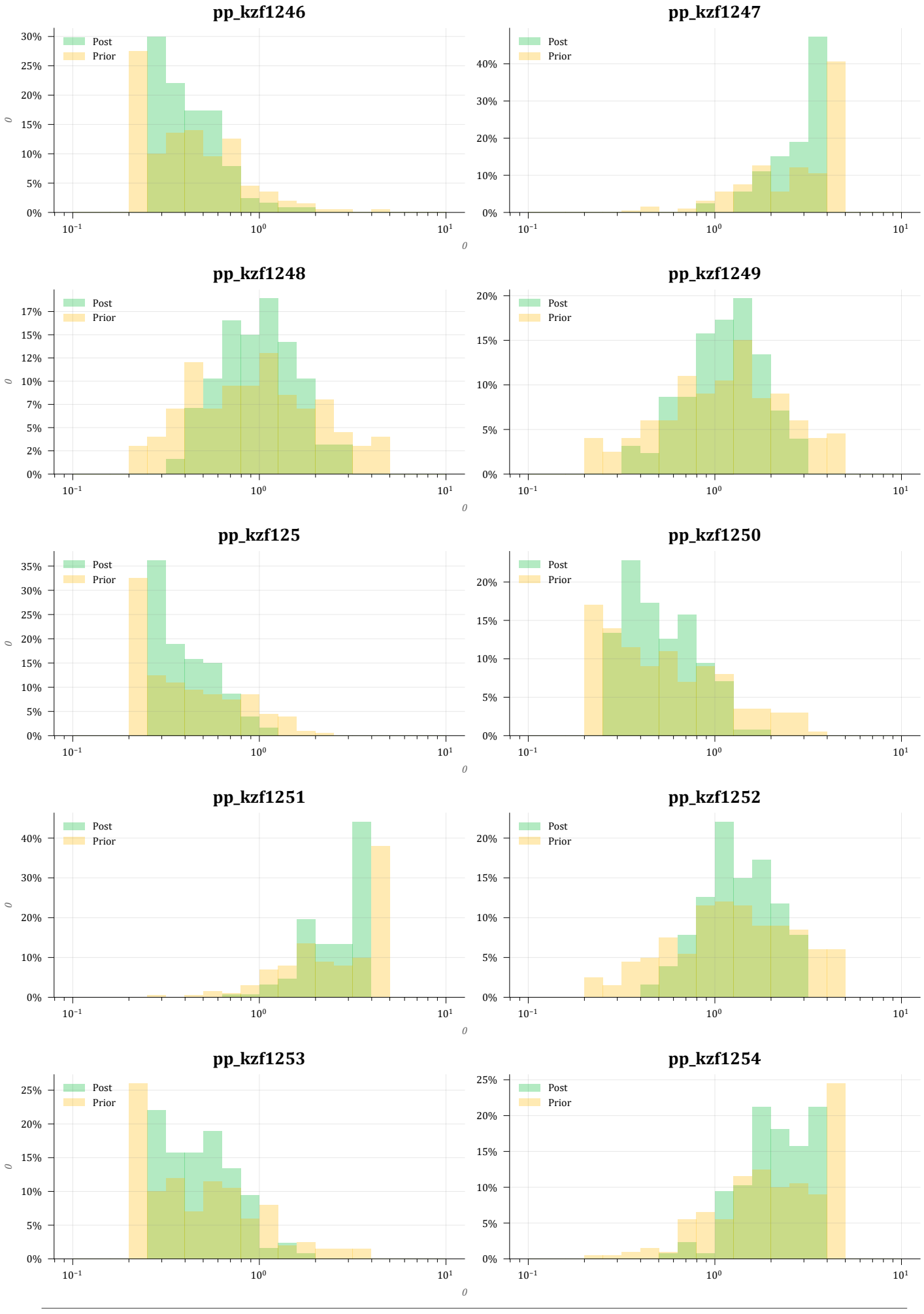

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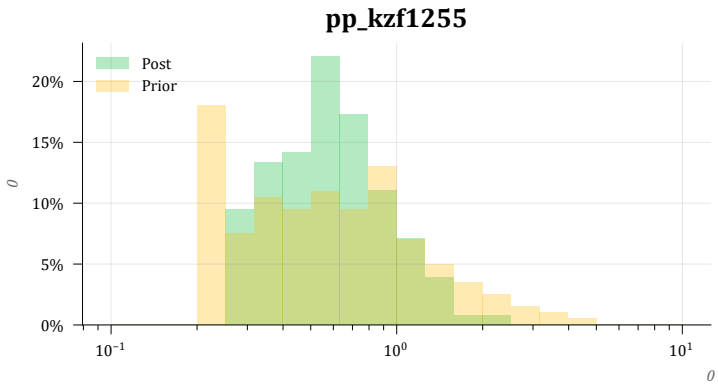

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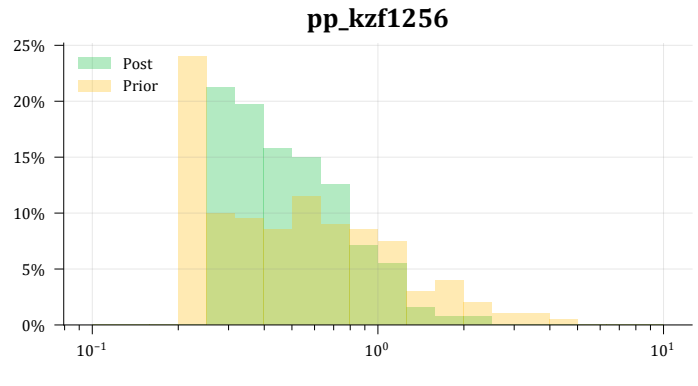

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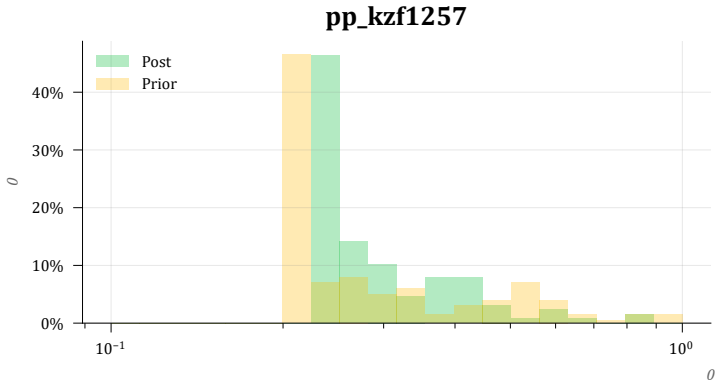

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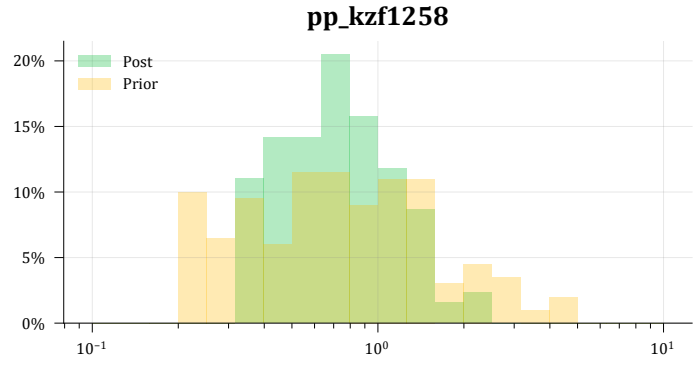

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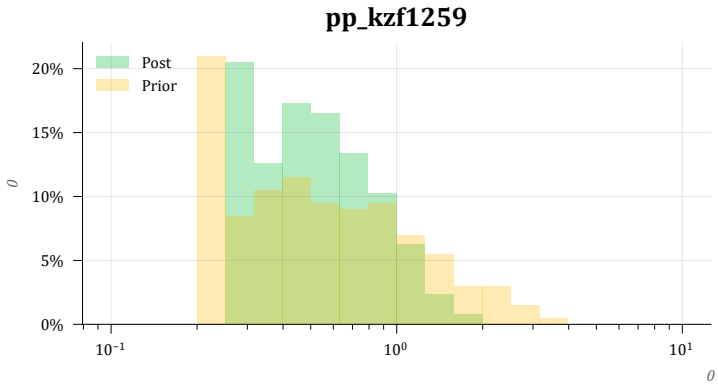

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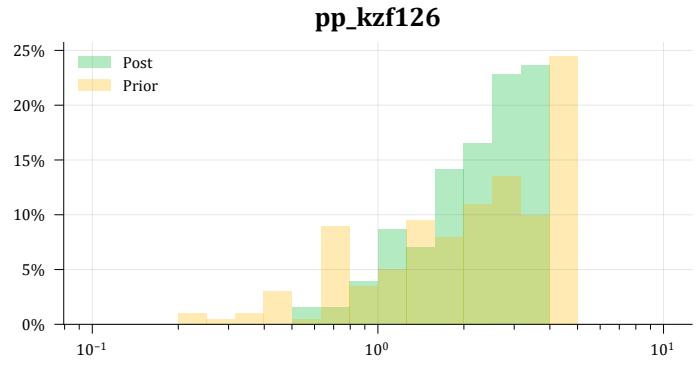

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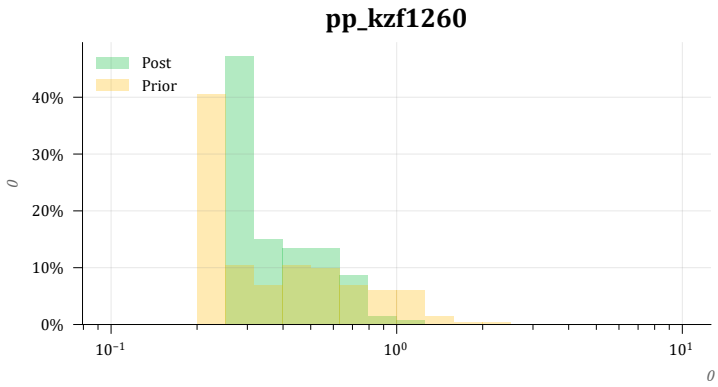

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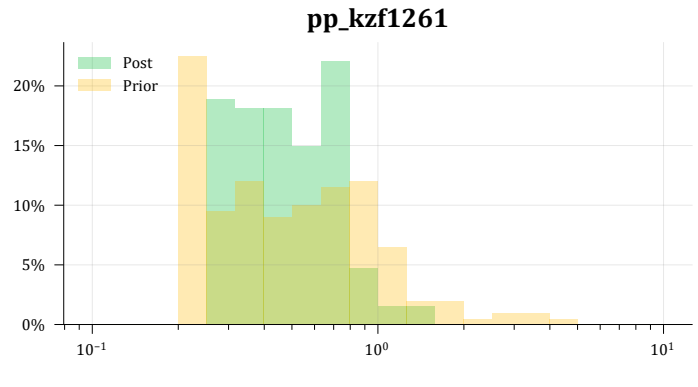

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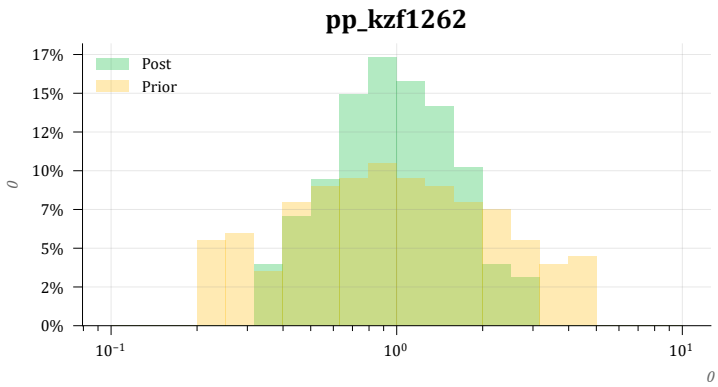

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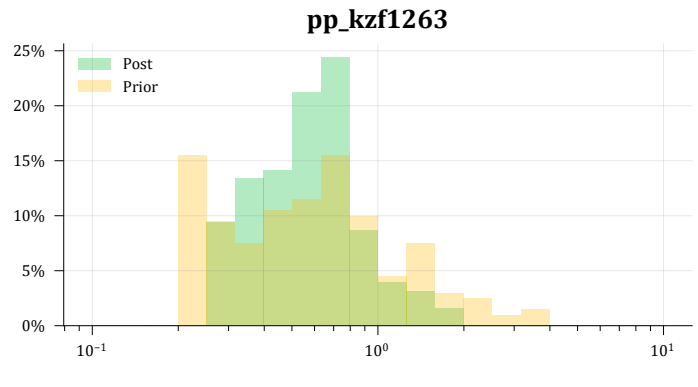

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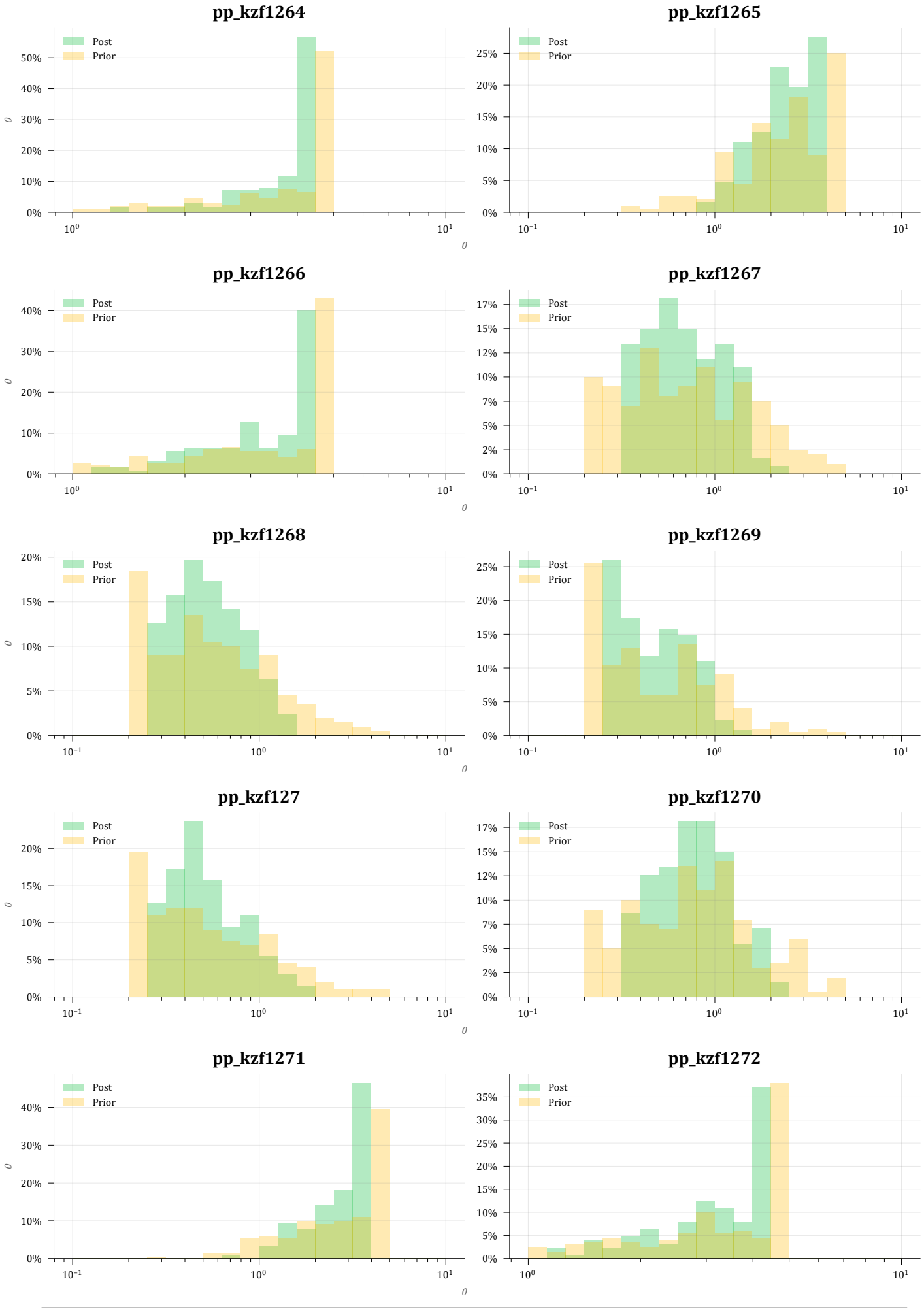

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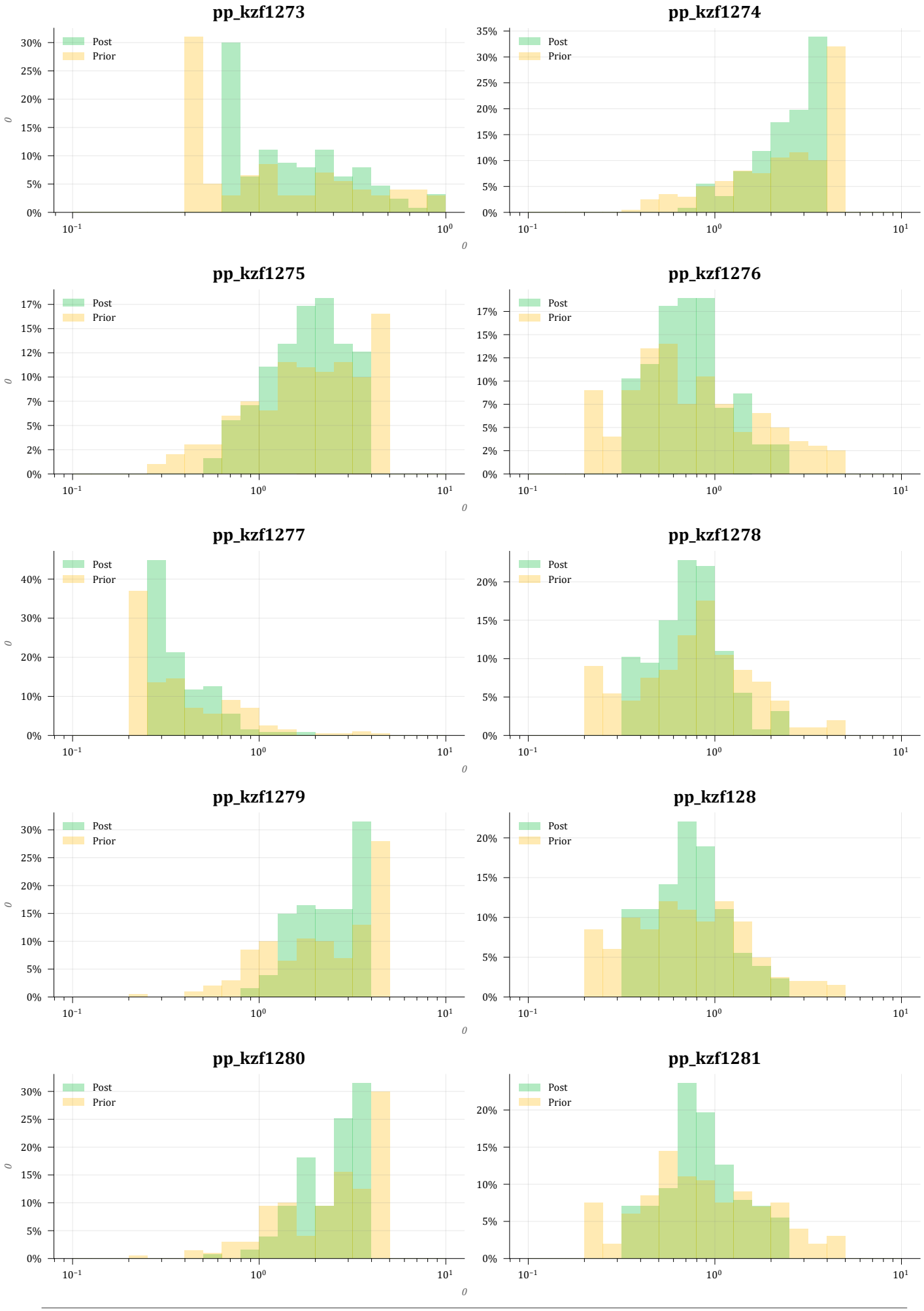

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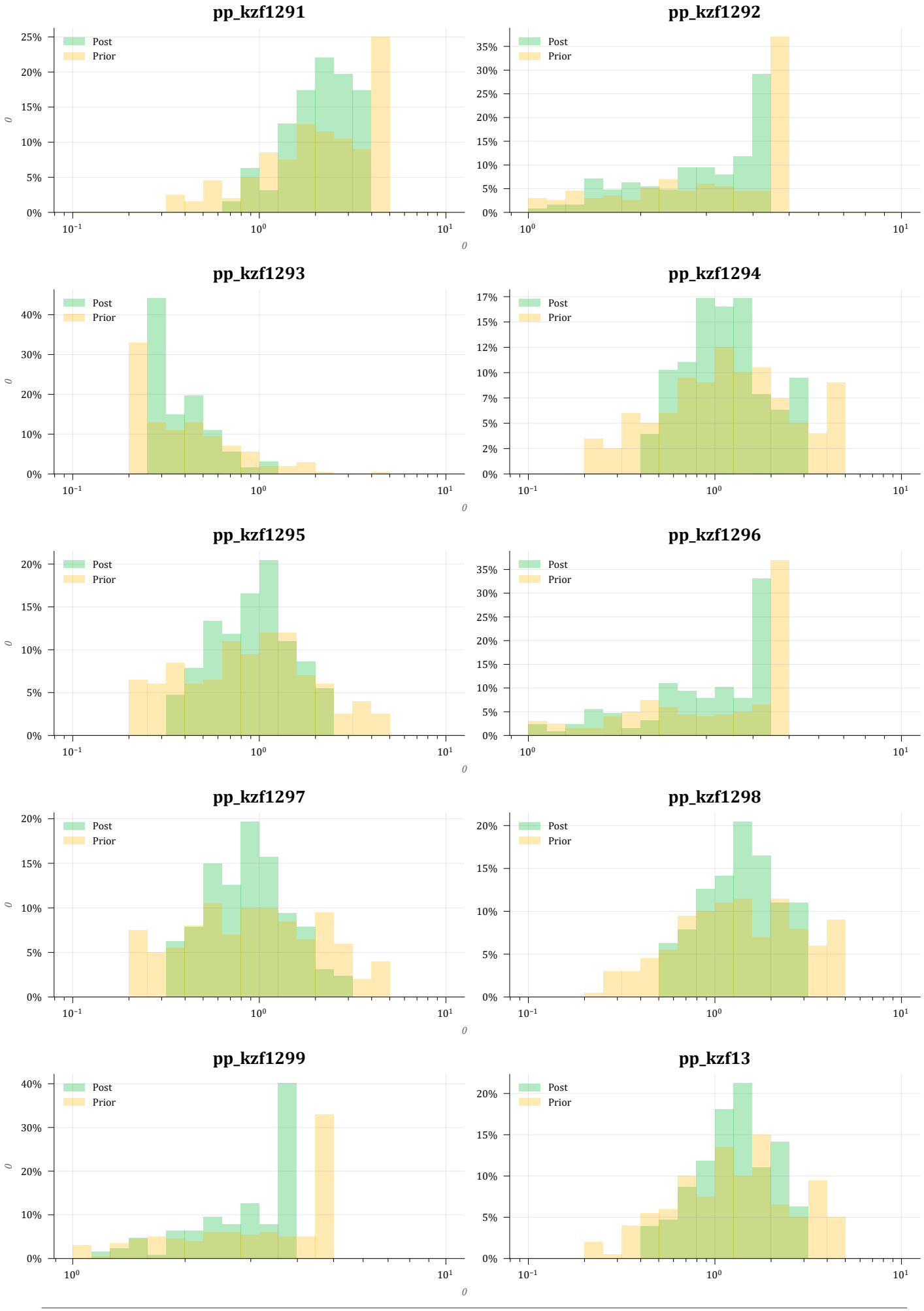

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pp_kzf1263
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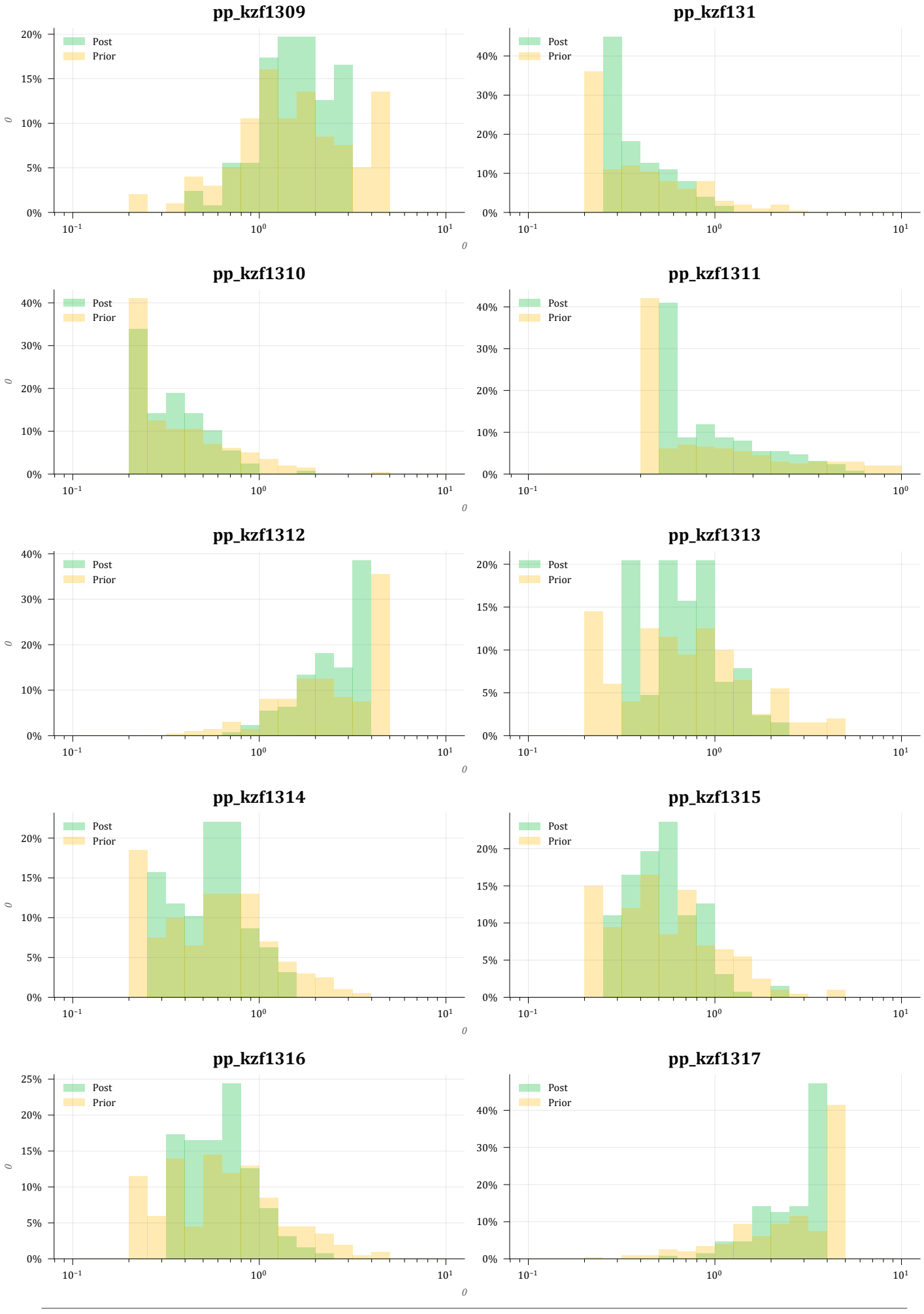

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Parameters


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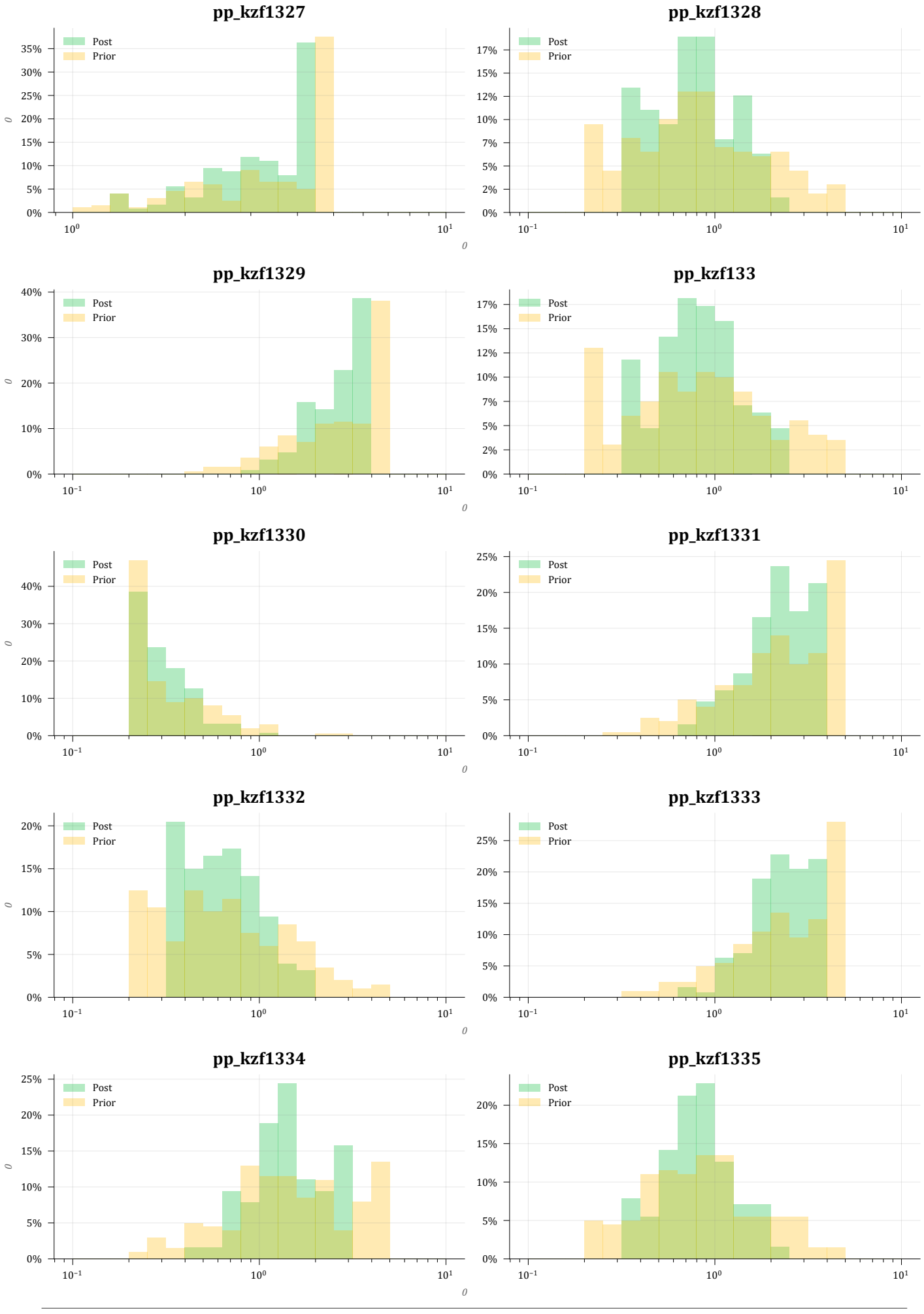

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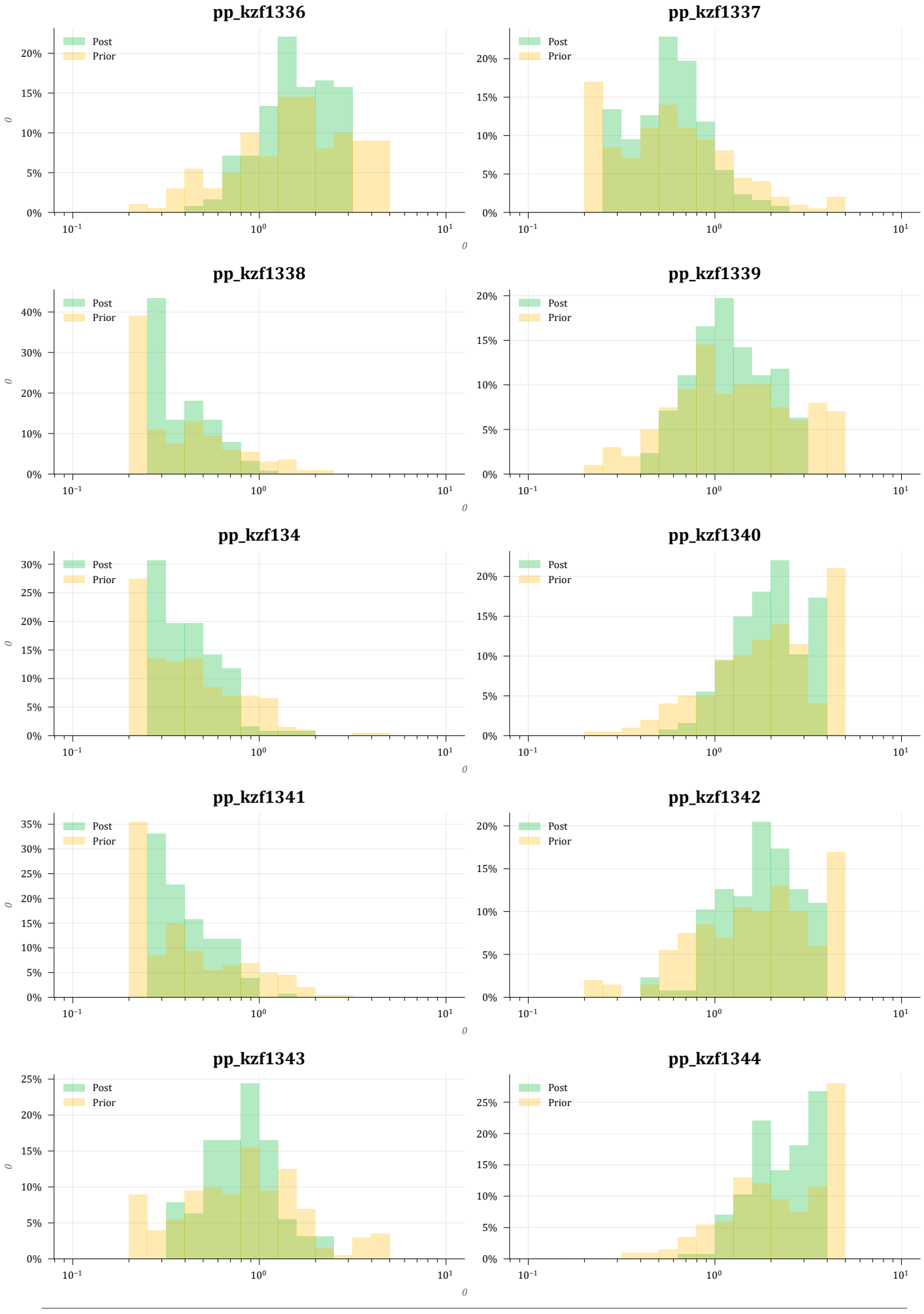

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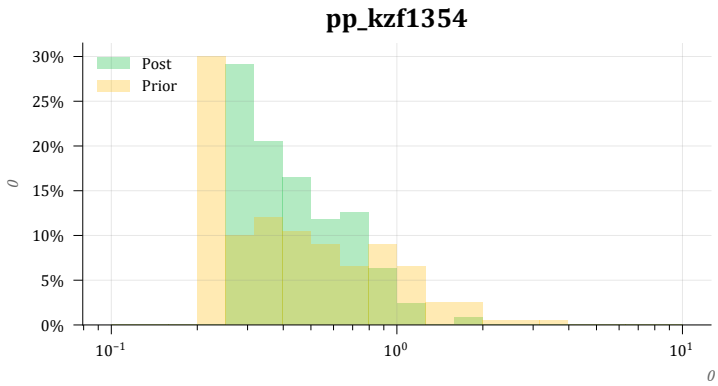

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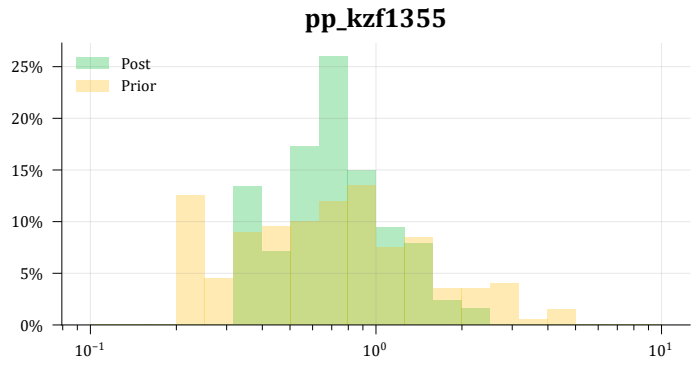

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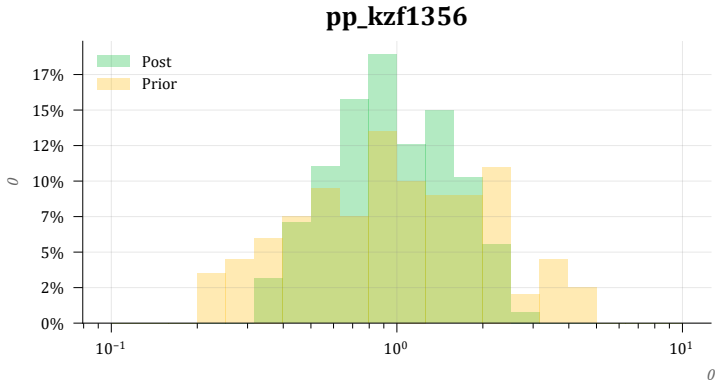

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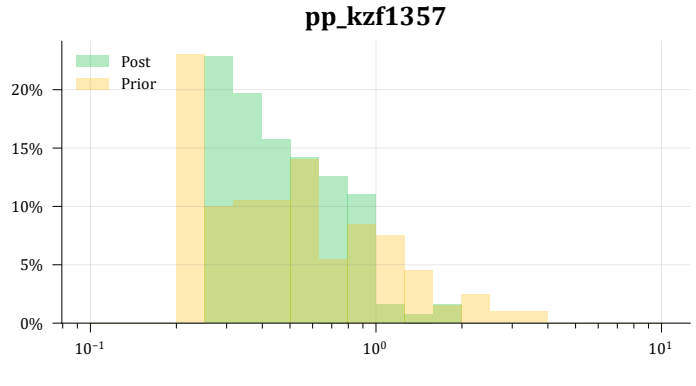

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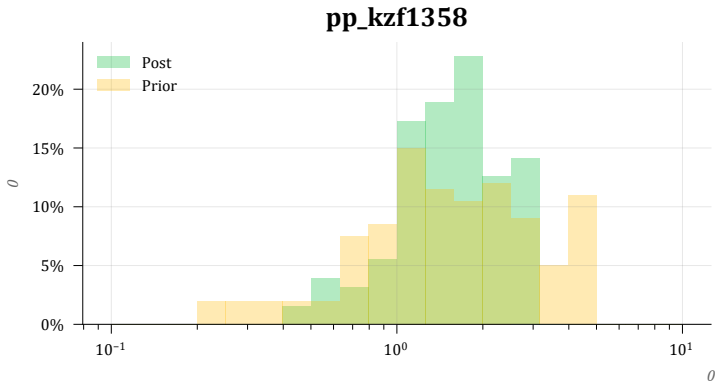

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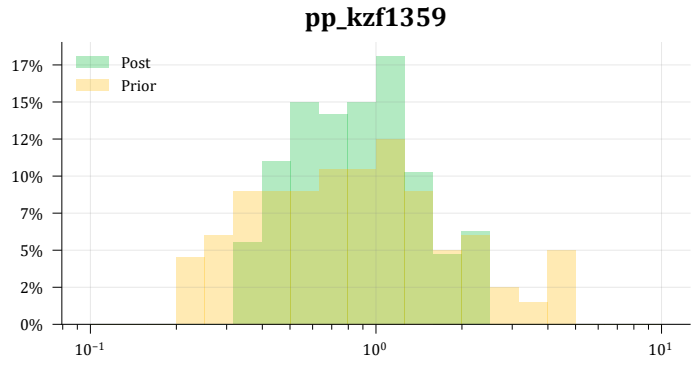

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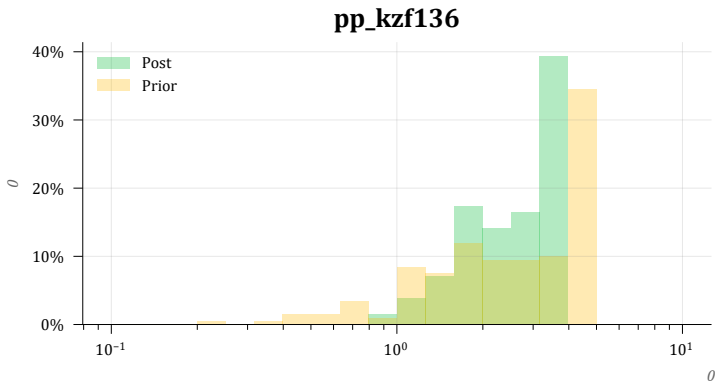

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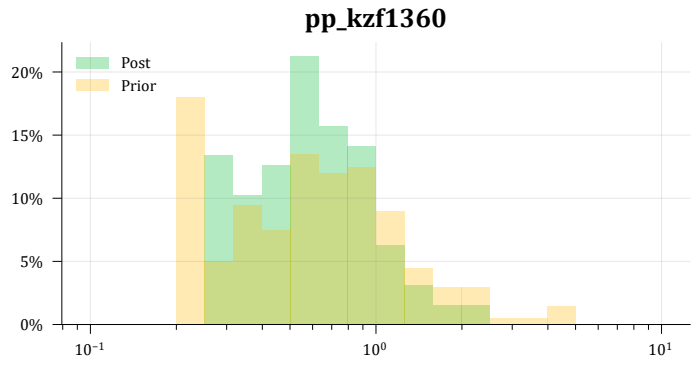

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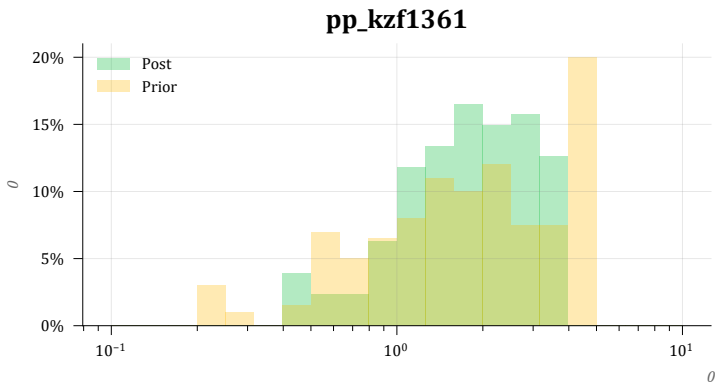

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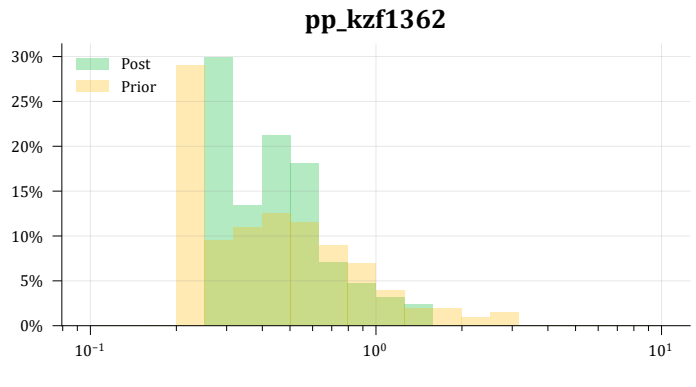

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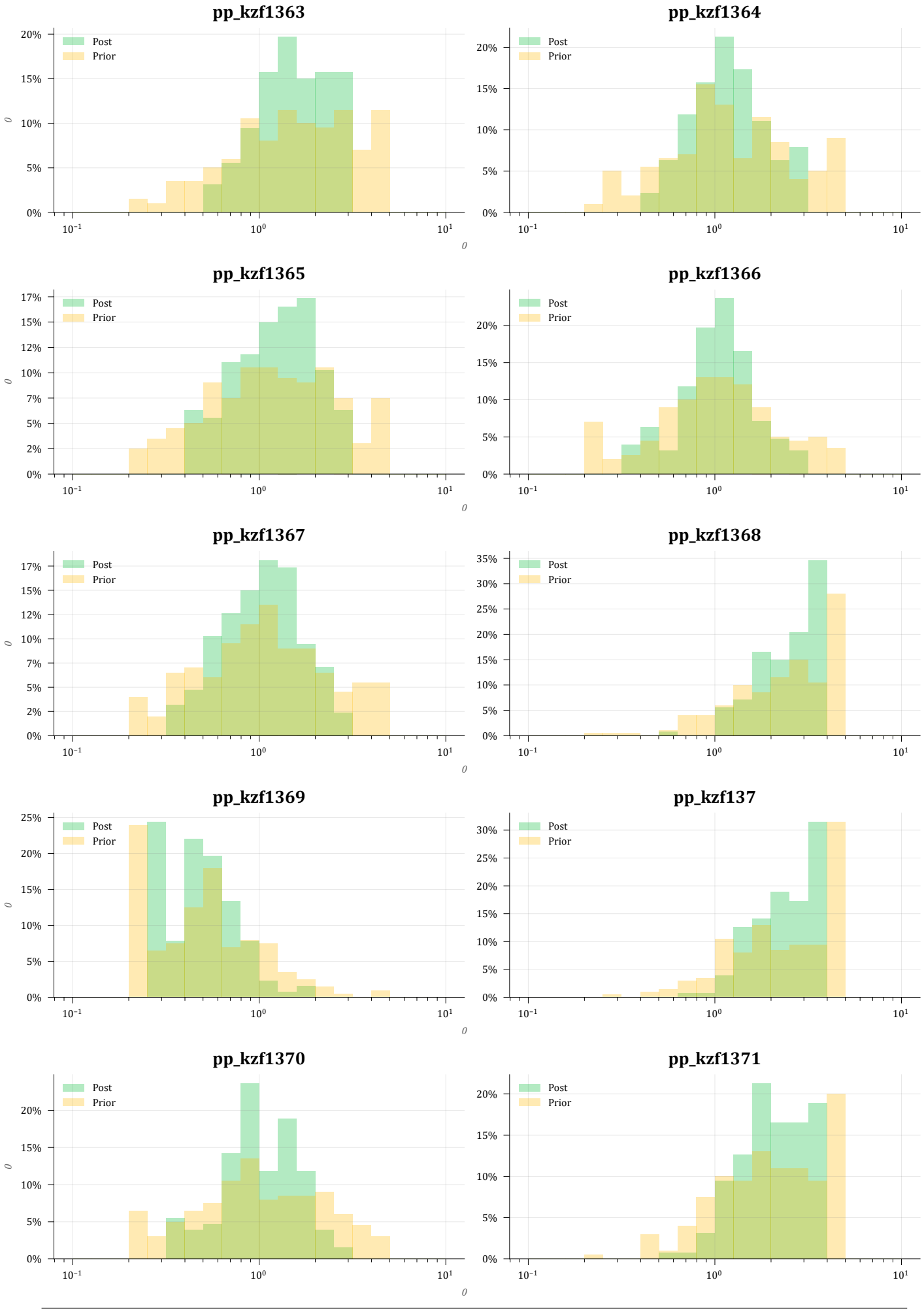

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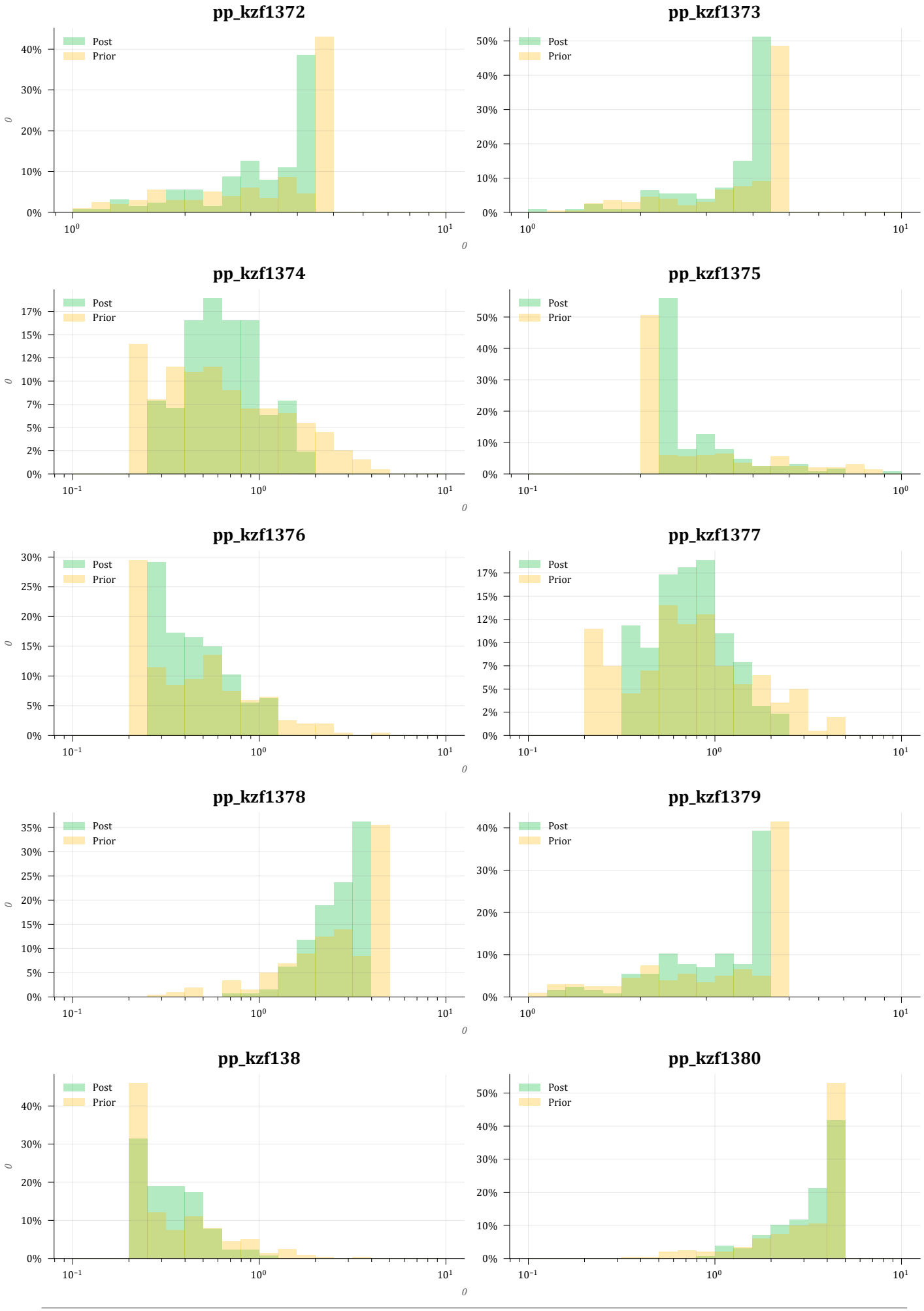

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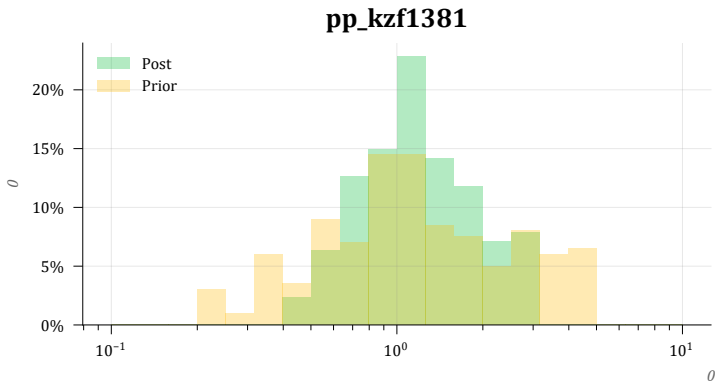

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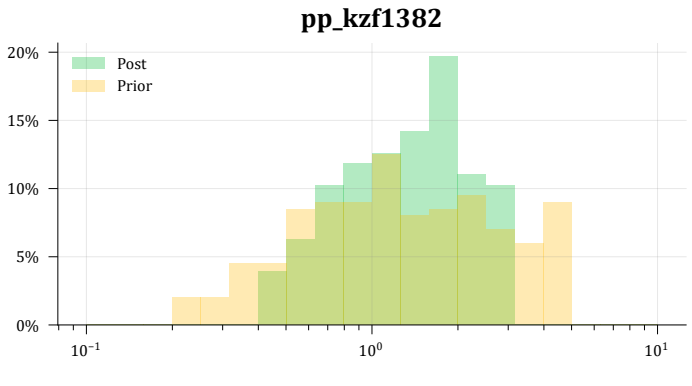

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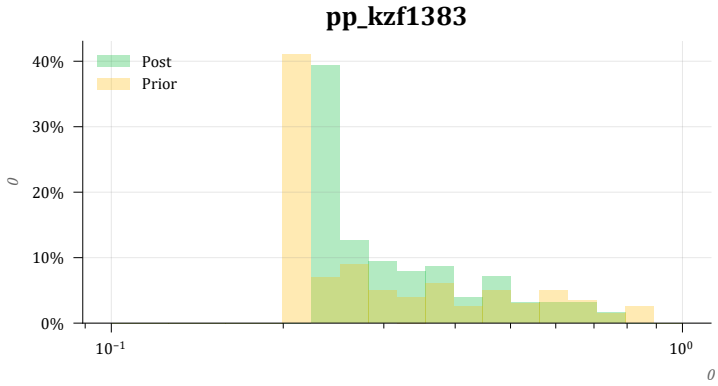
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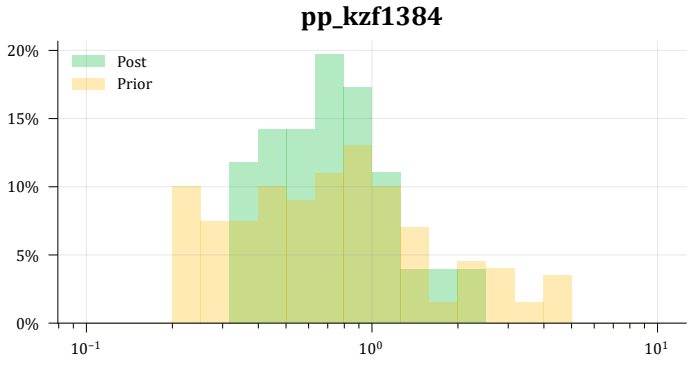

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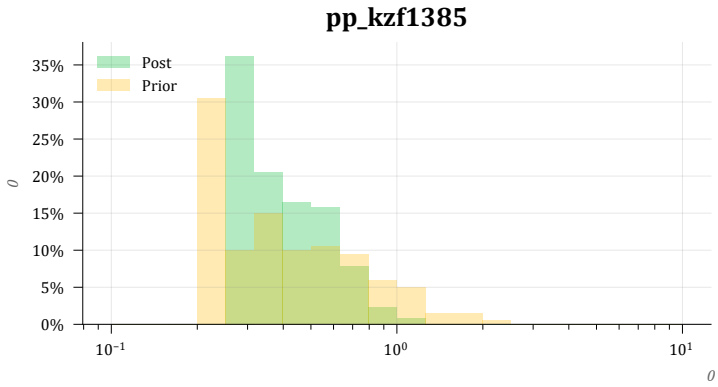

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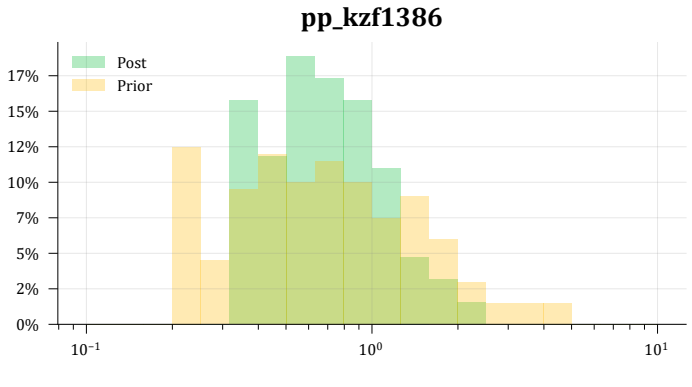

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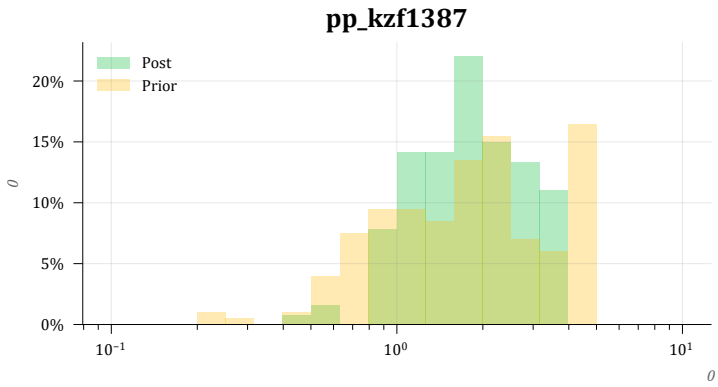

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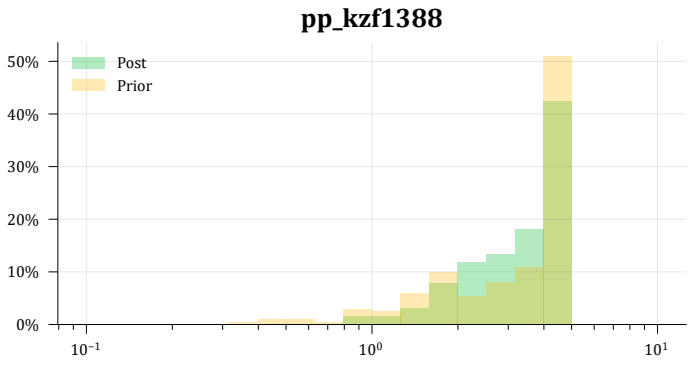

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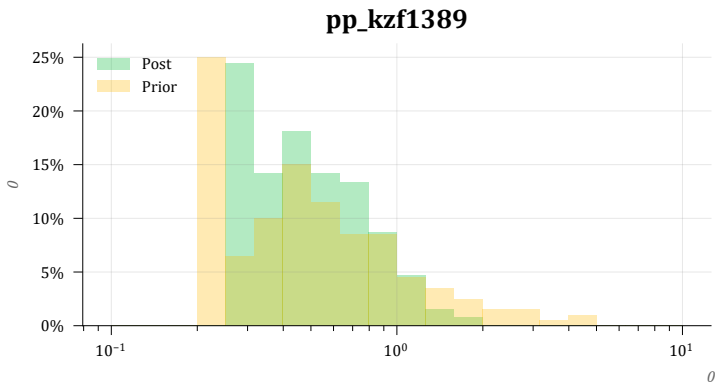

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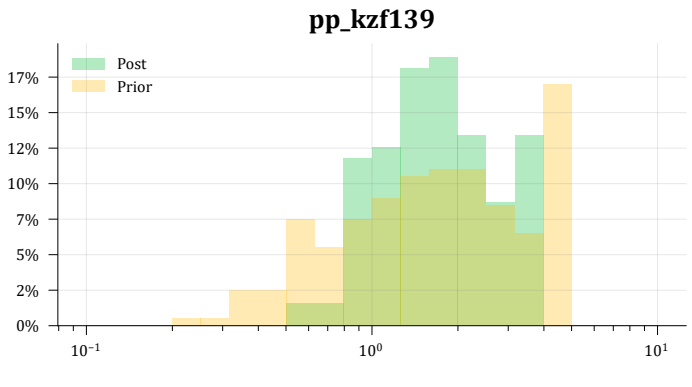

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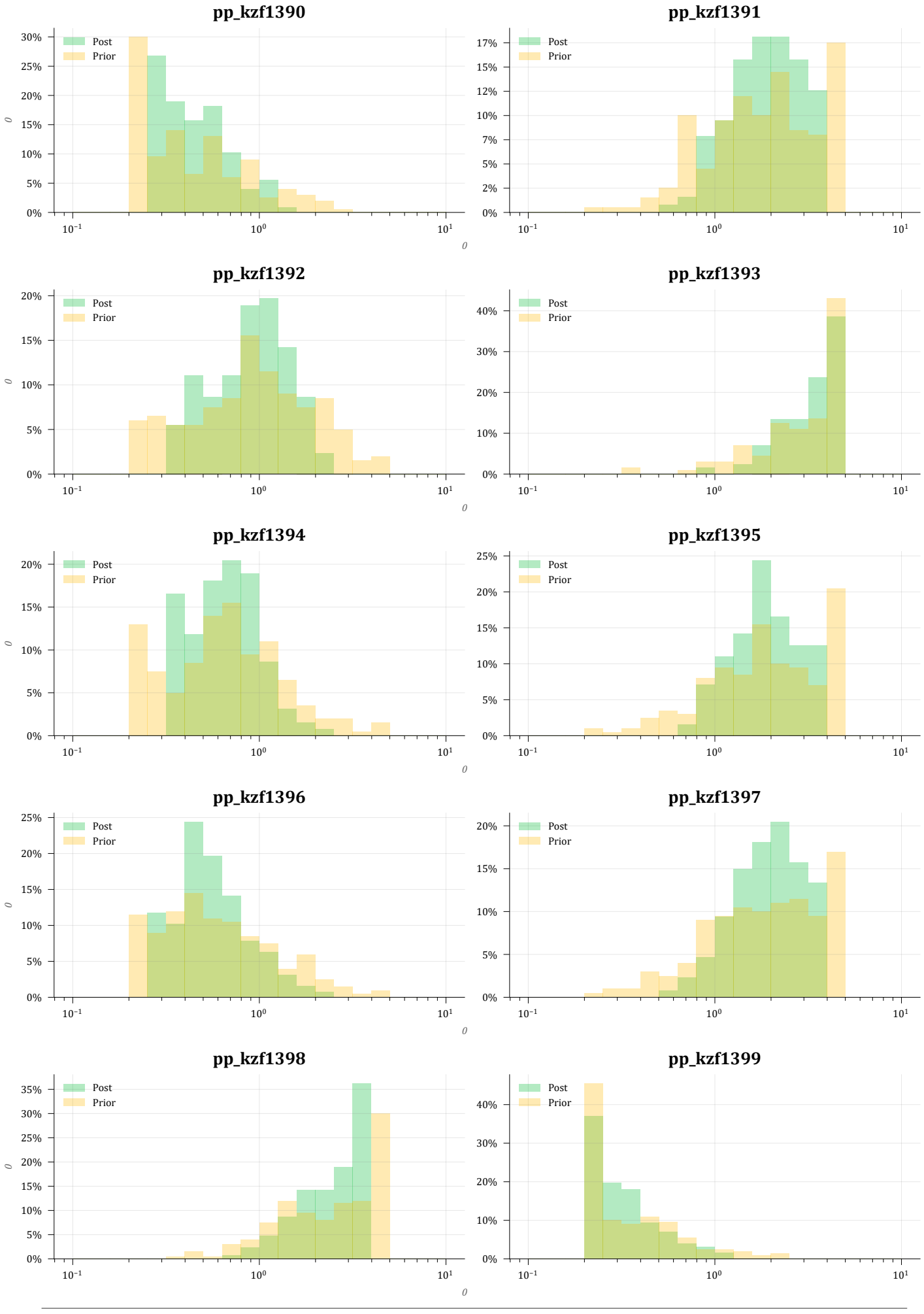

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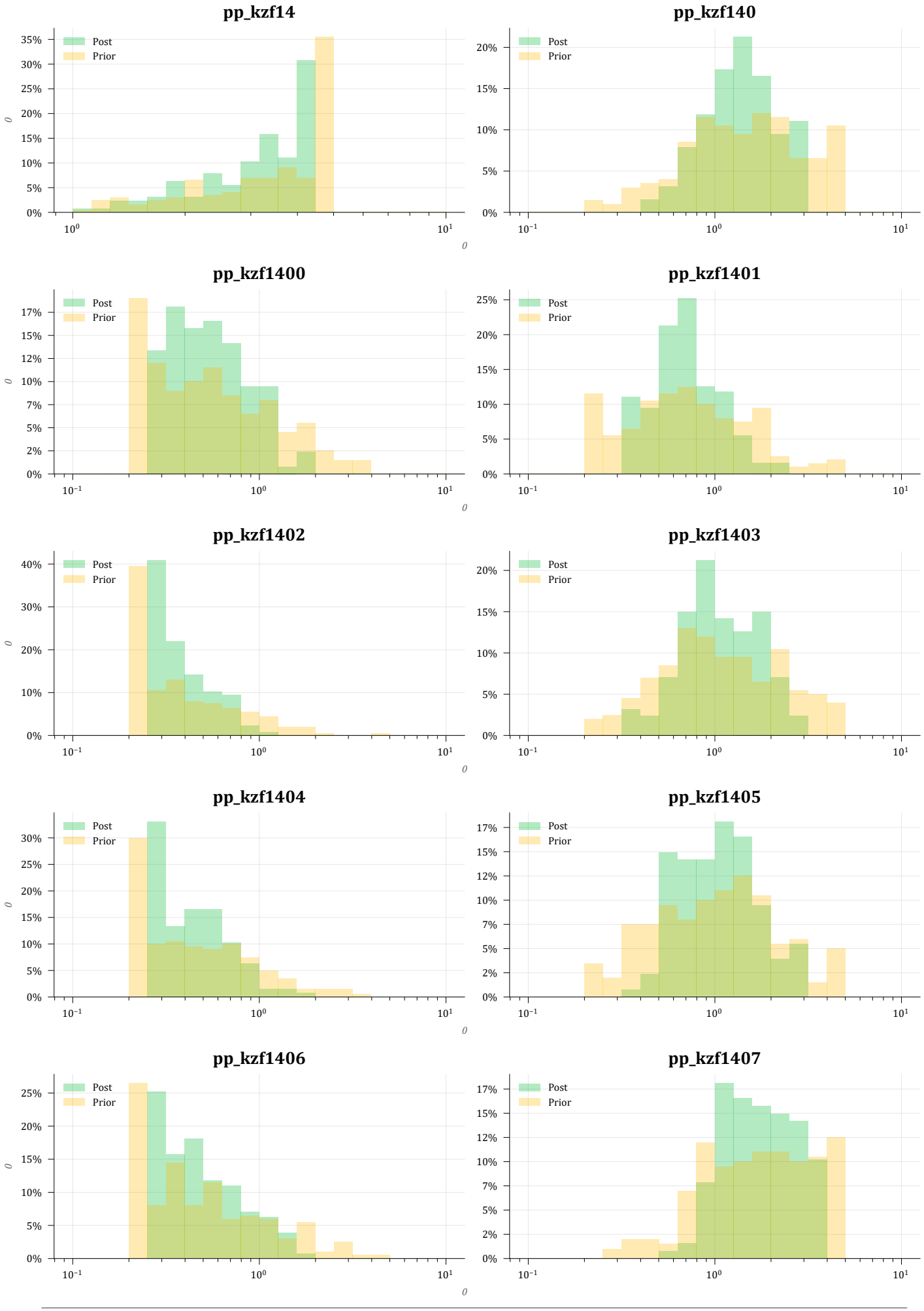

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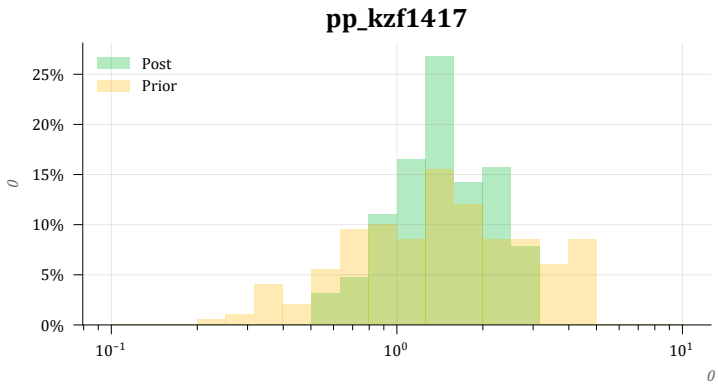

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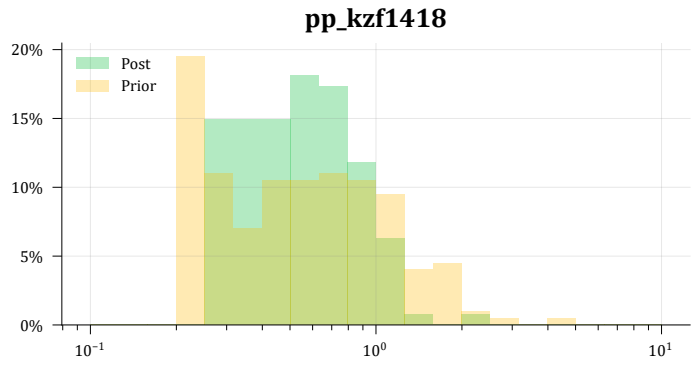
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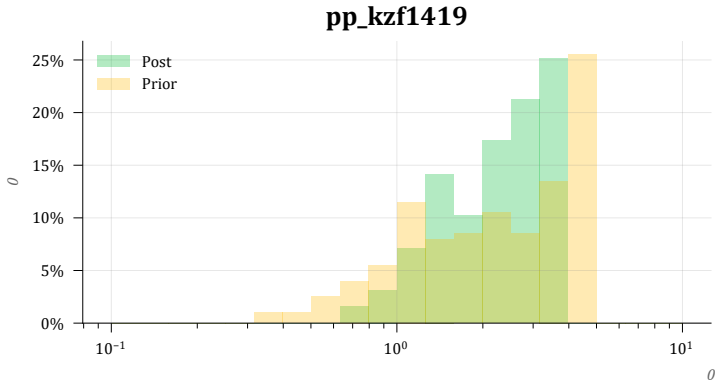

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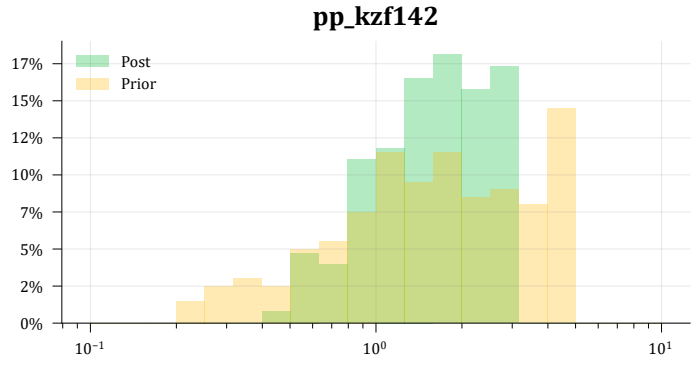

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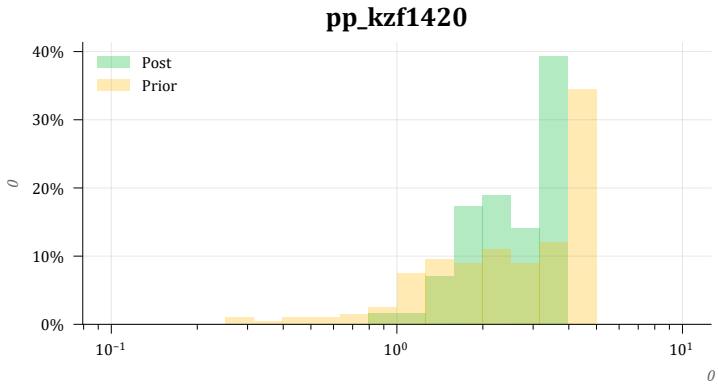

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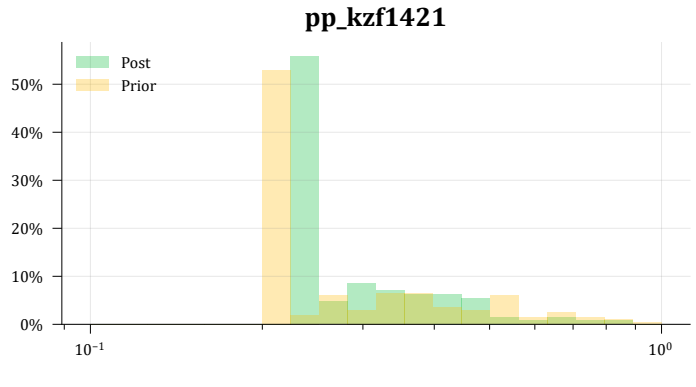

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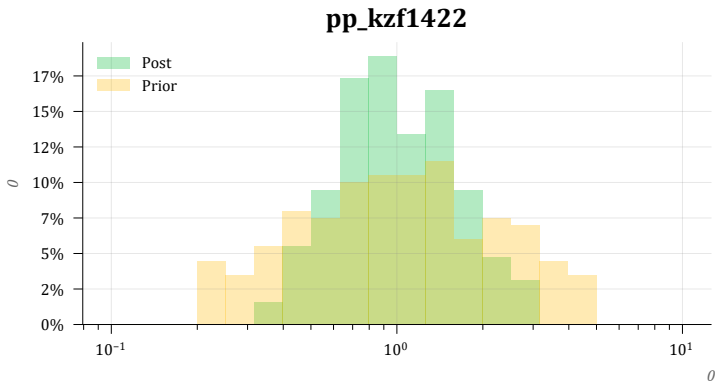

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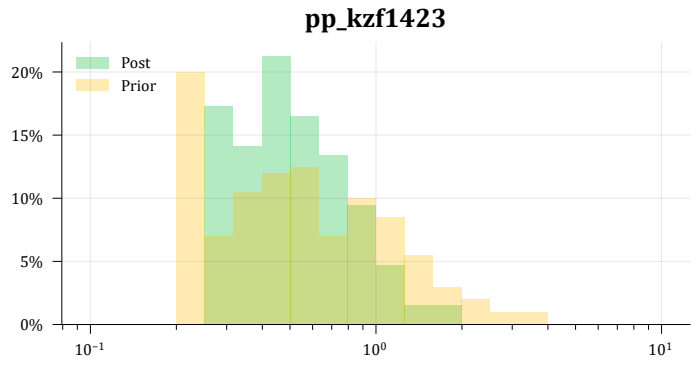

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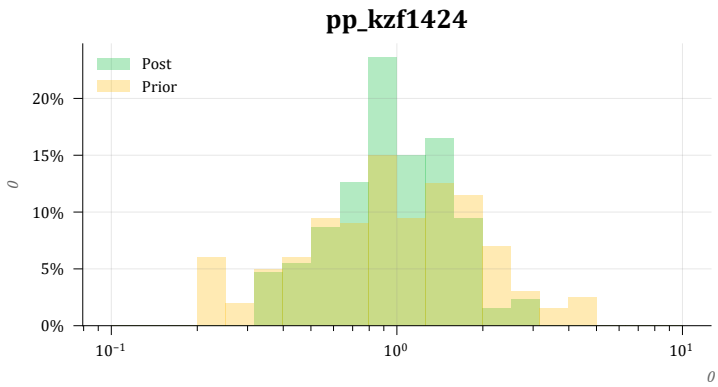

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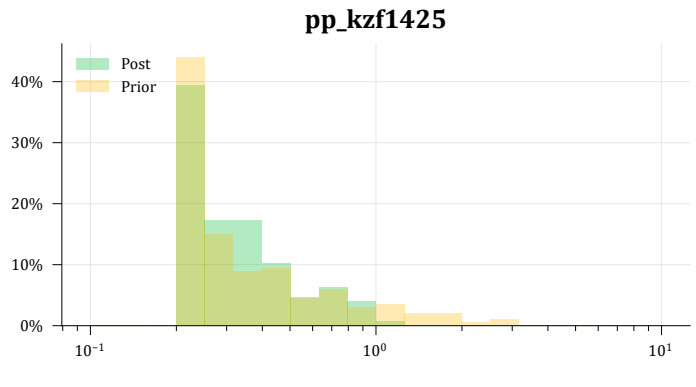

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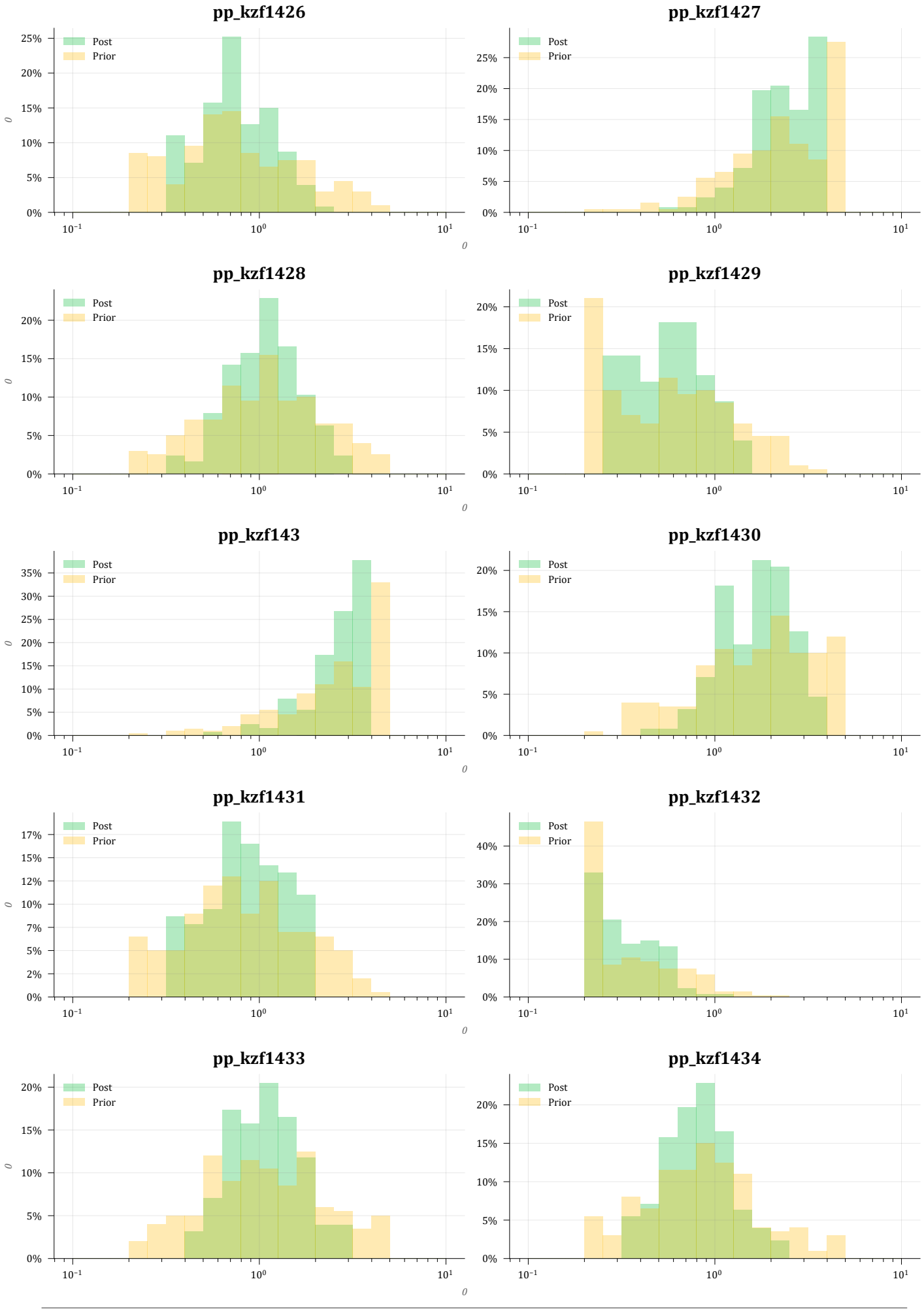

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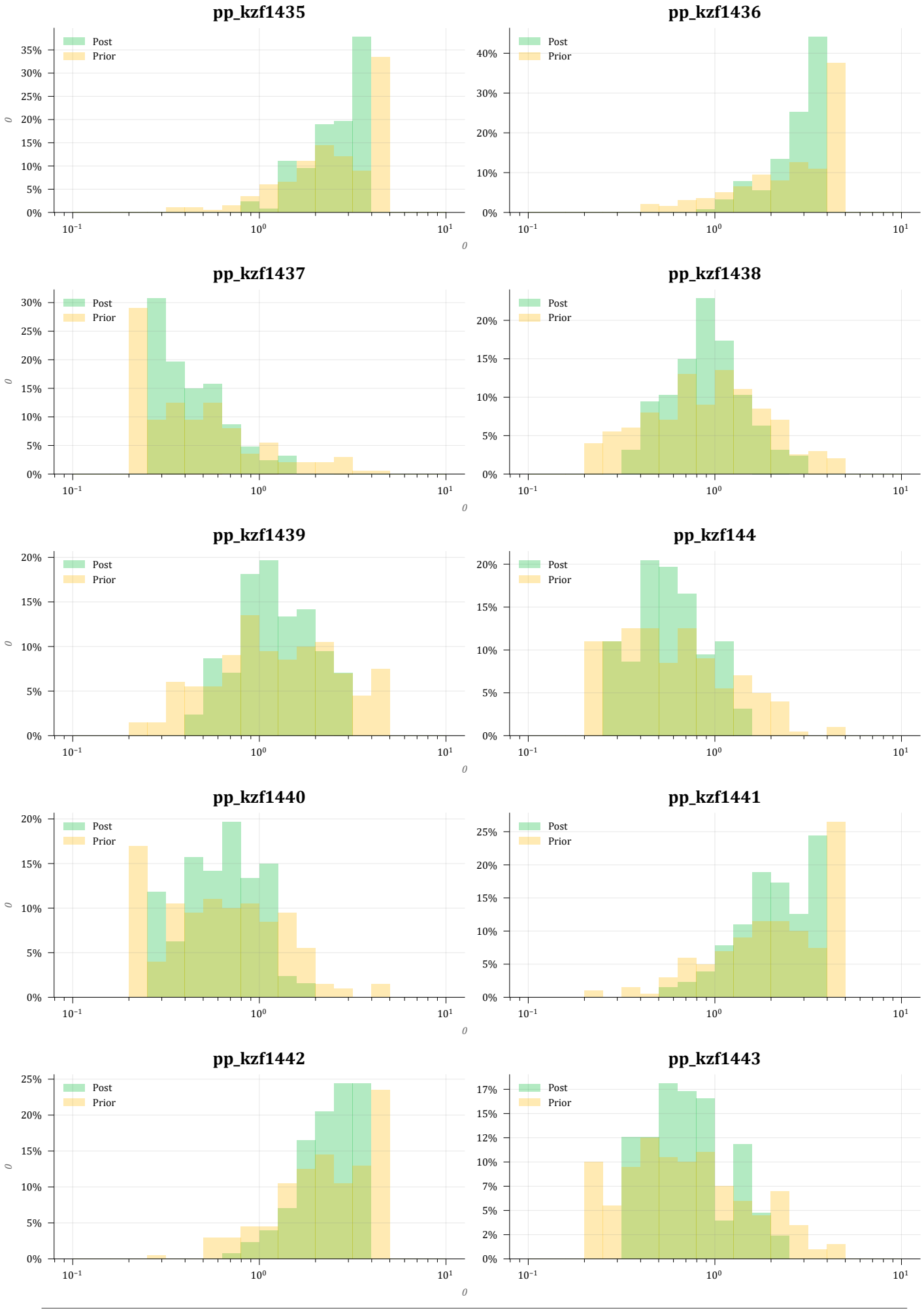

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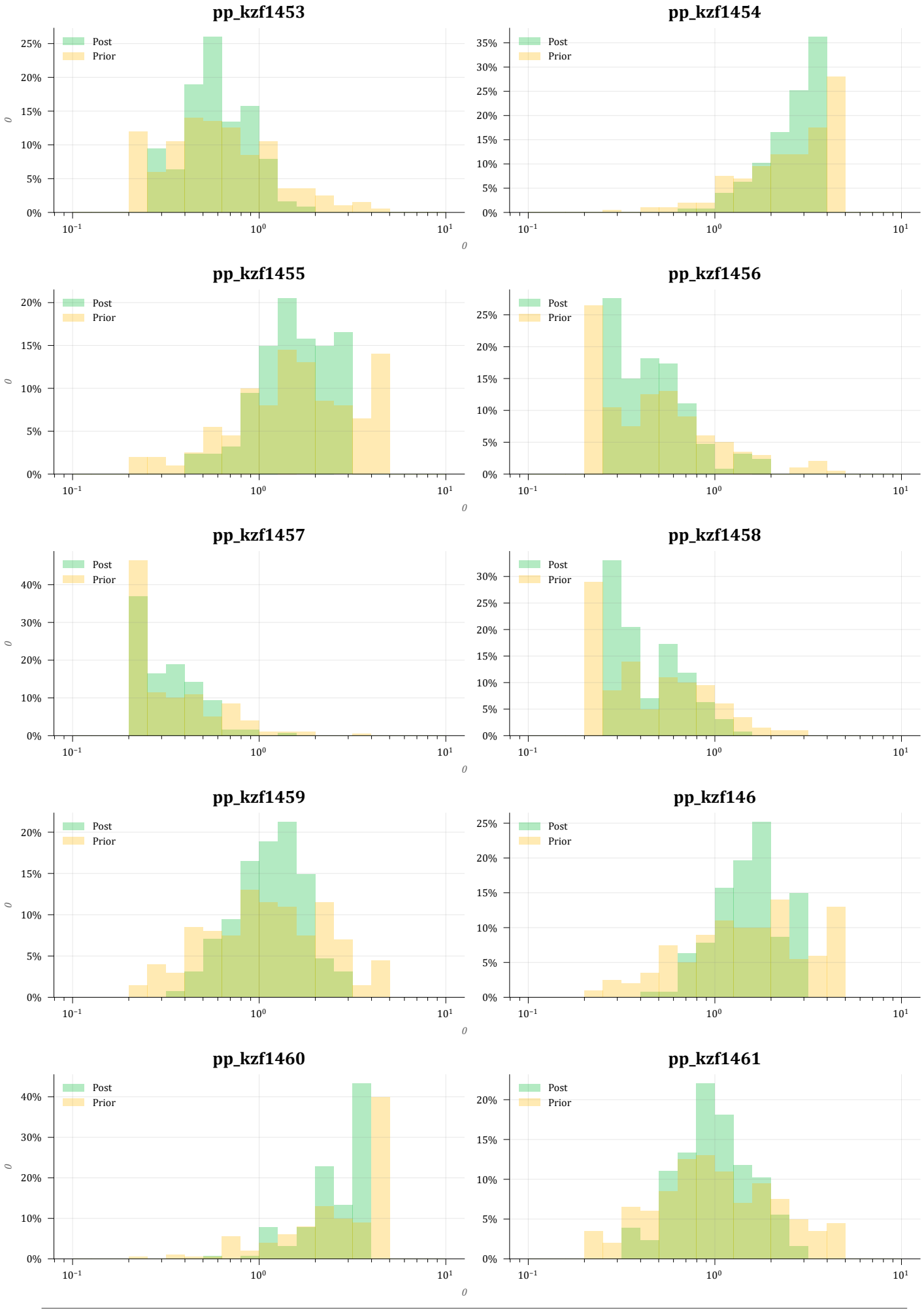

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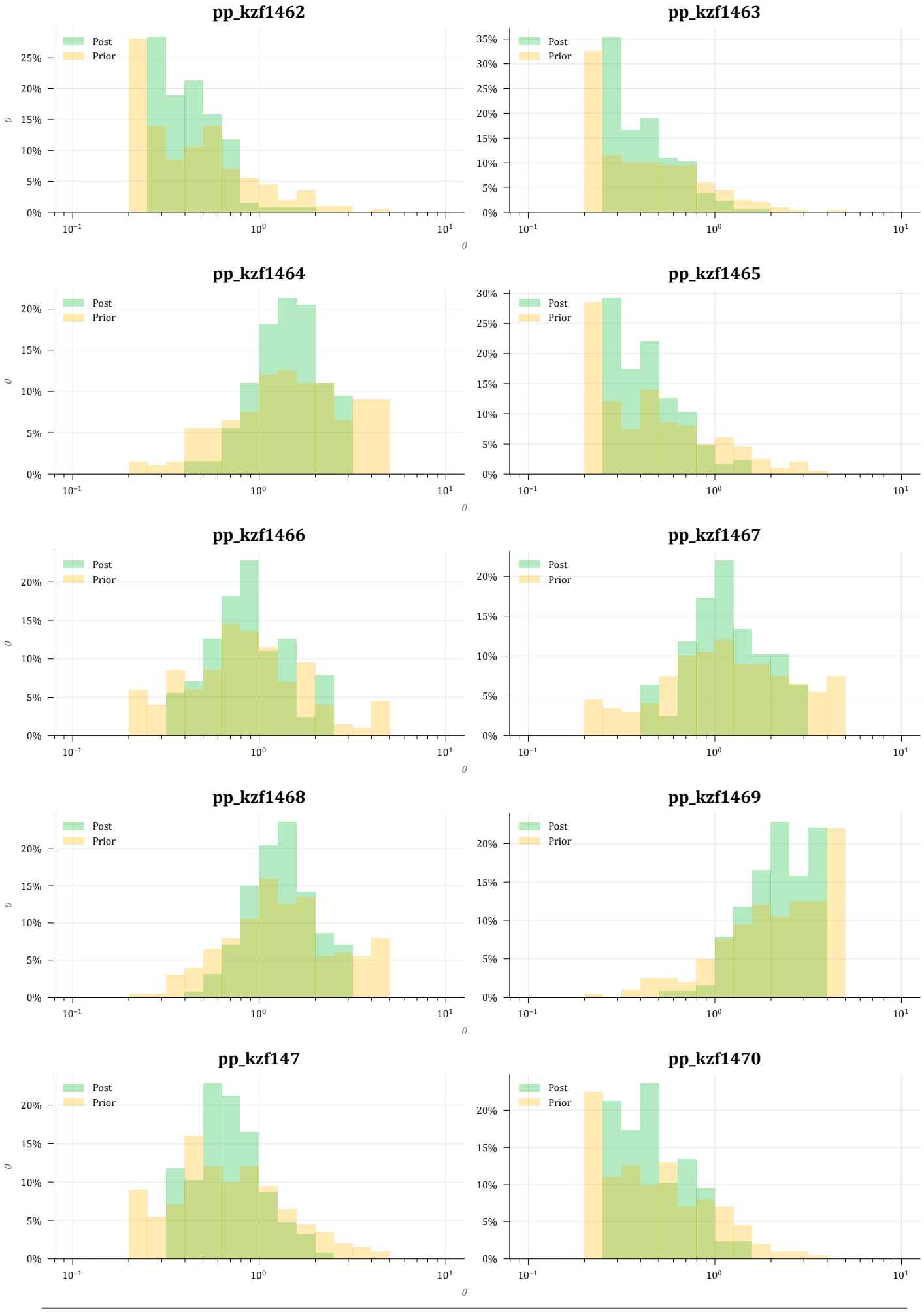
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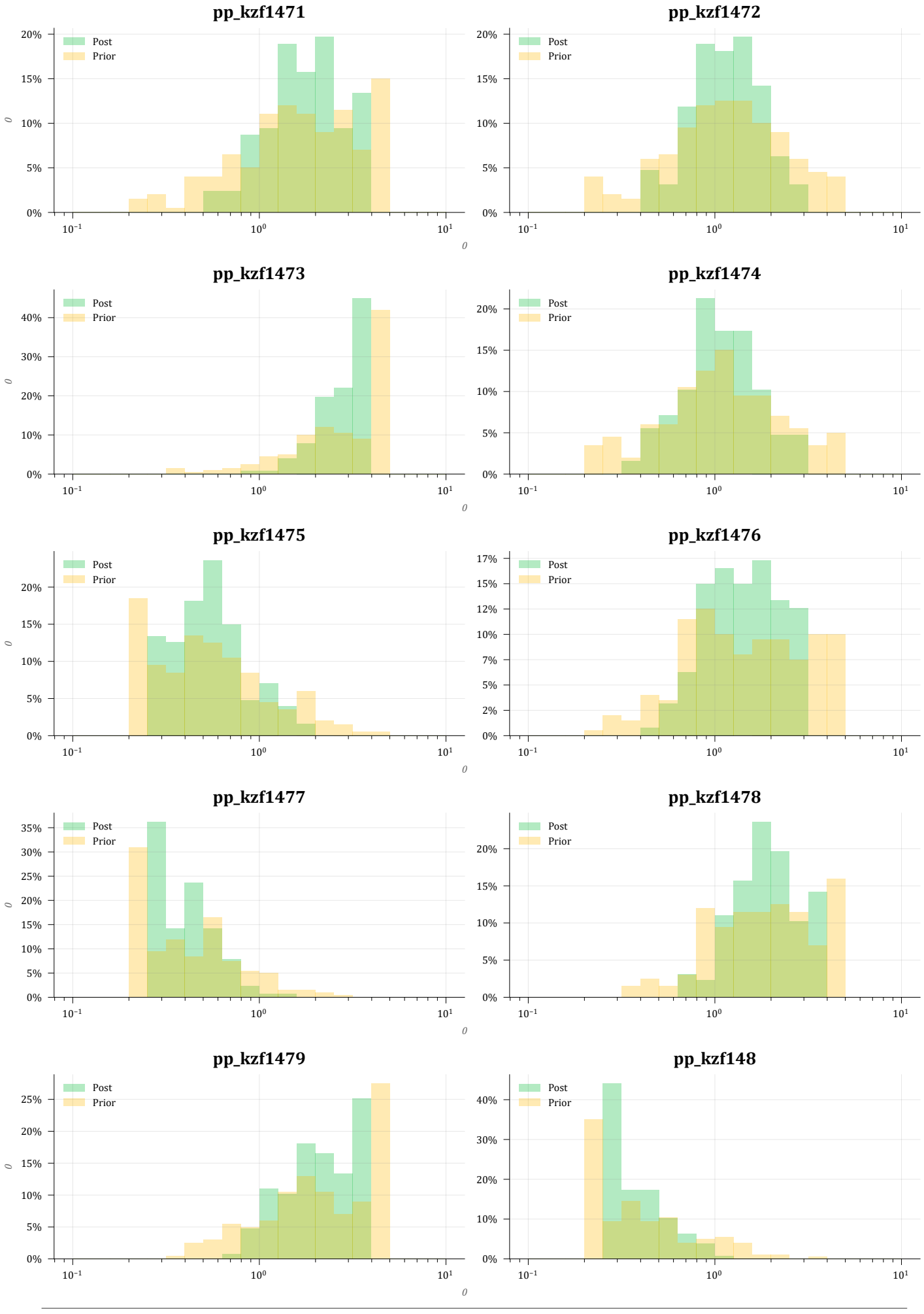

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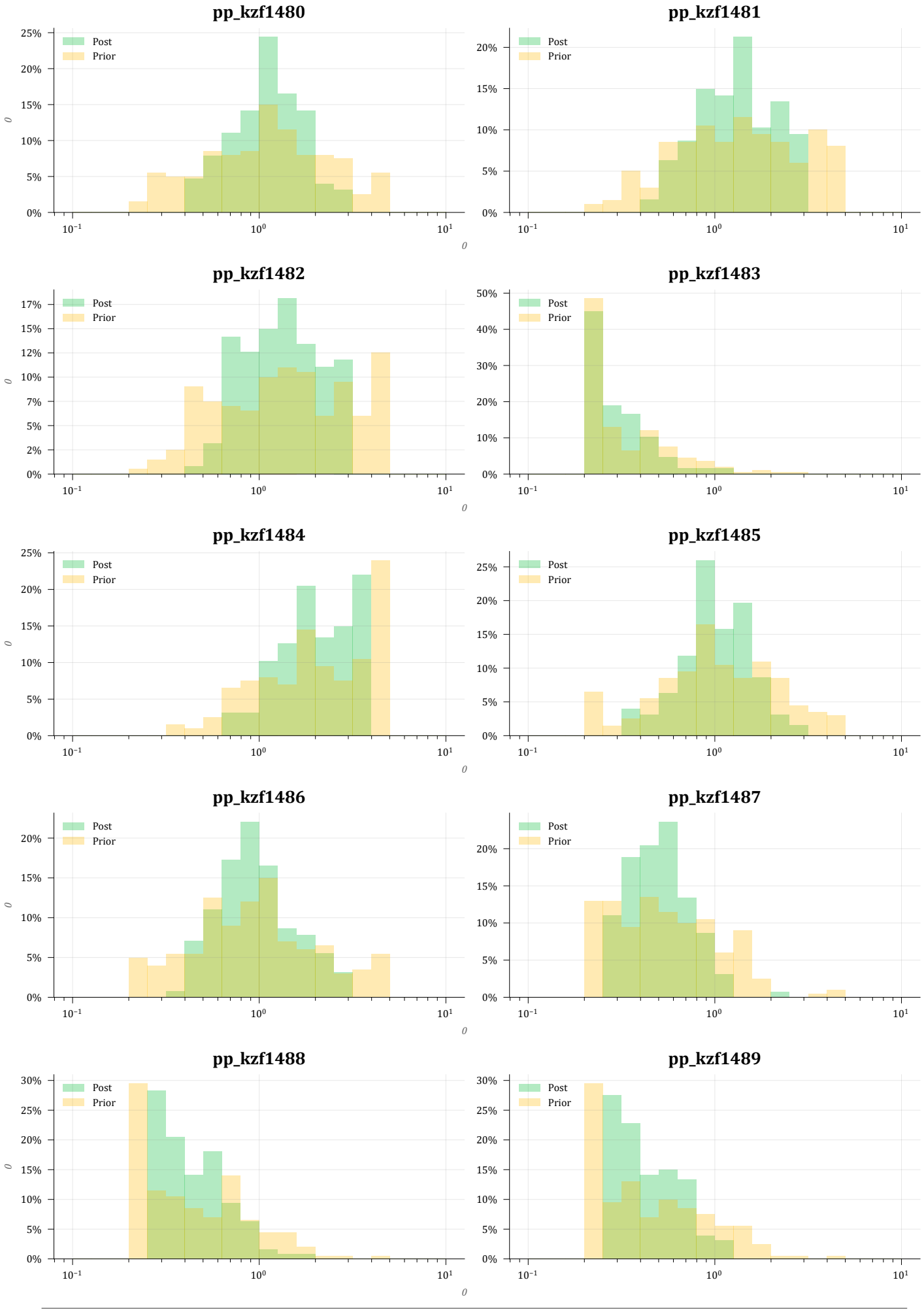

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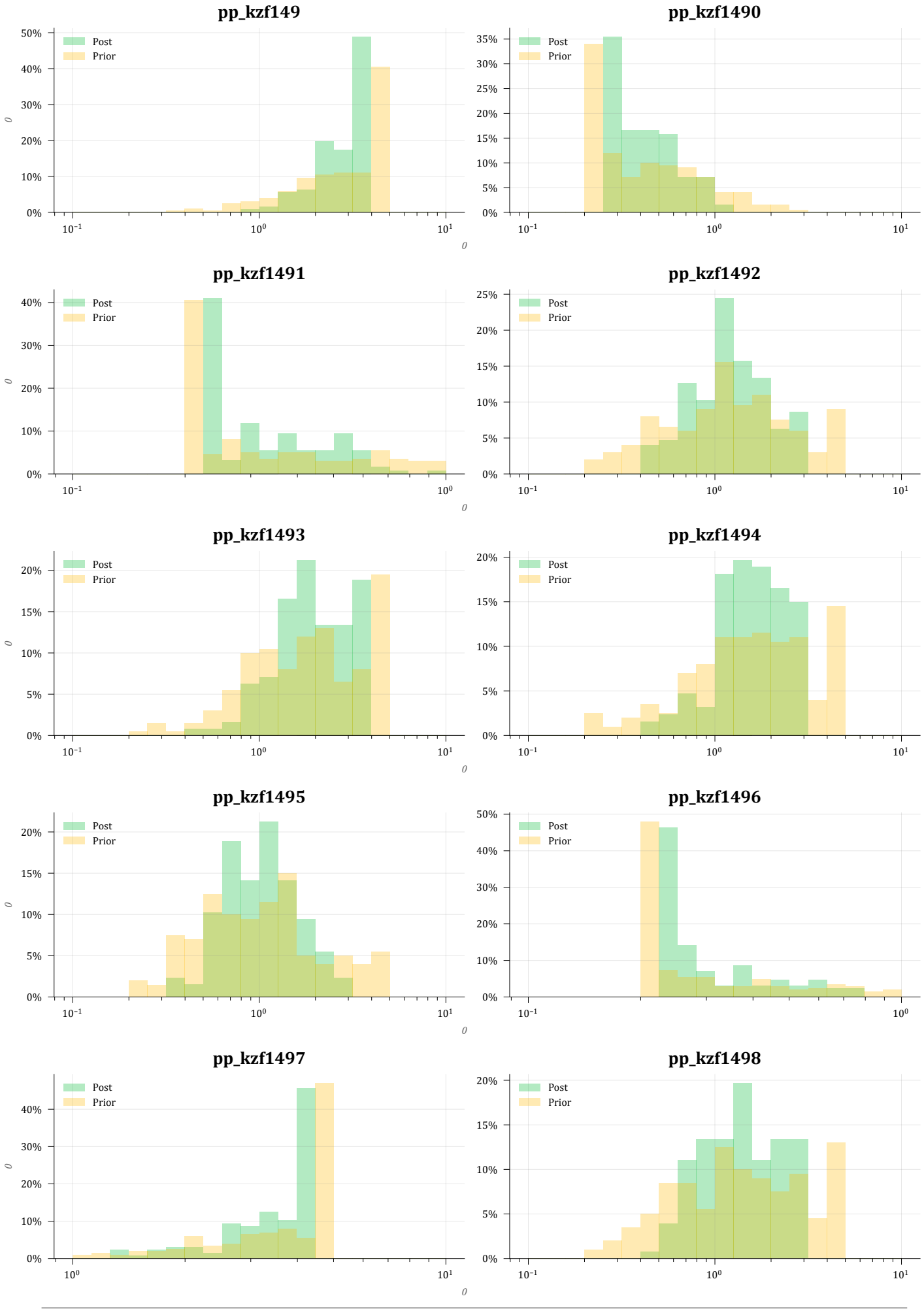

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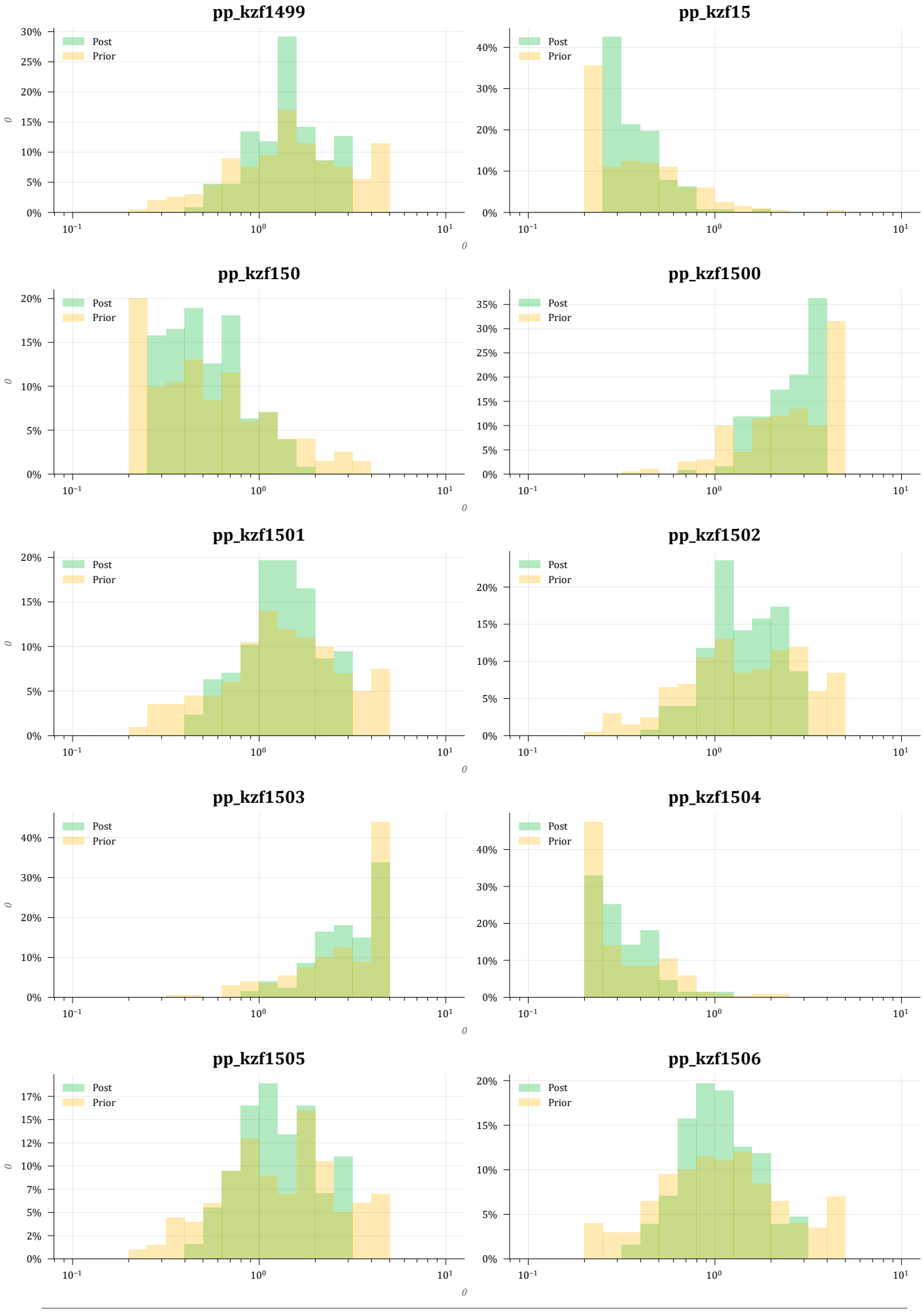

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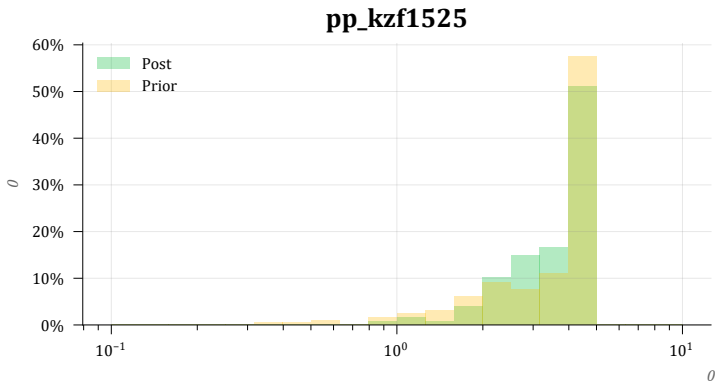

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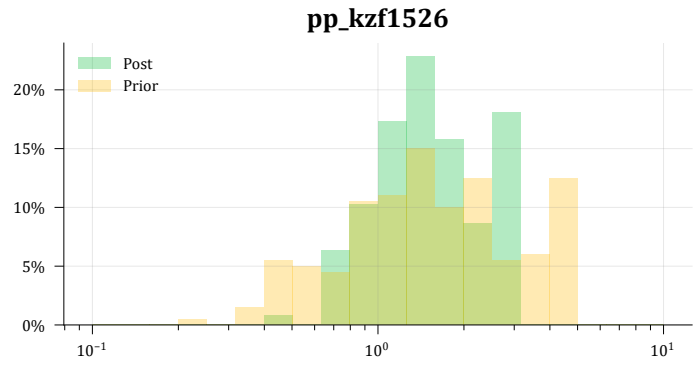

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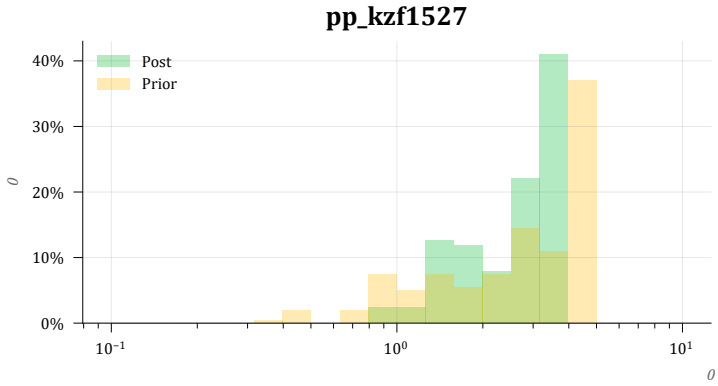

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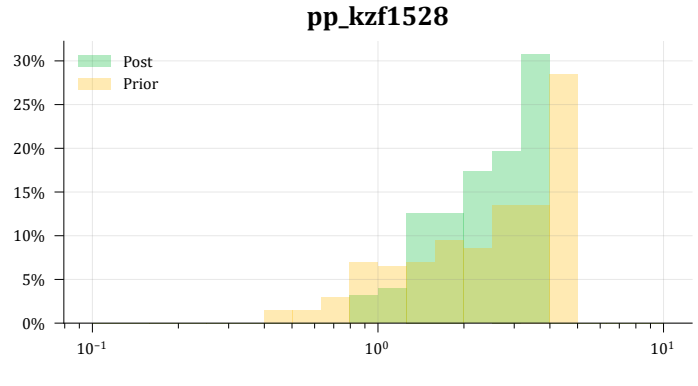

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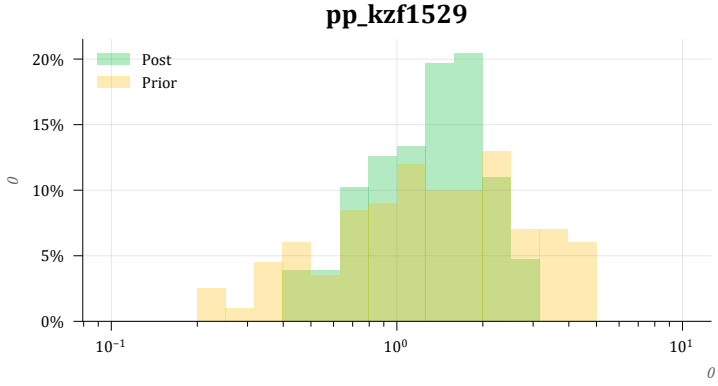

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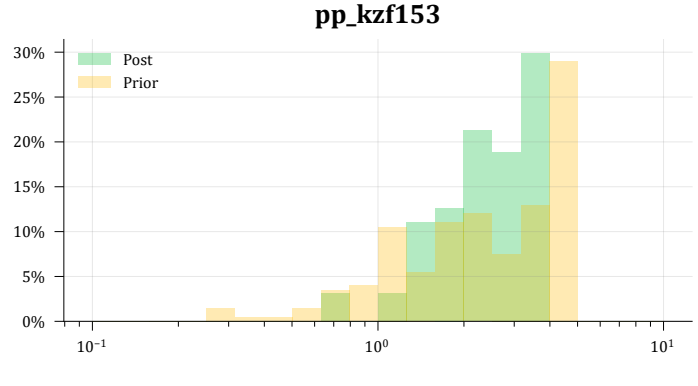

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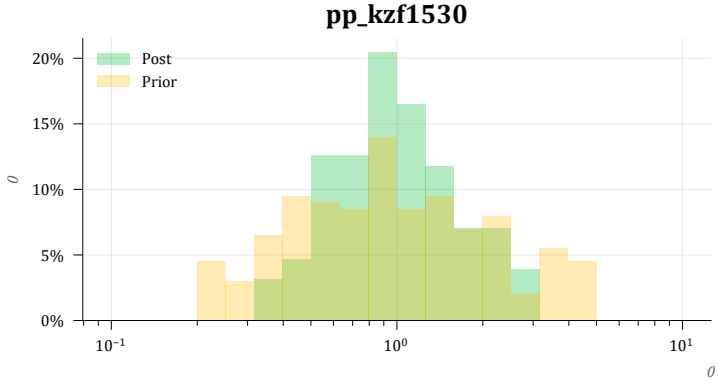

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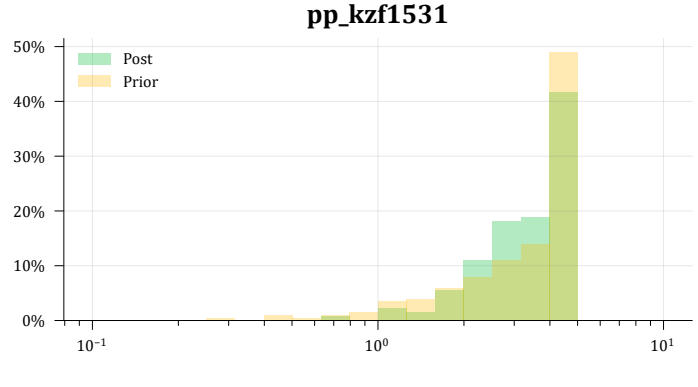

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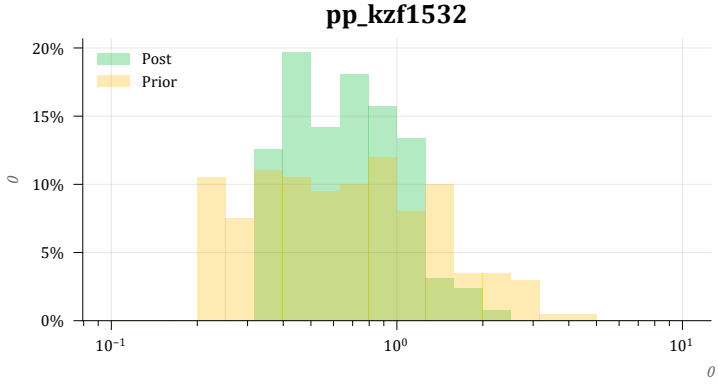

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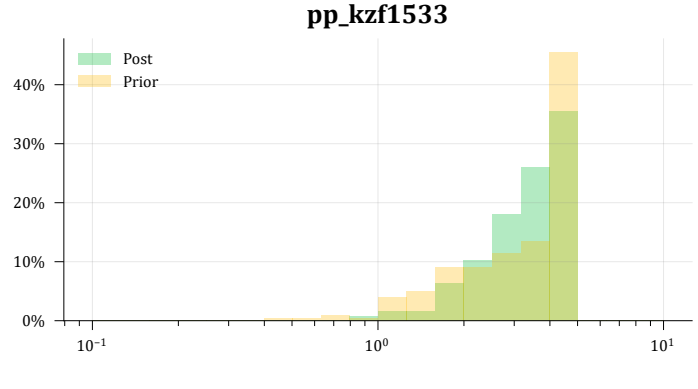

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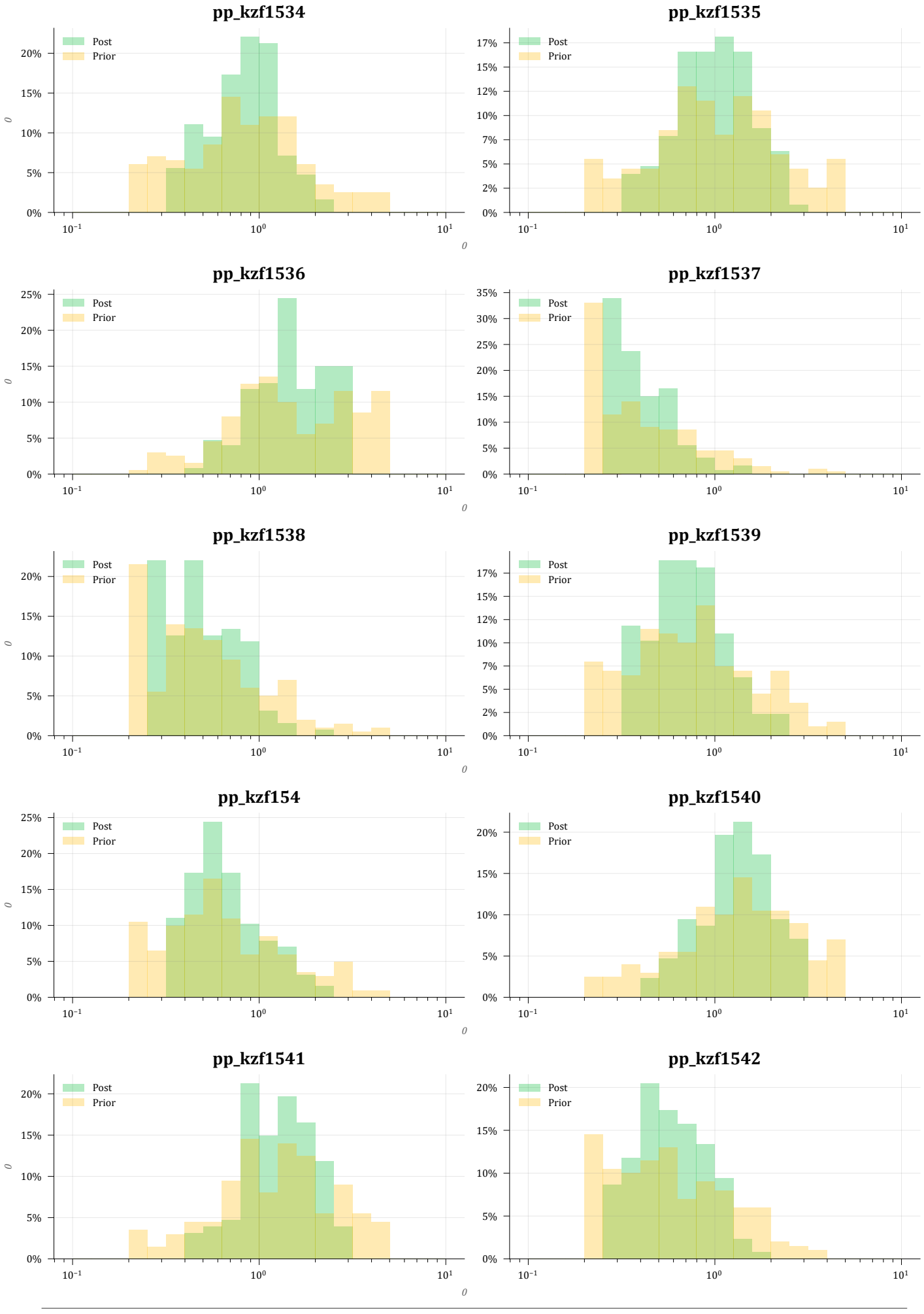

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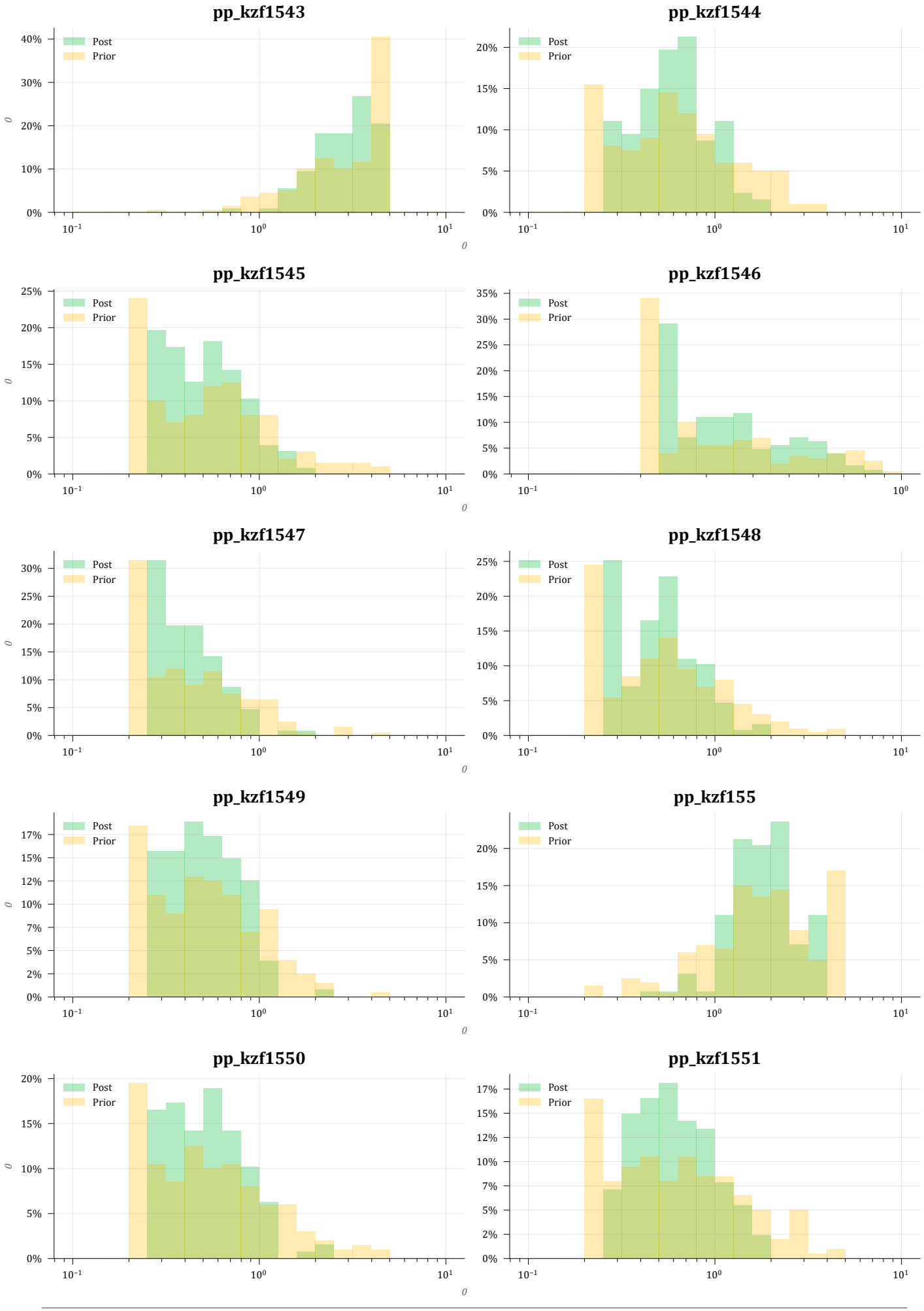

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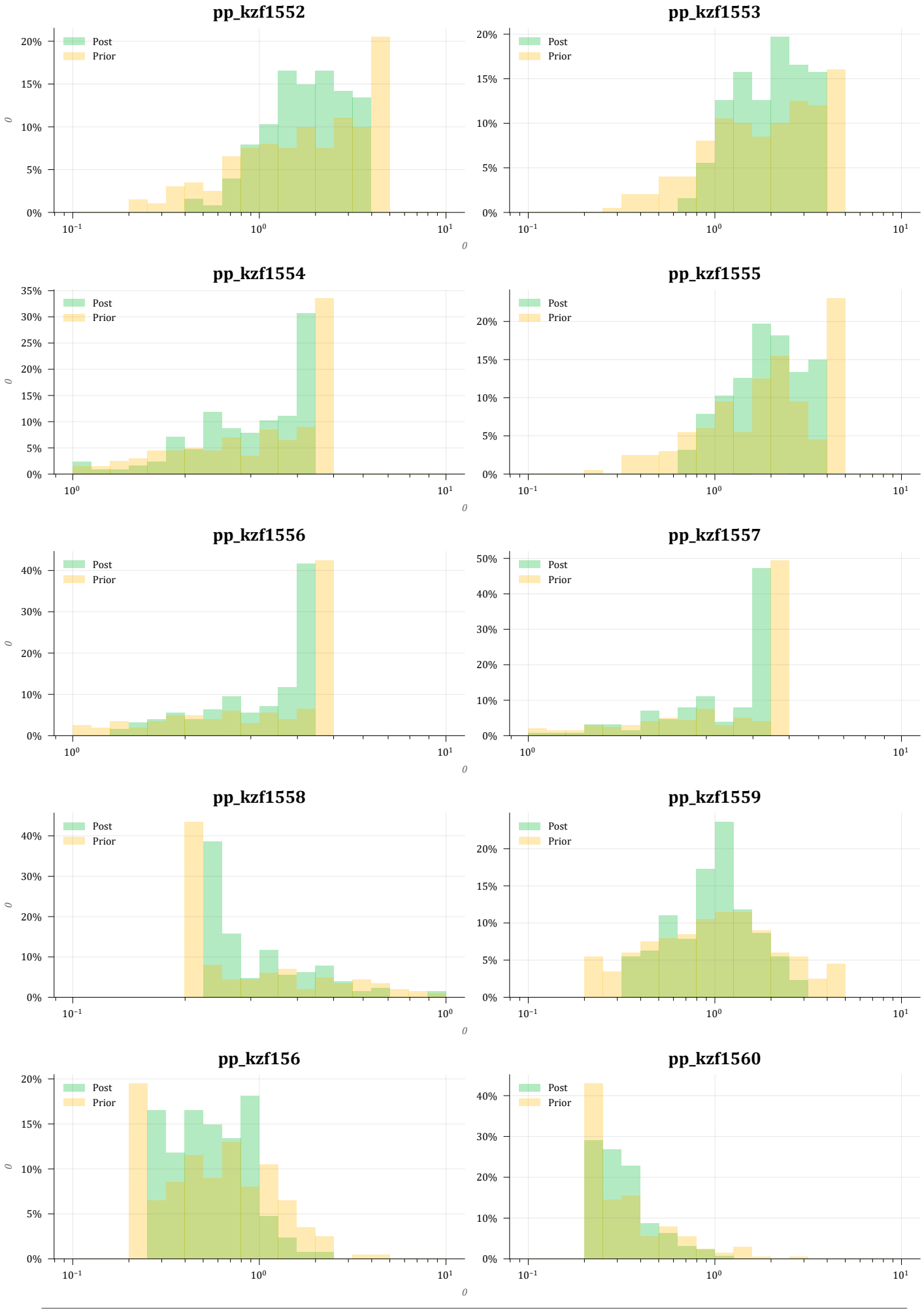

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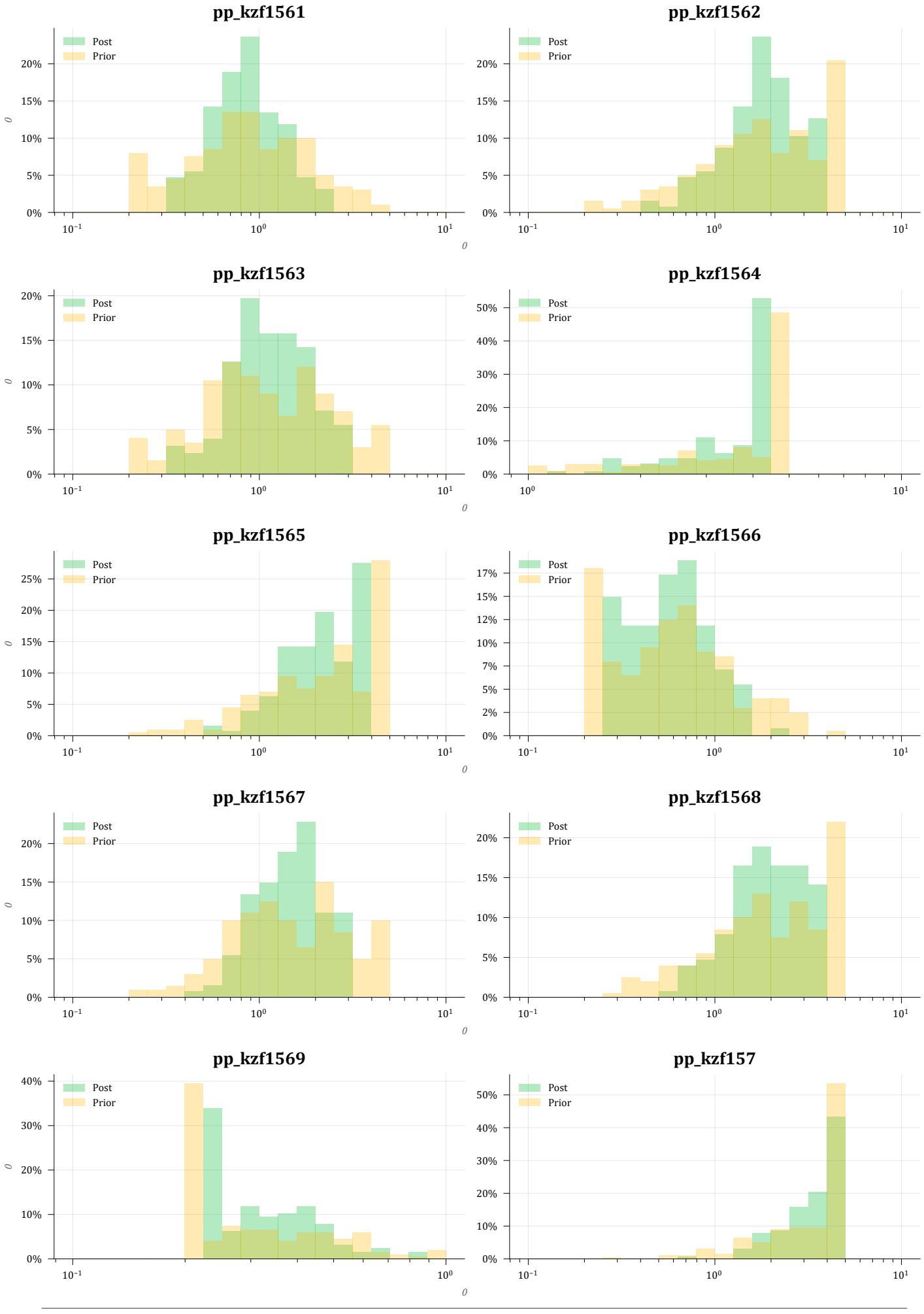

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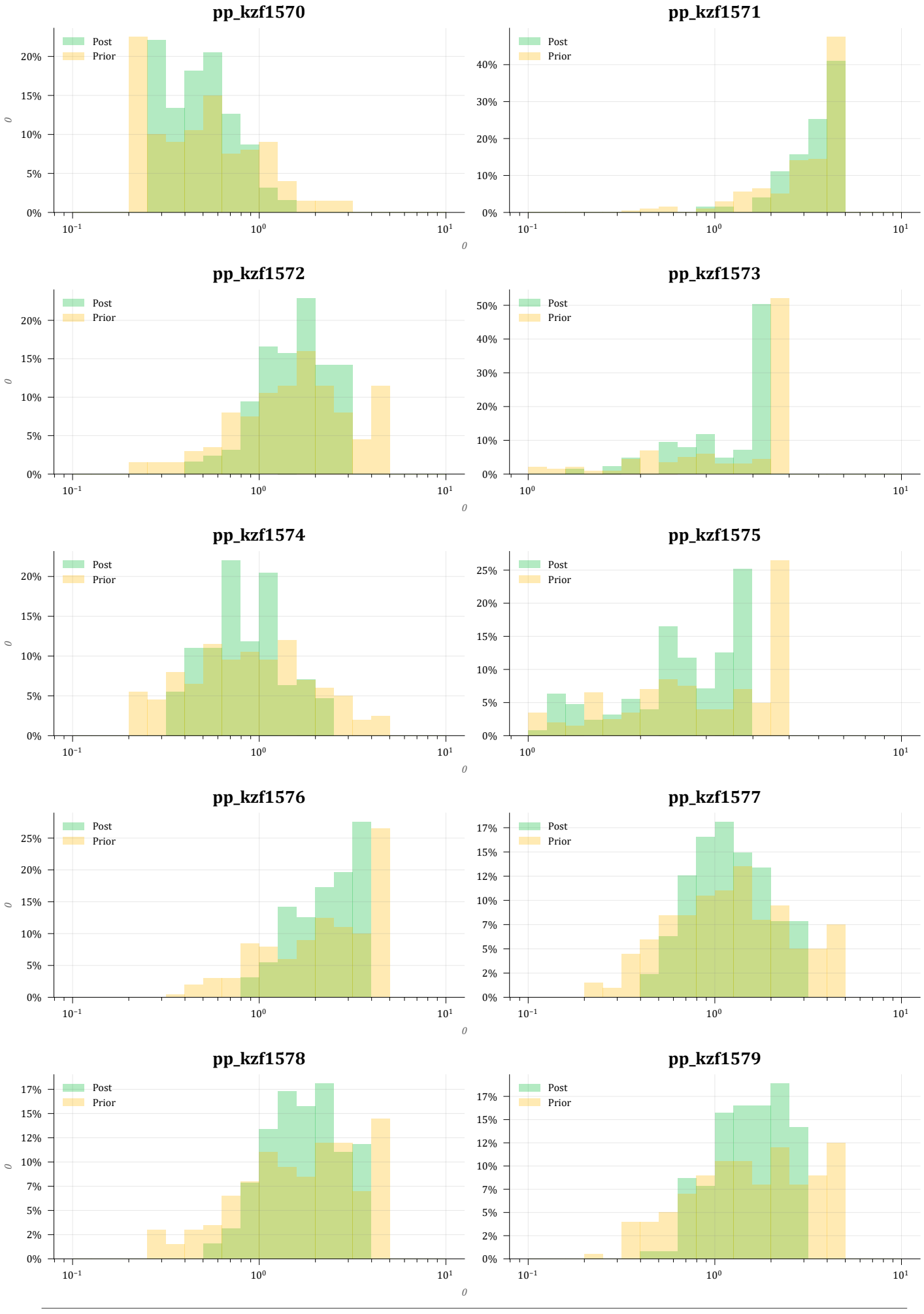
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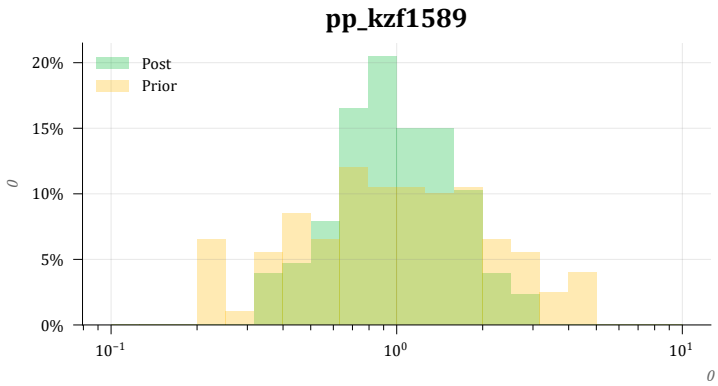

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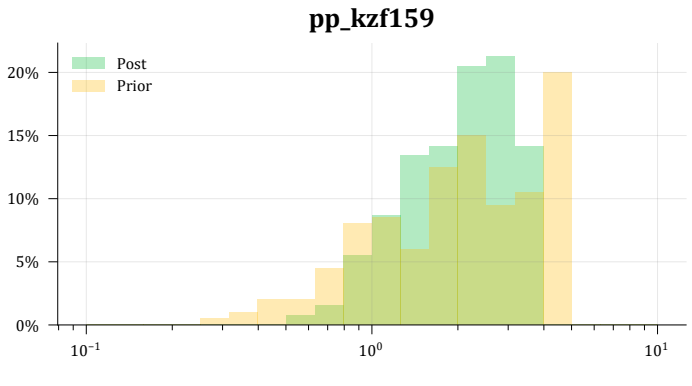

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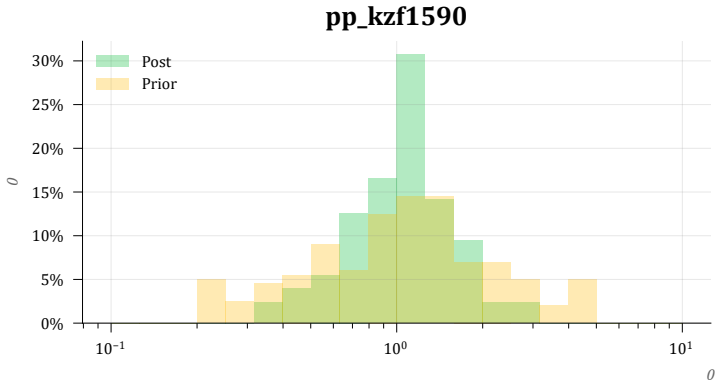

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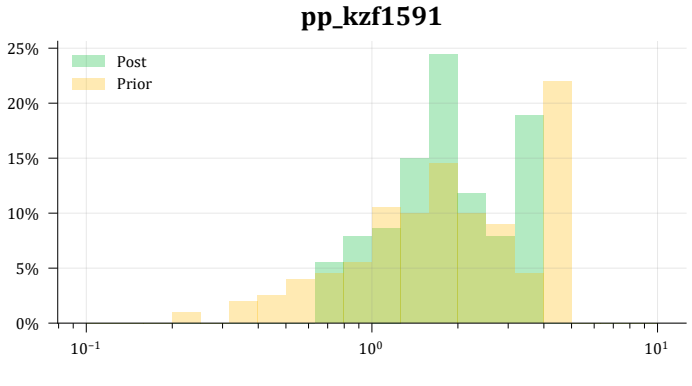

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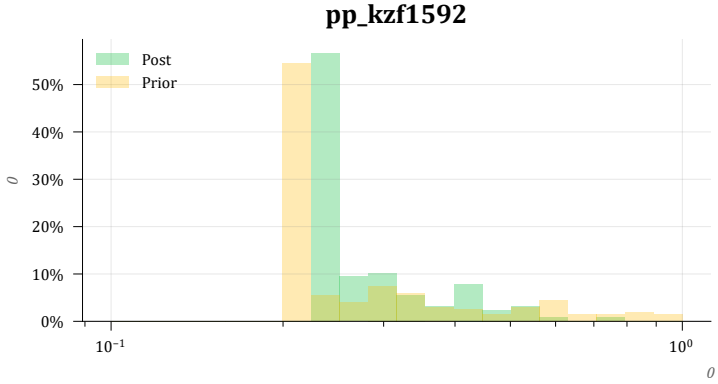

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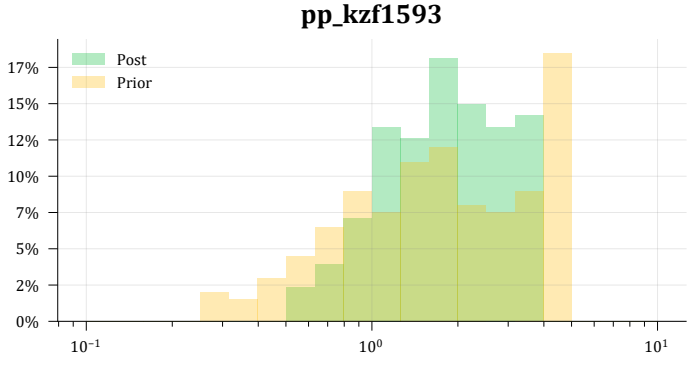

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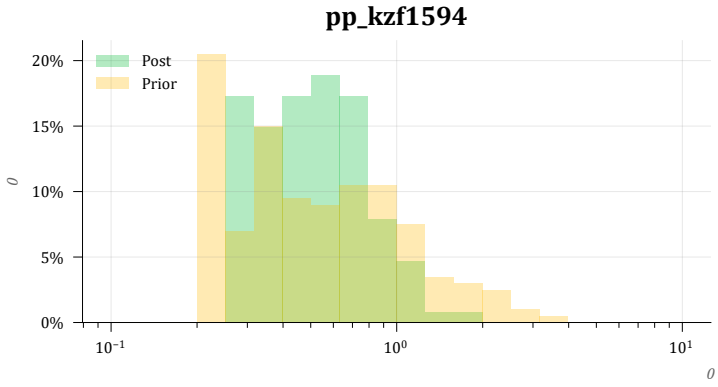

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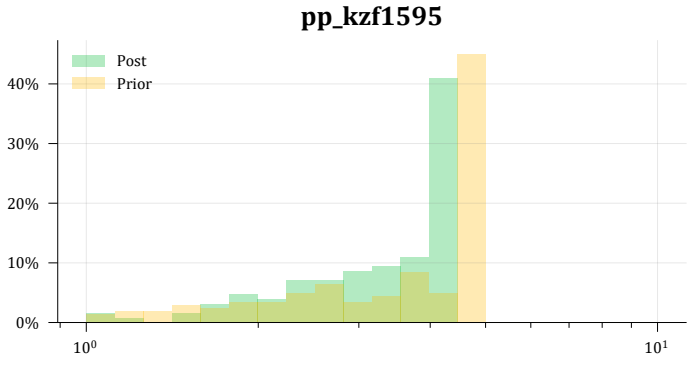

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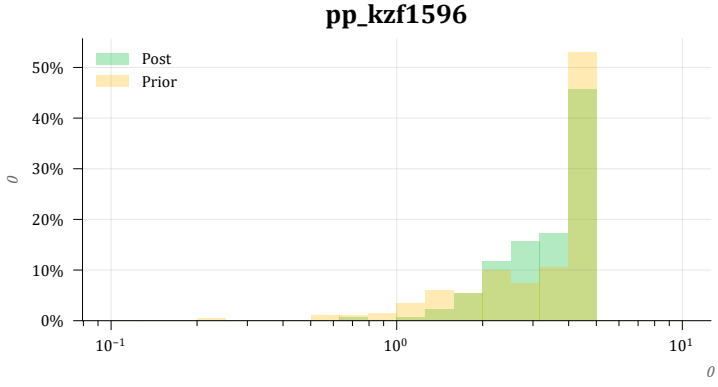

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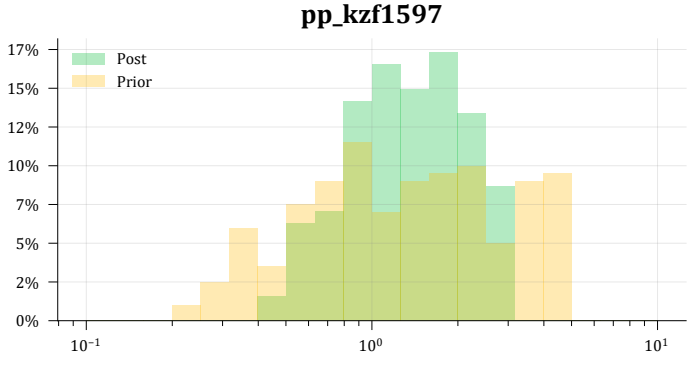

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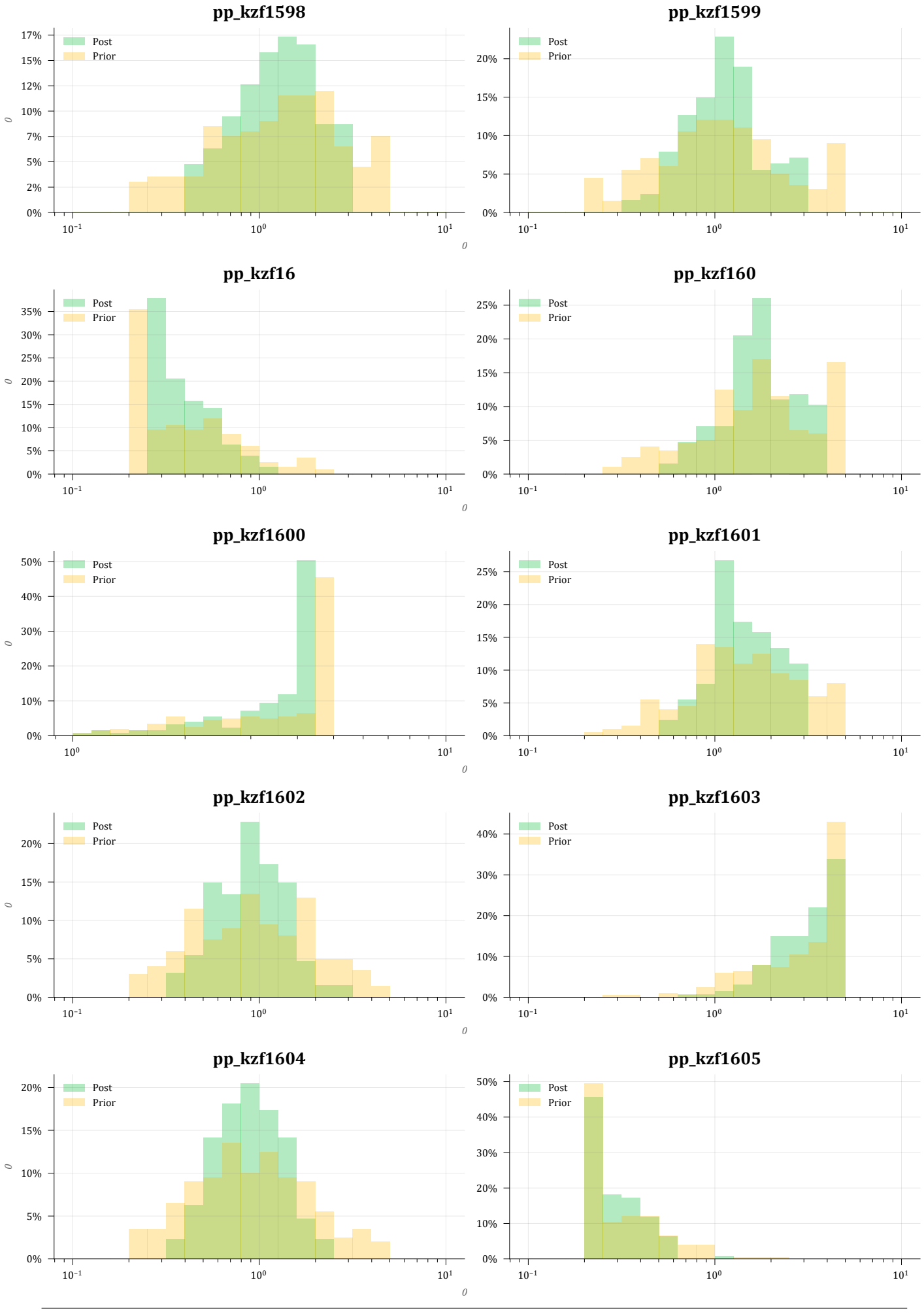

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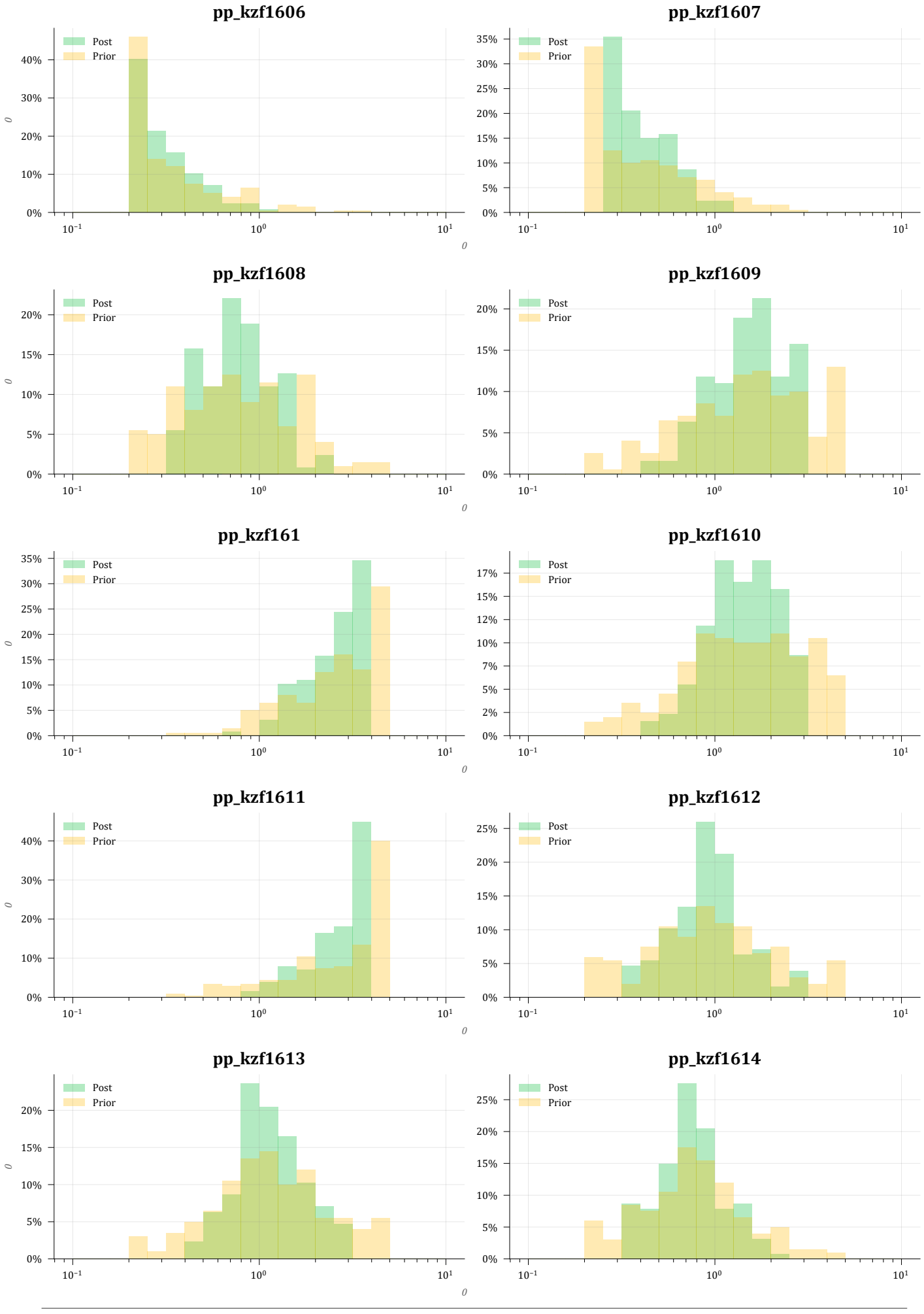

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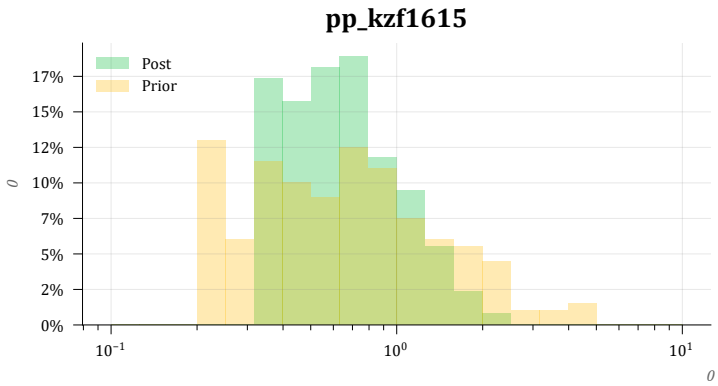

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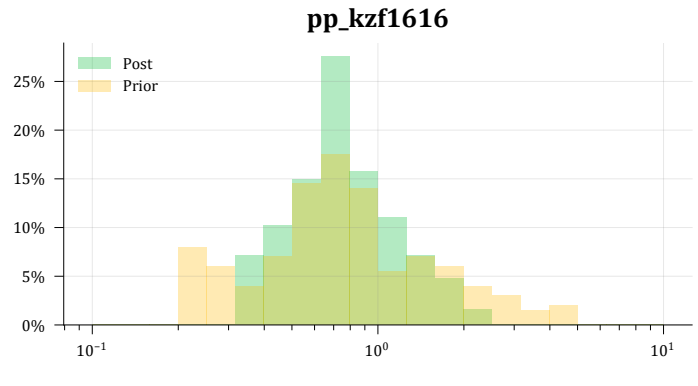

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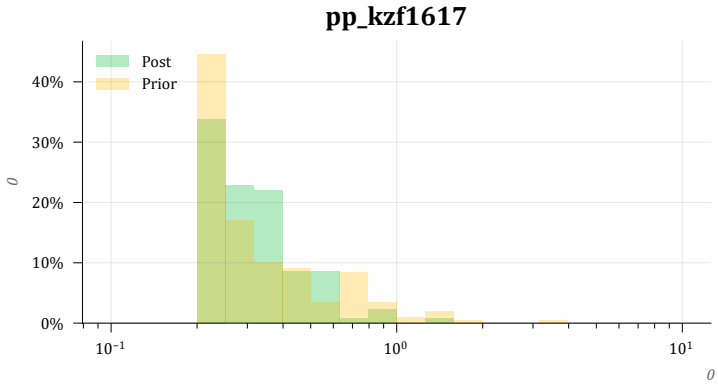

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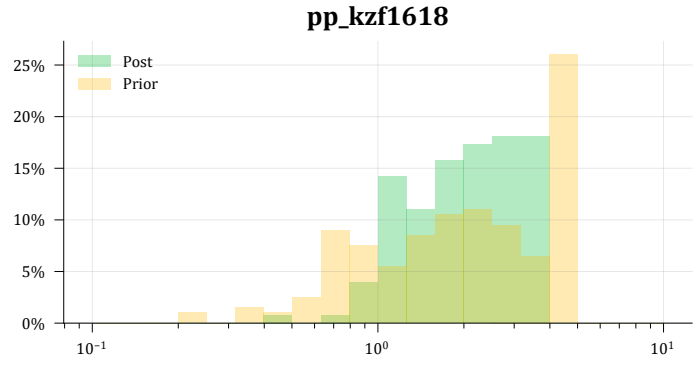

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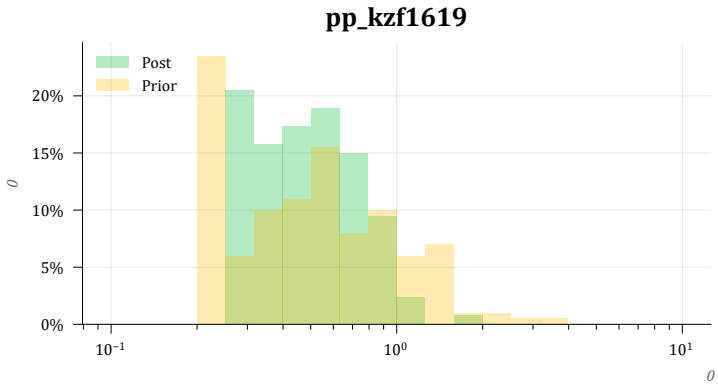

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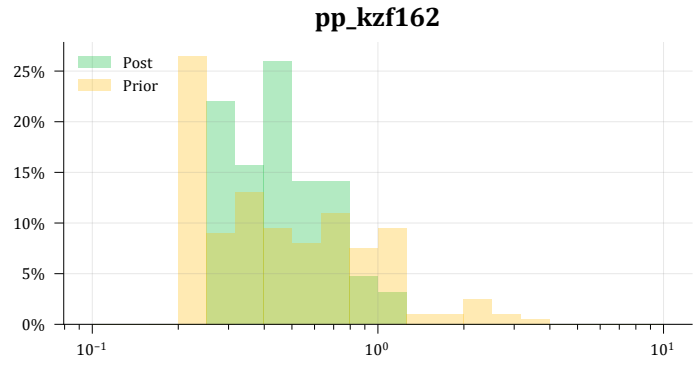

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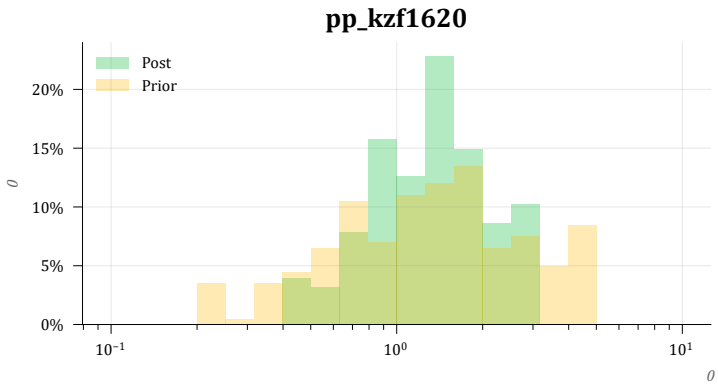

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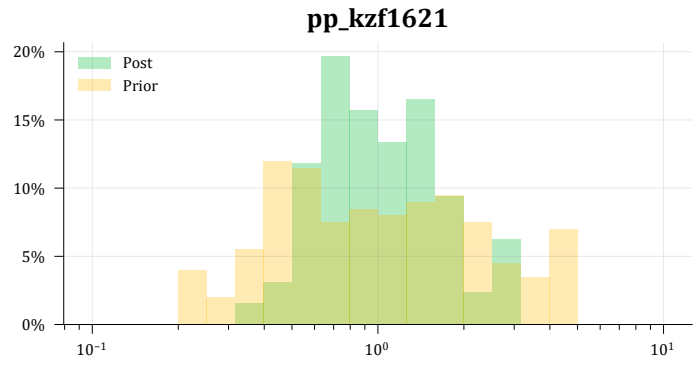

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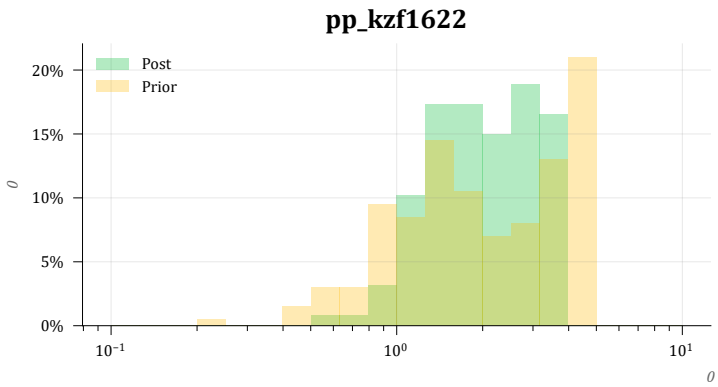

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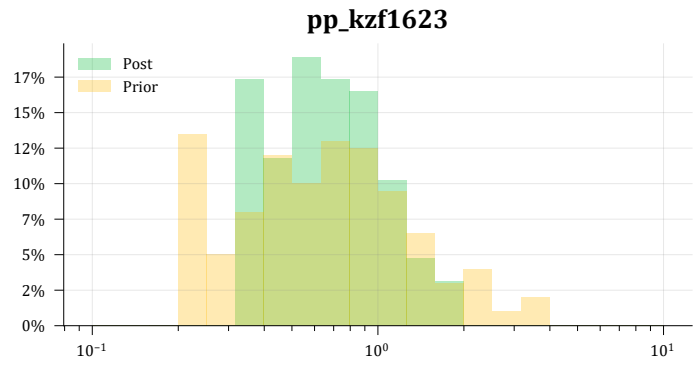

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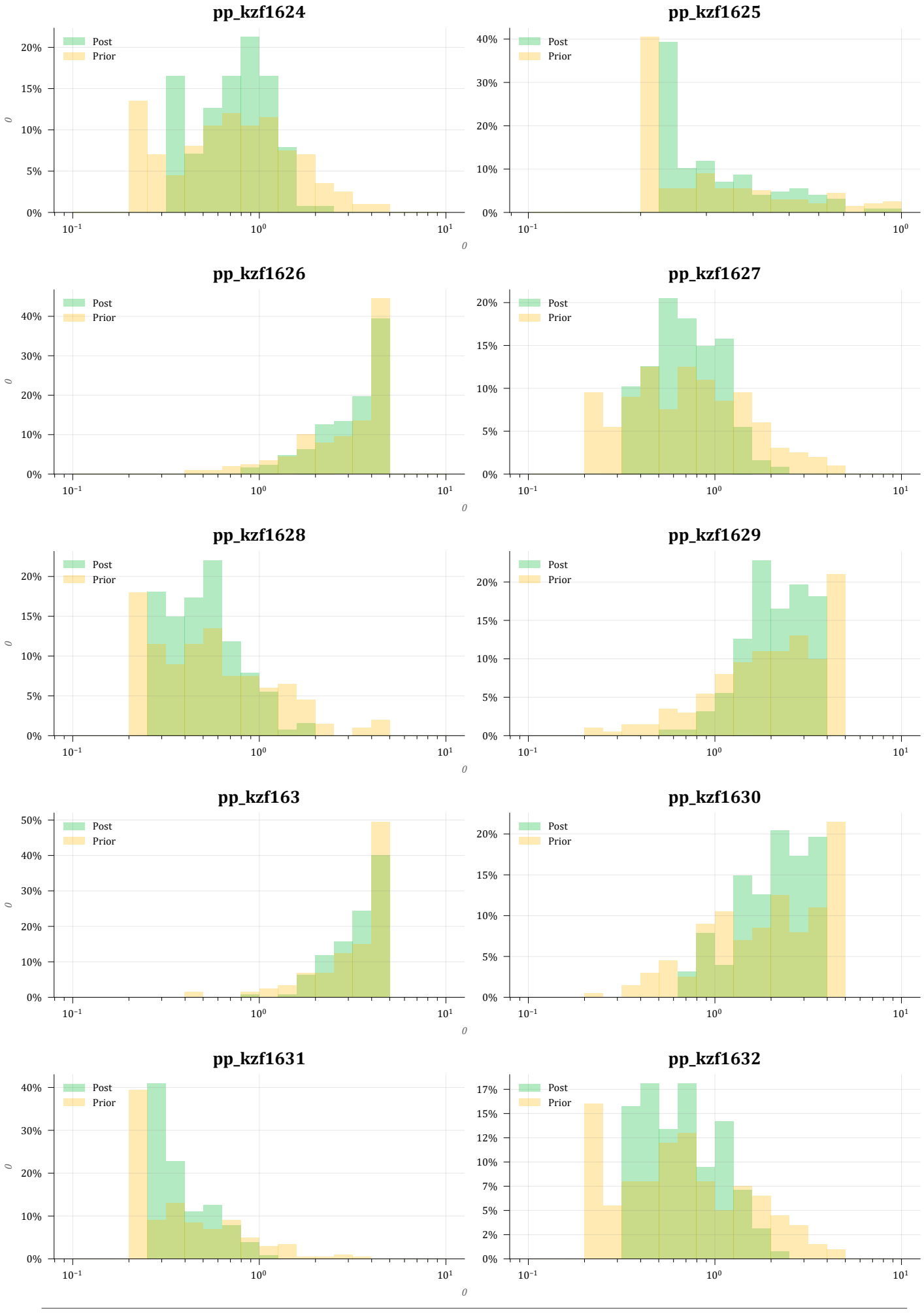

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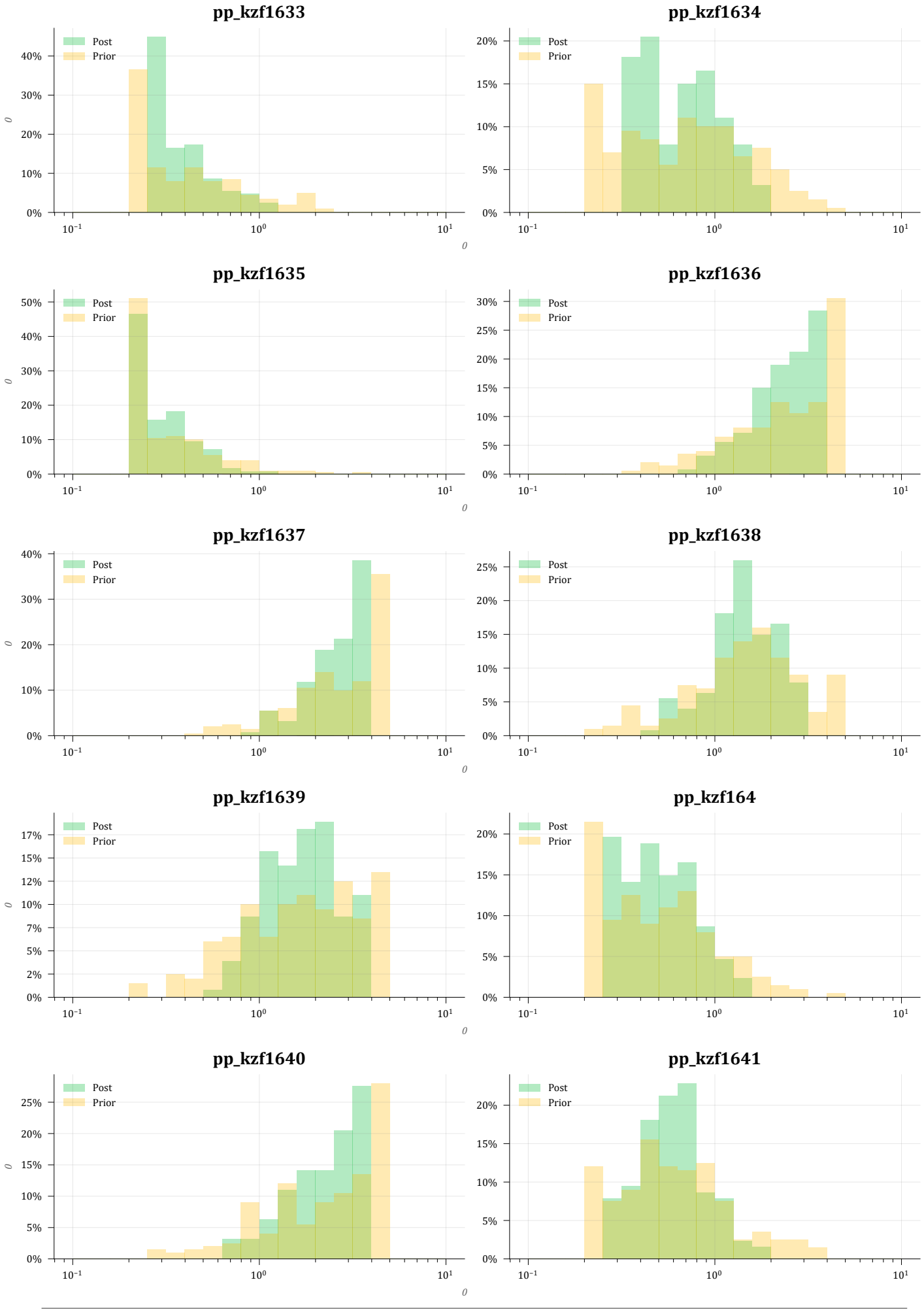

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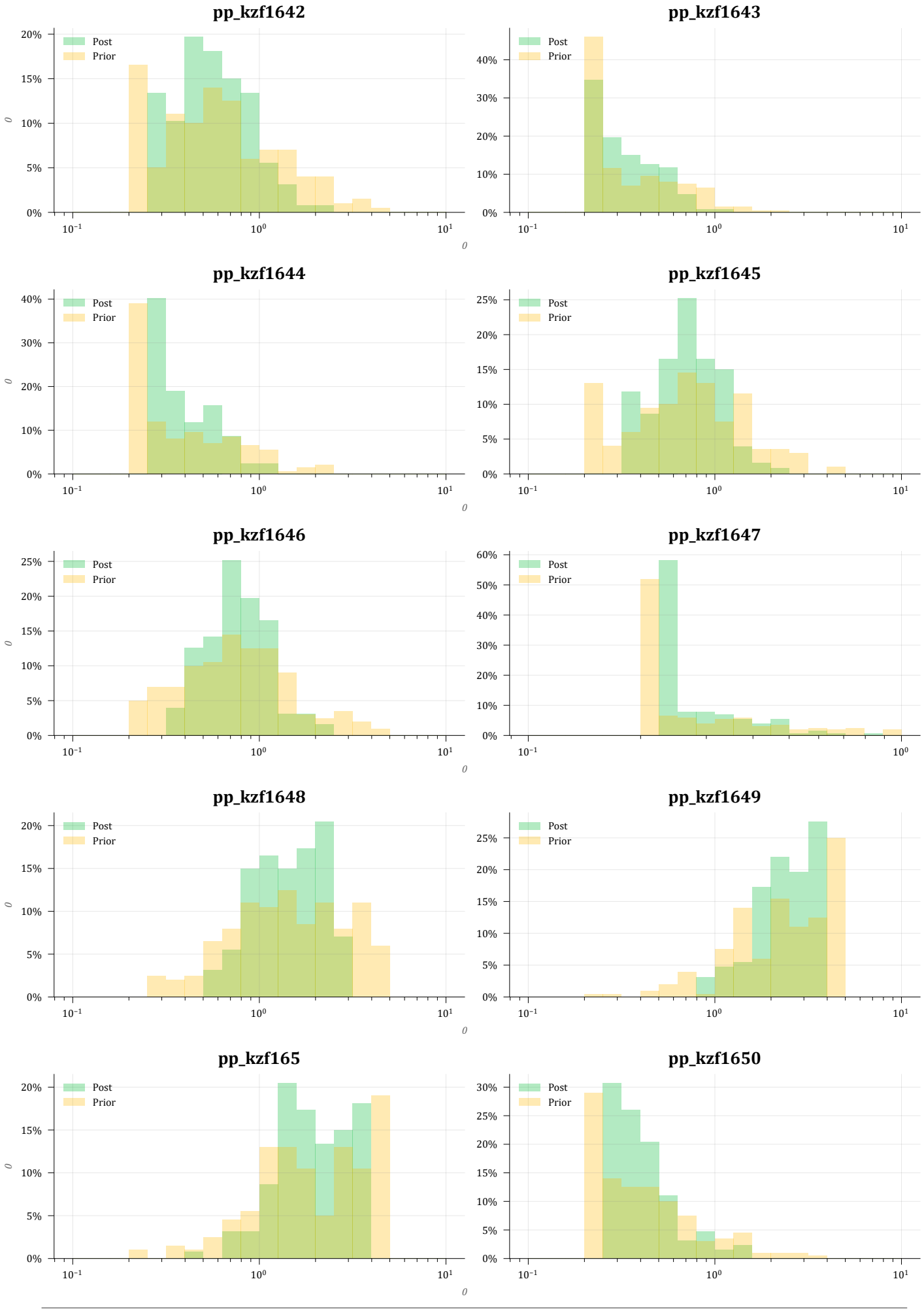

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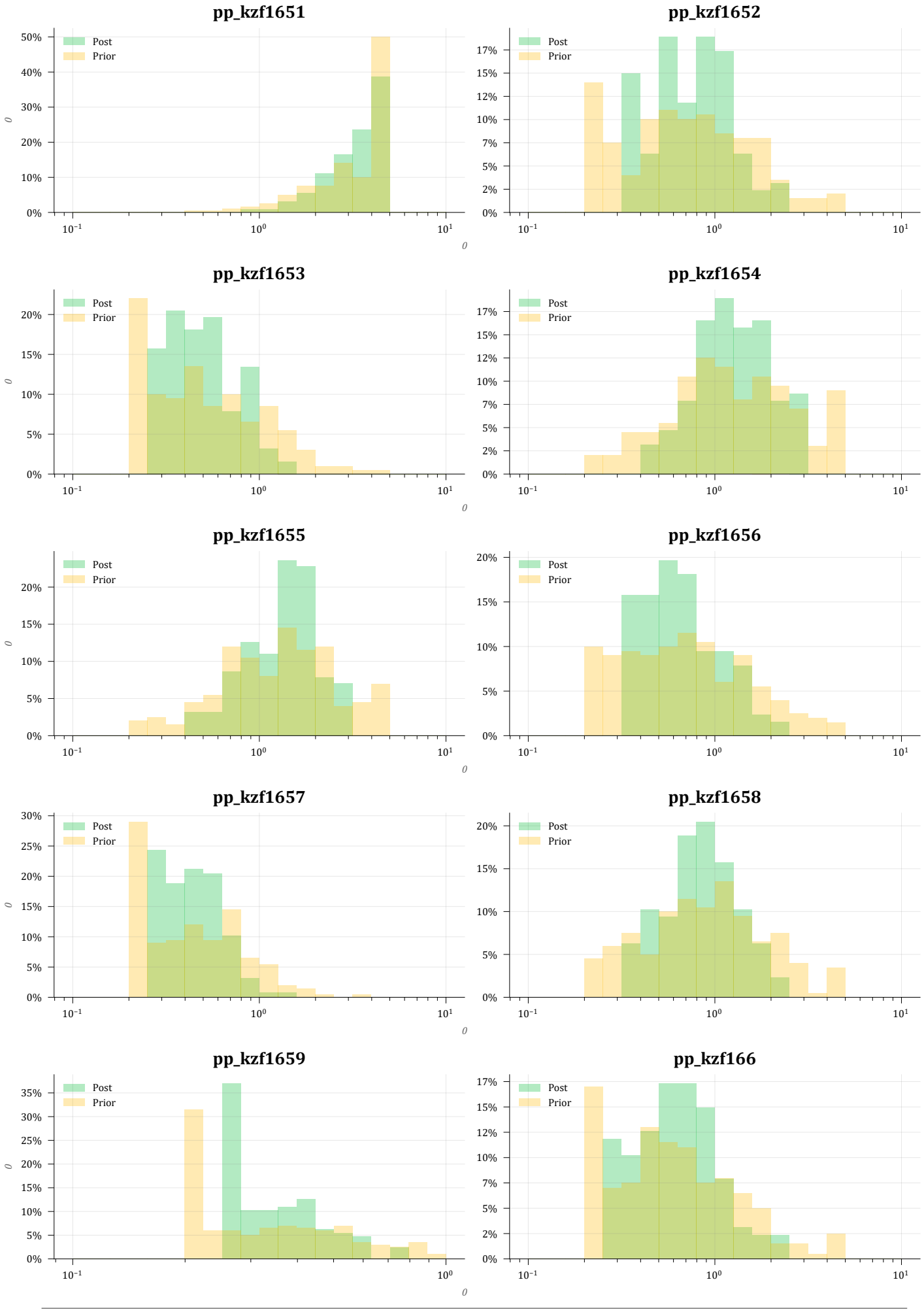

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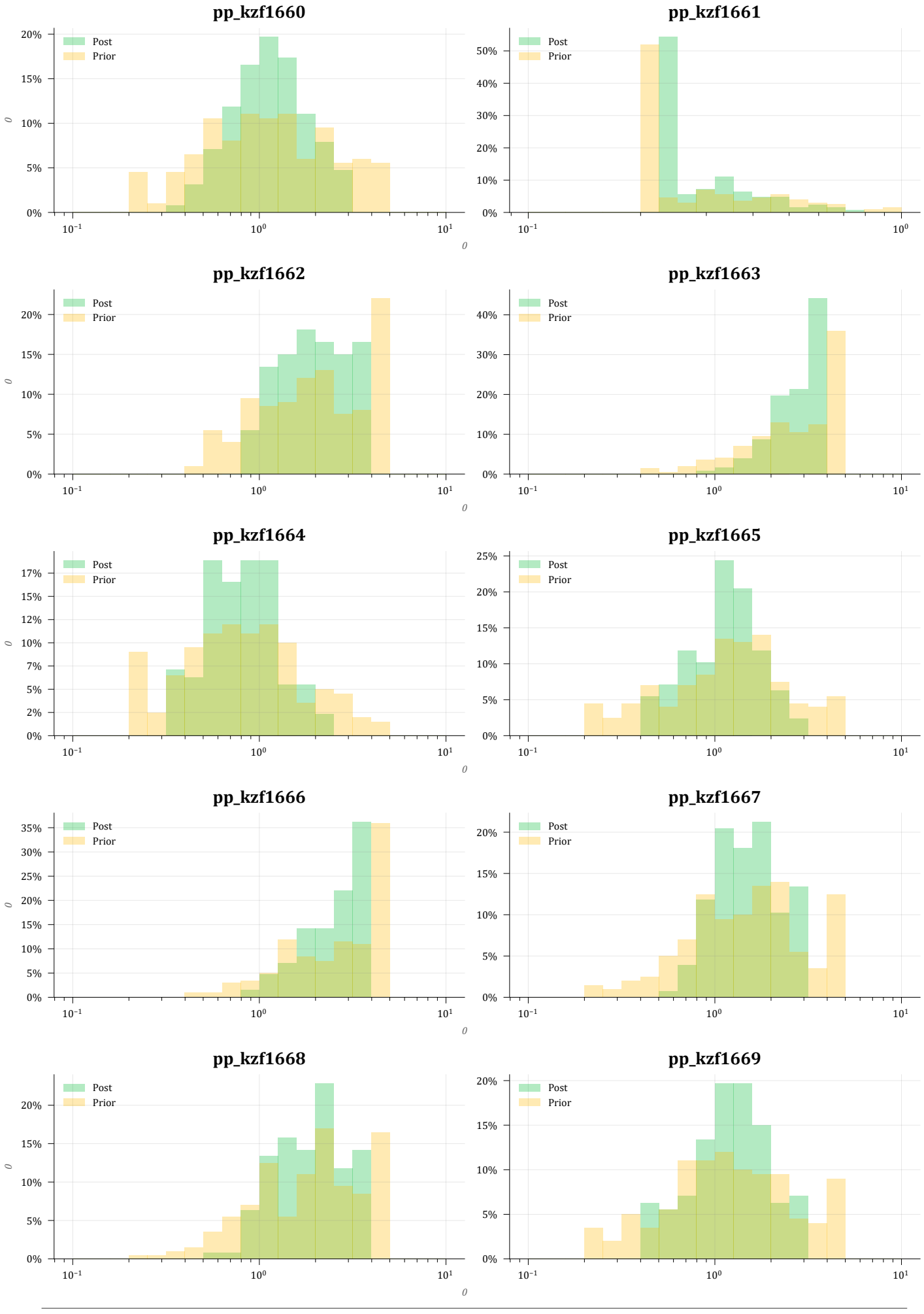

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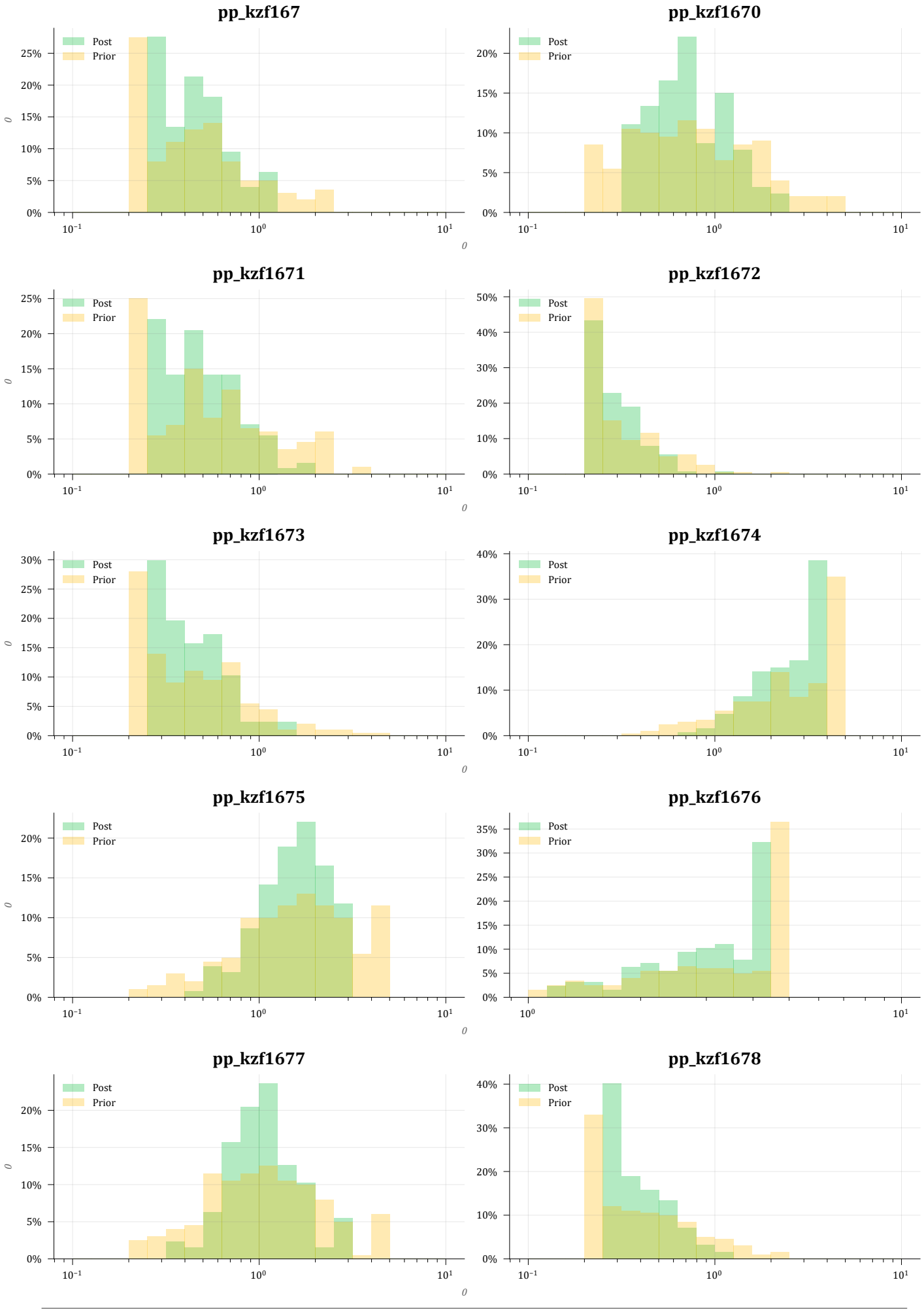

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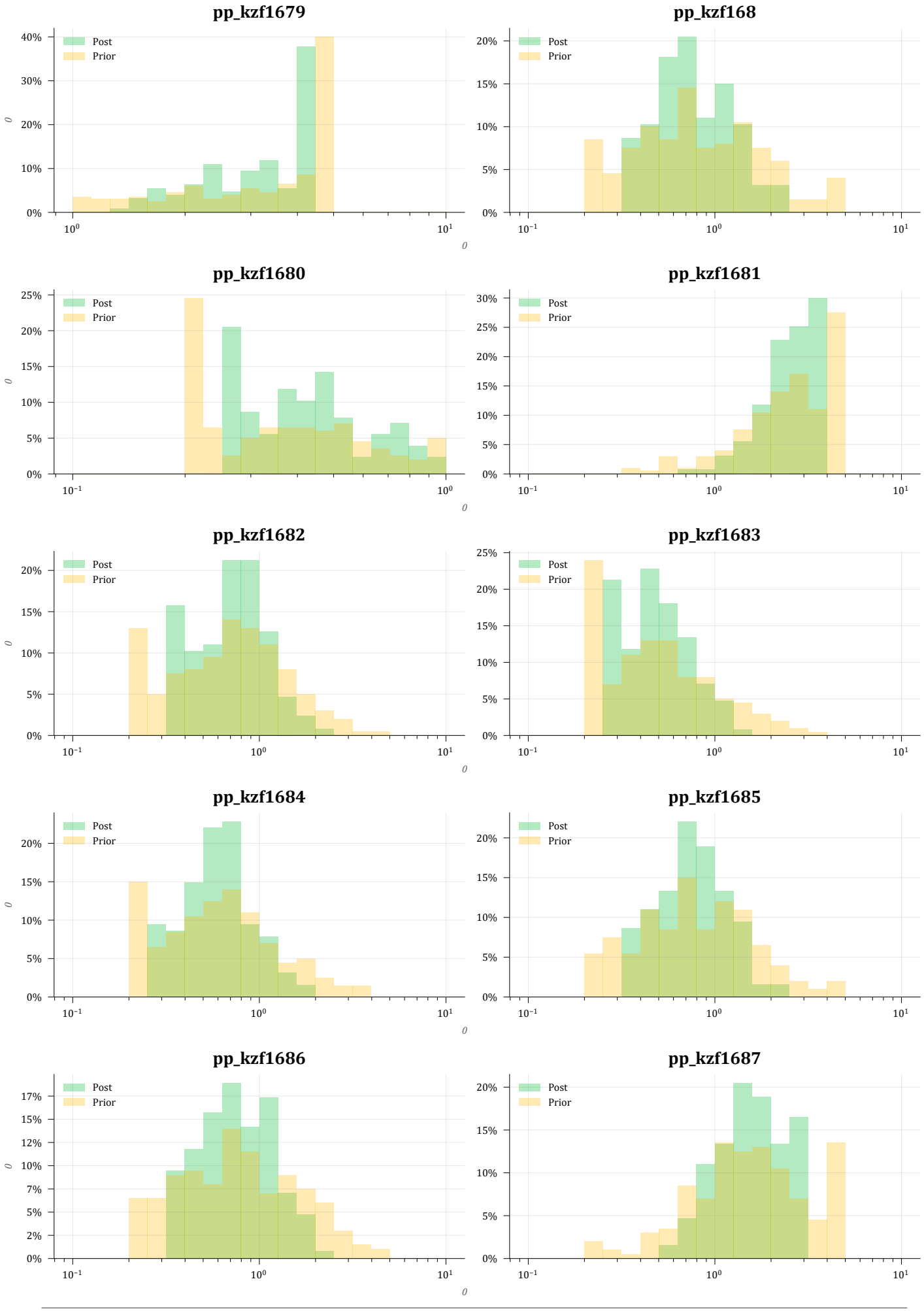

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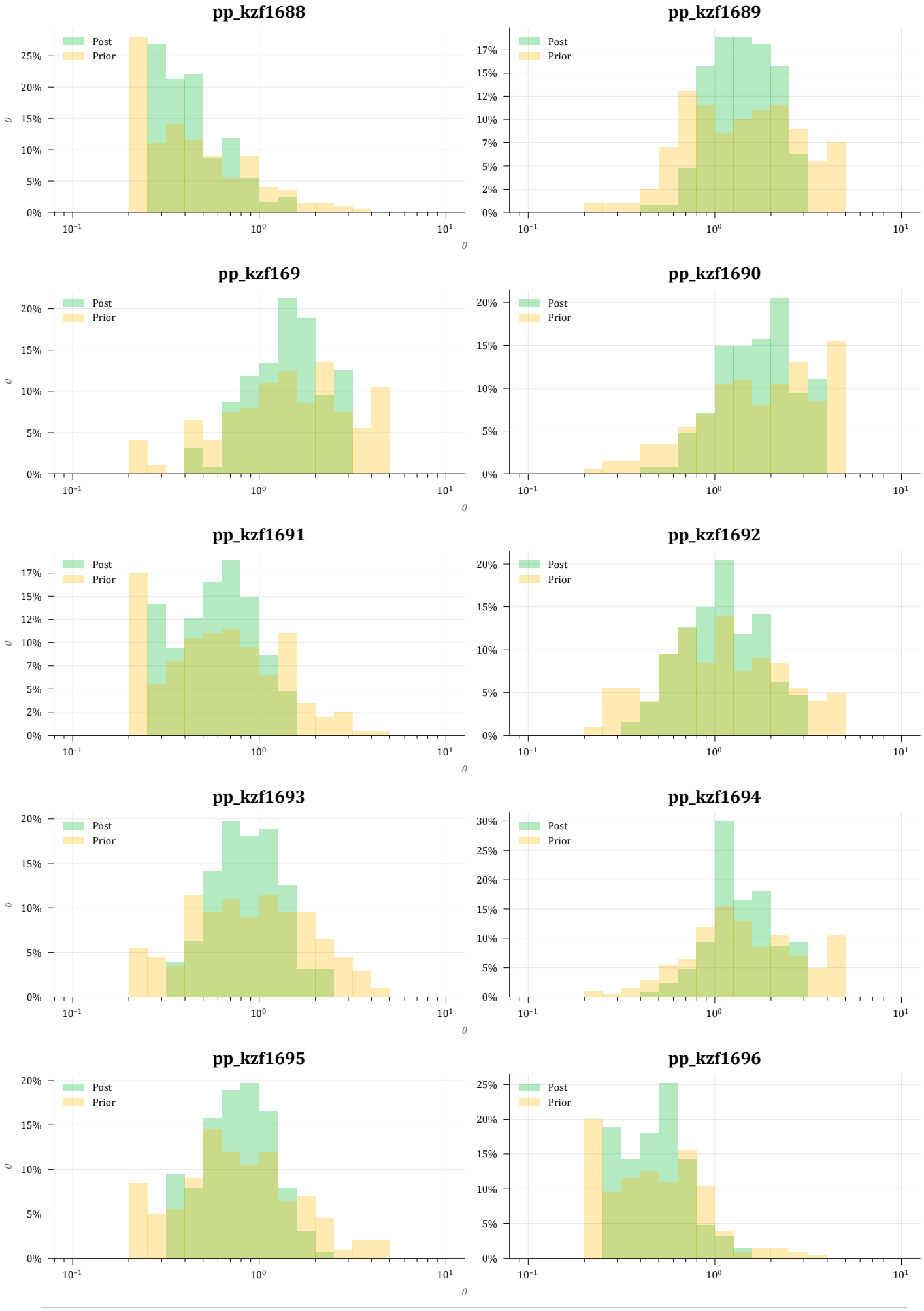

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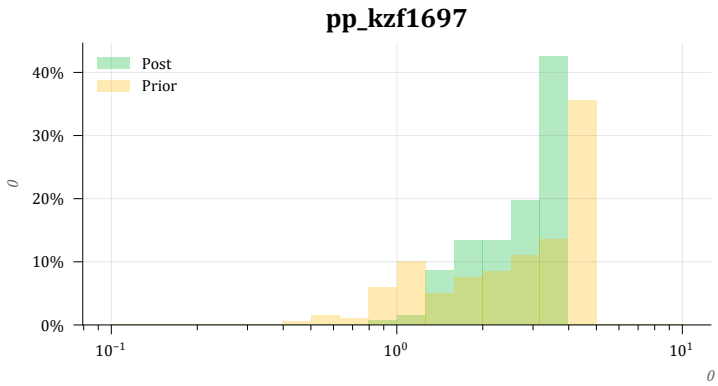

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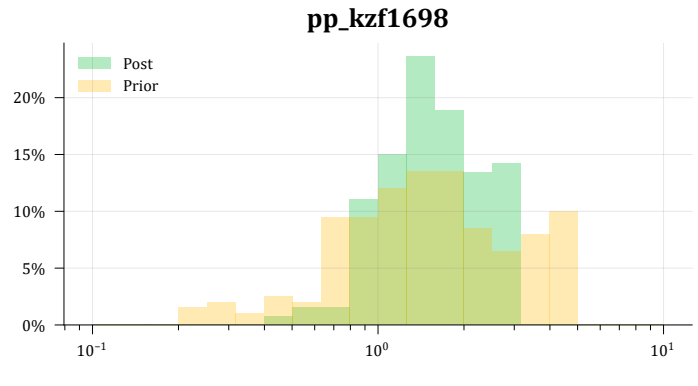

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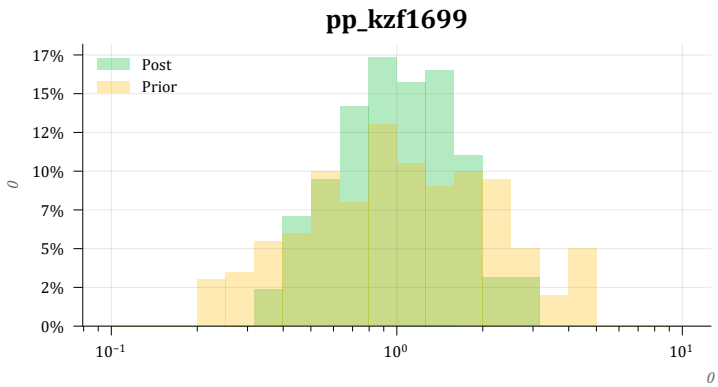

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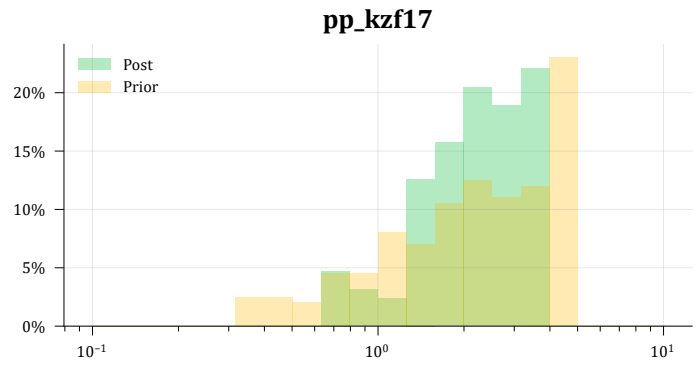

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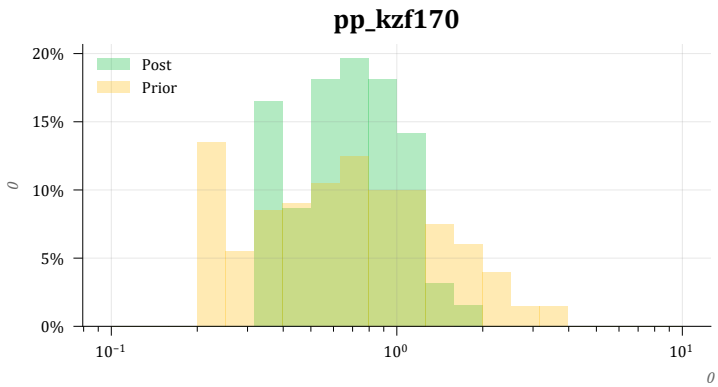

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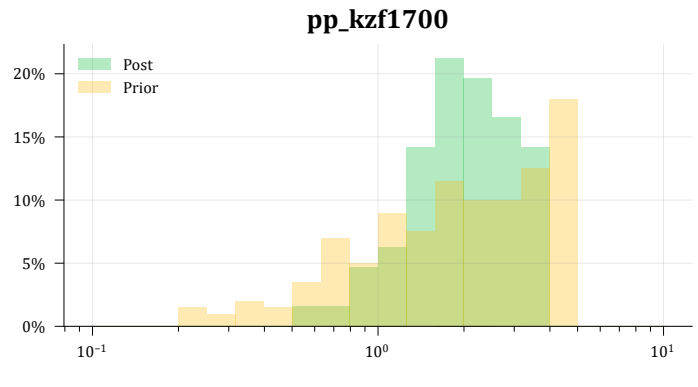

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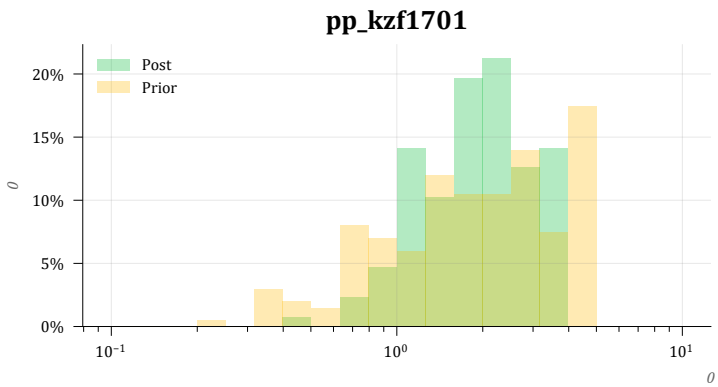

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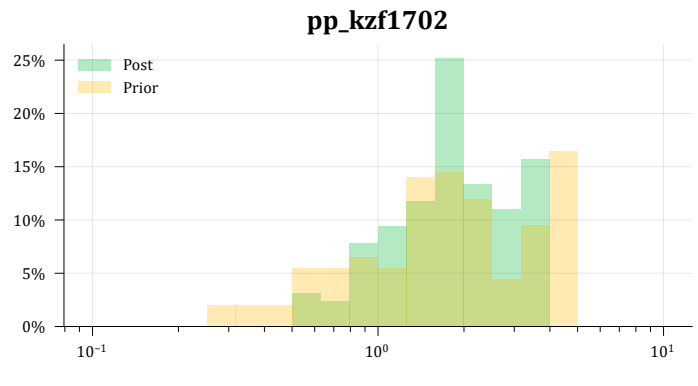

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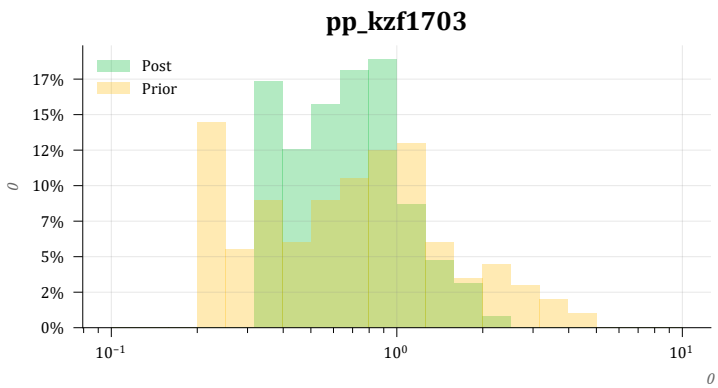

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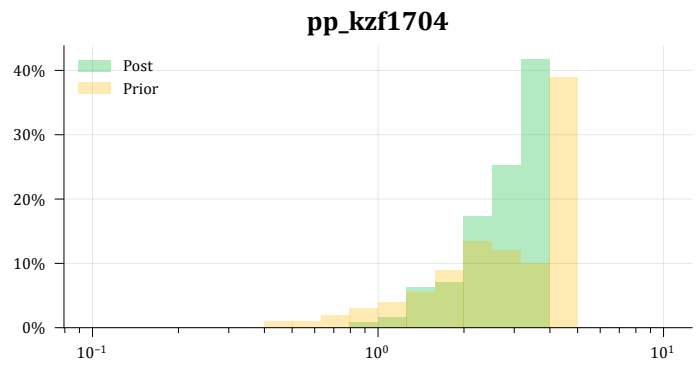

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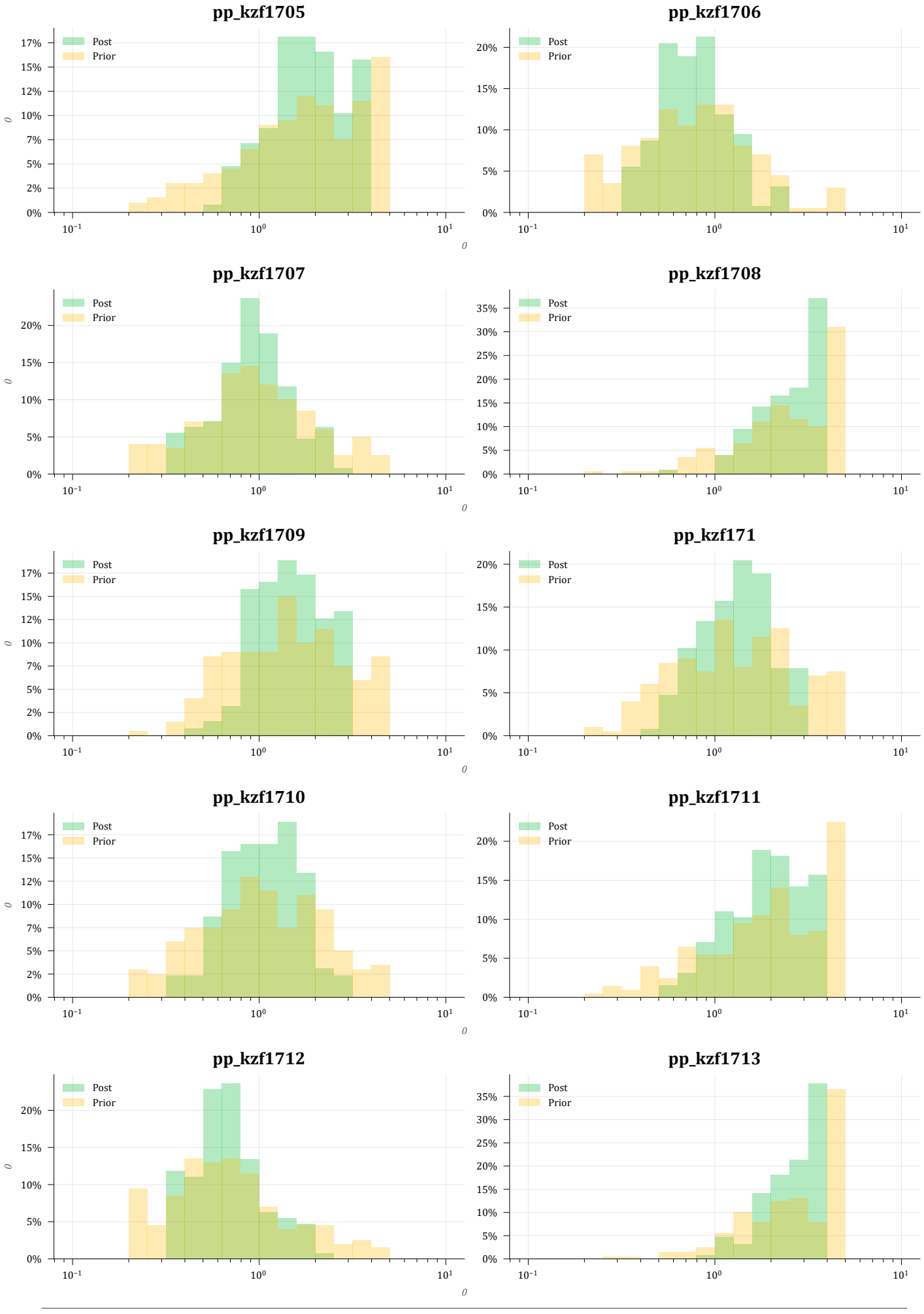

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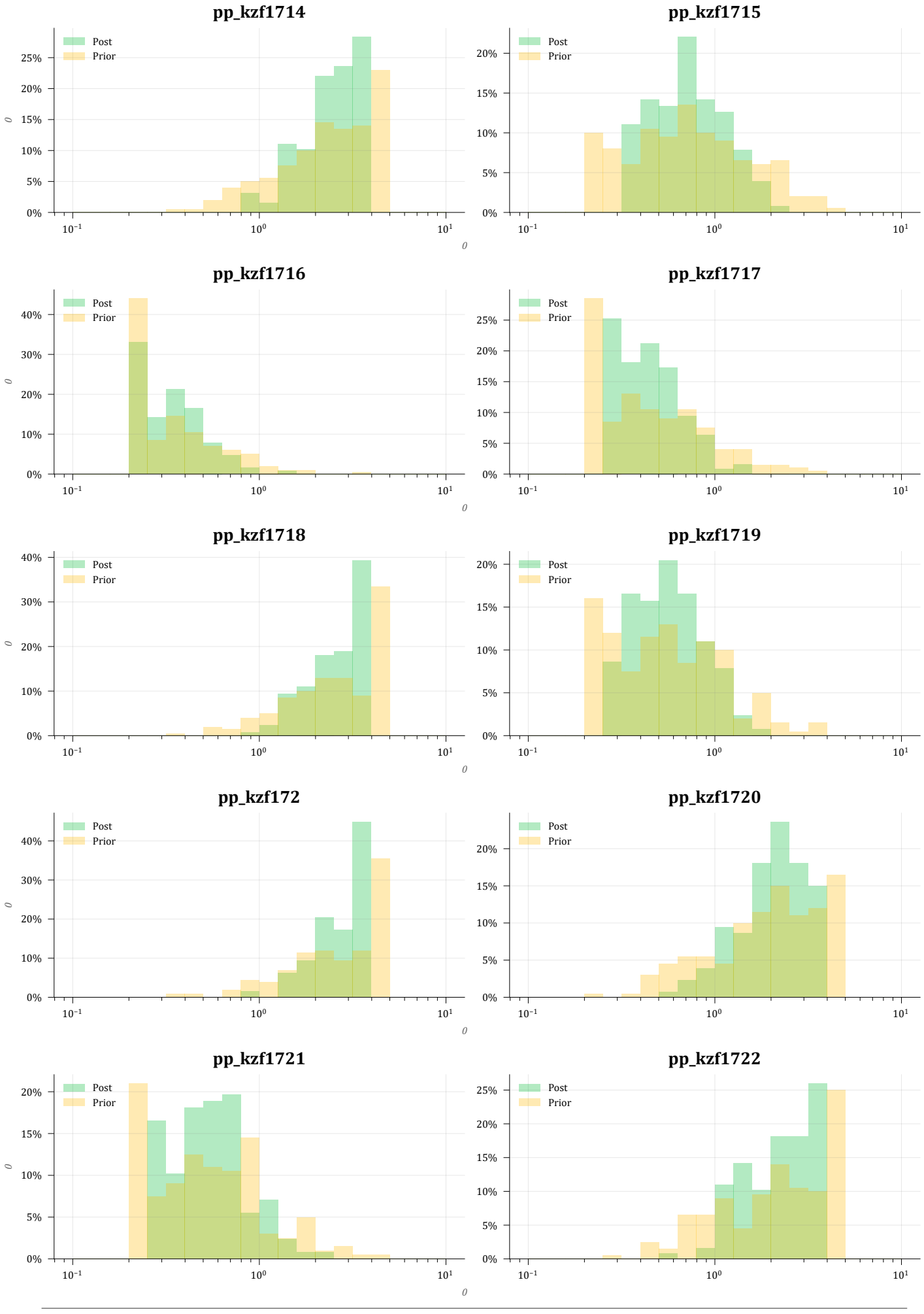

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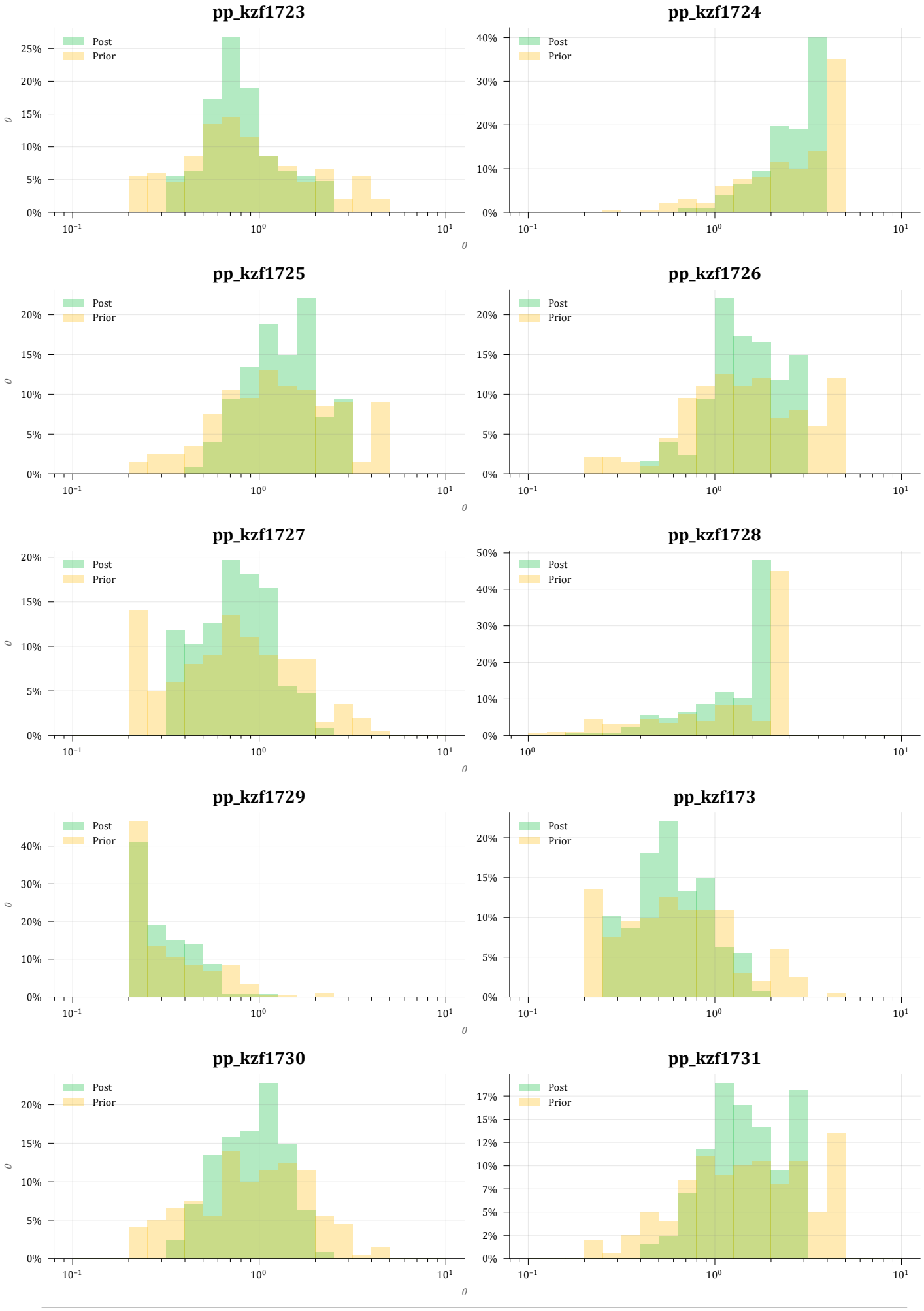

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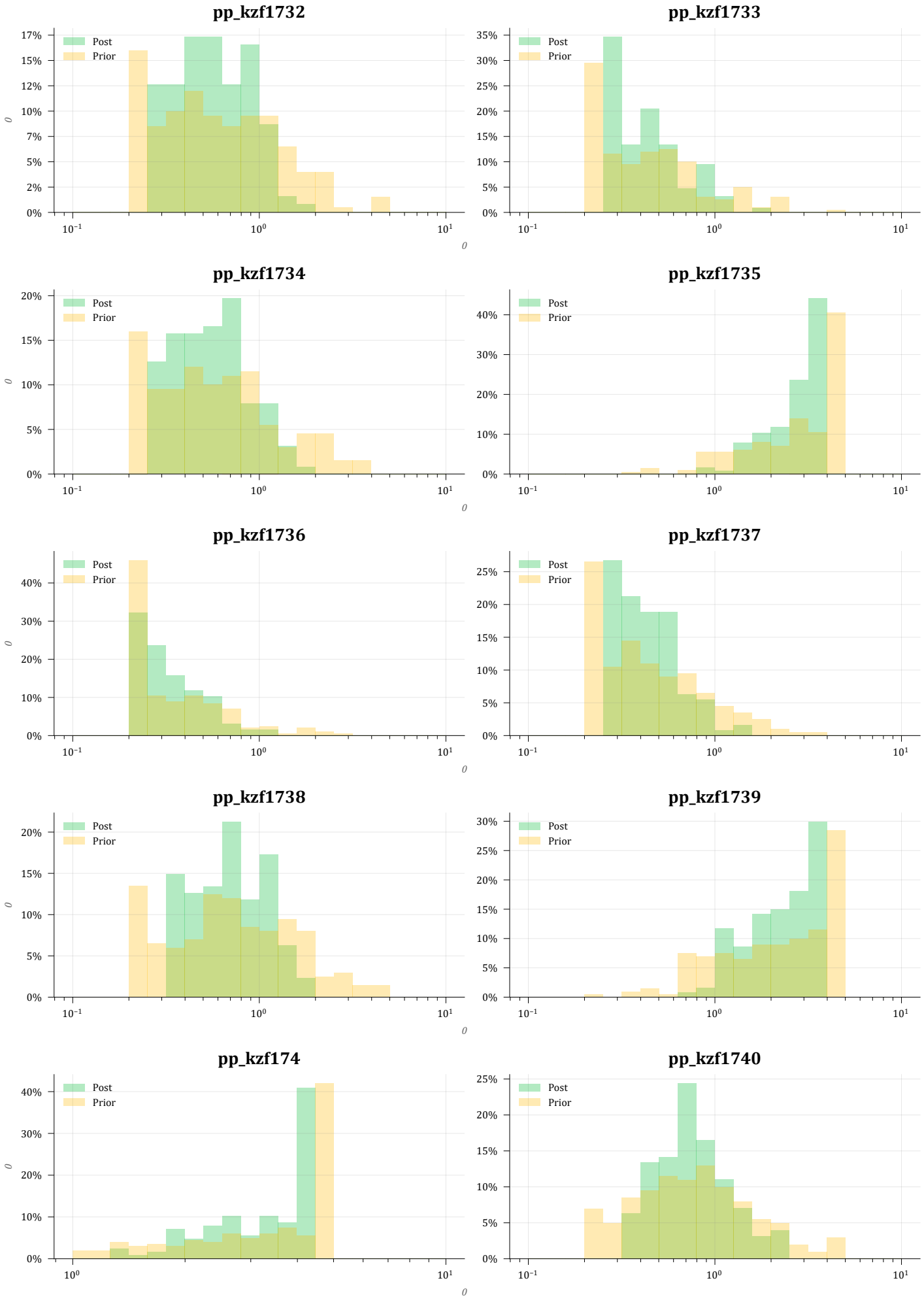

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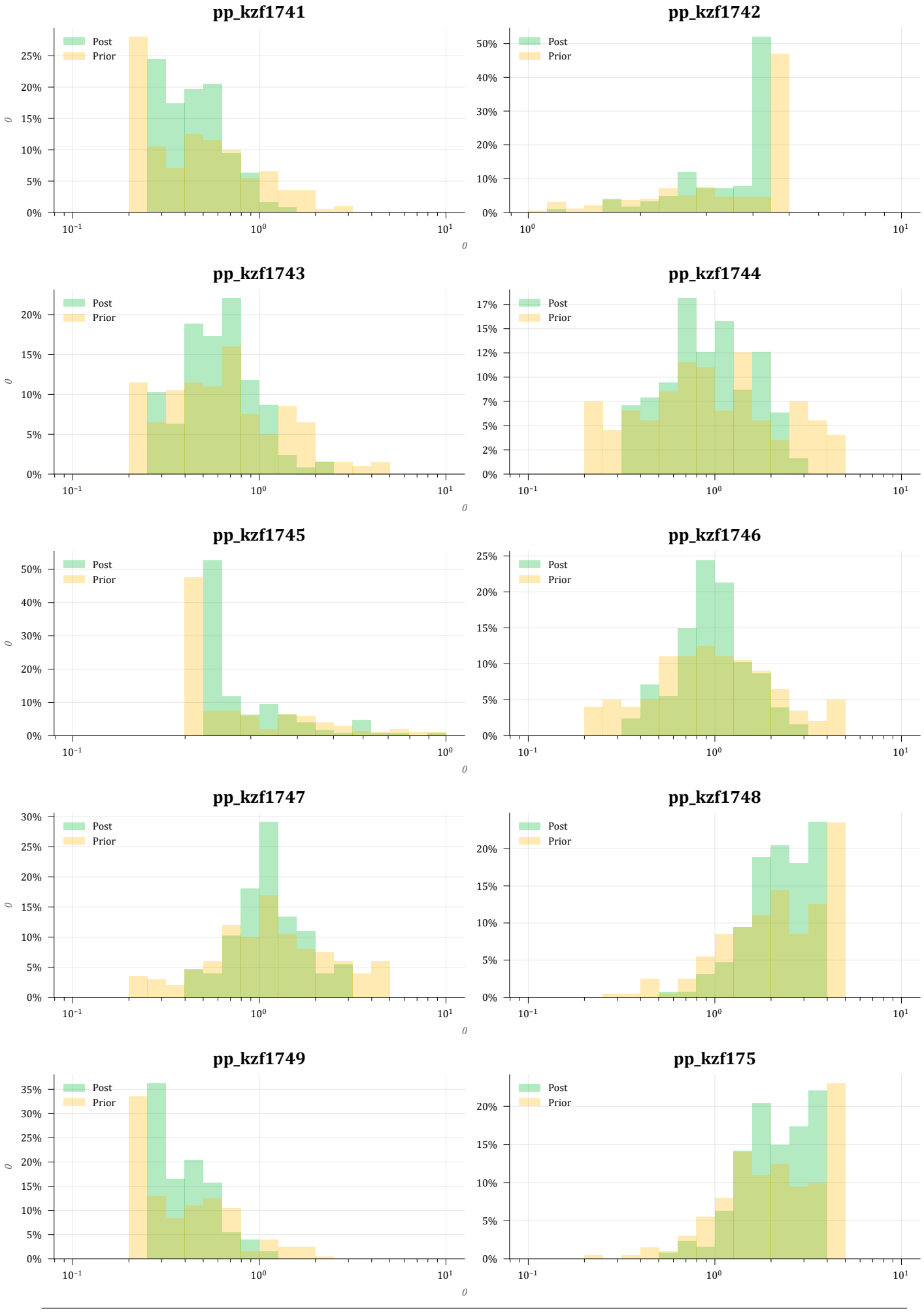

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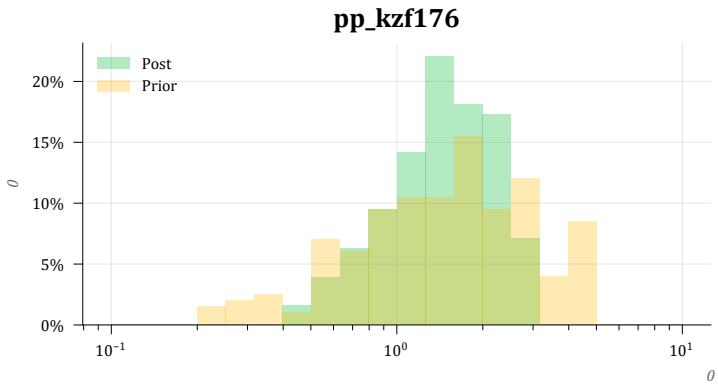

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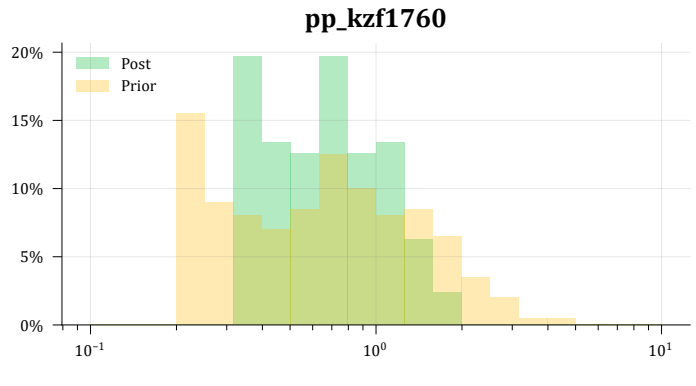

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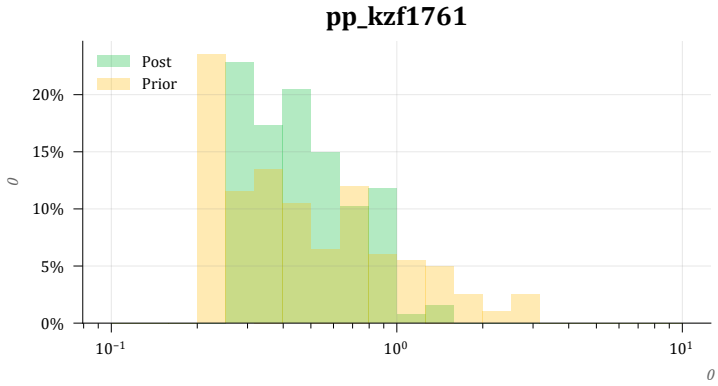

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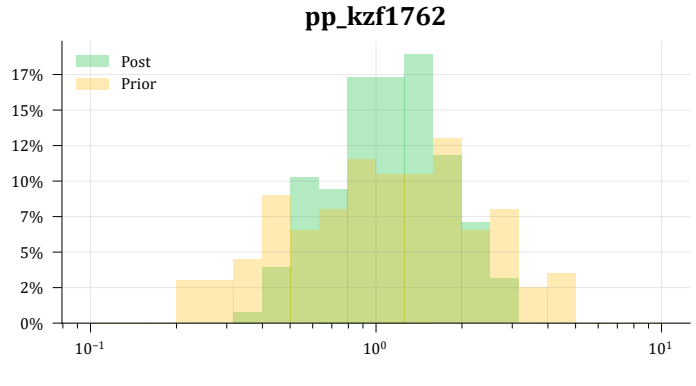

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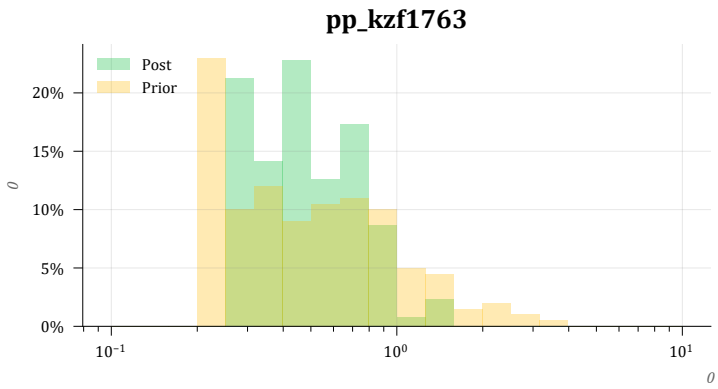

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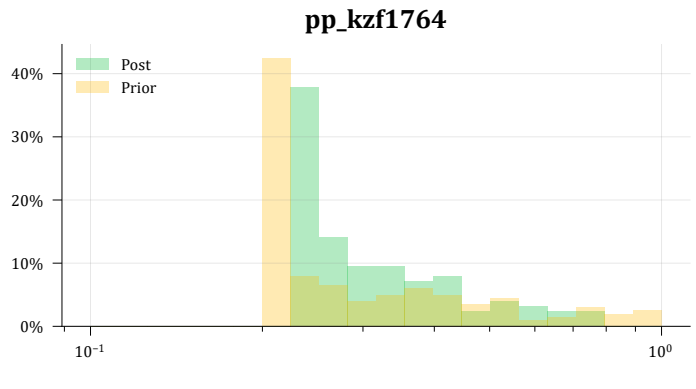

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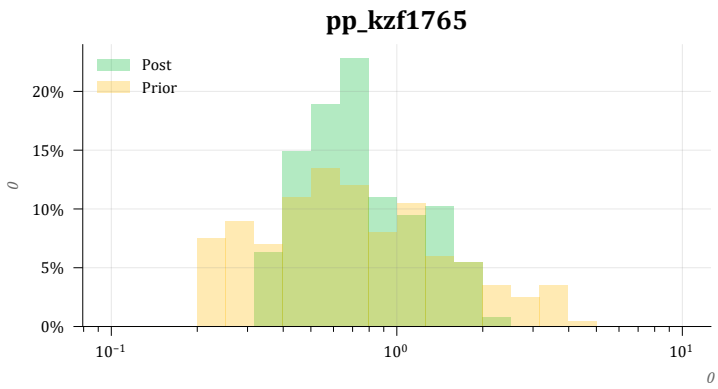

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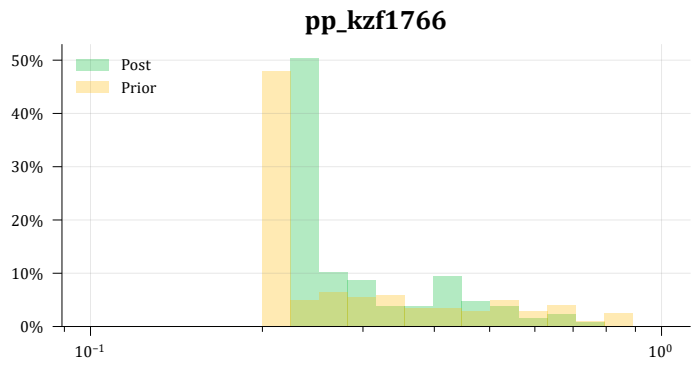

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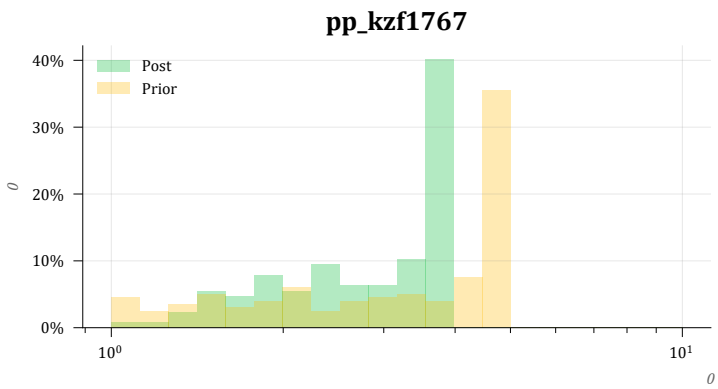

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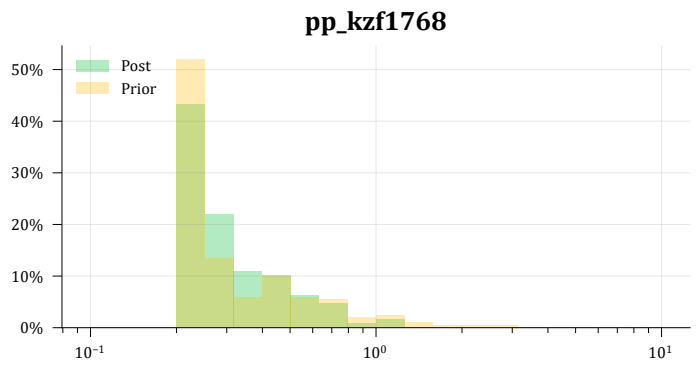

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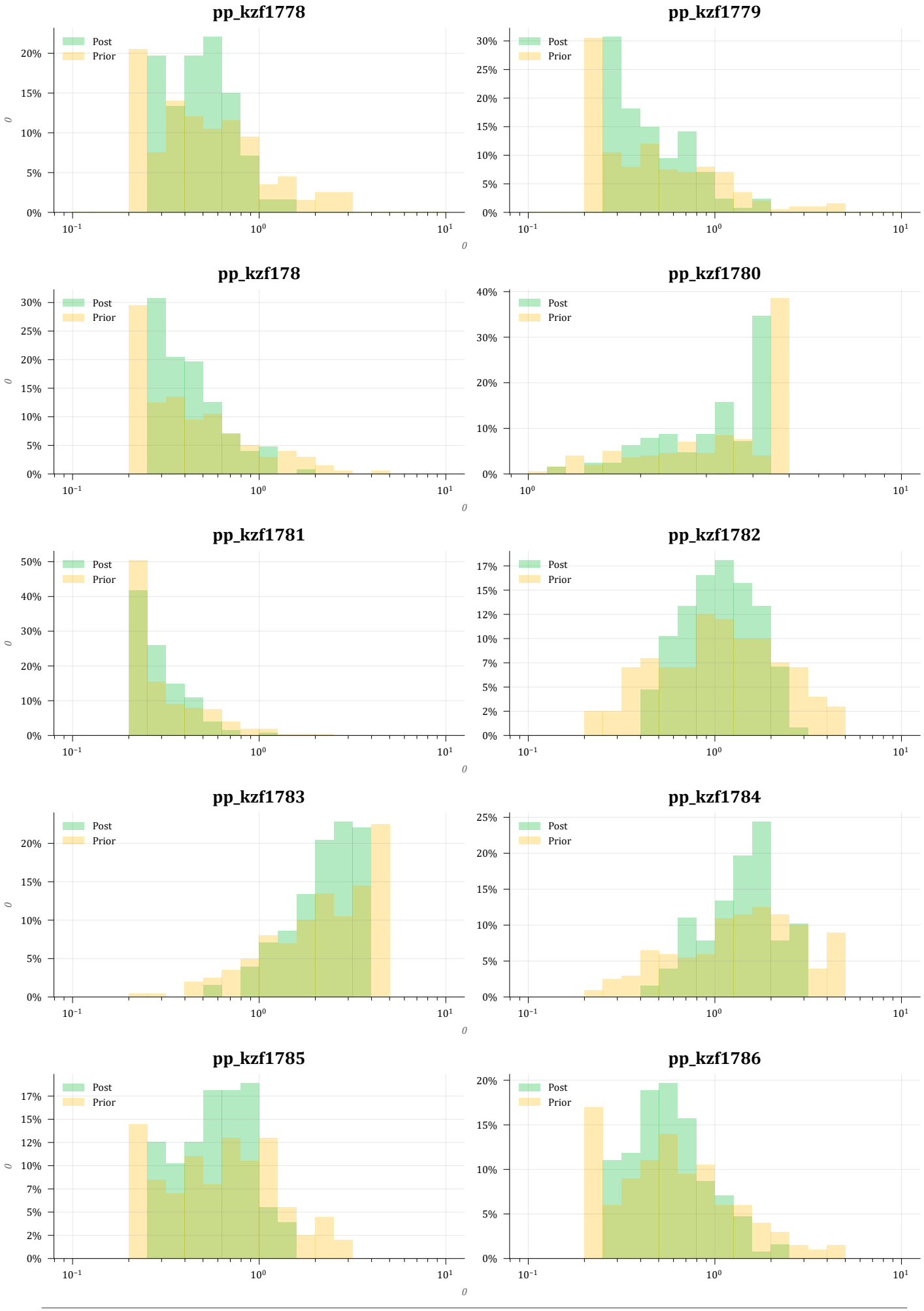

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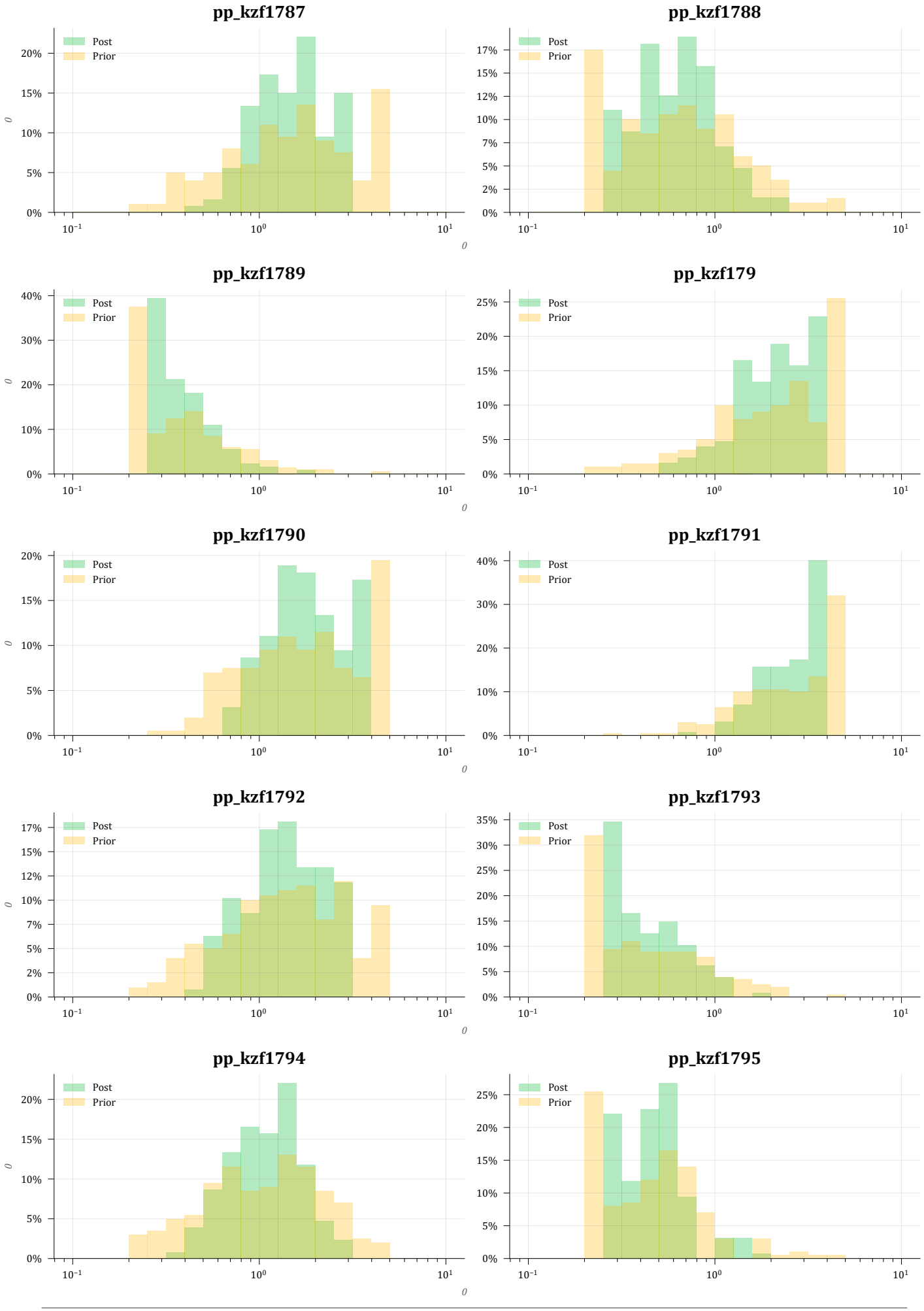

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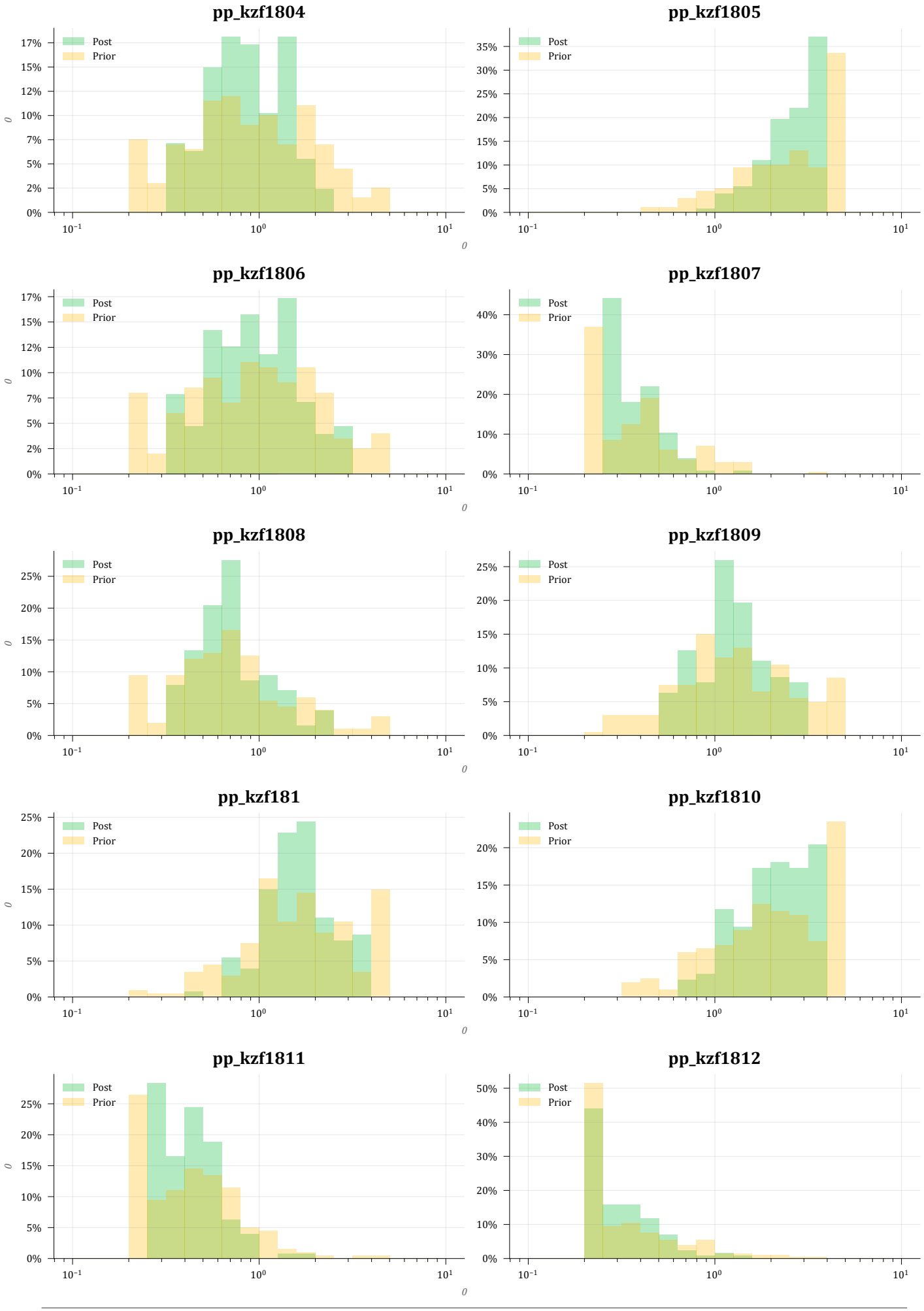

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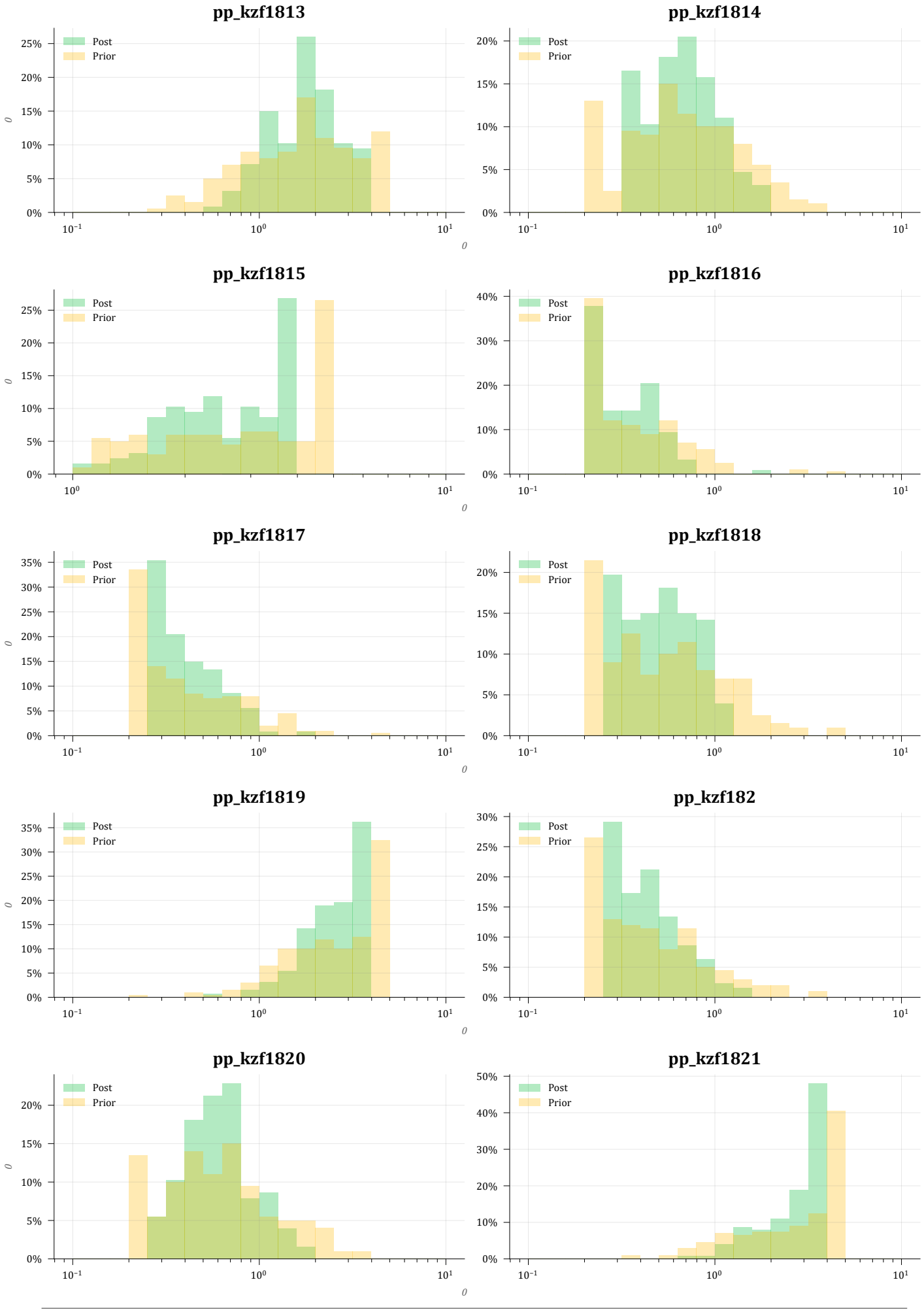

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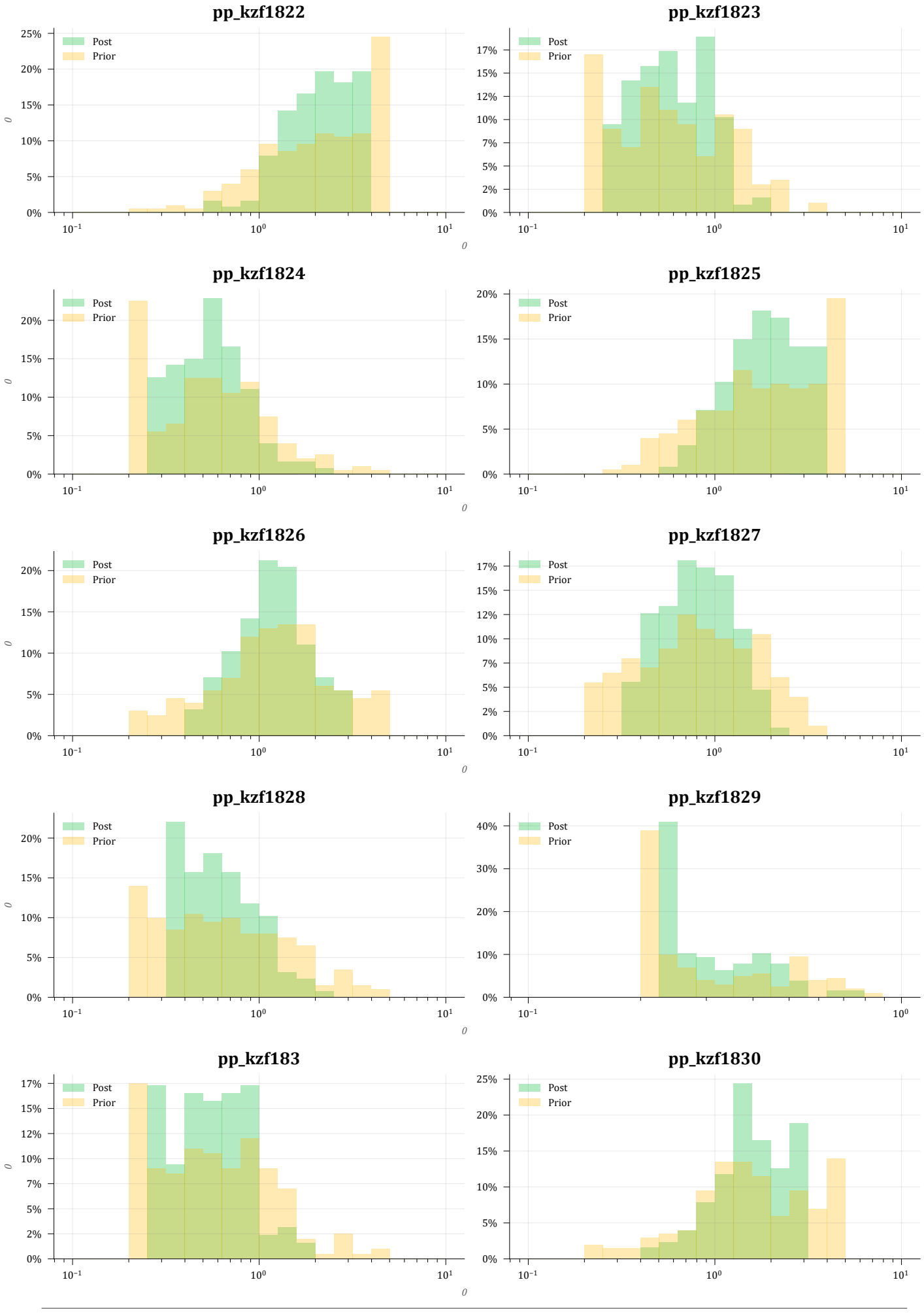

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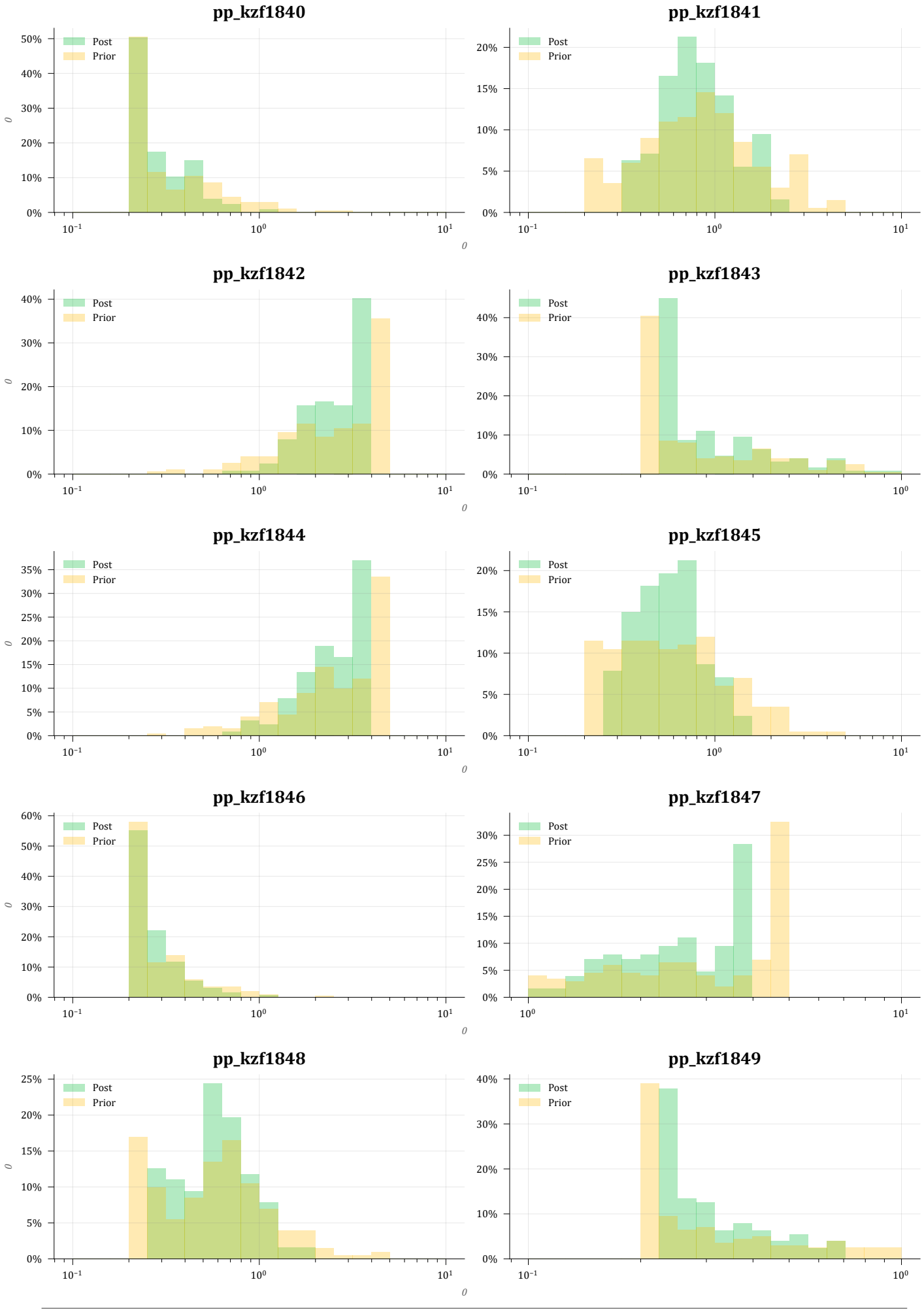

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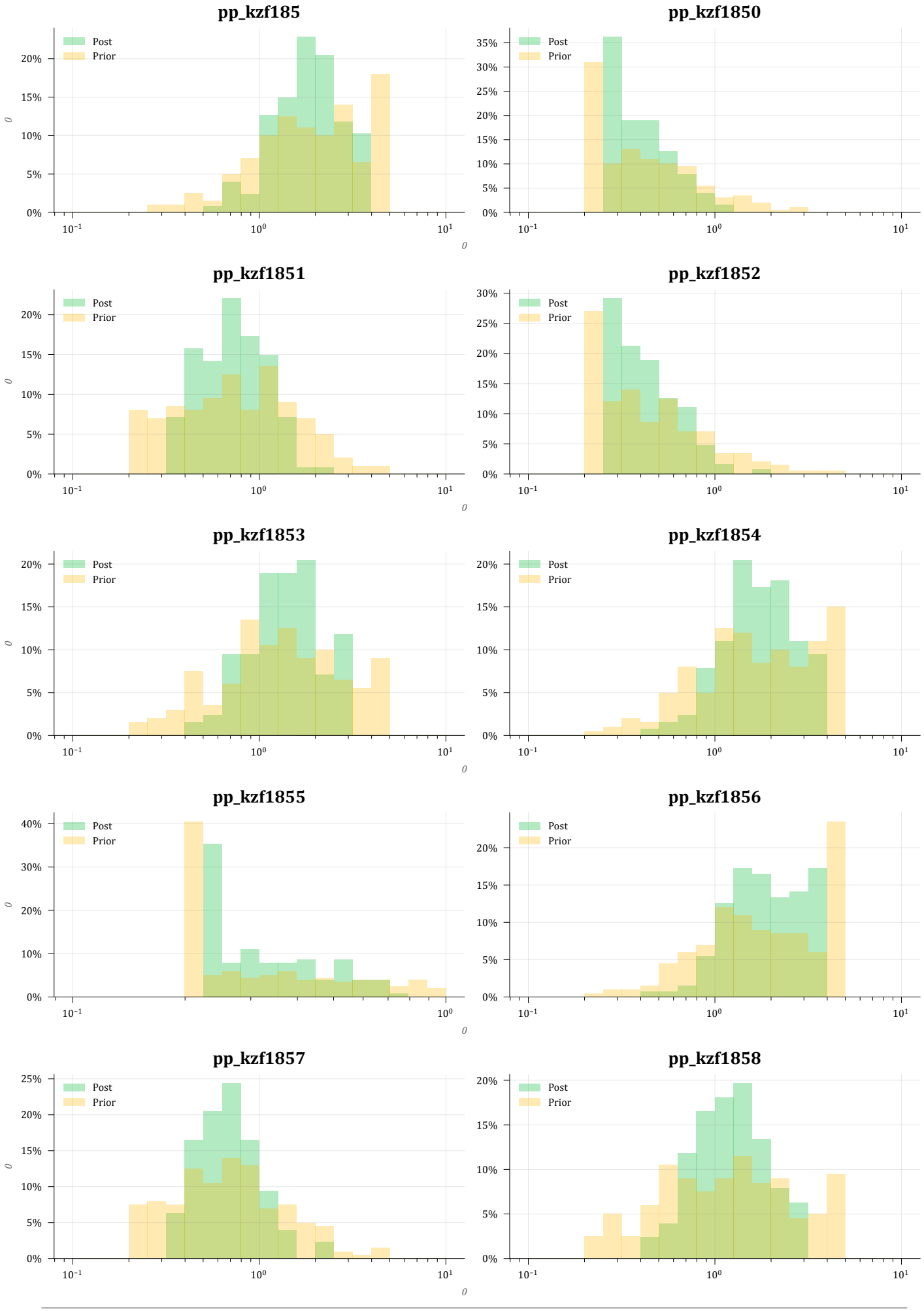

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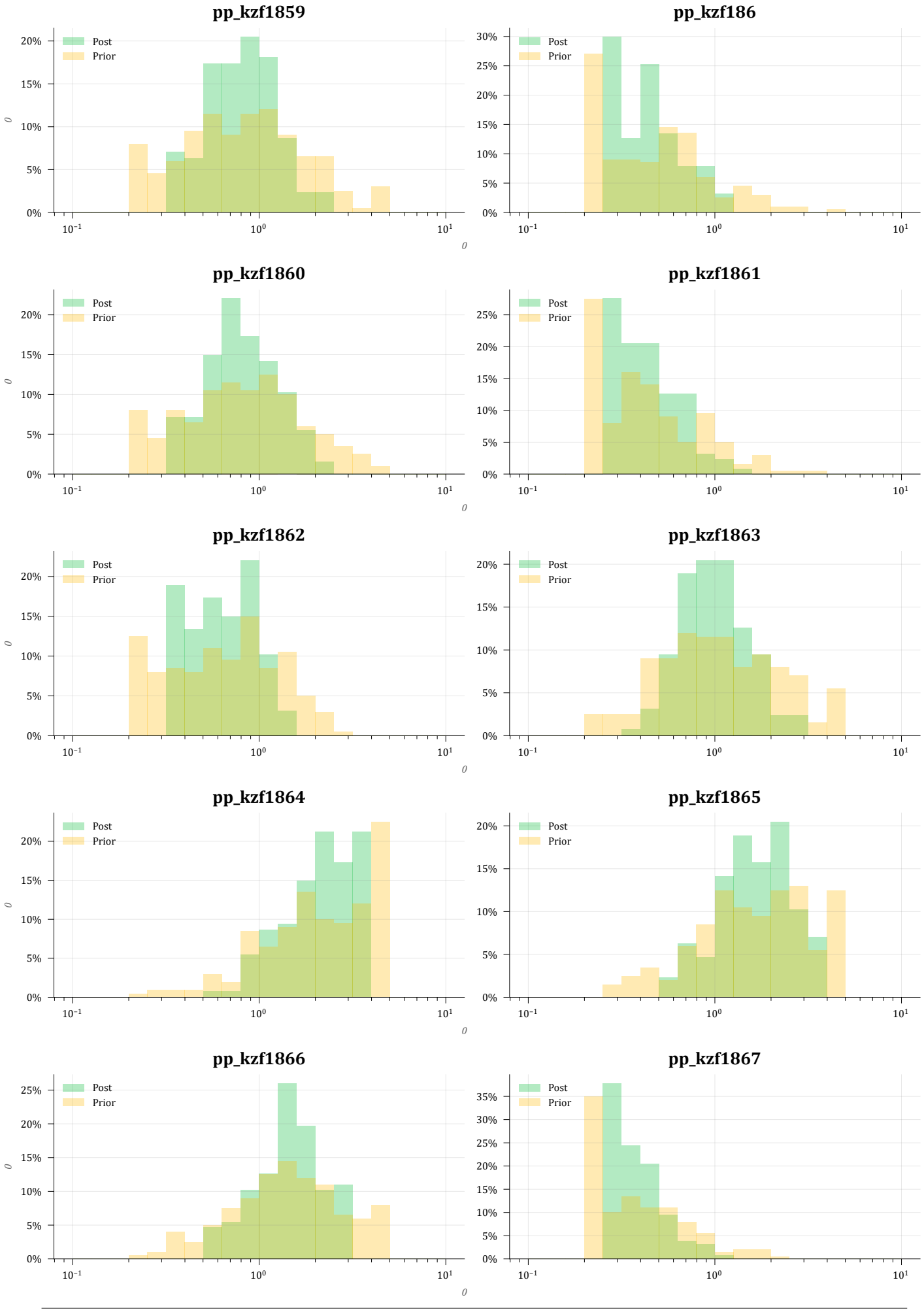

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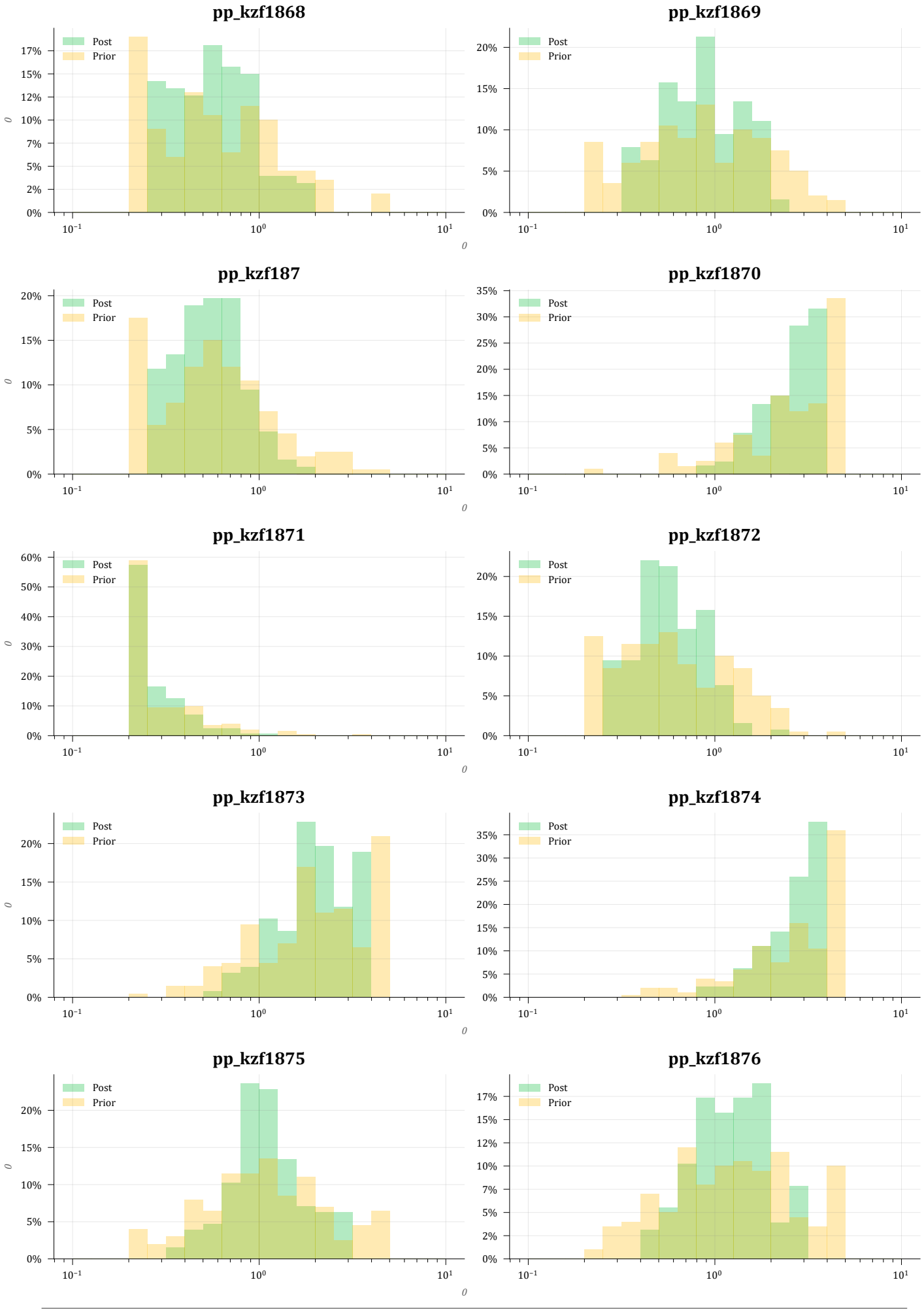

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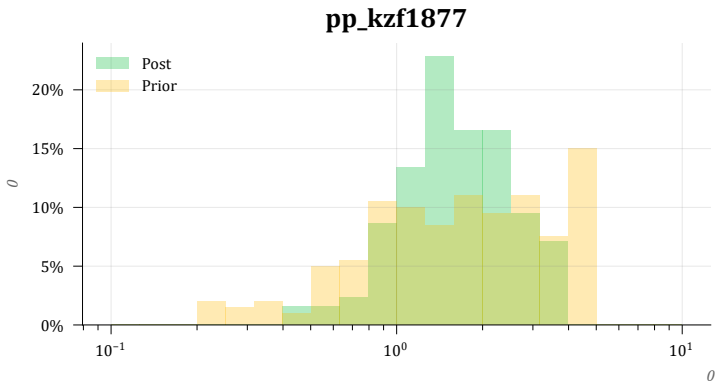

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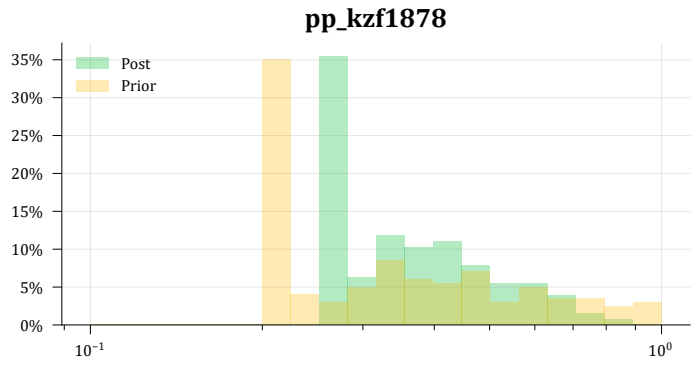

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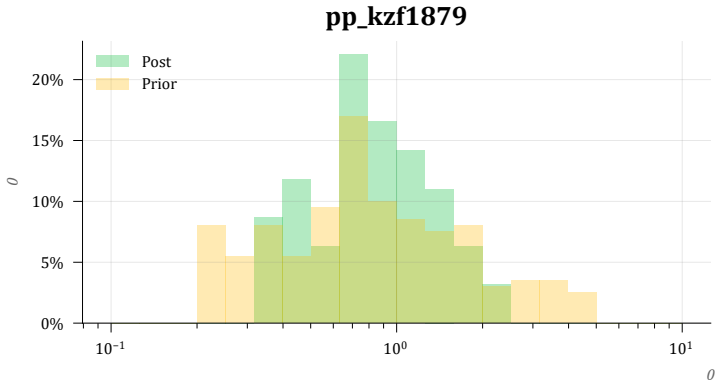

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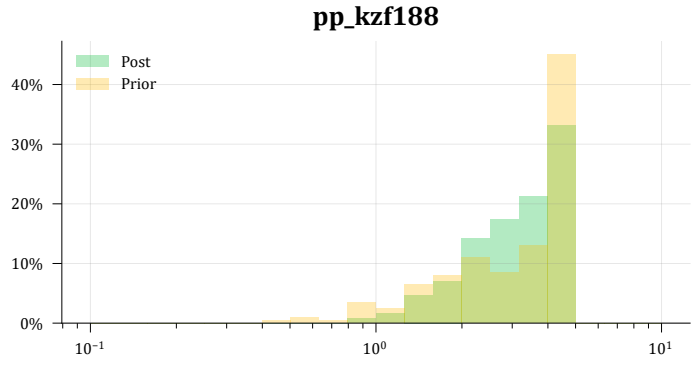

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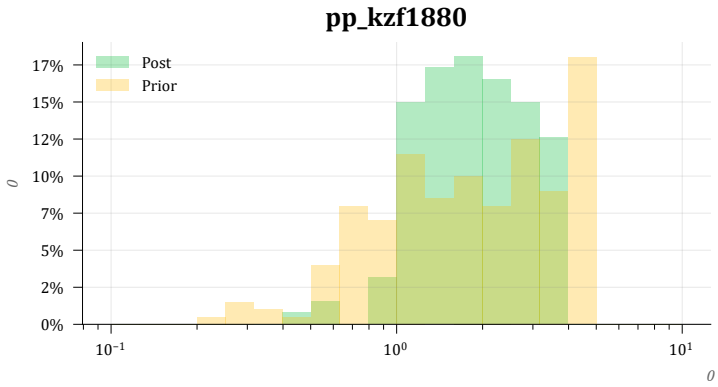

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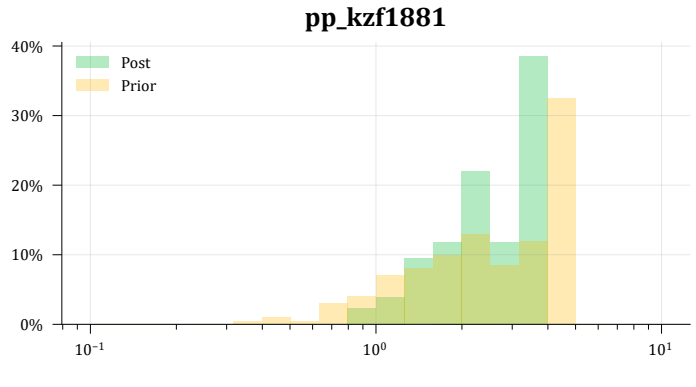

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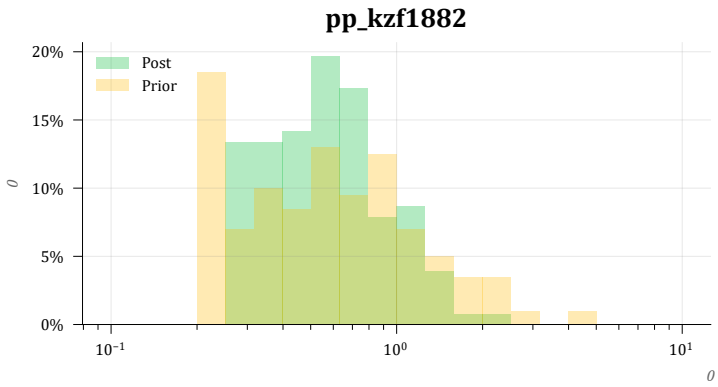

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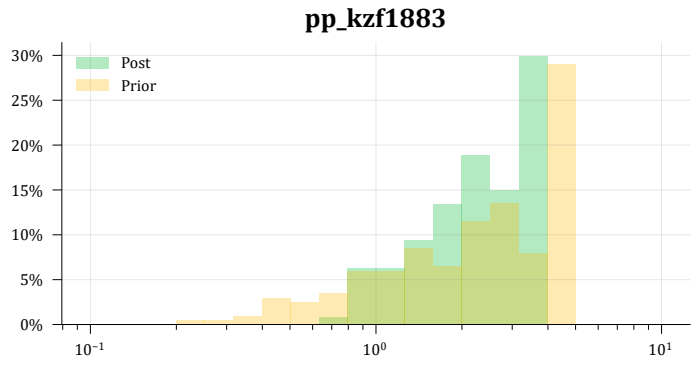

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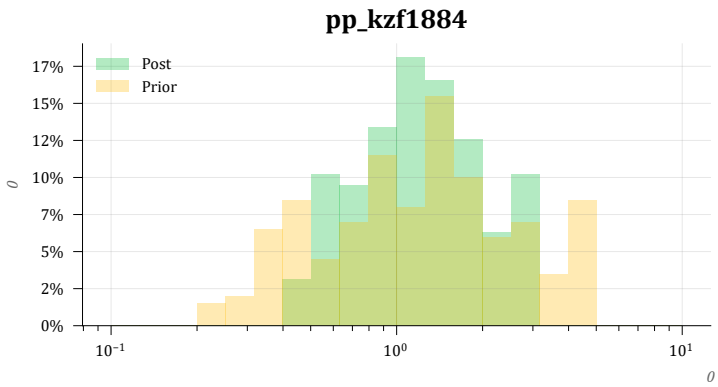

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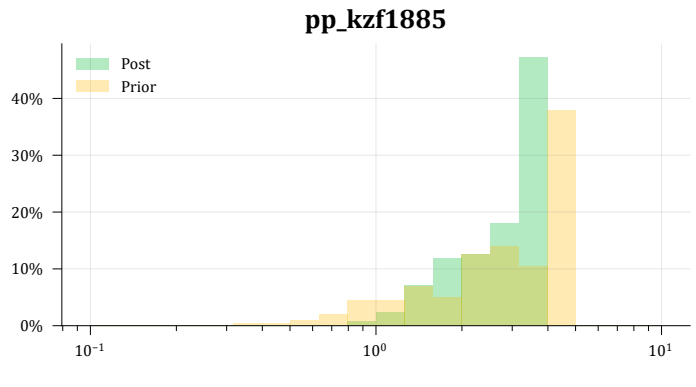

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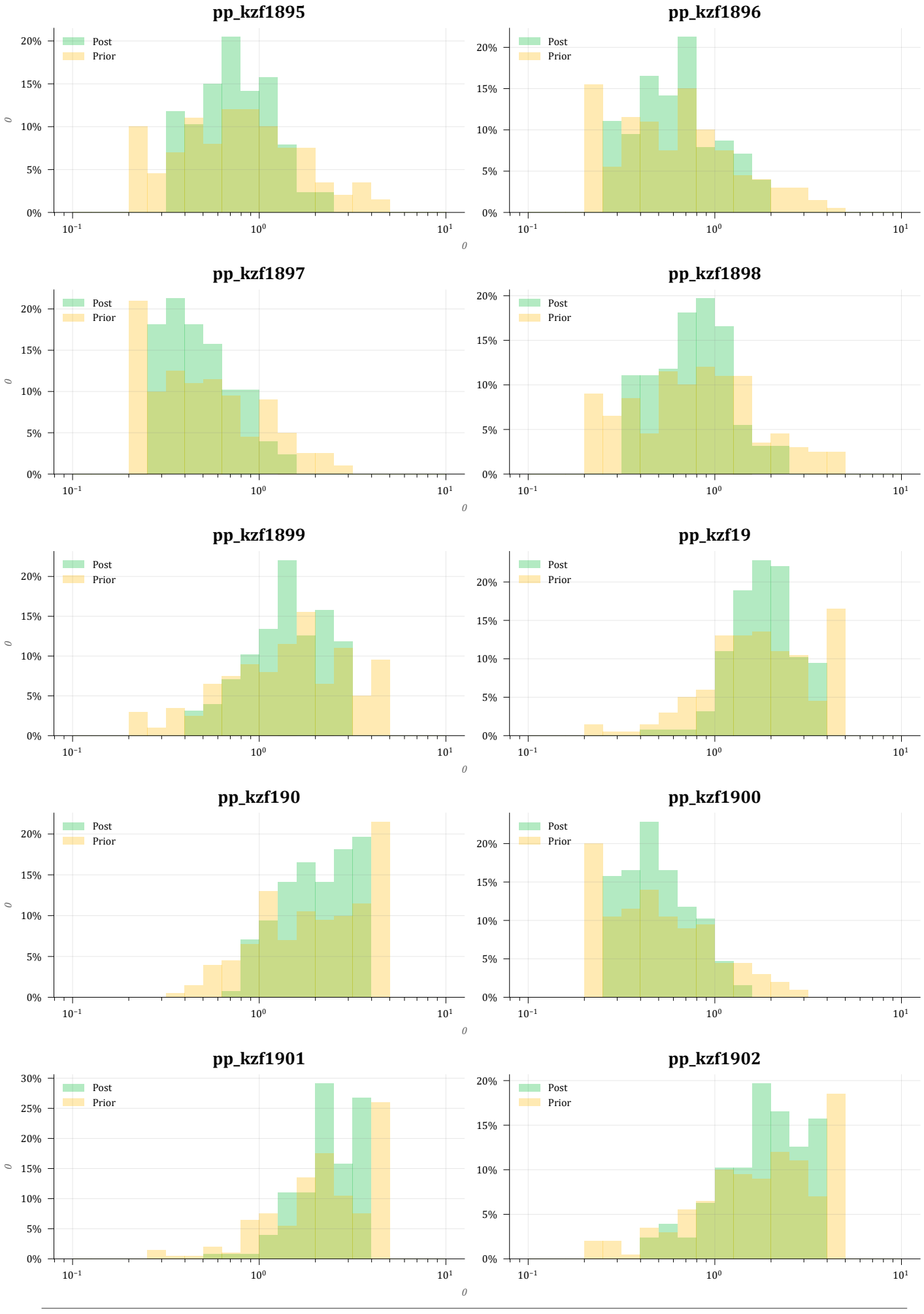

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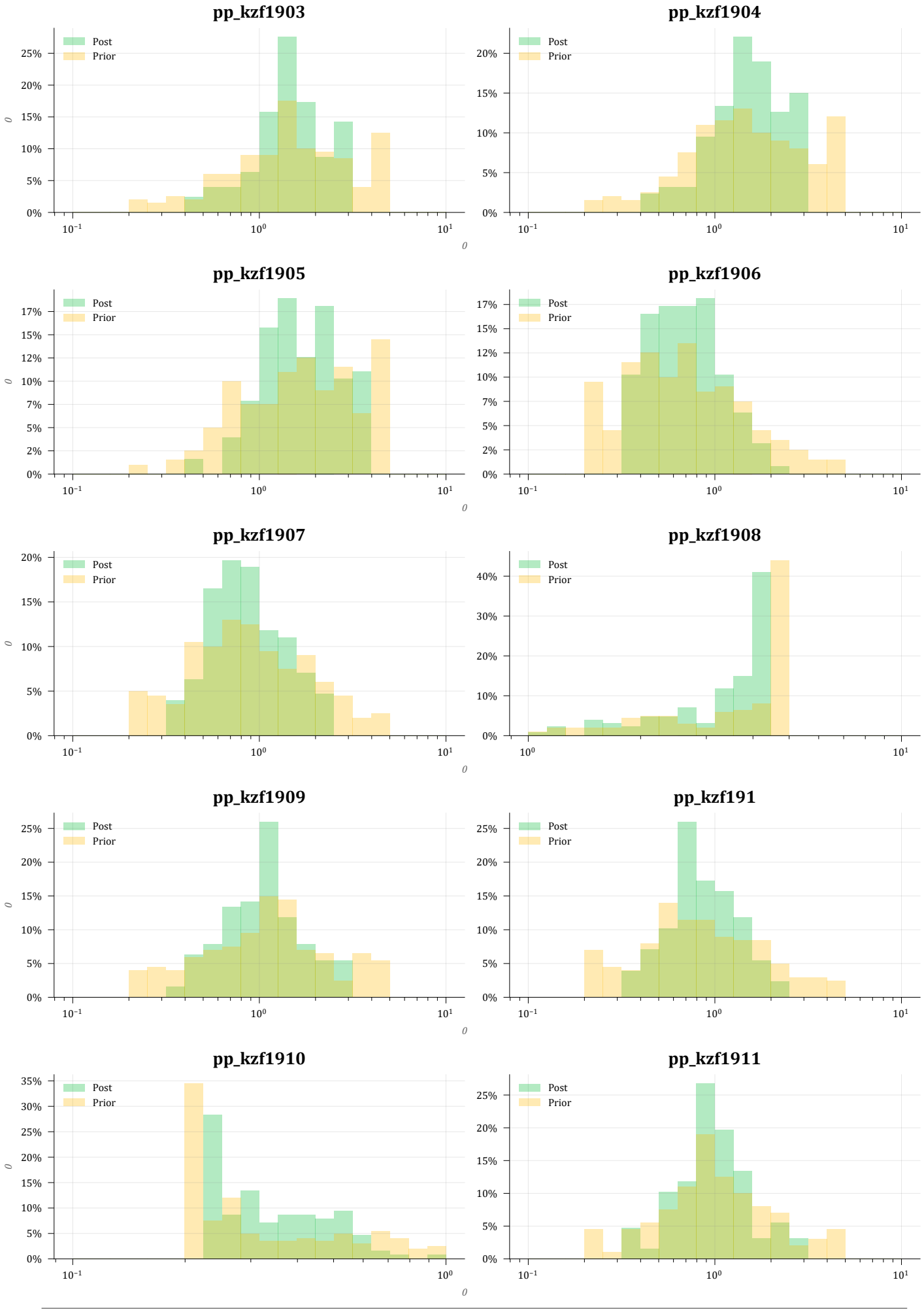

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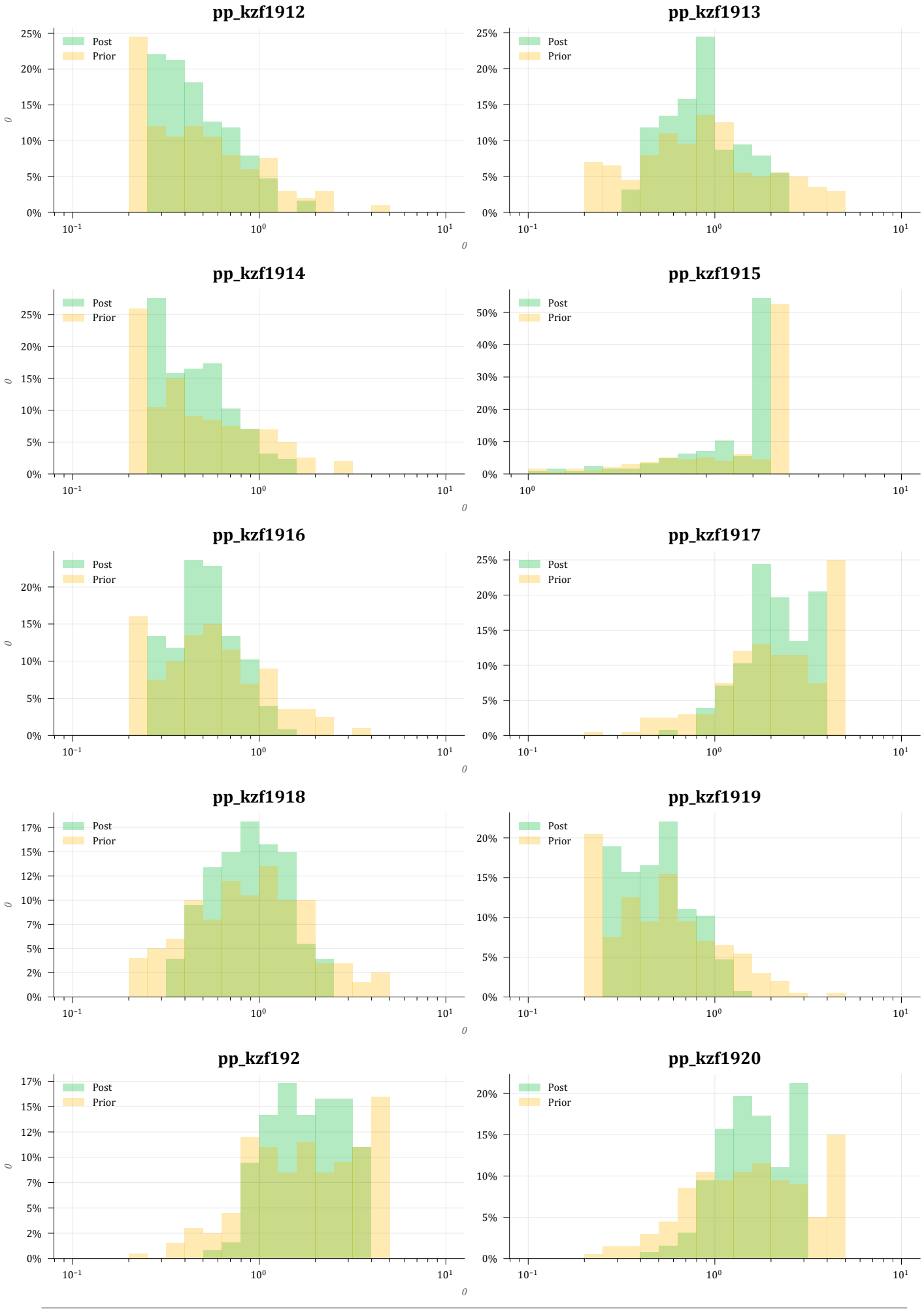

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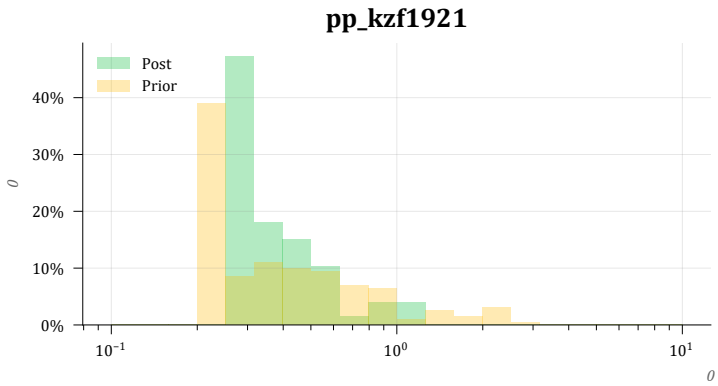

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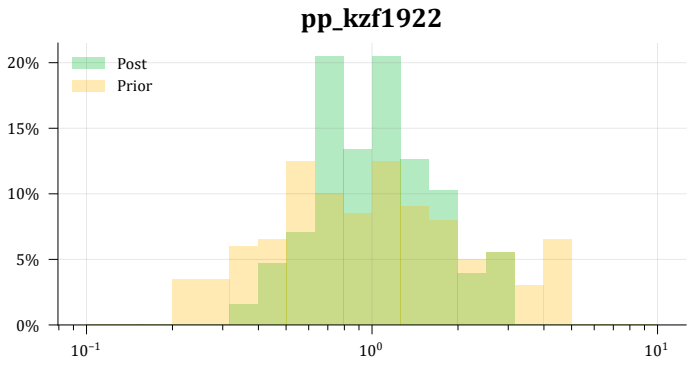

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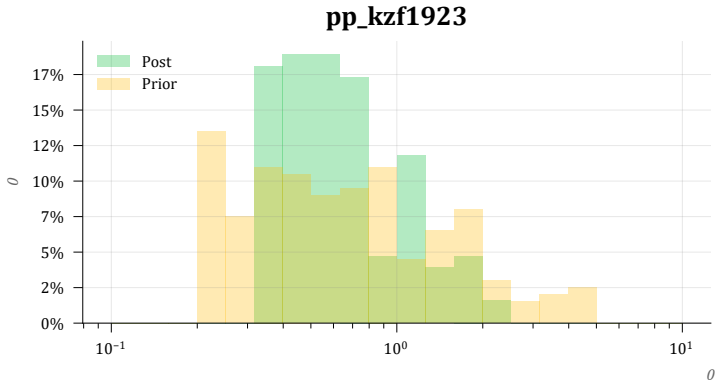

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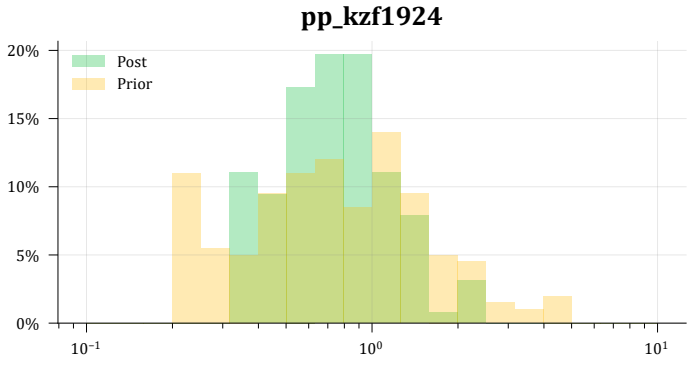

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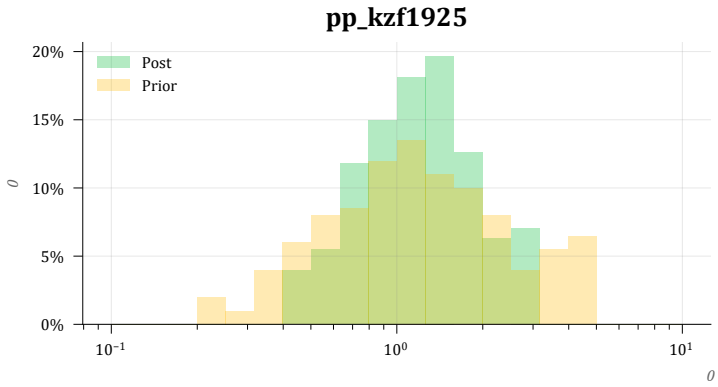

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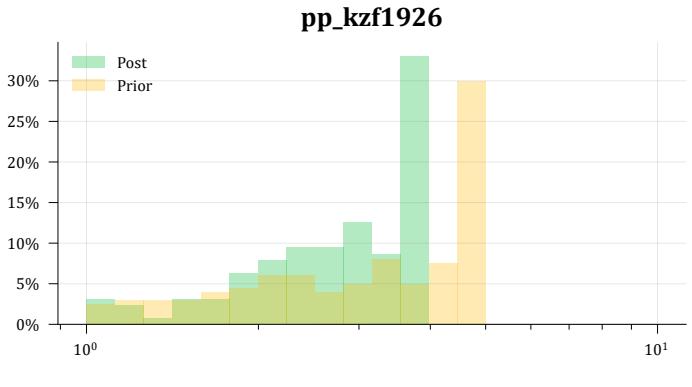

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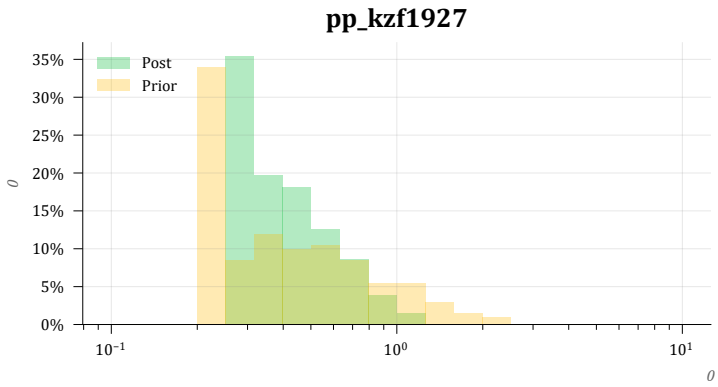

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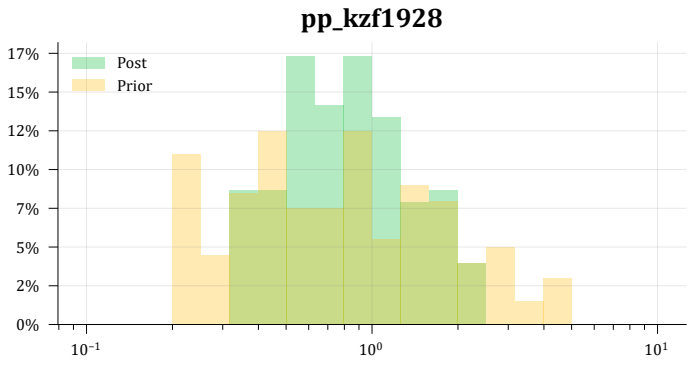

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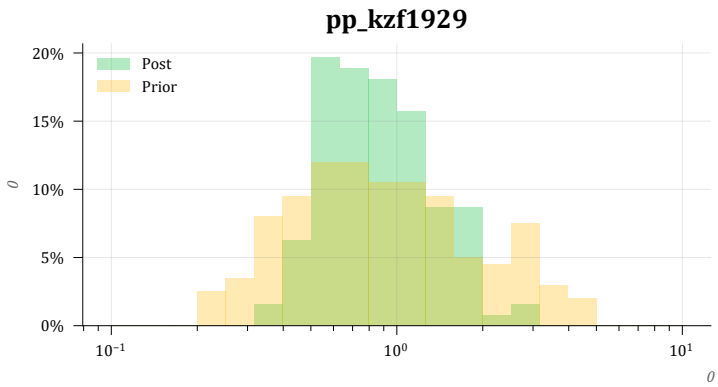

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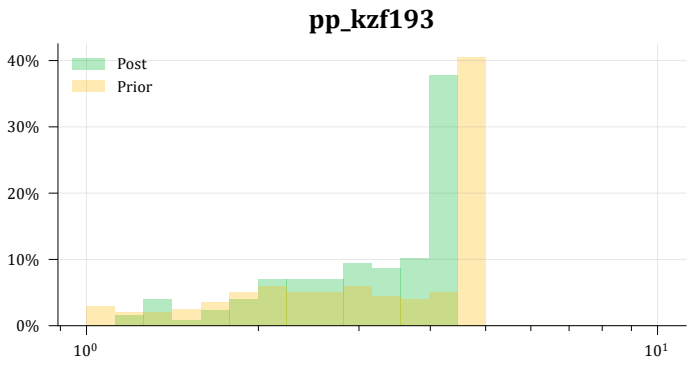

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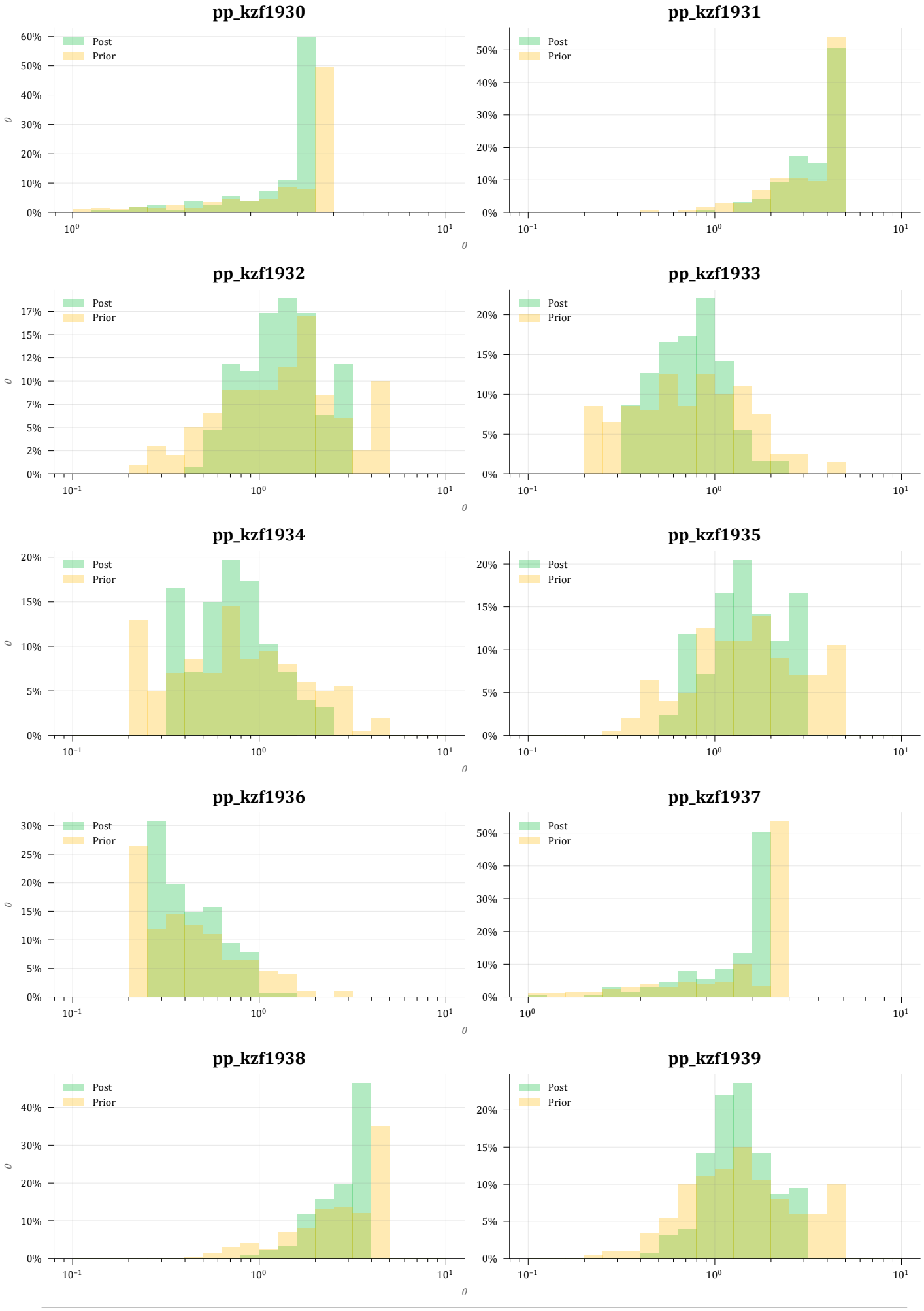

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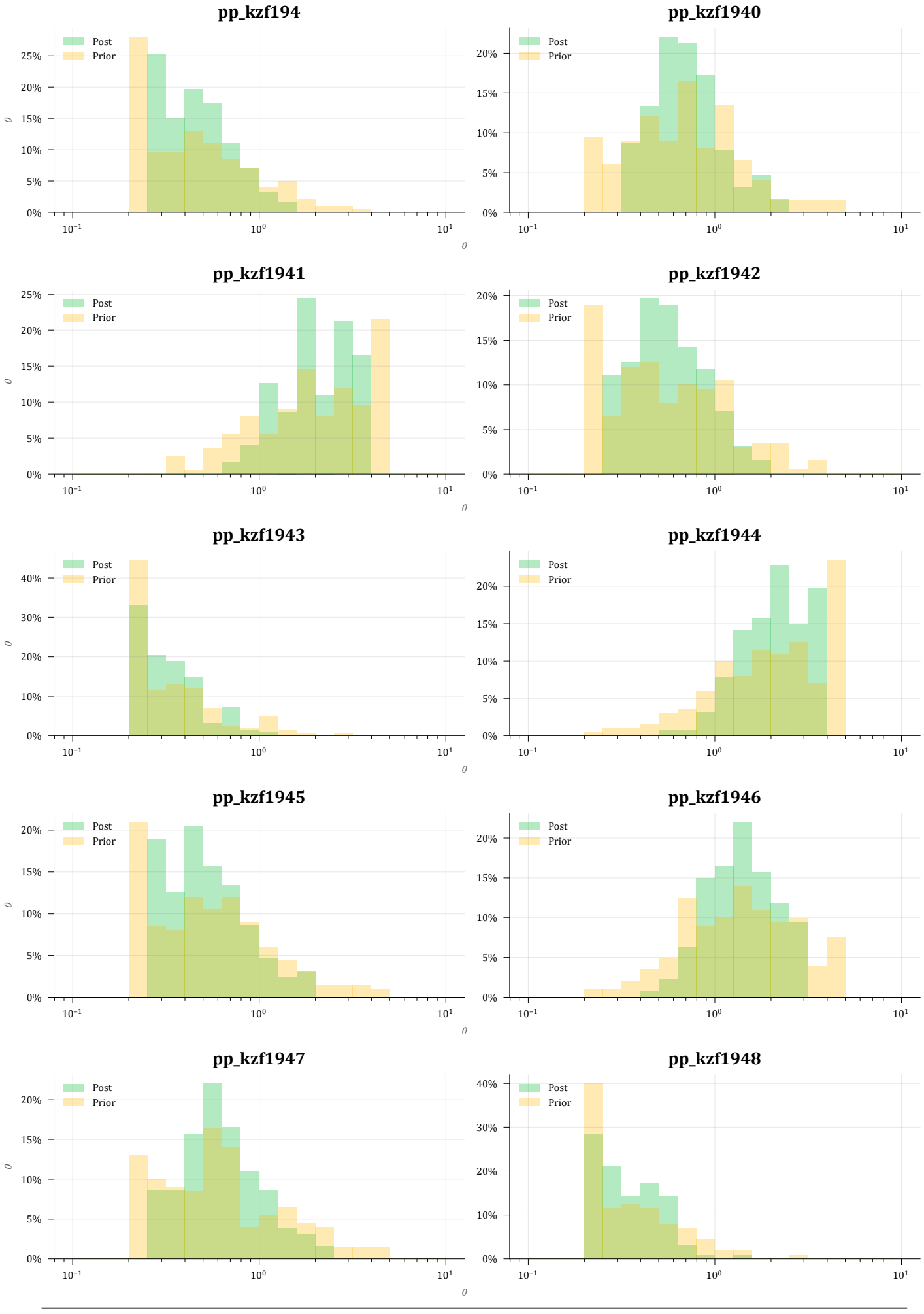

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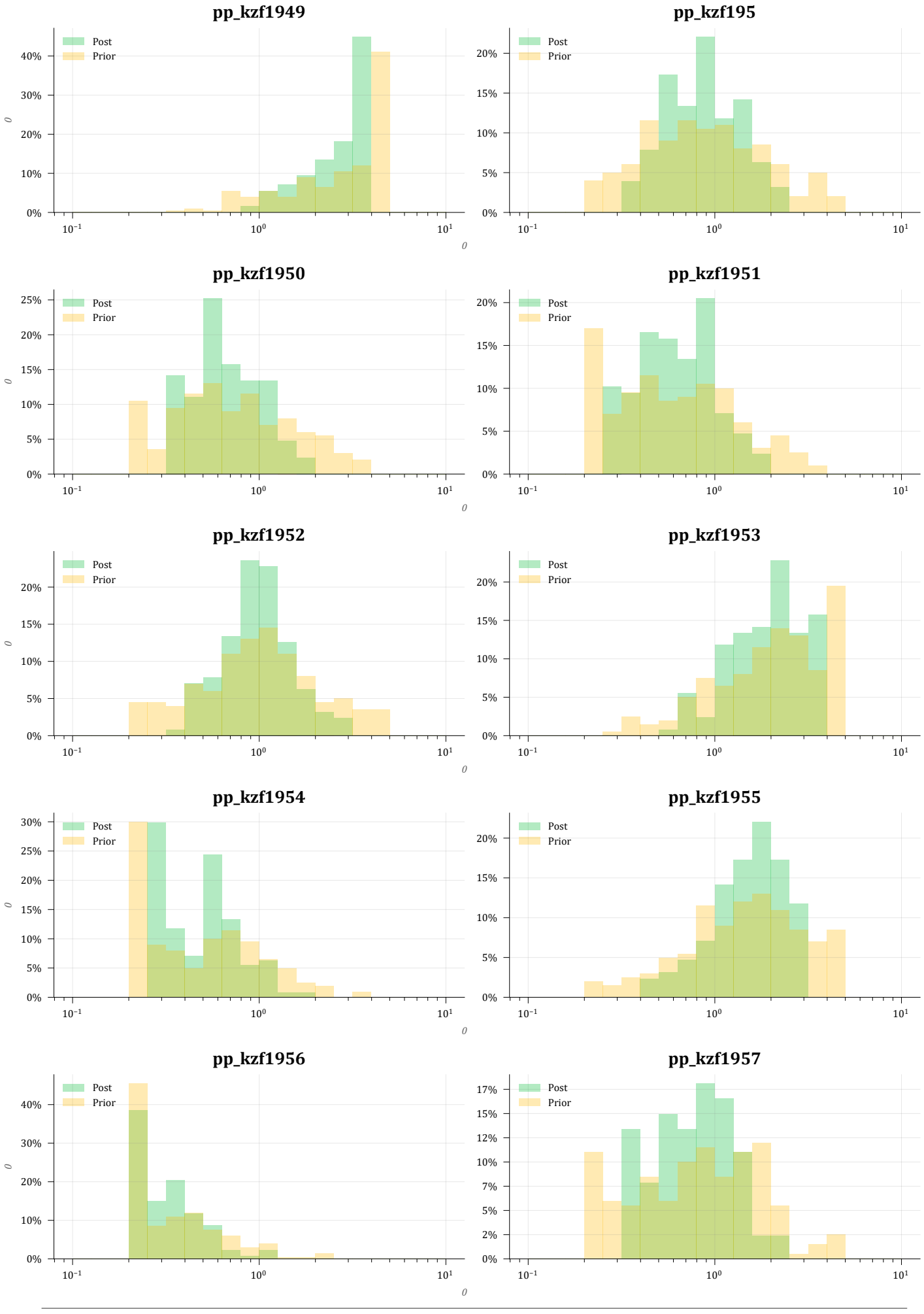

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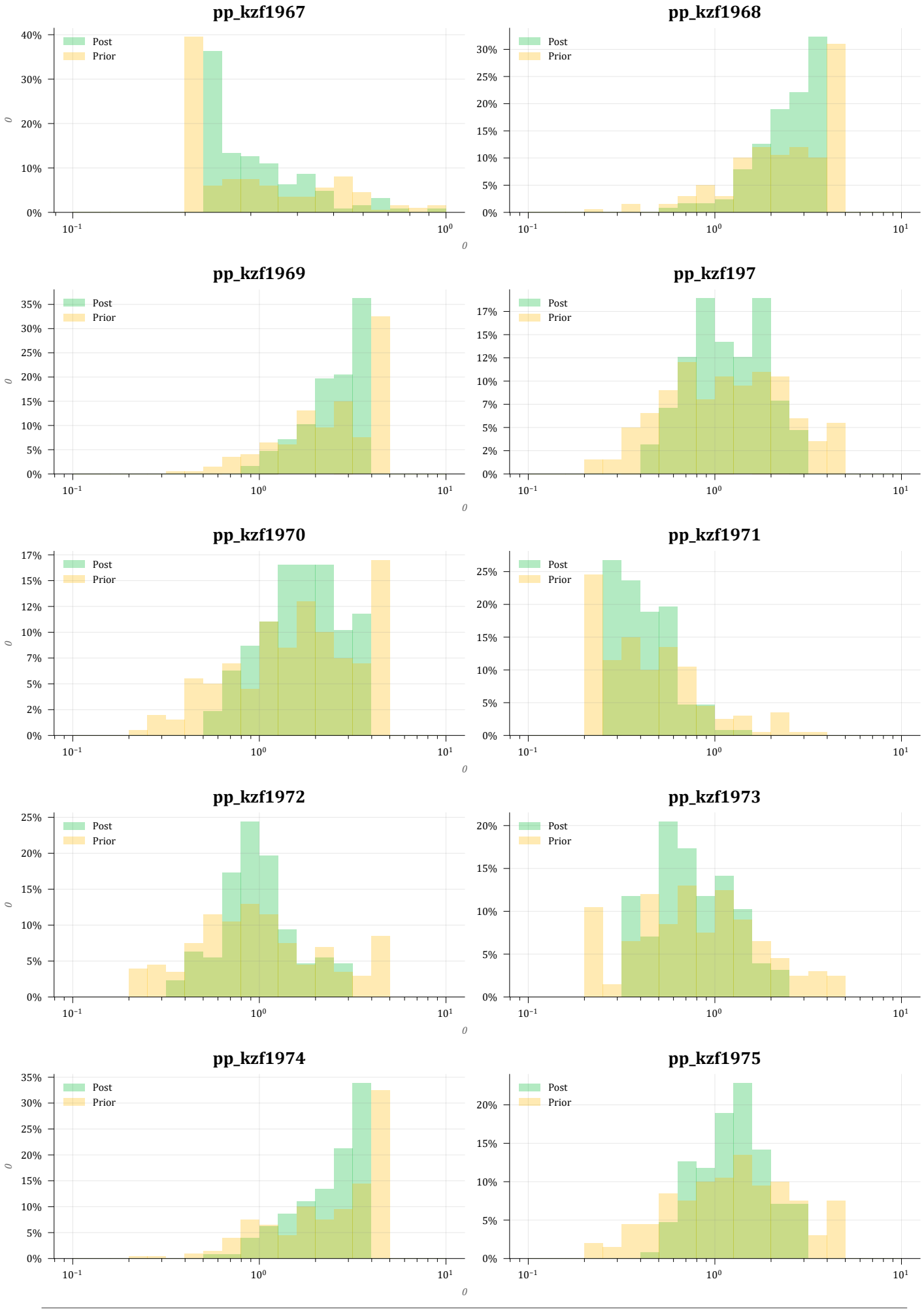
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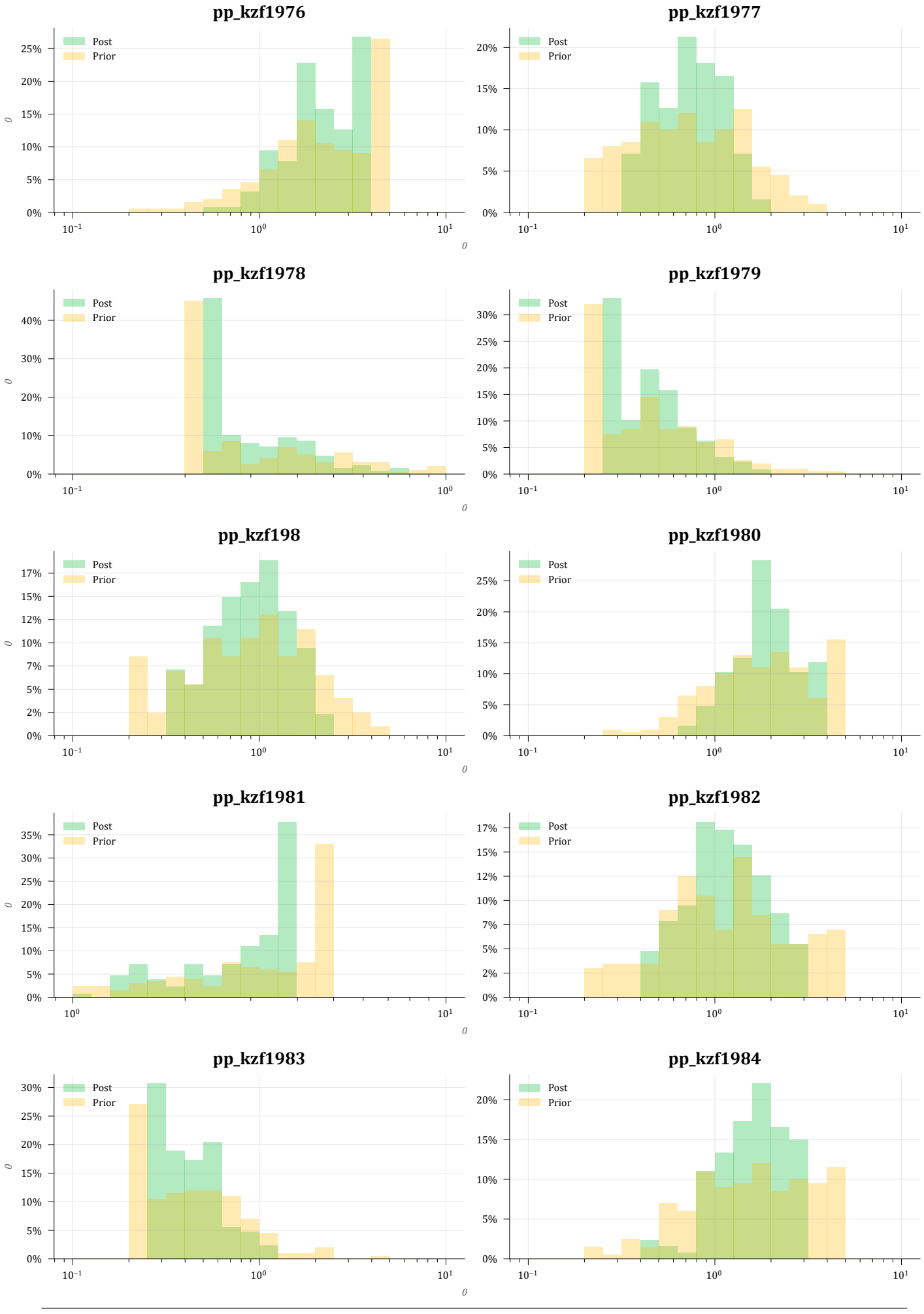

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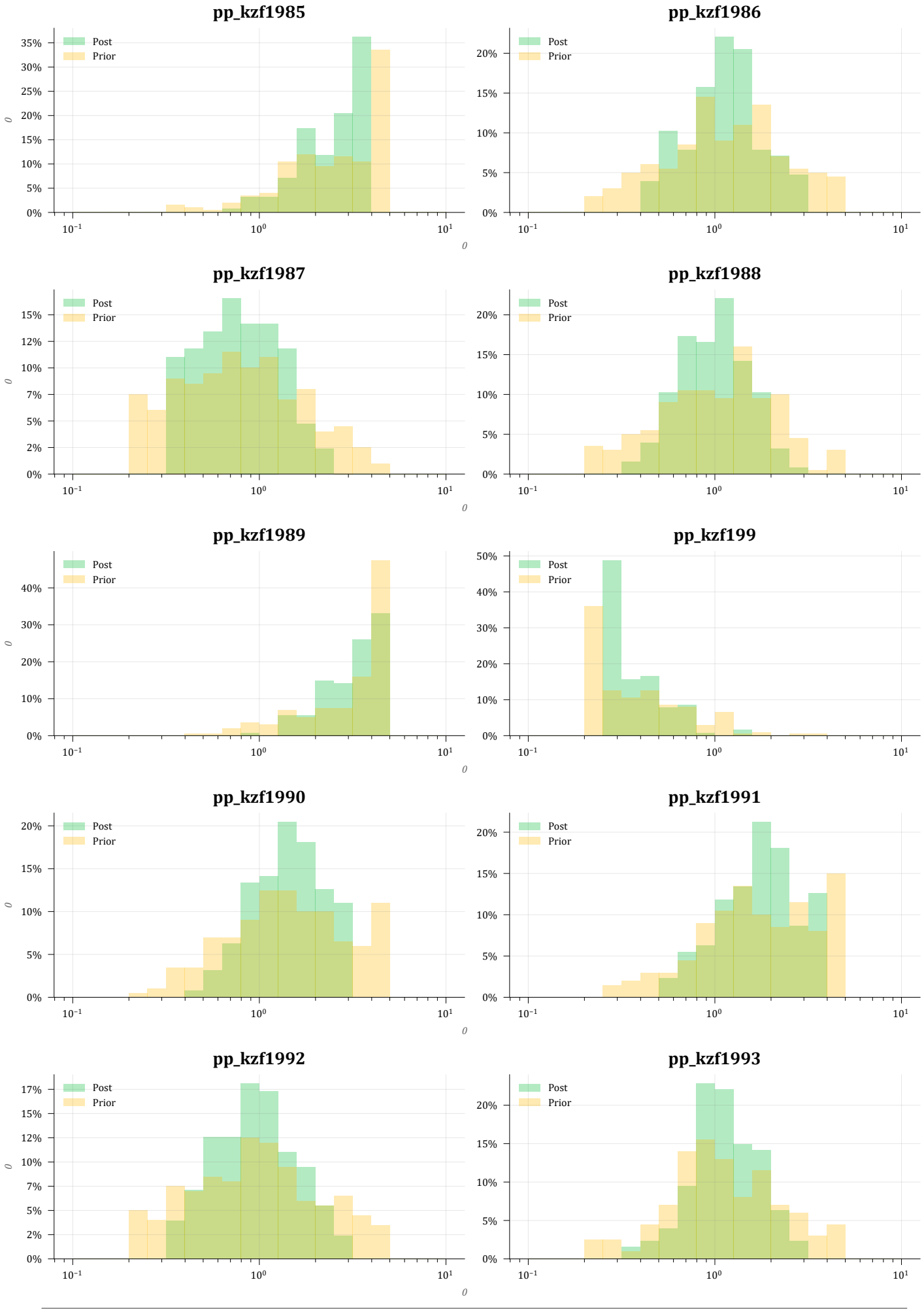

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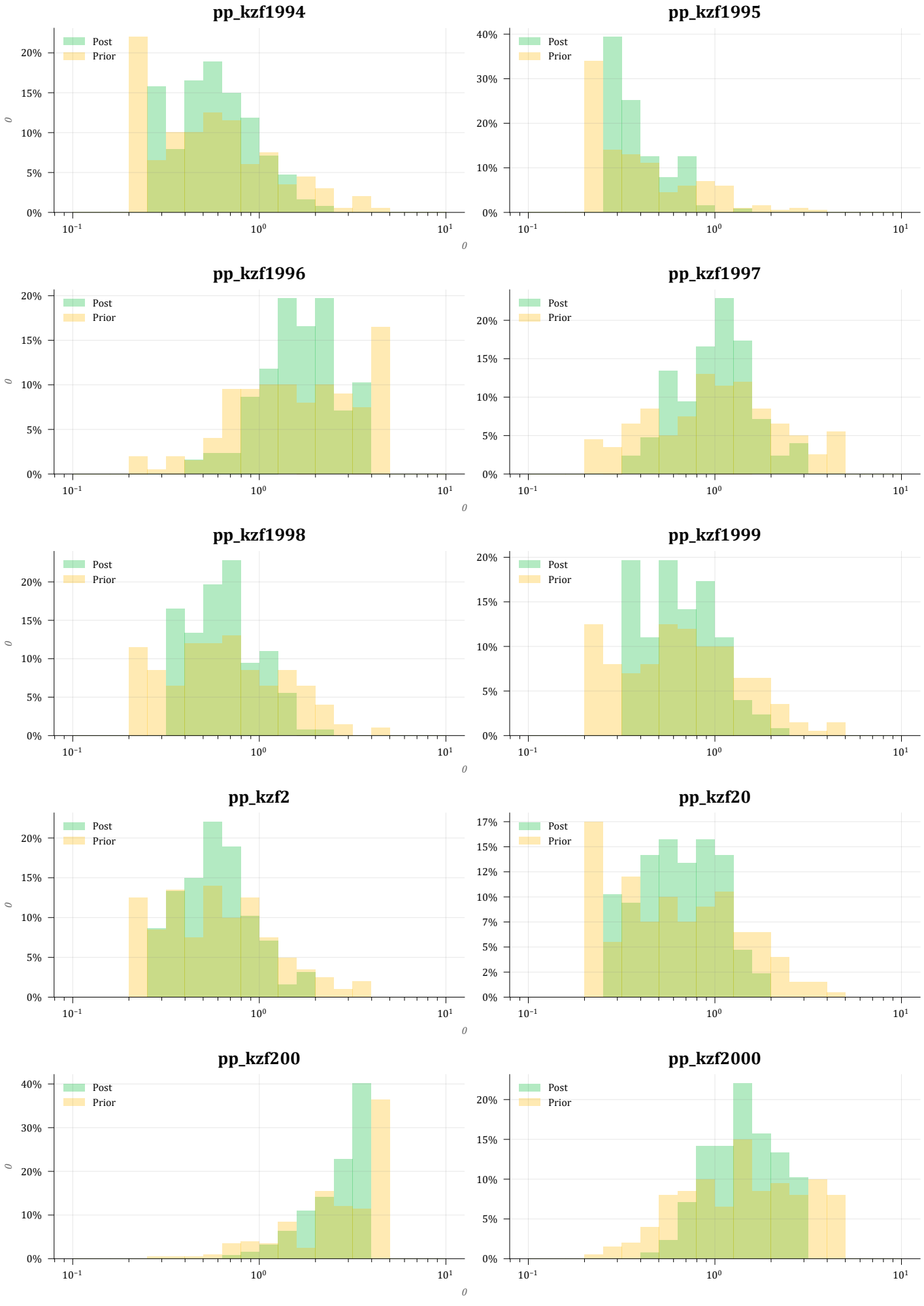

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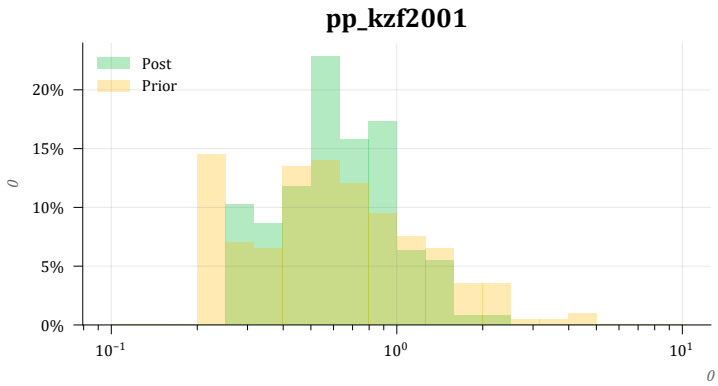

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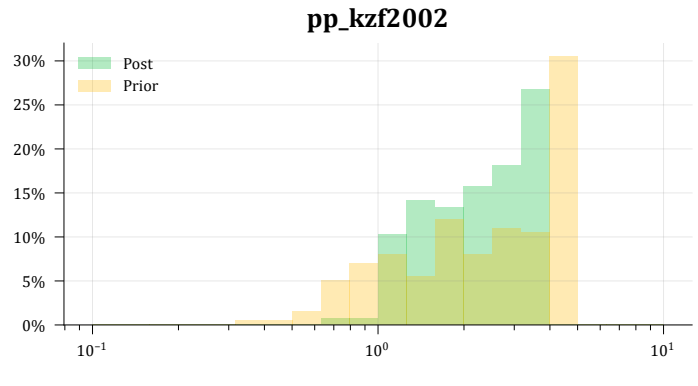

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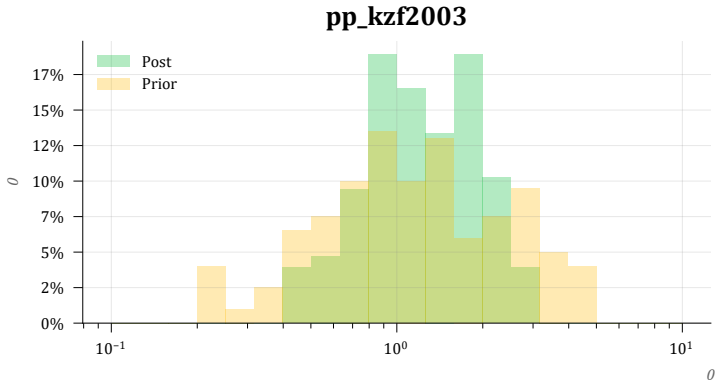

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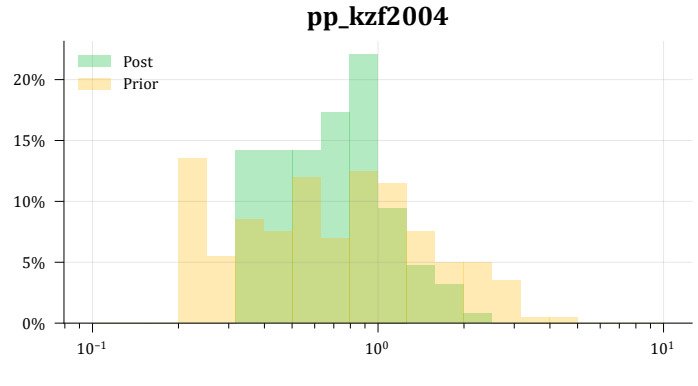

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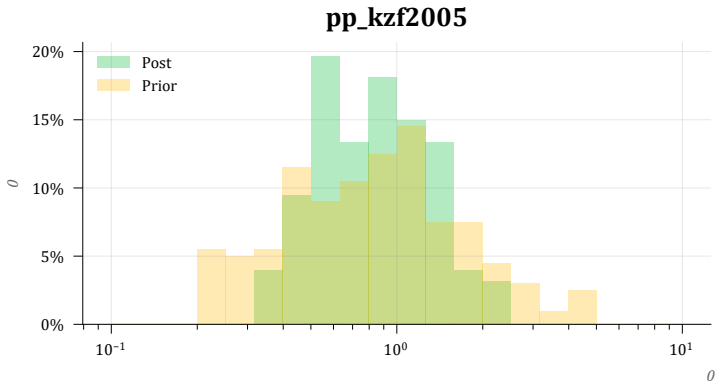

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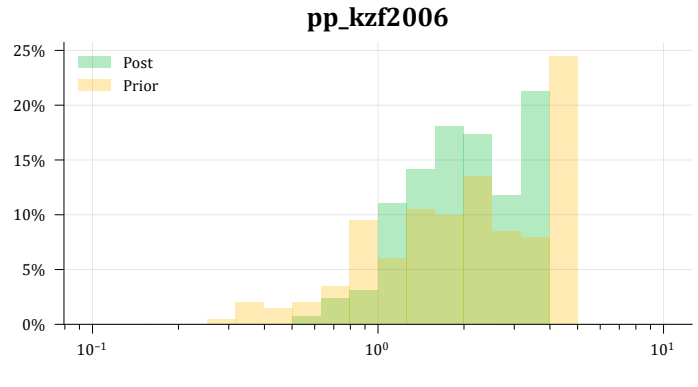

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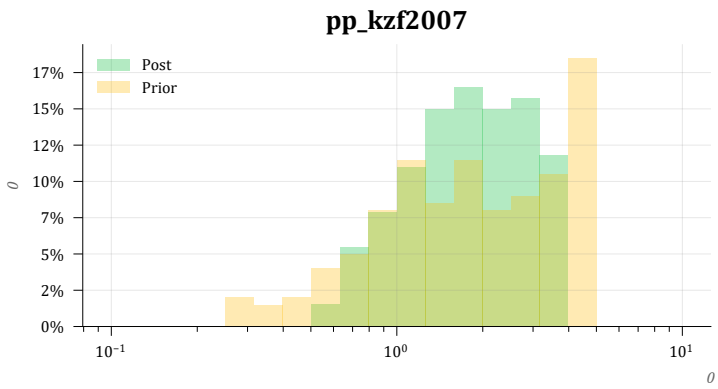

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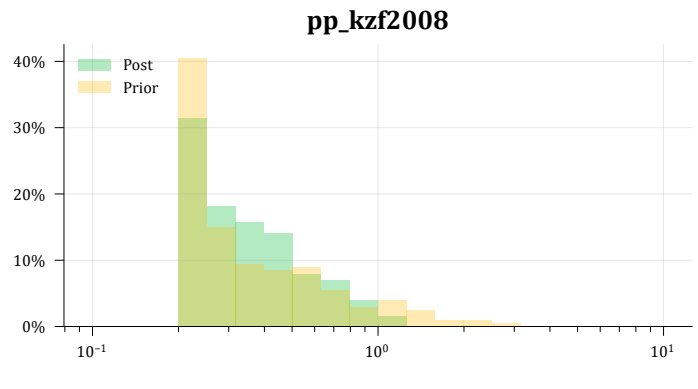

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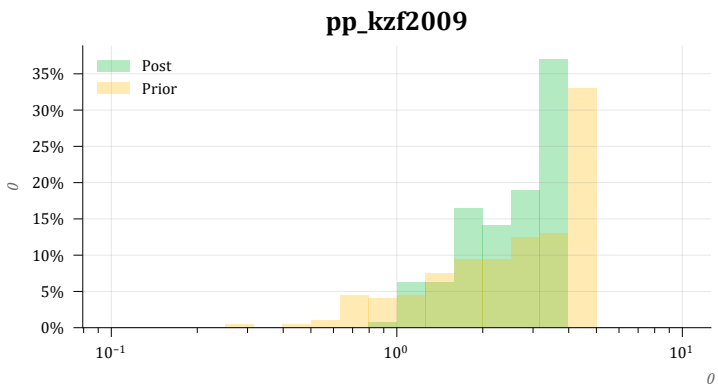

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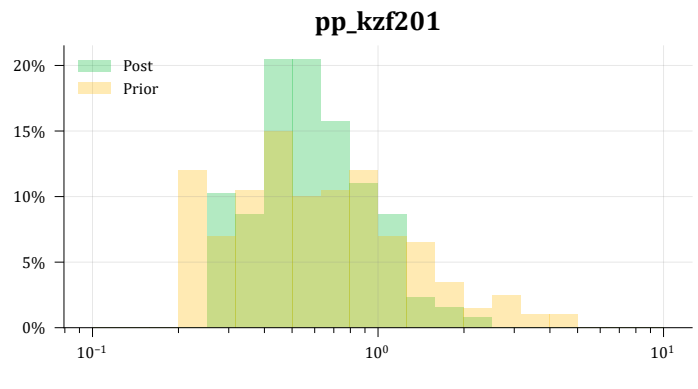

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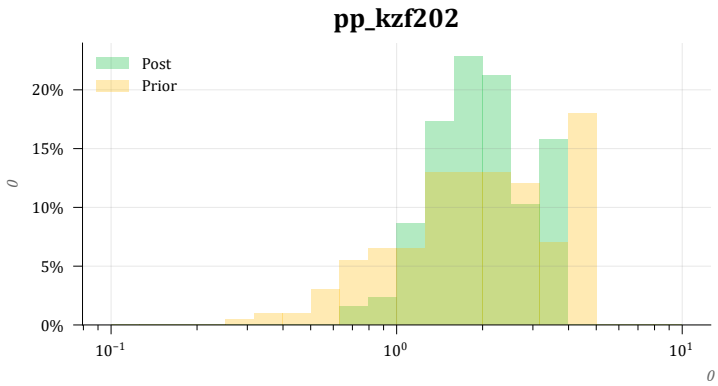

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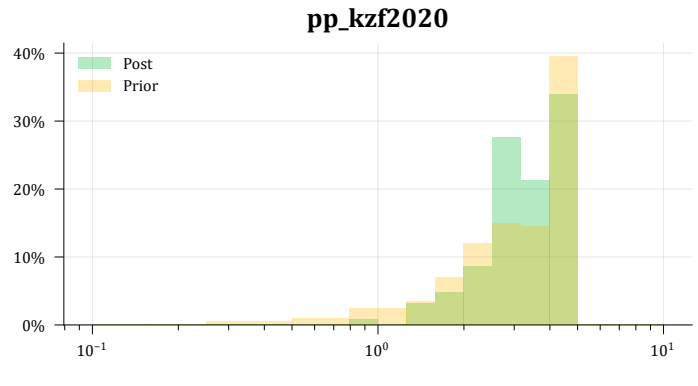

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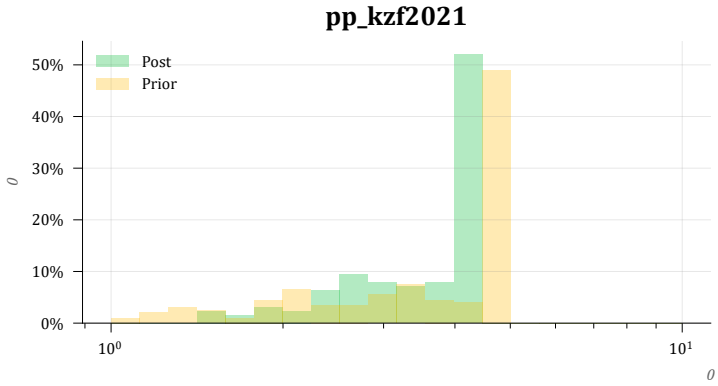

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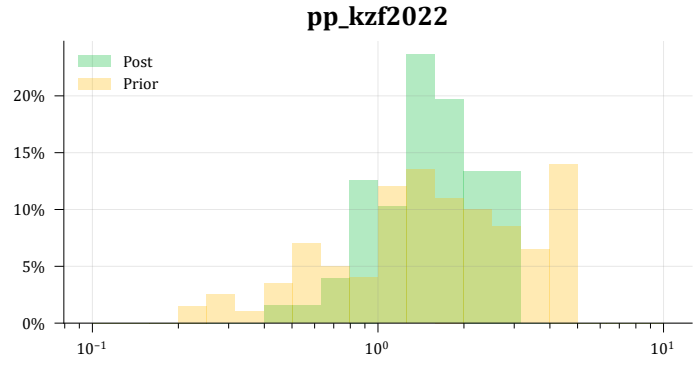

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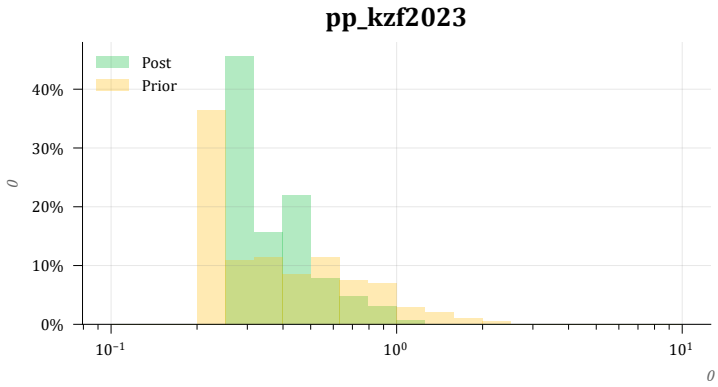

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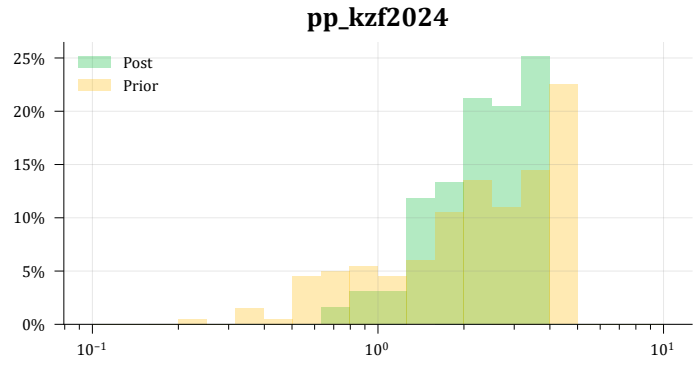

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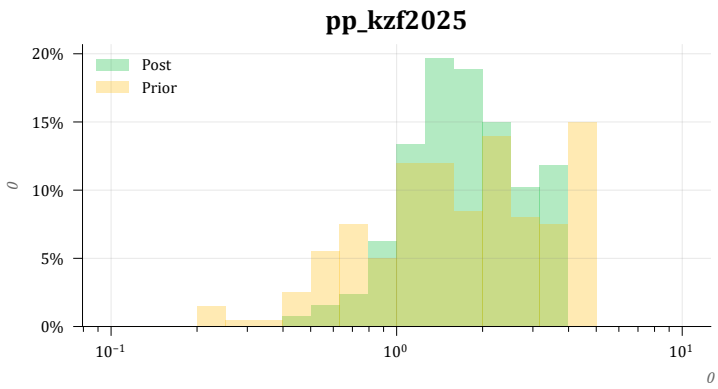

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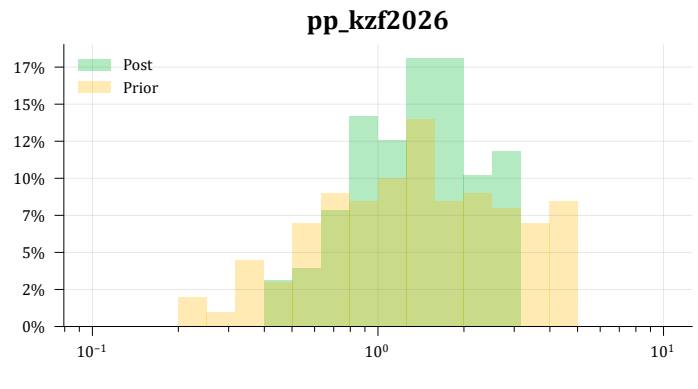

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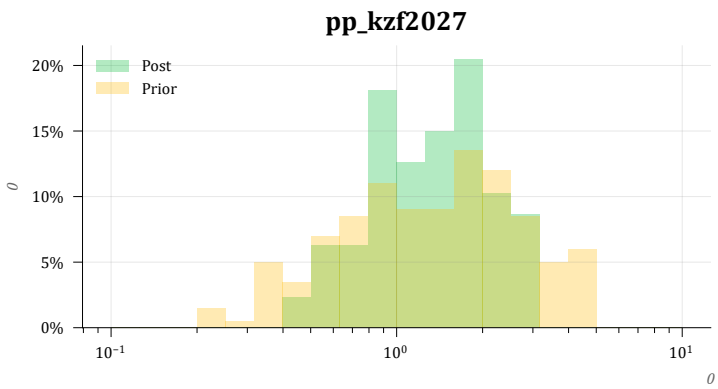

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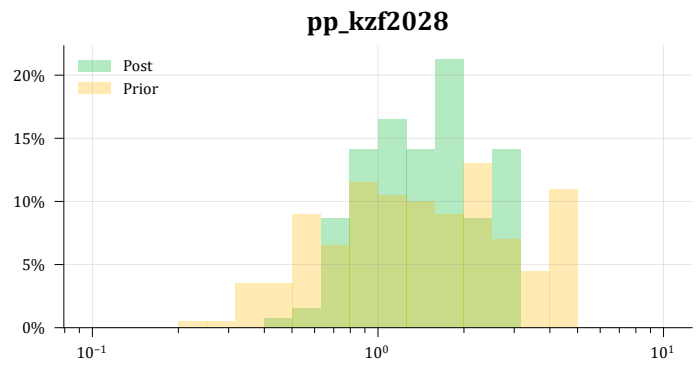

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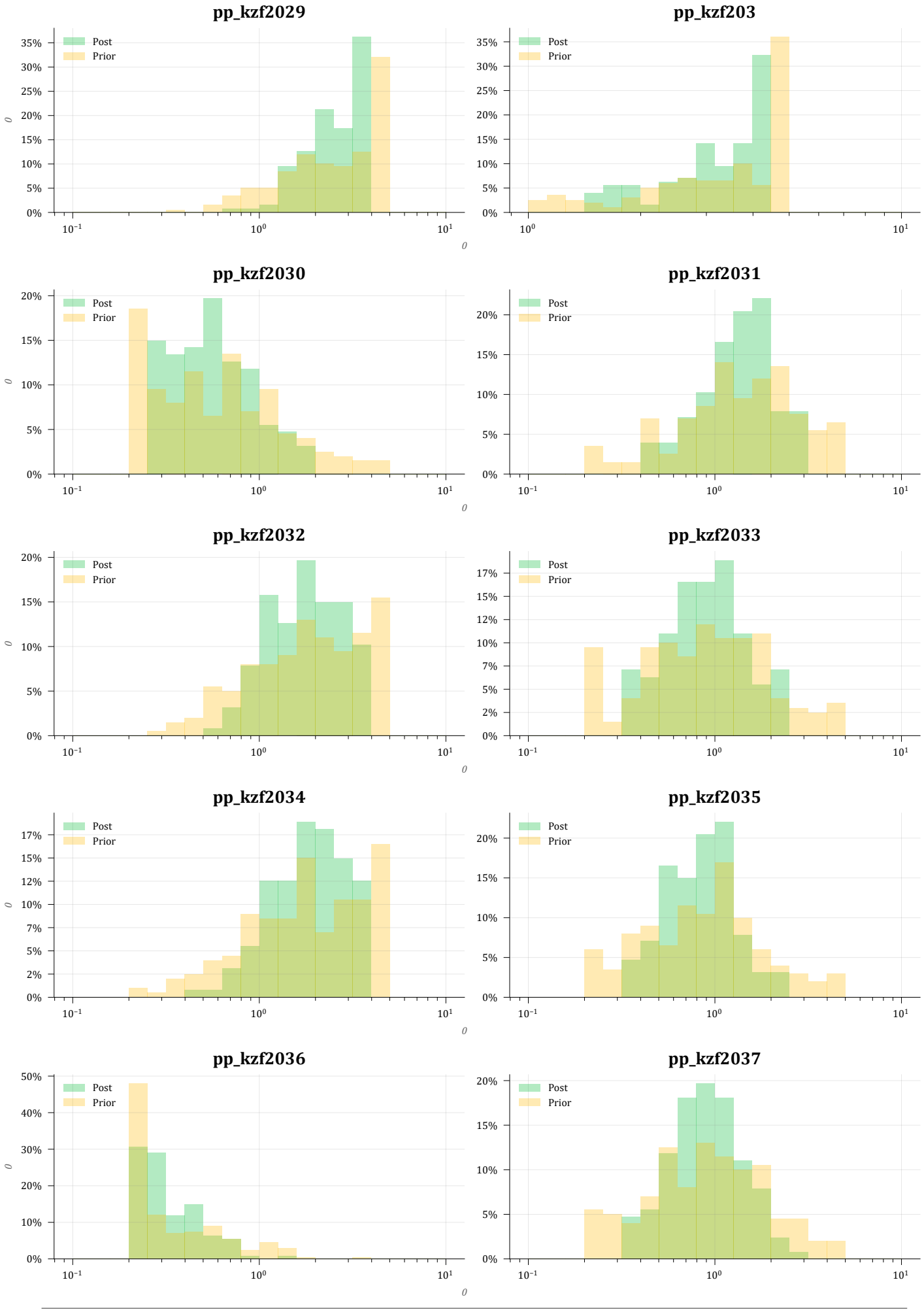

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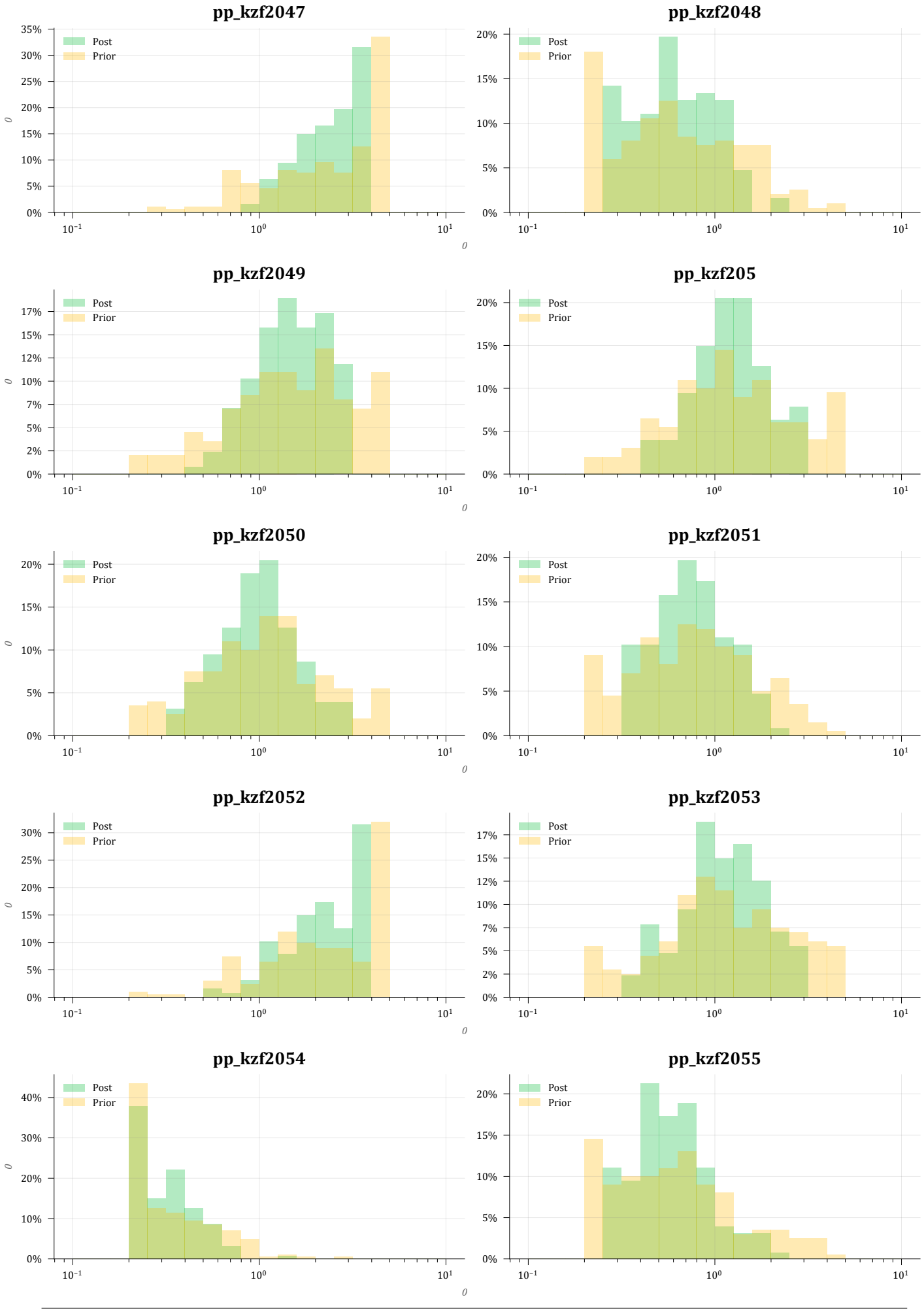

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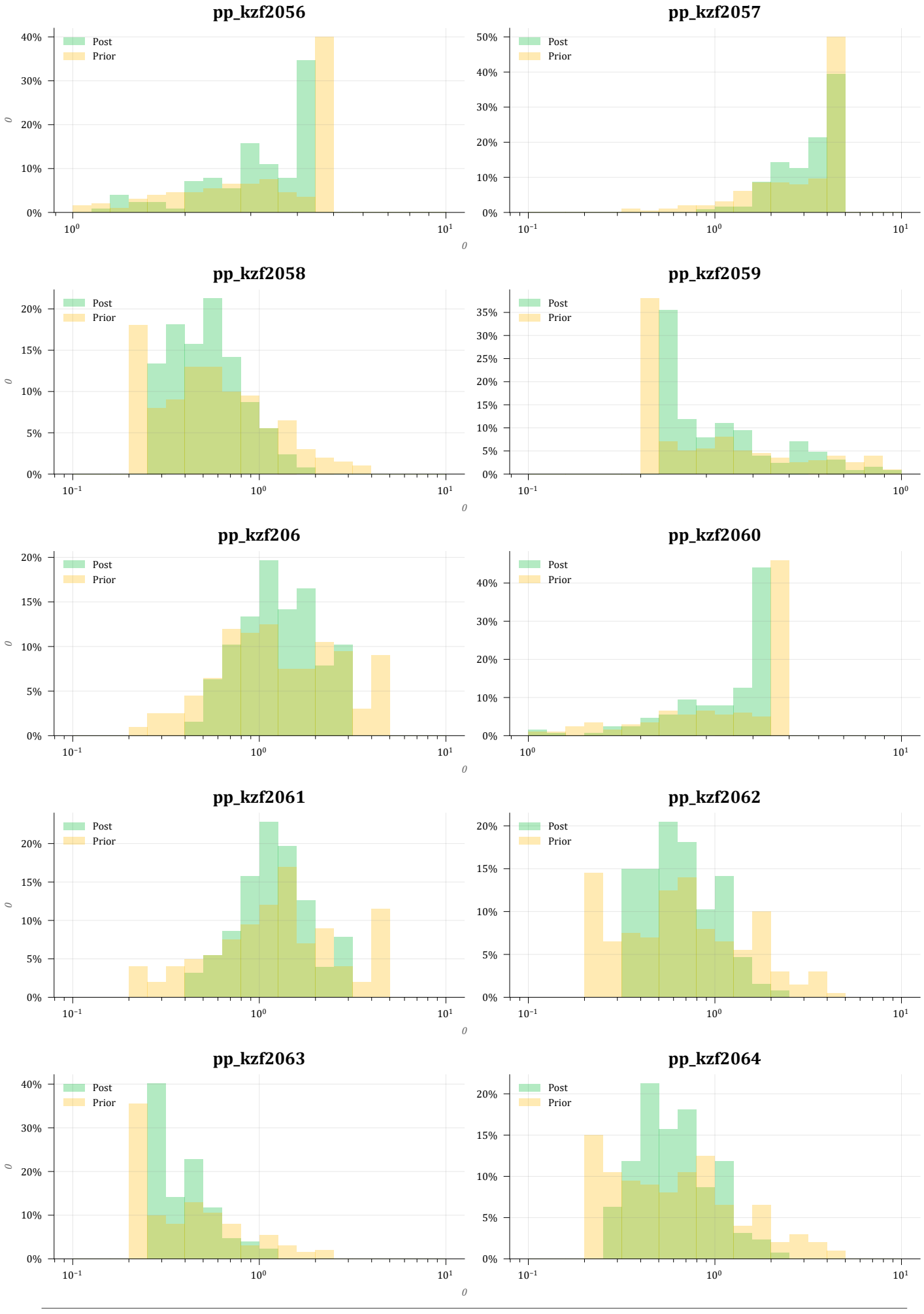

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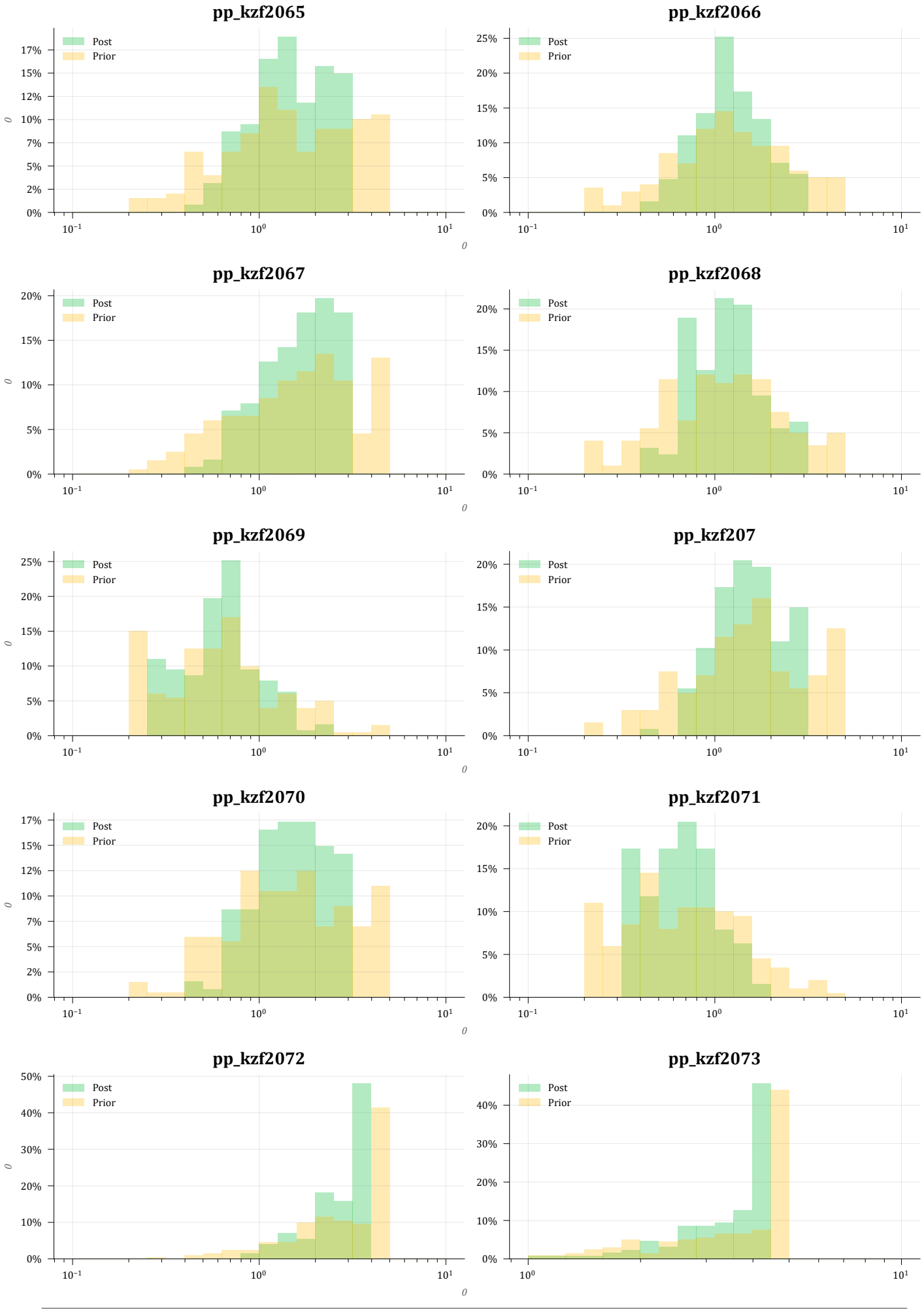

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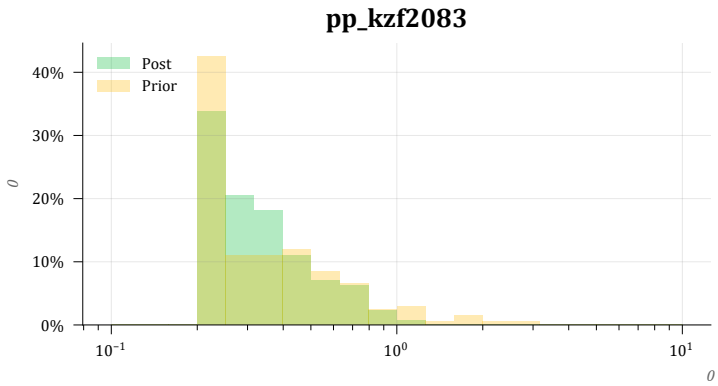

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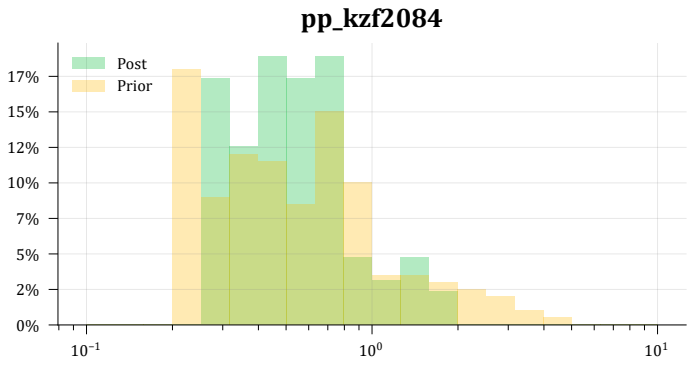

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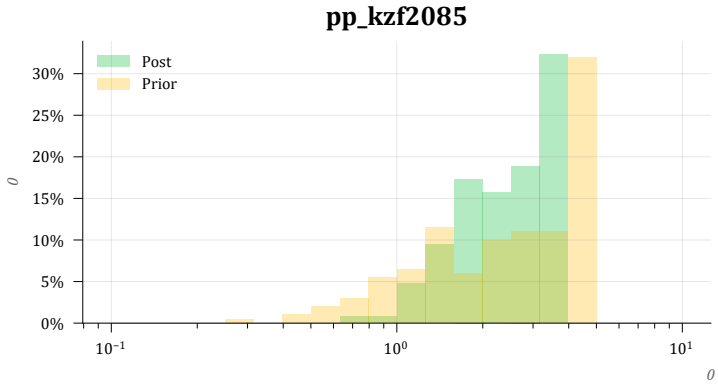

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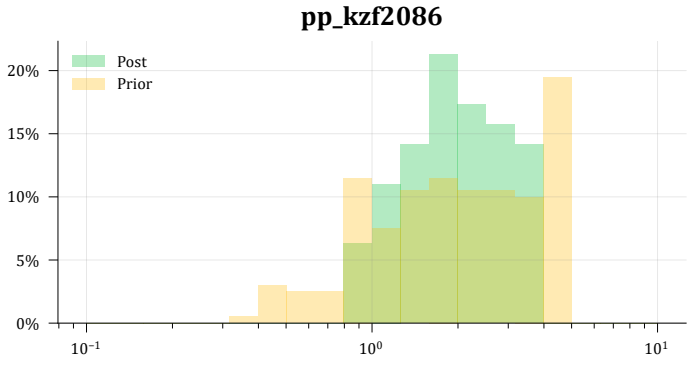

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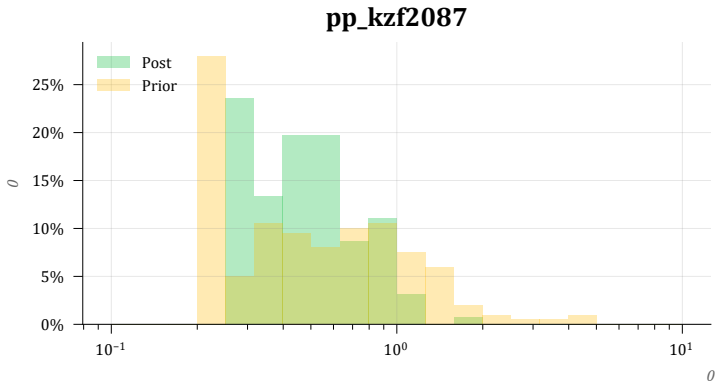

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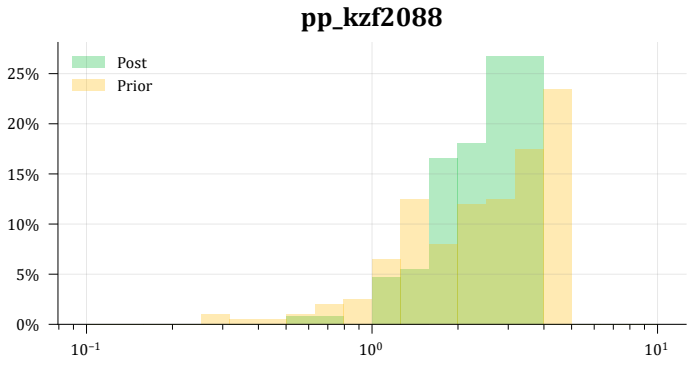

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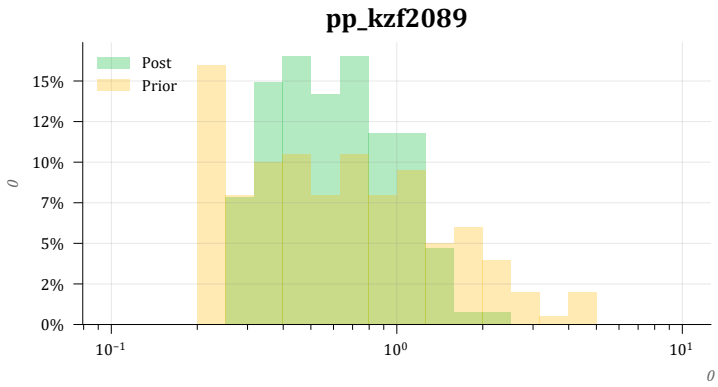

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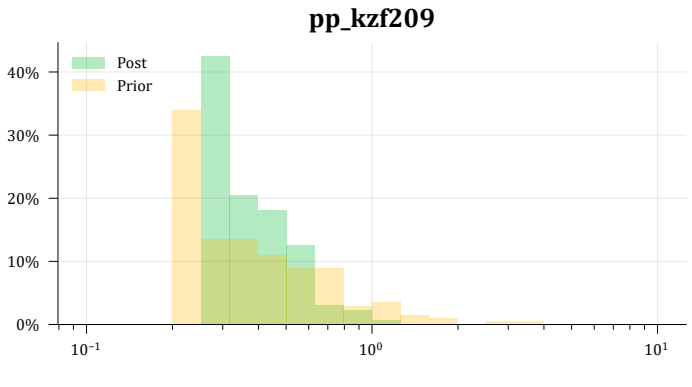

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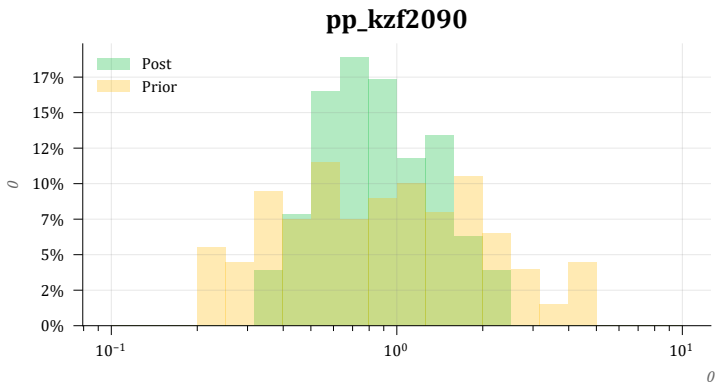

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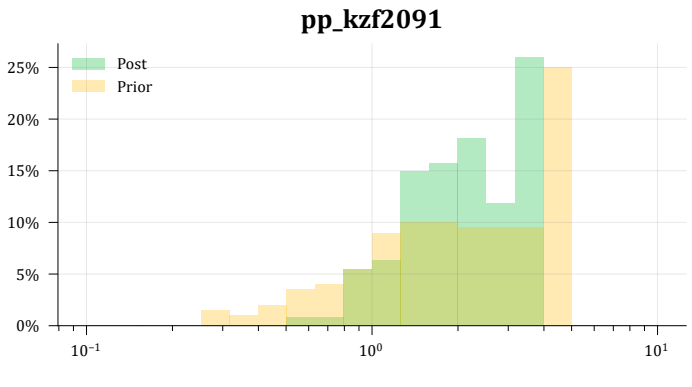

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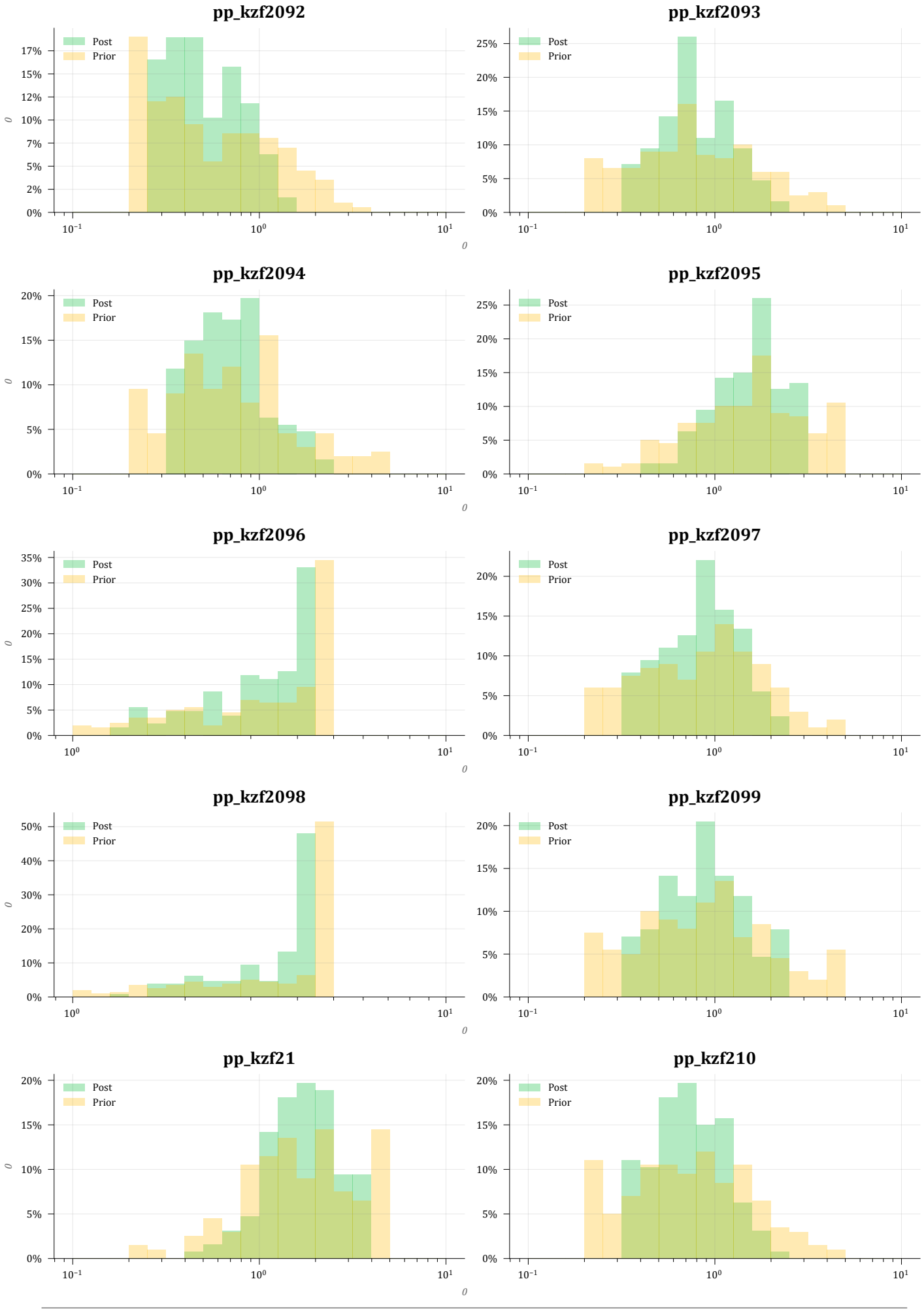

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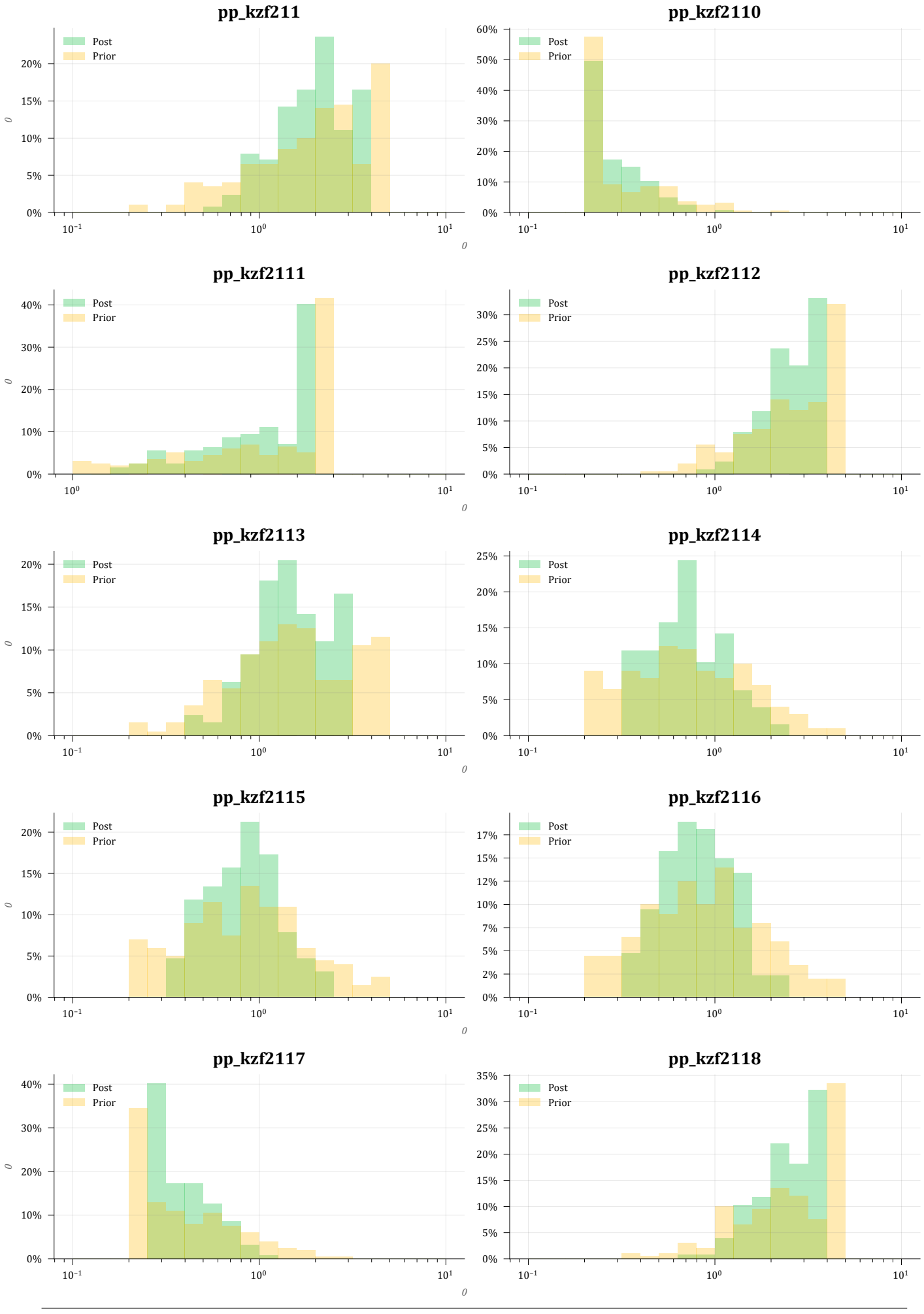

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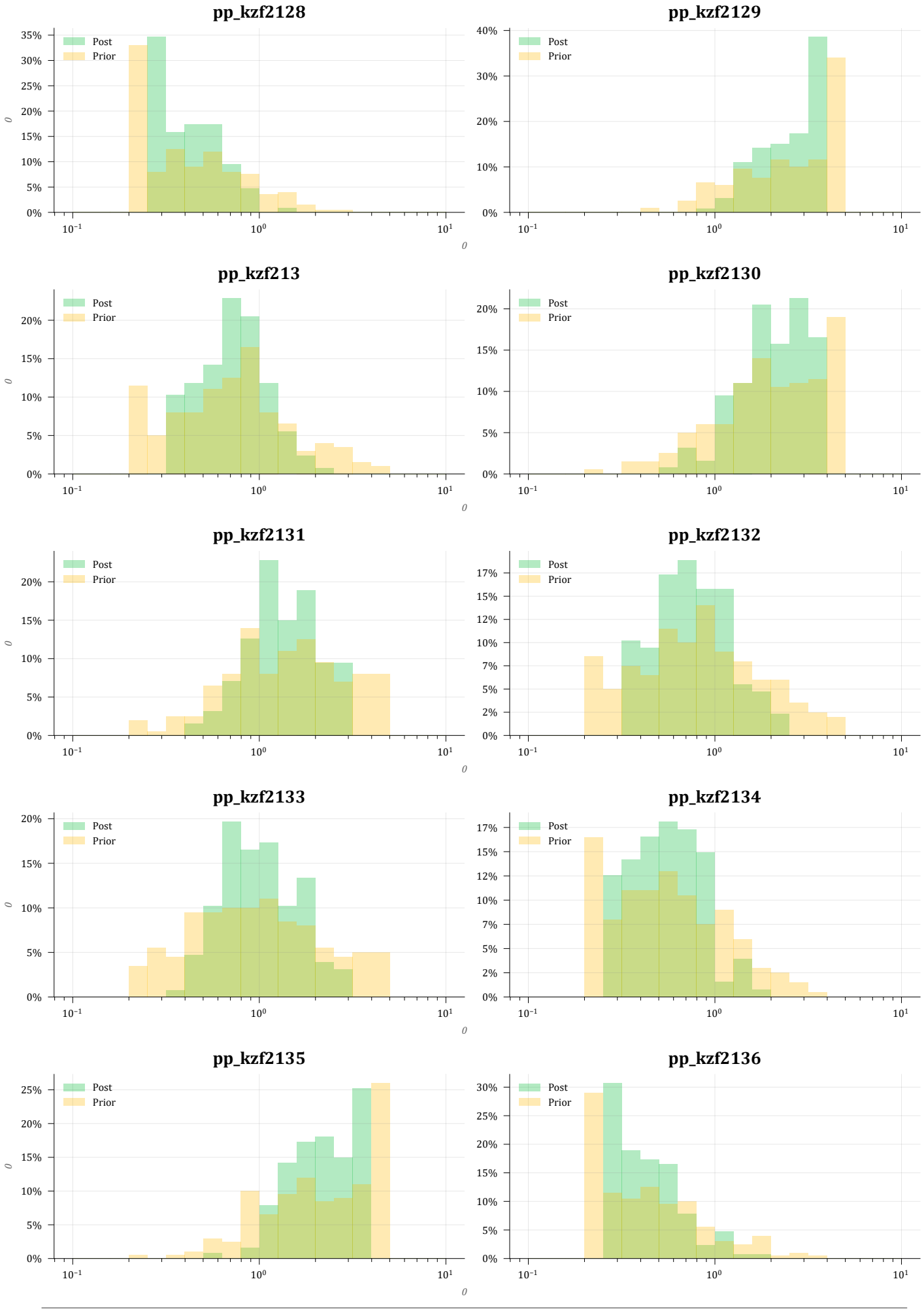
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Prior
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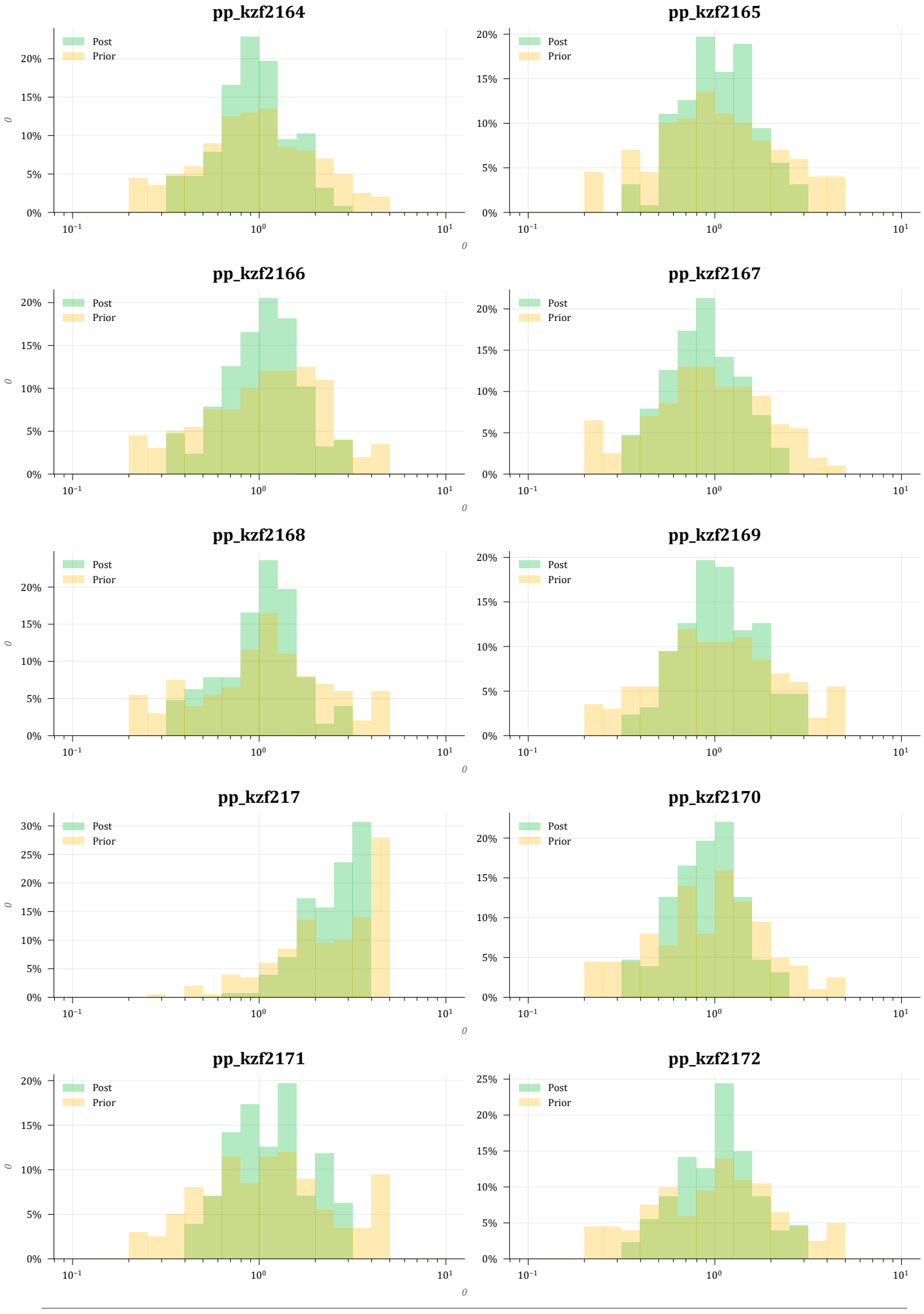

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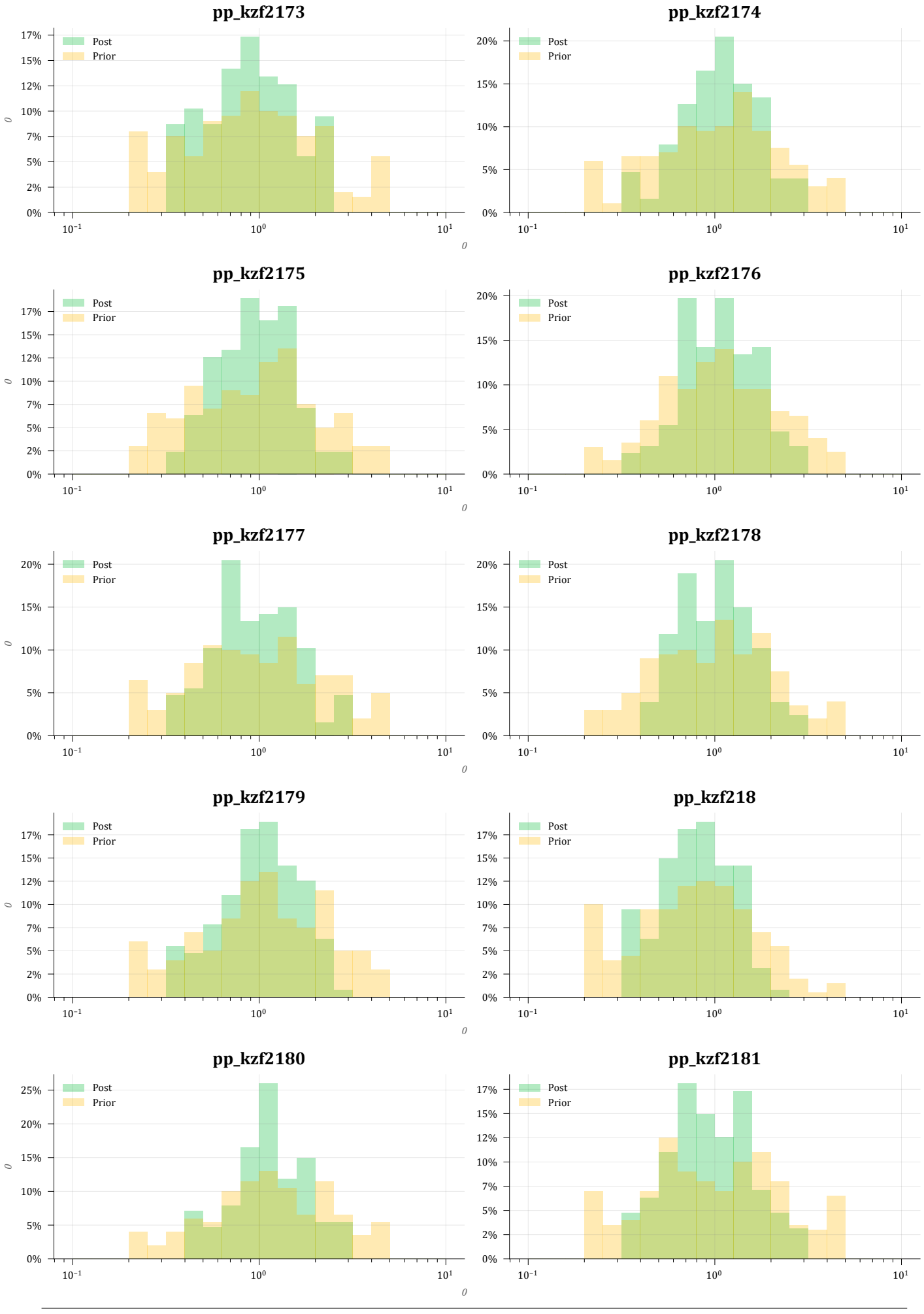

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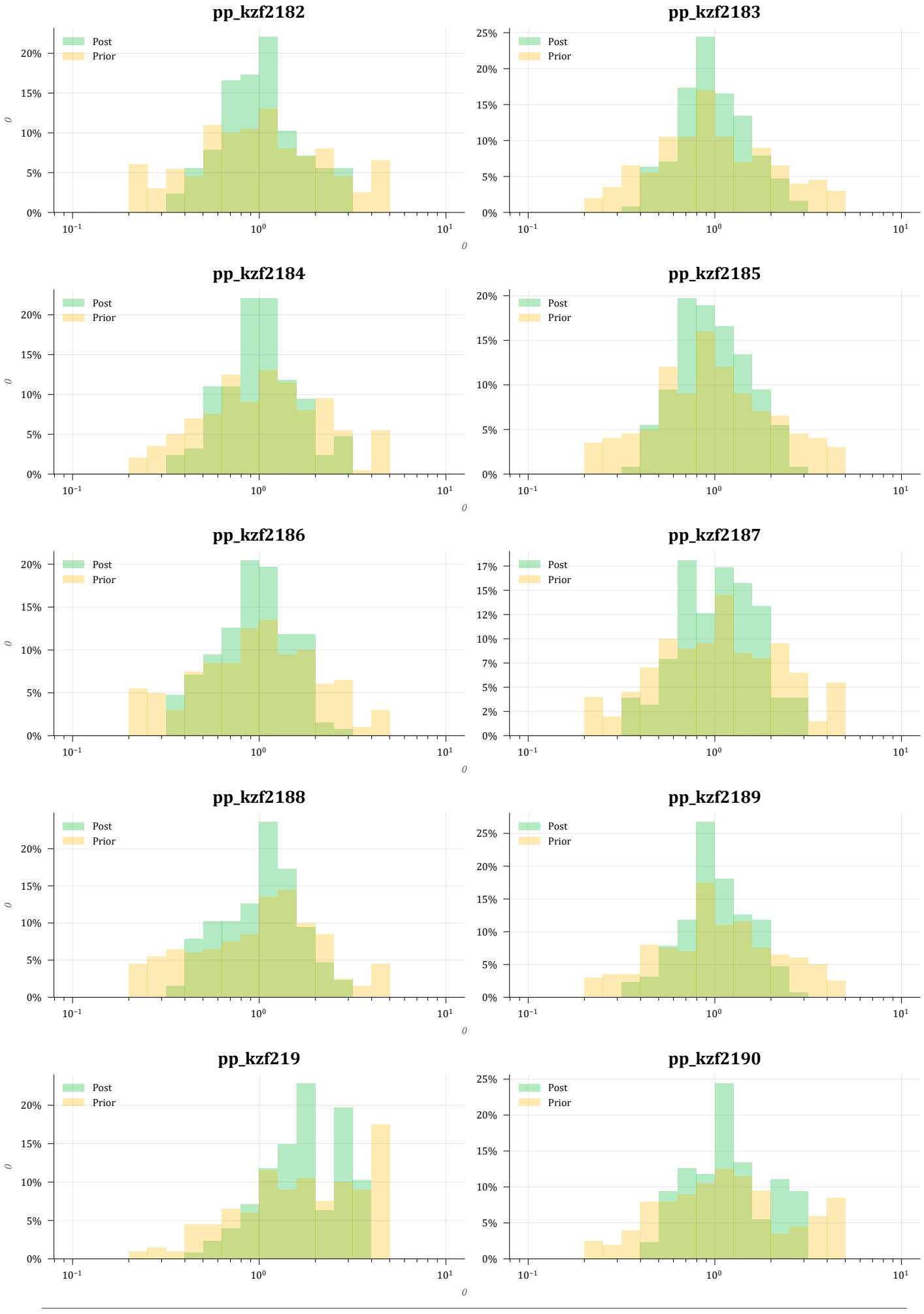

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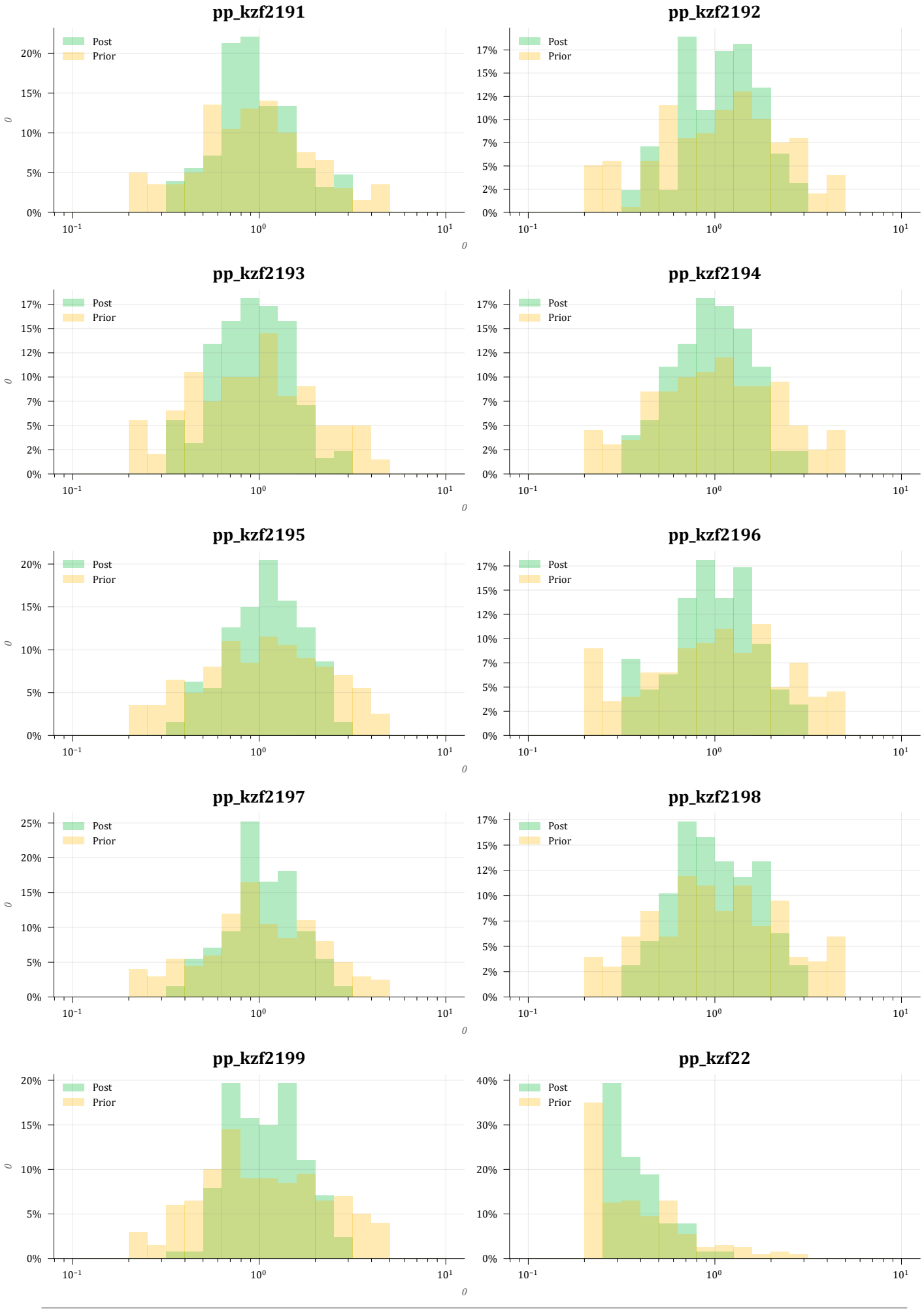

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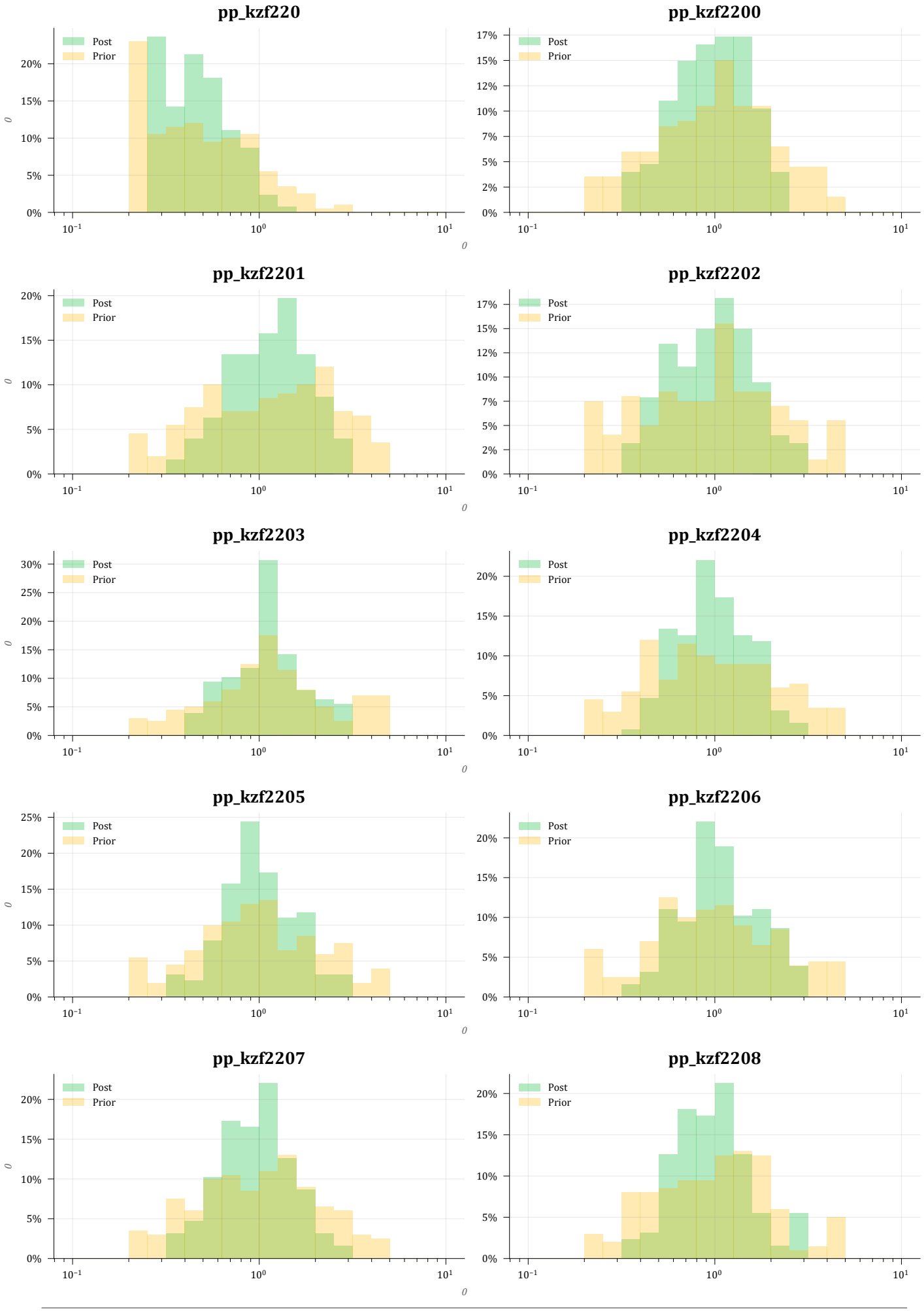

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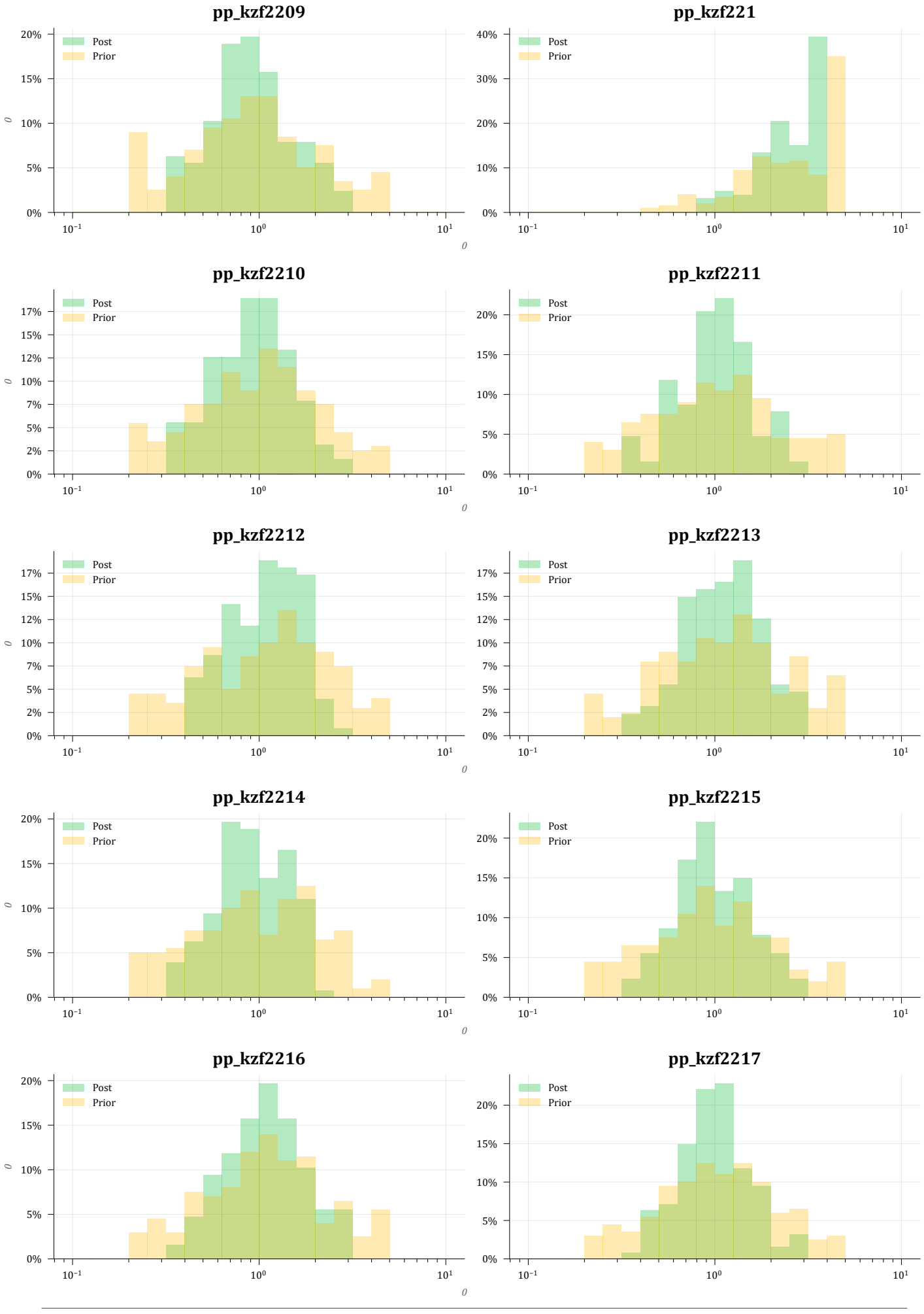

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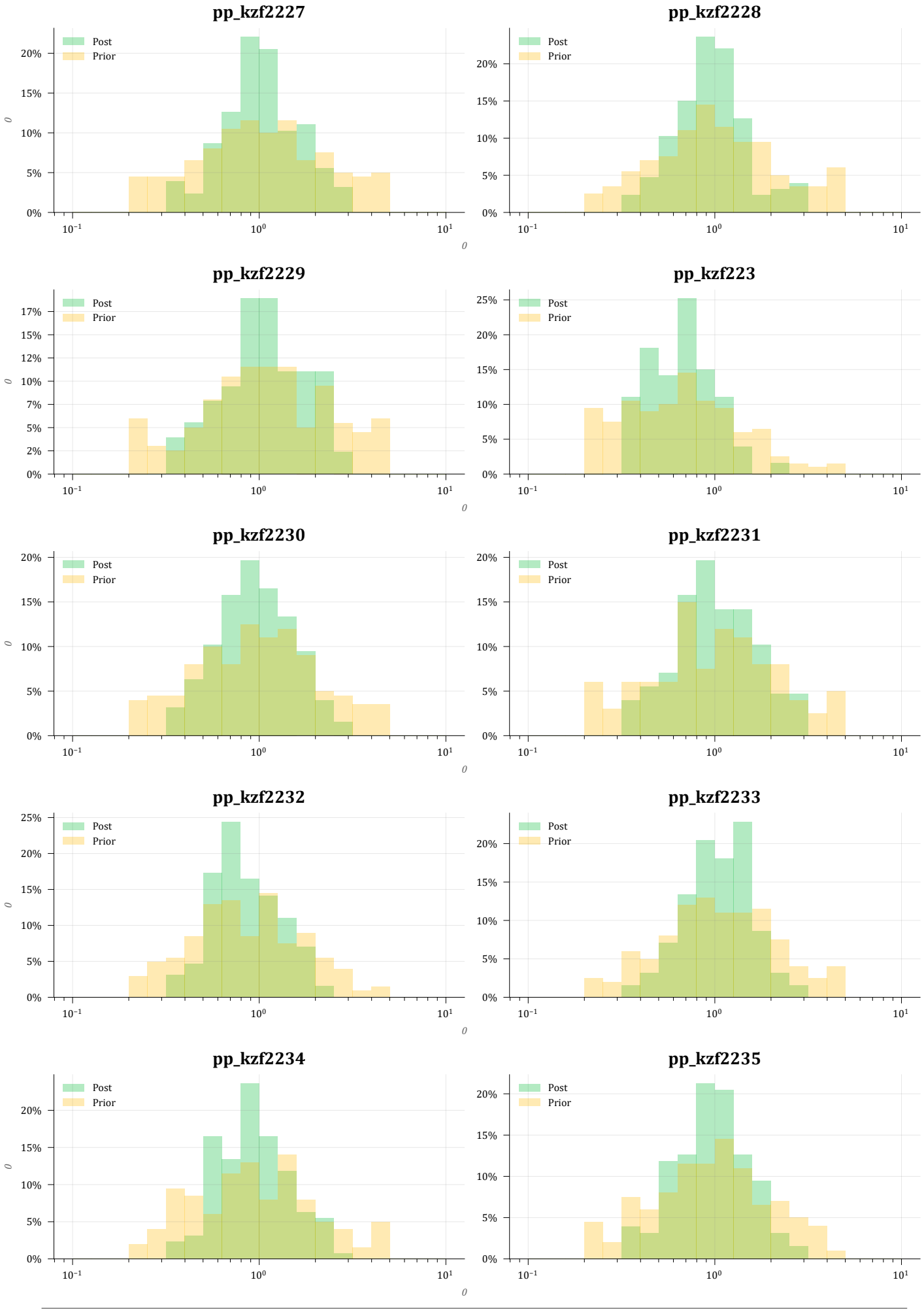

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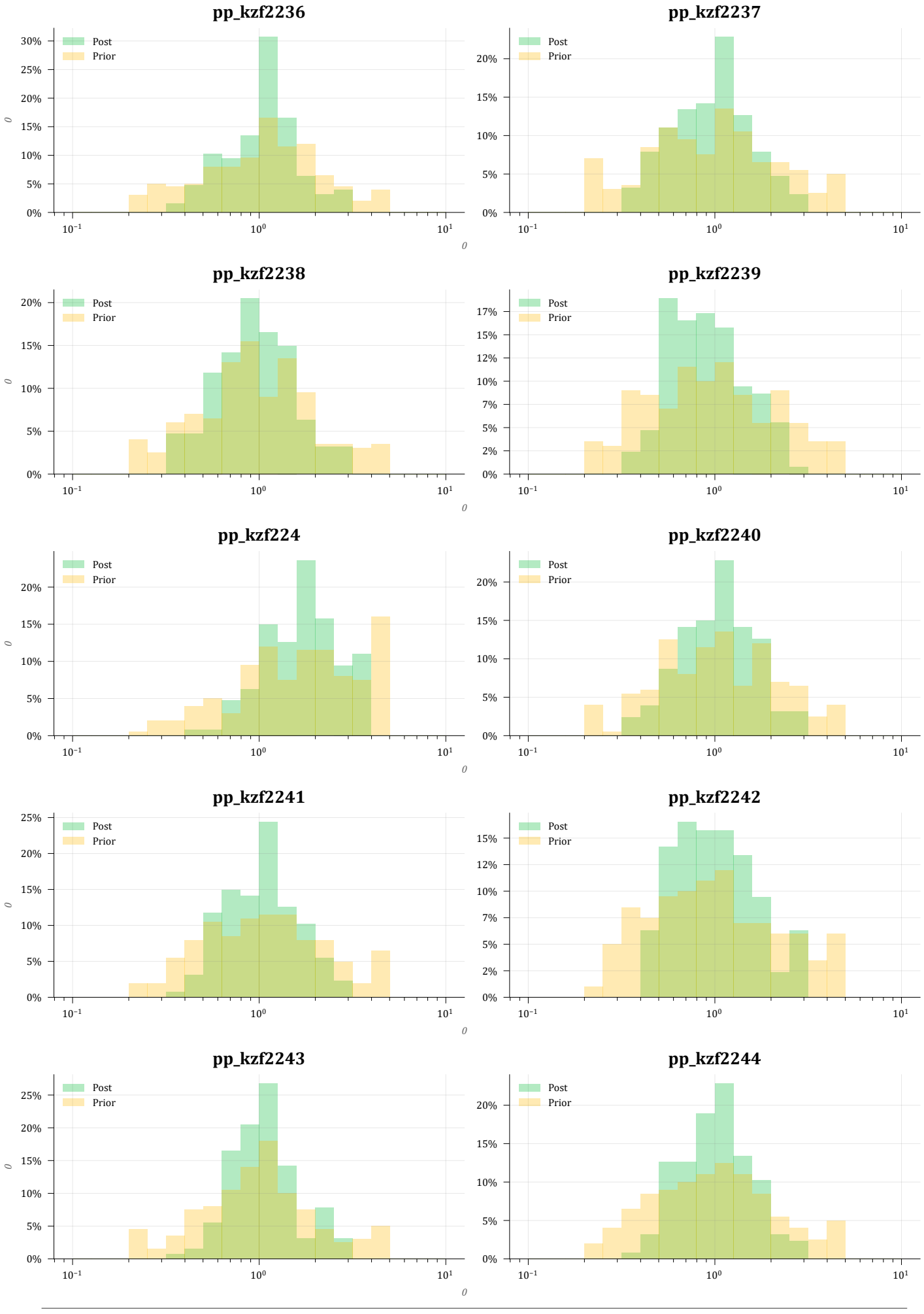

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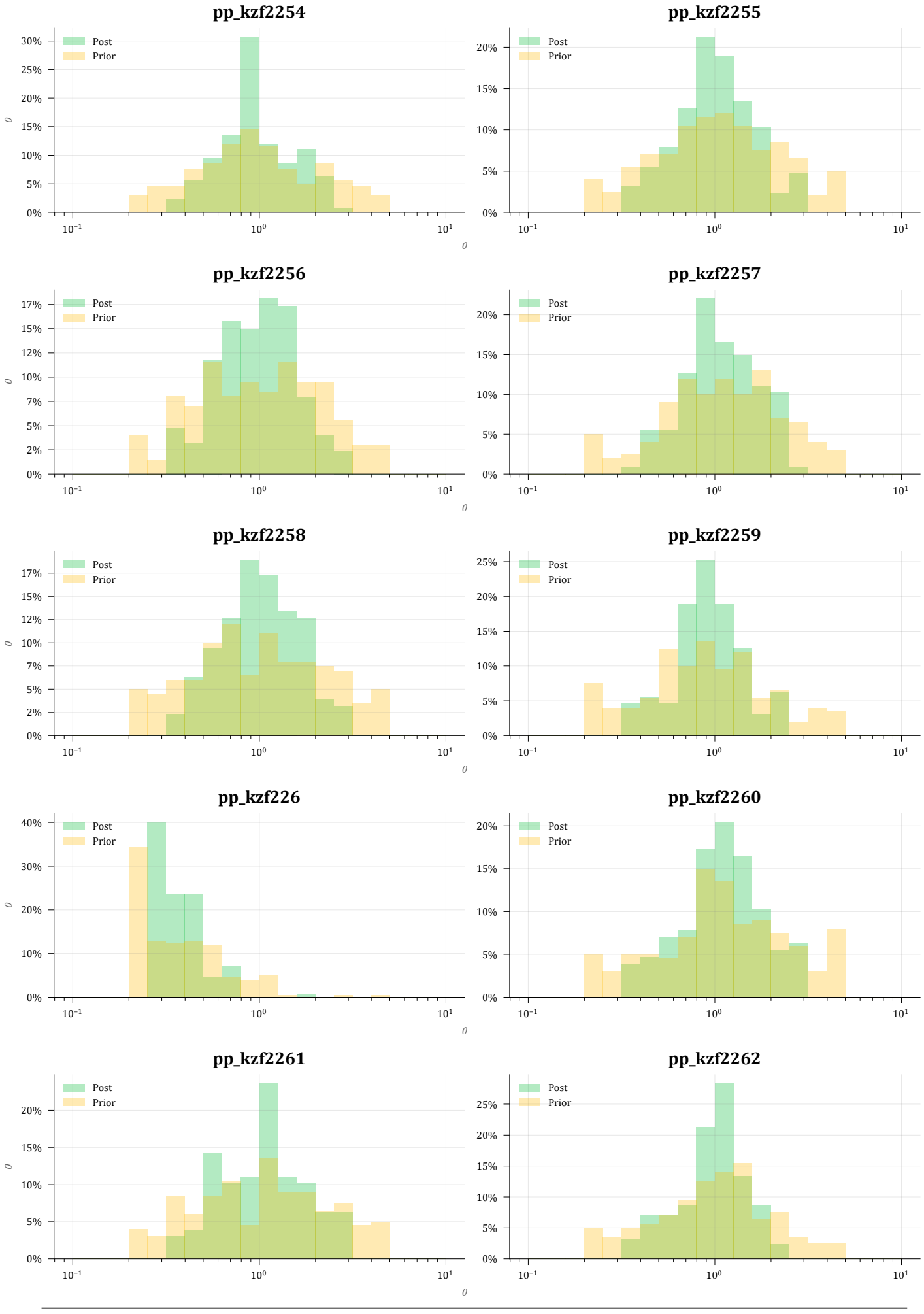

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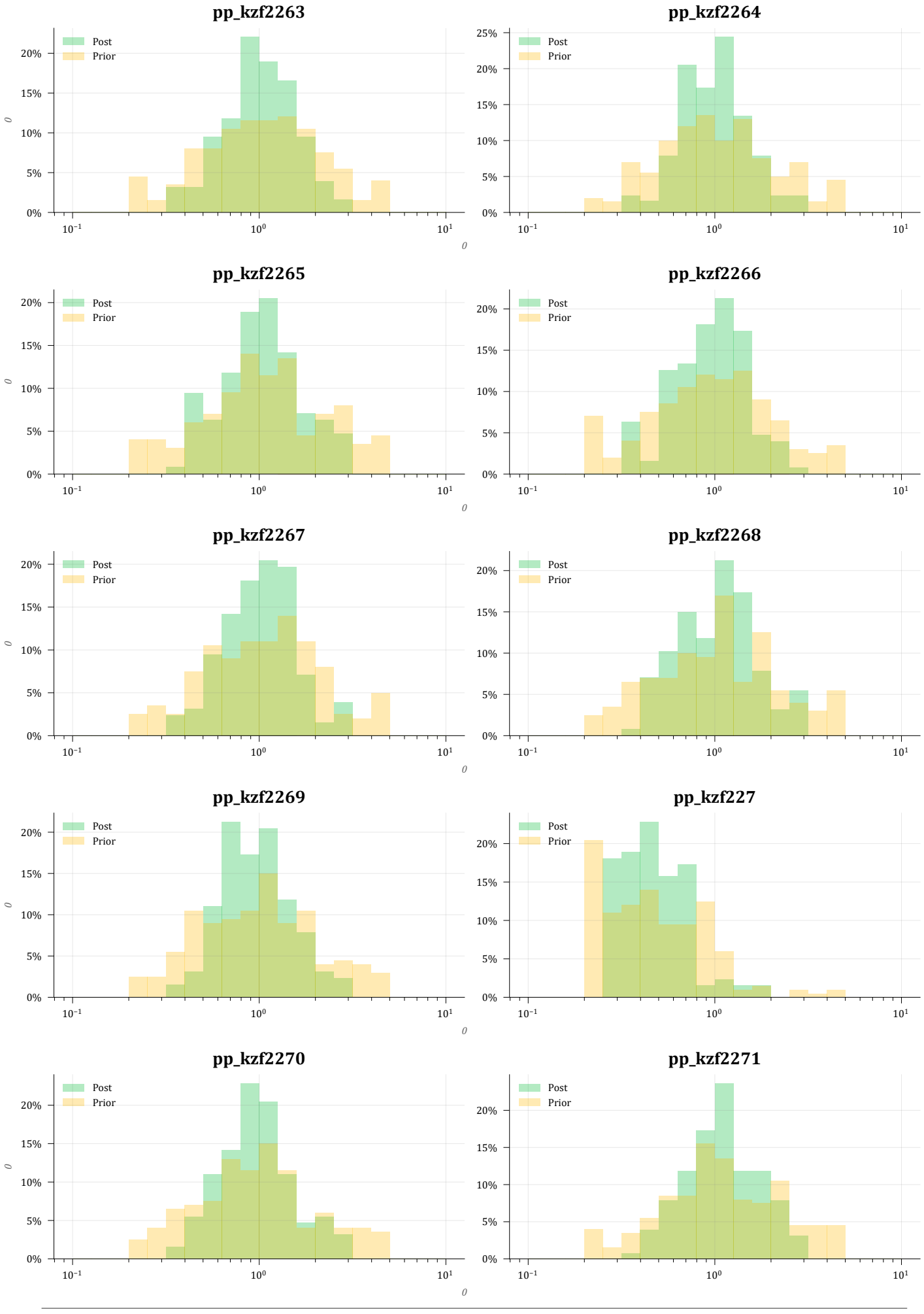

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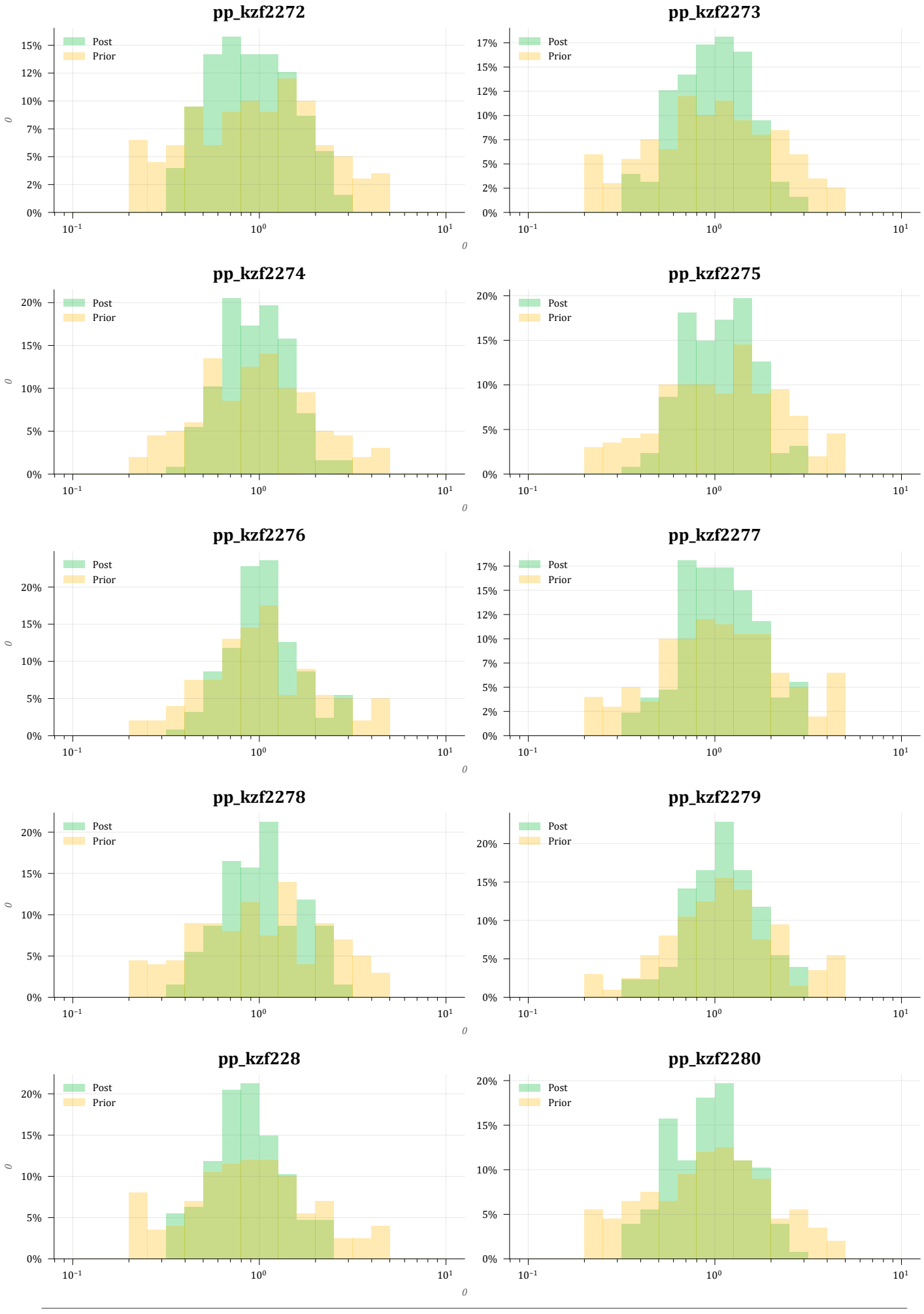

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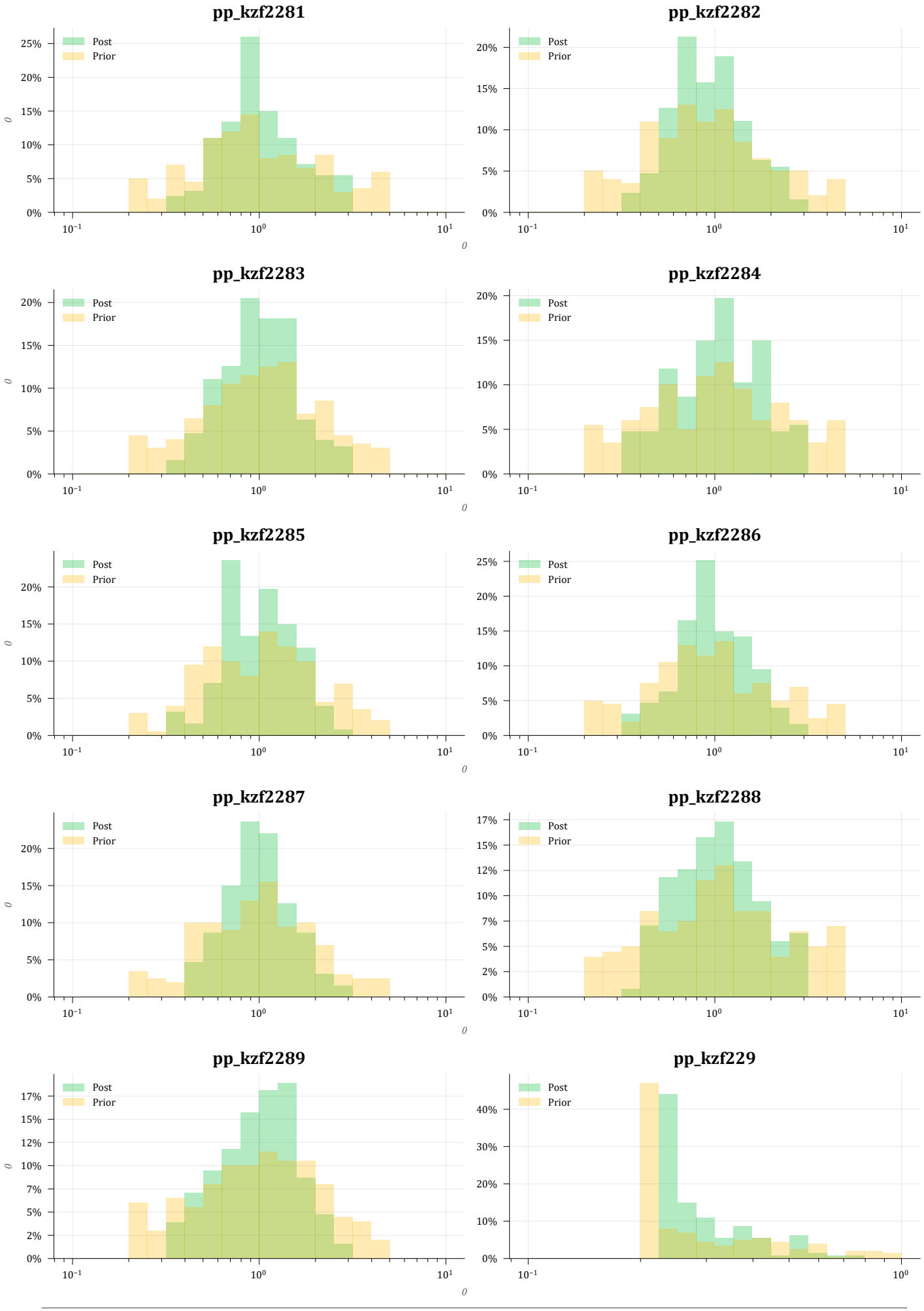

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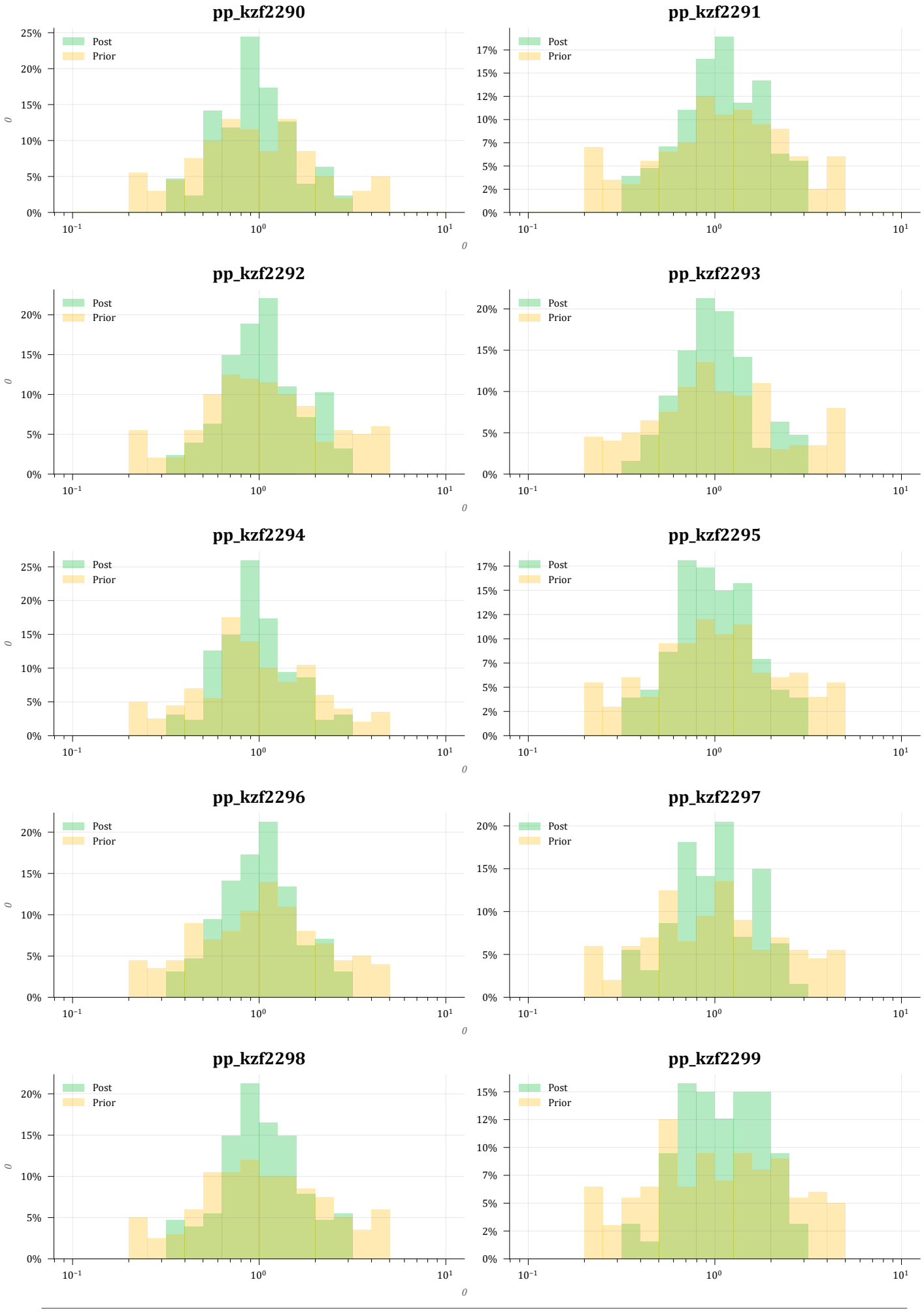

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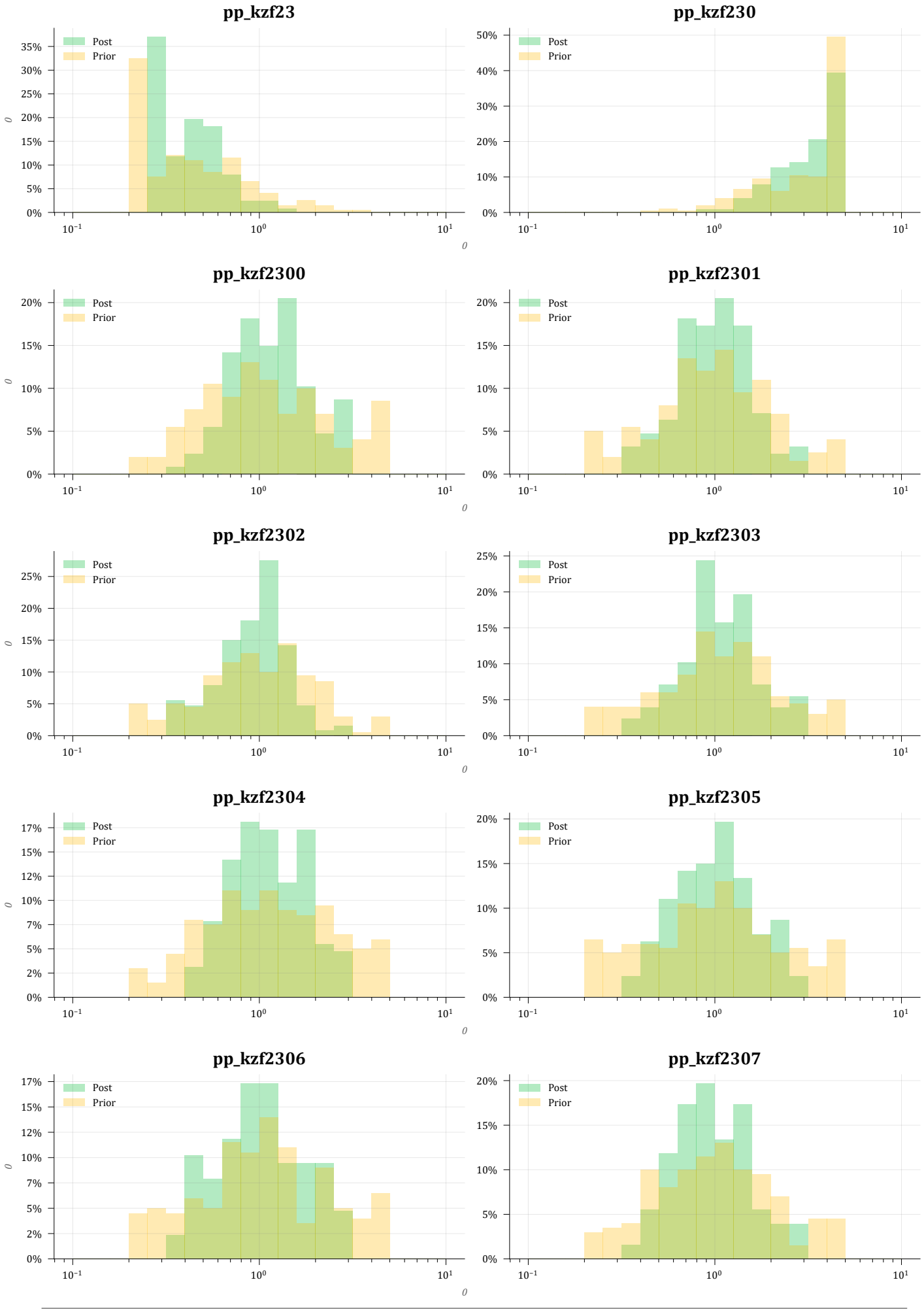

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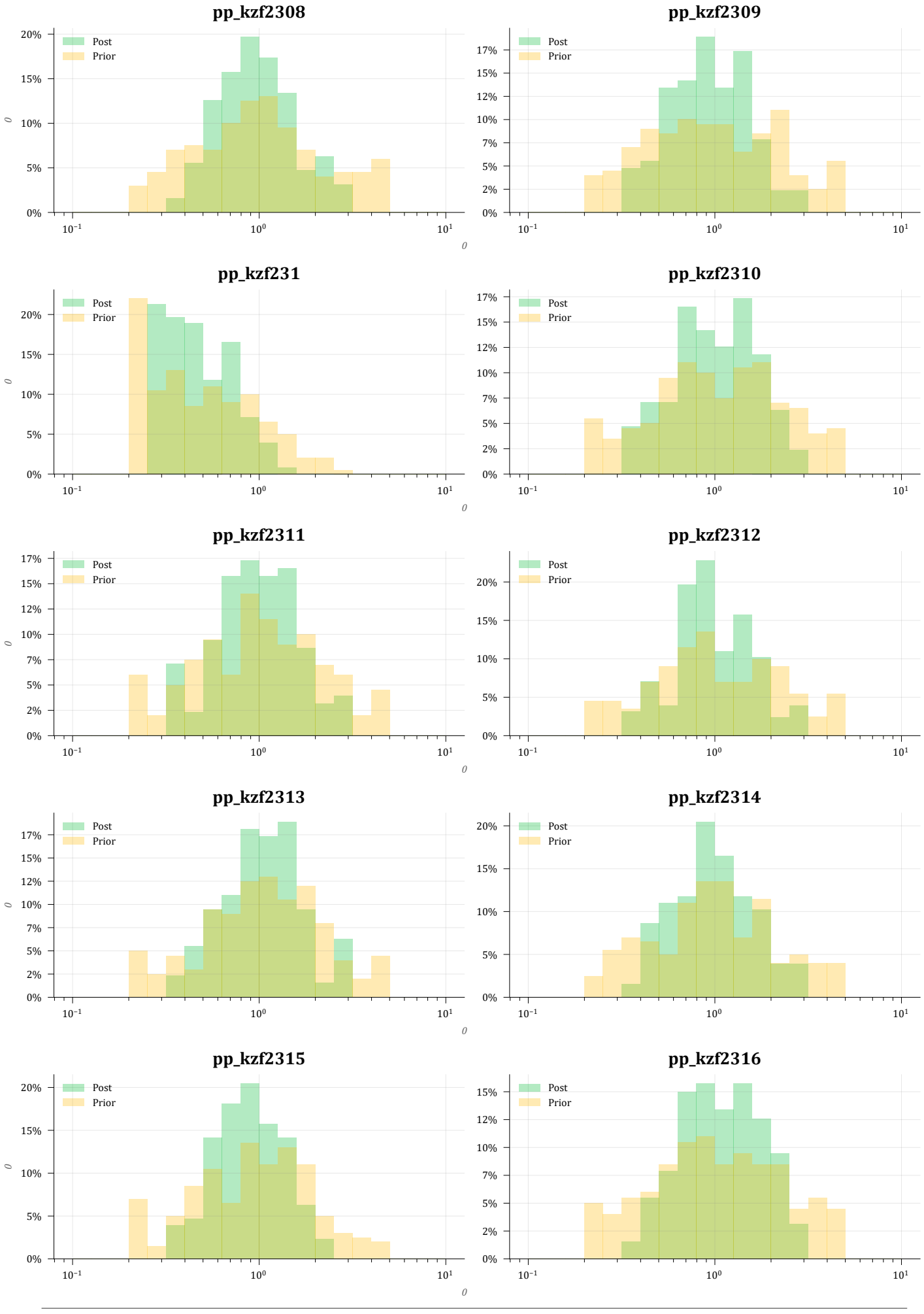

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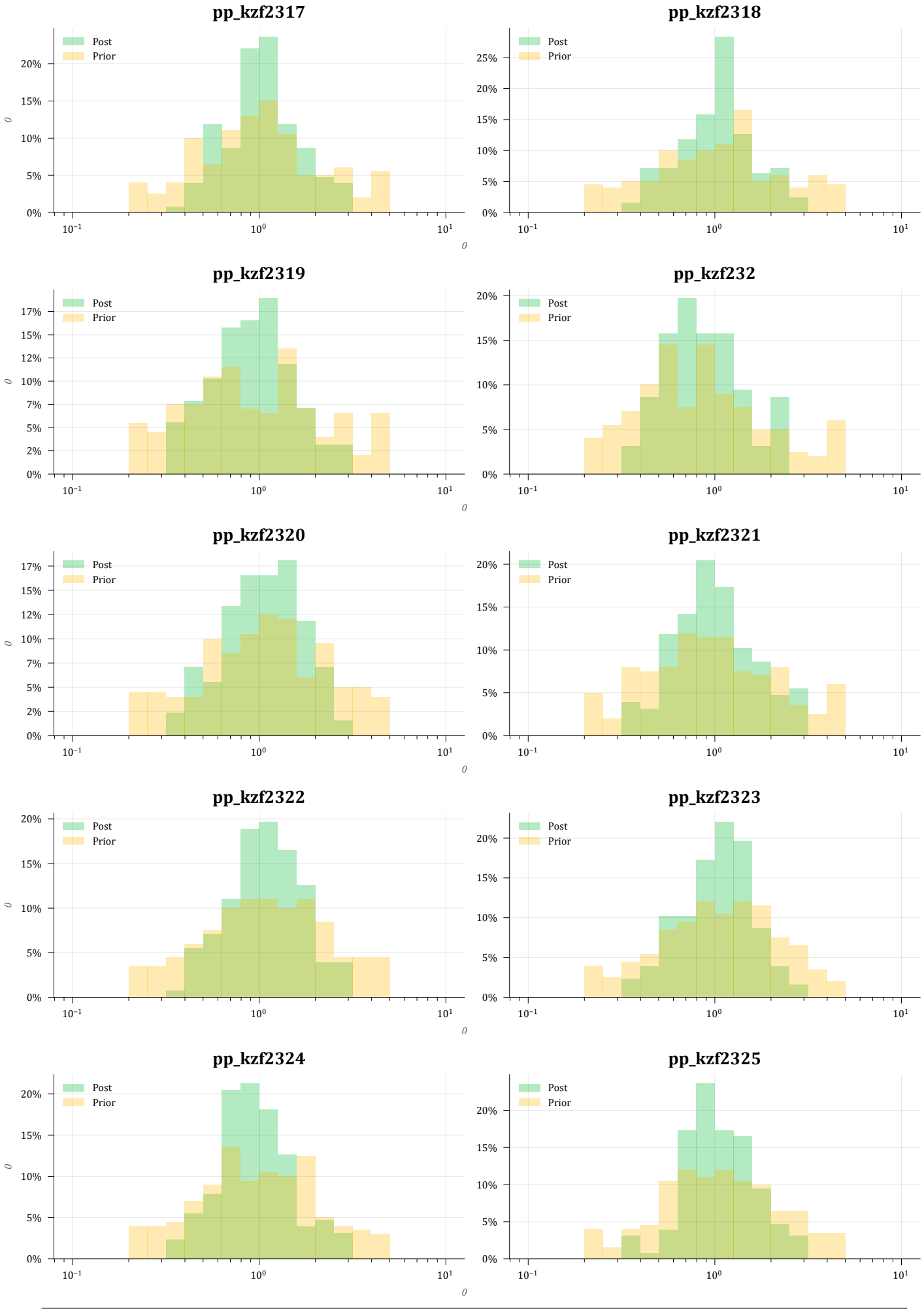

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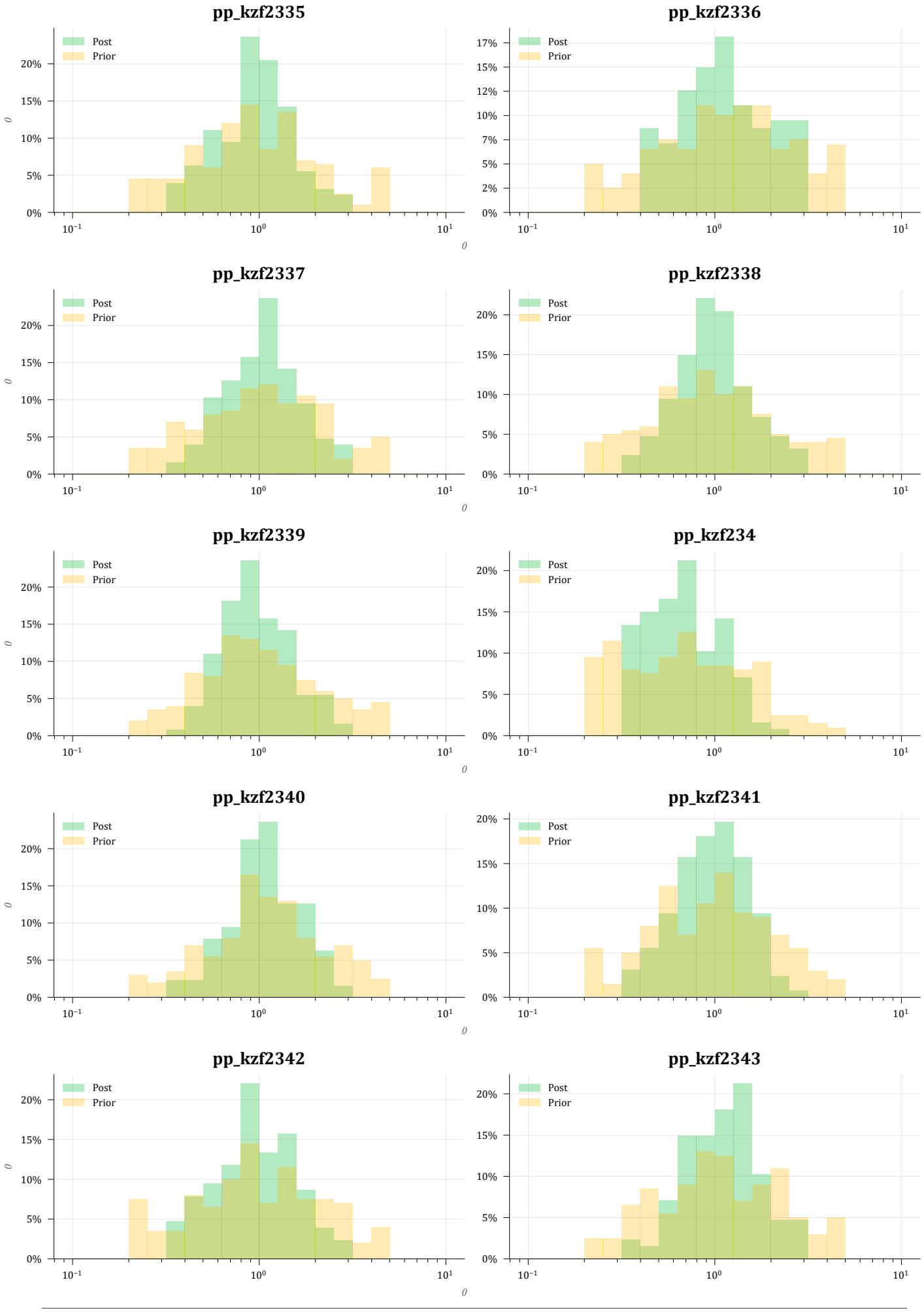

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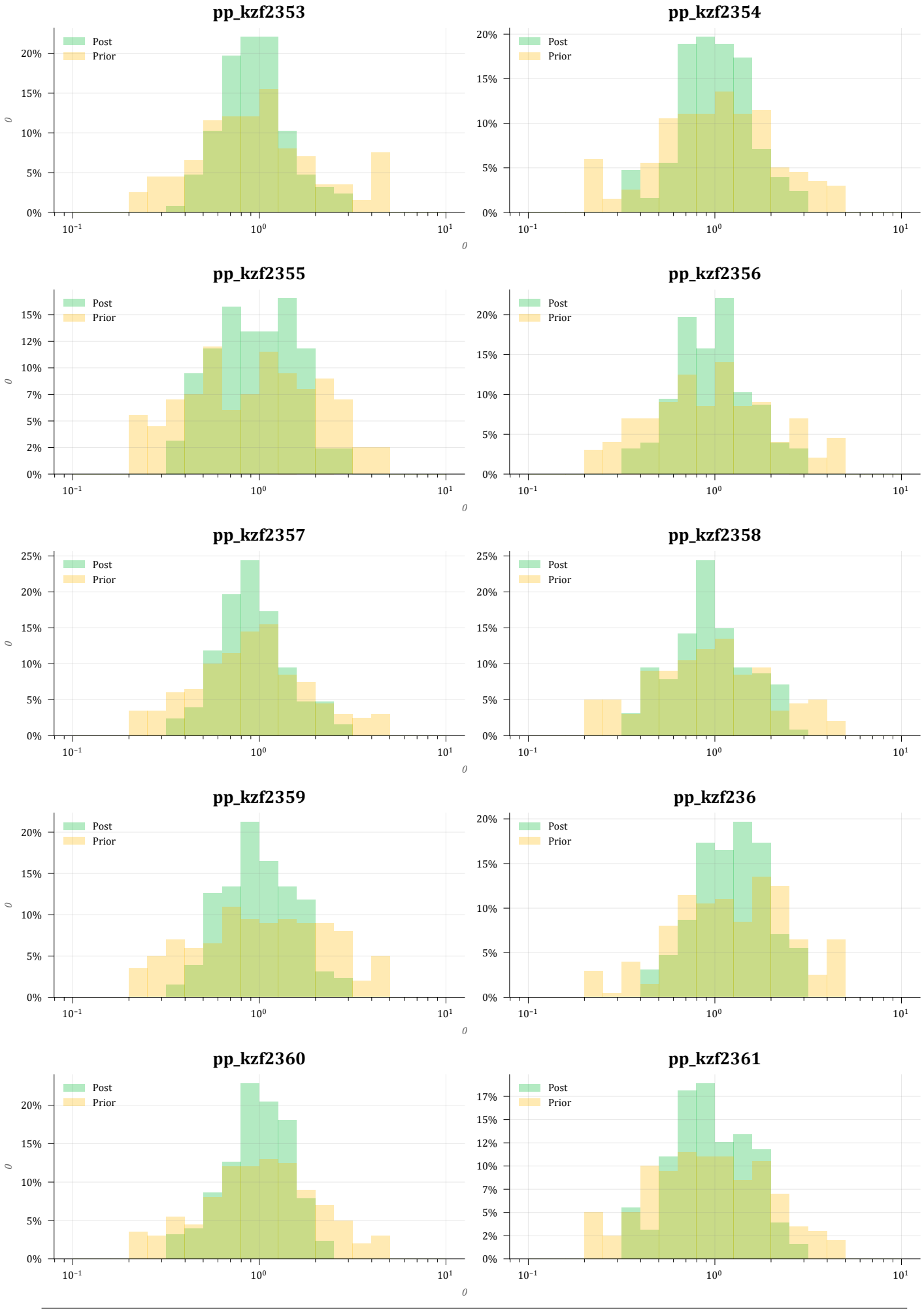

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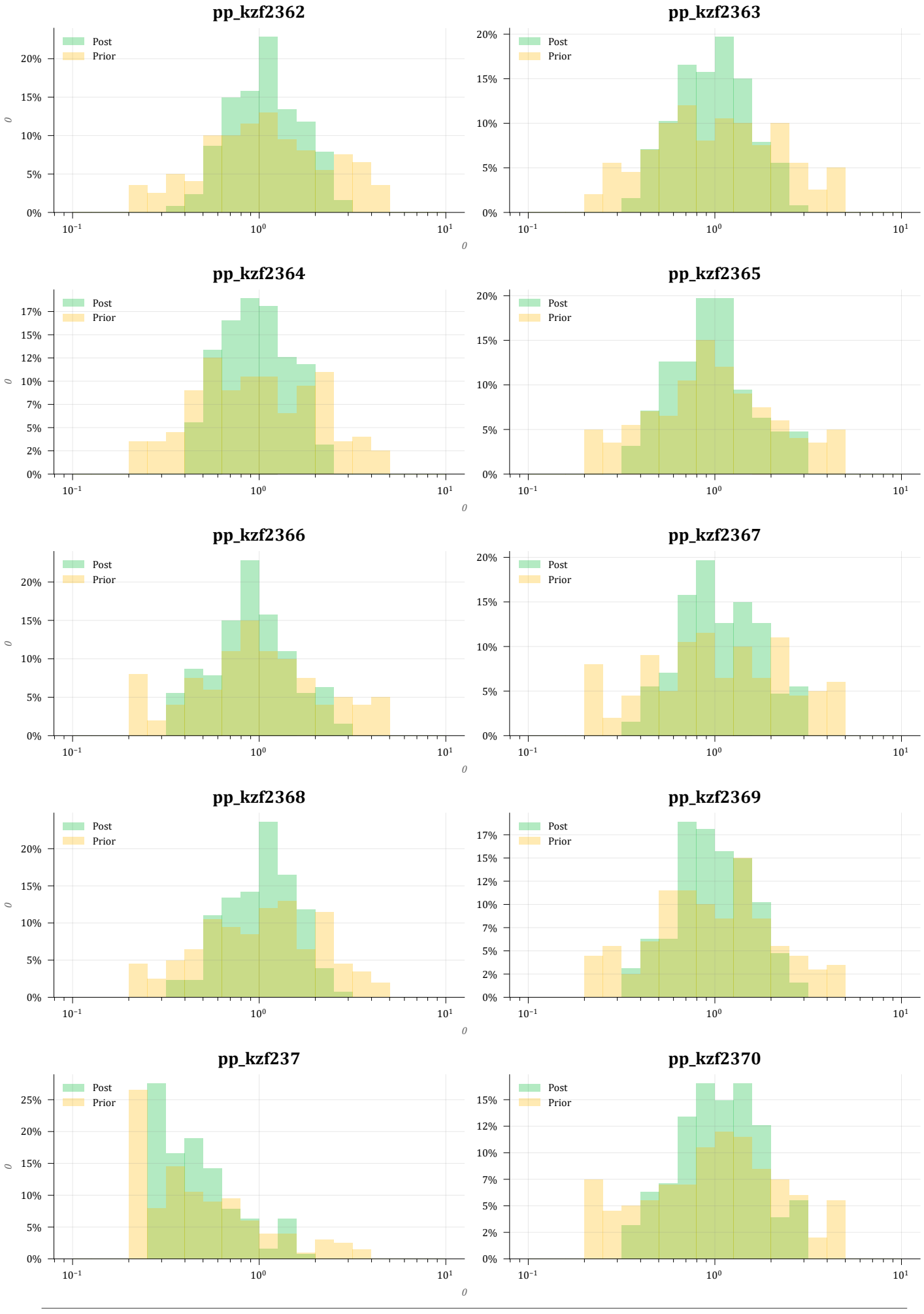

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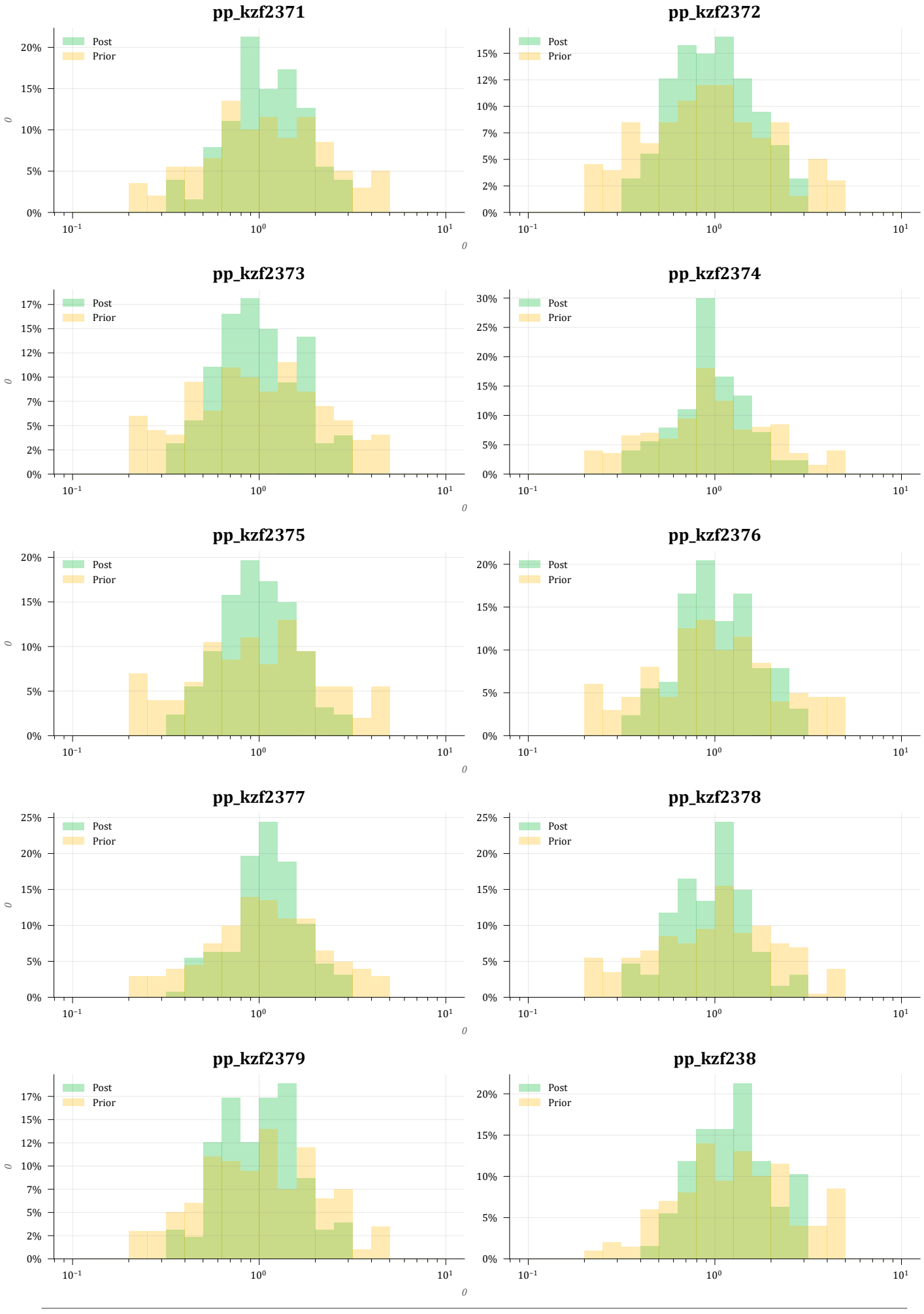

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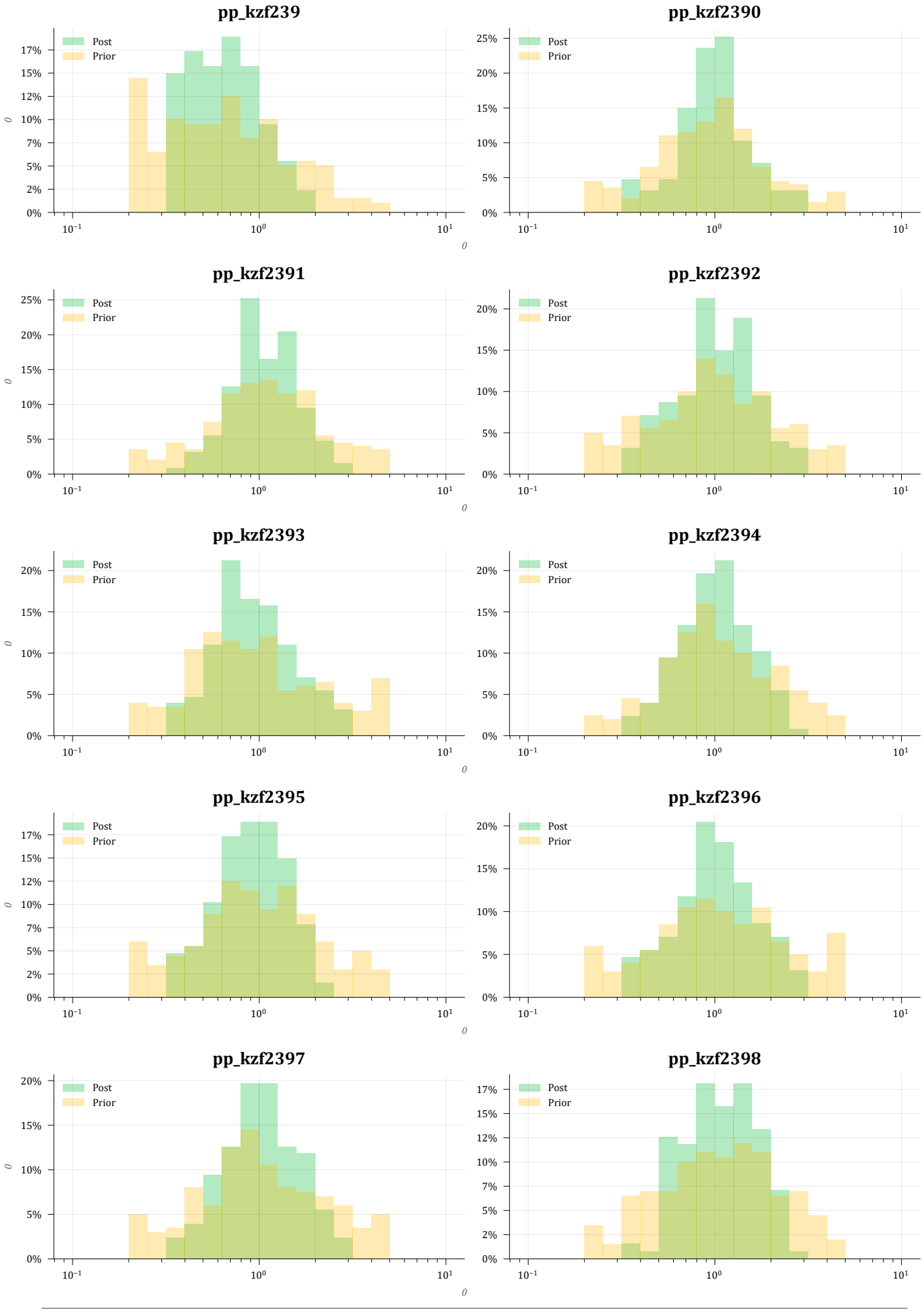

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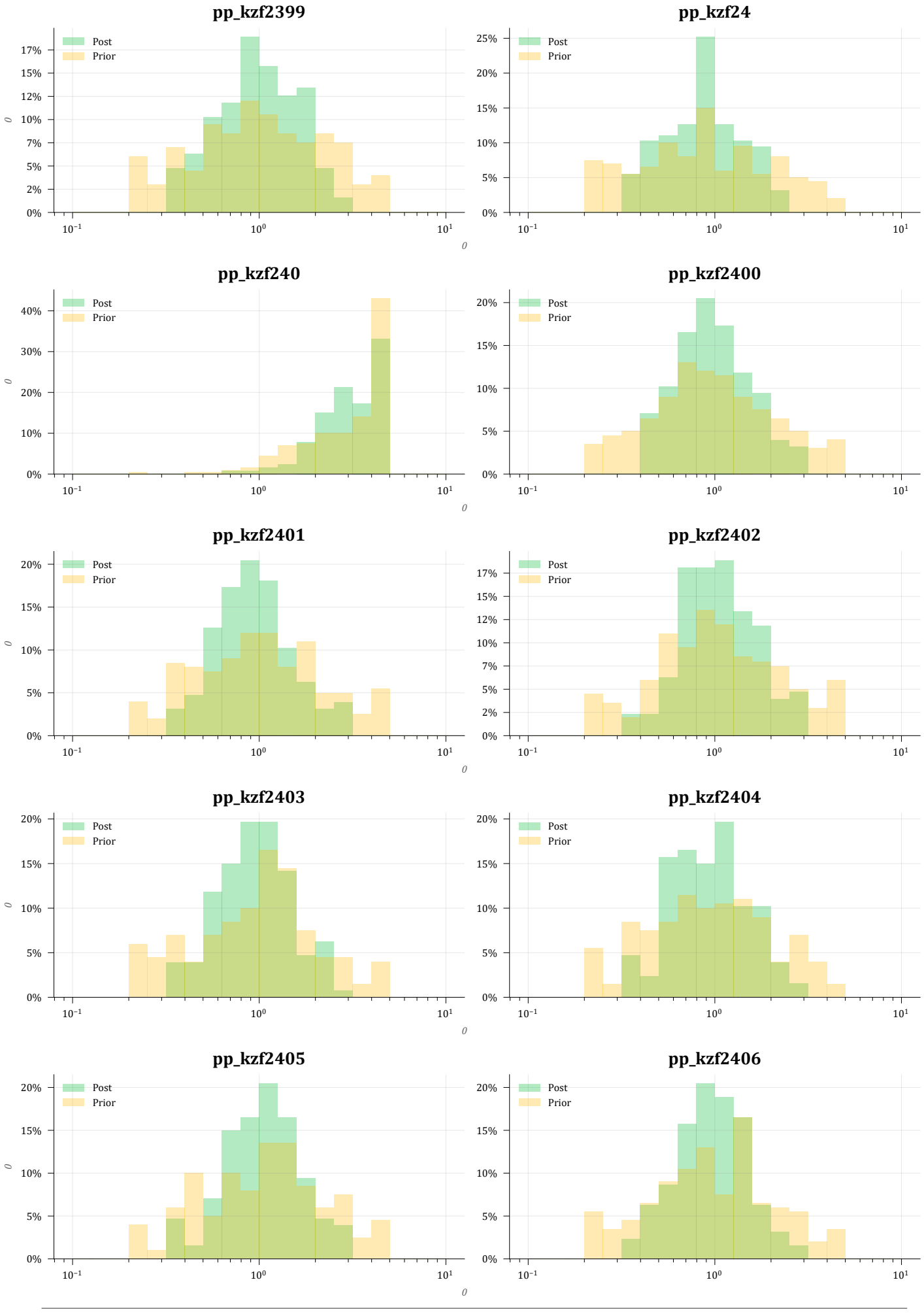

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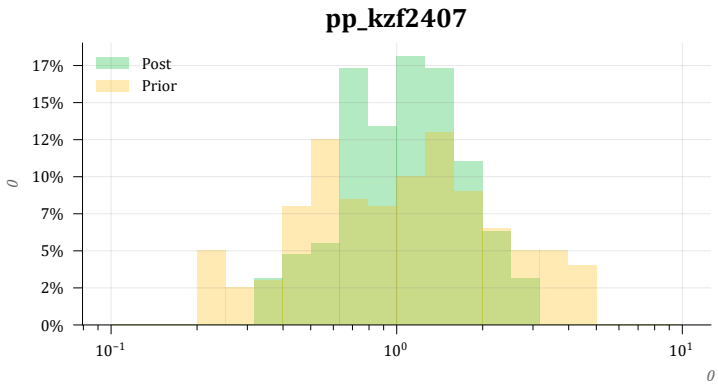

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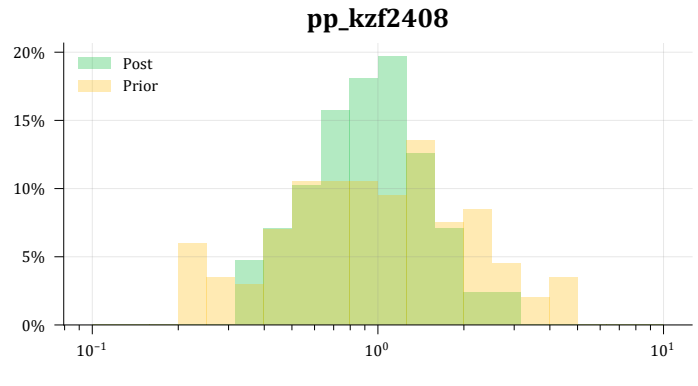

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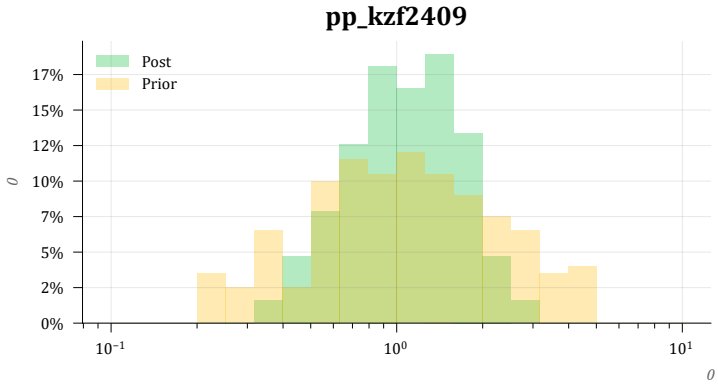

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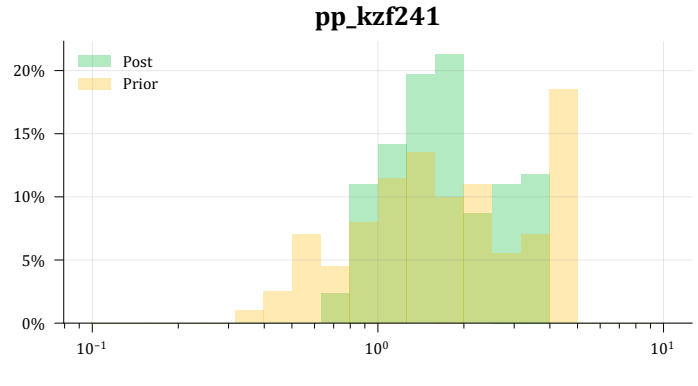

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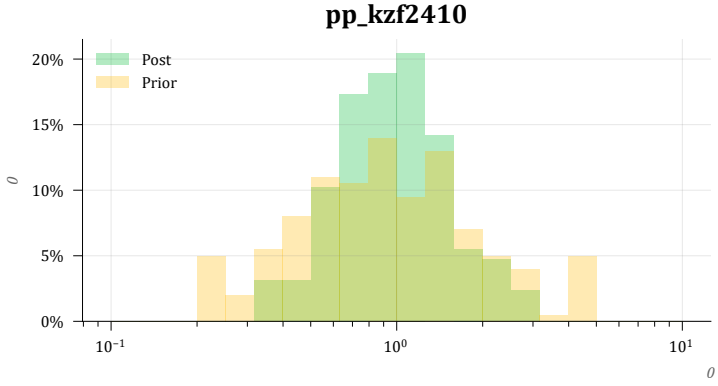

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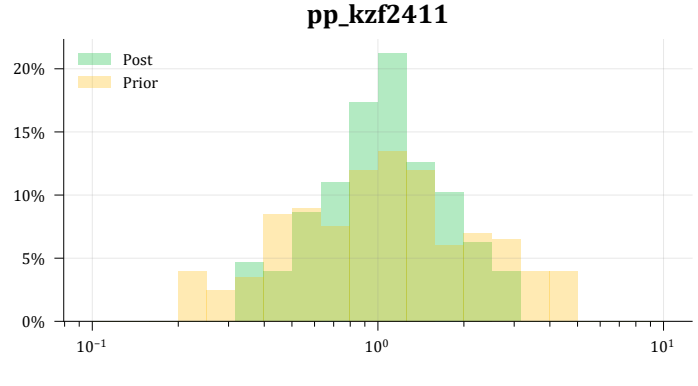

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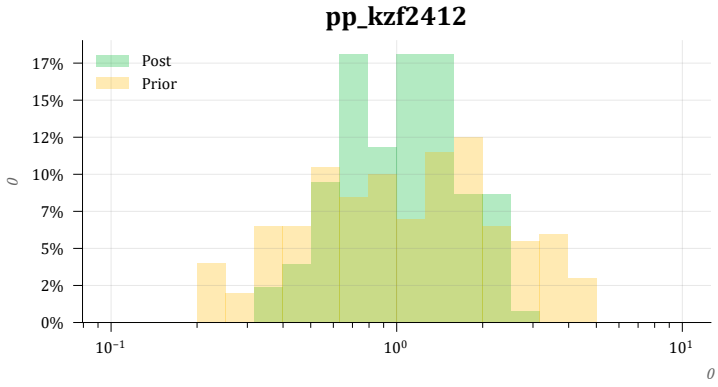

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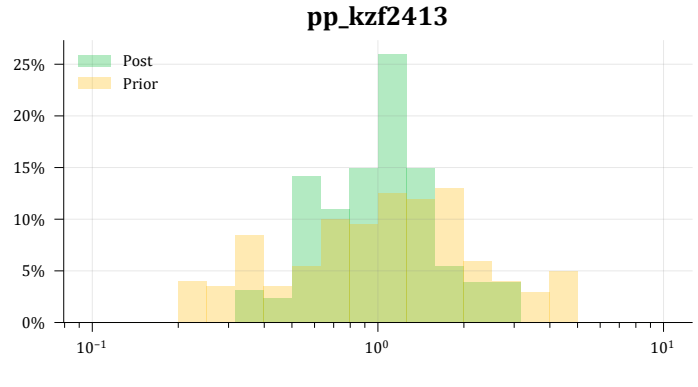

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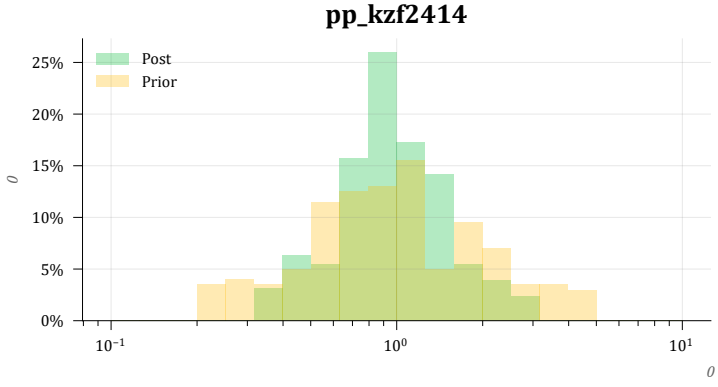

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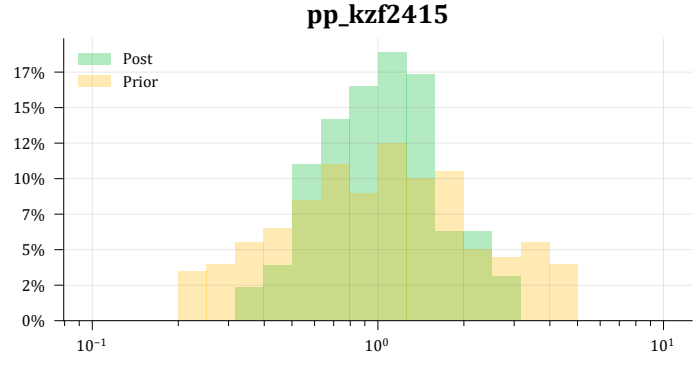

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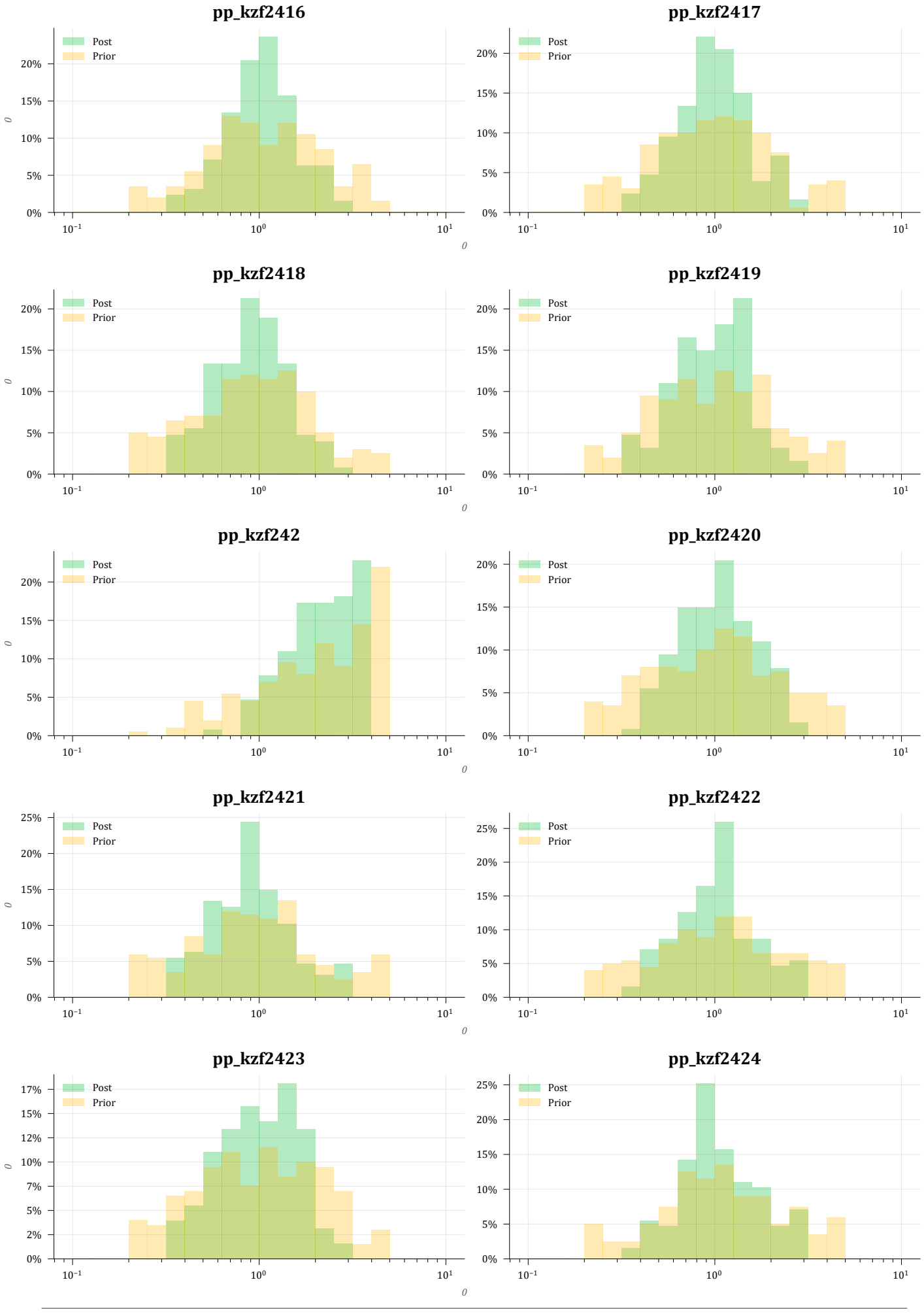

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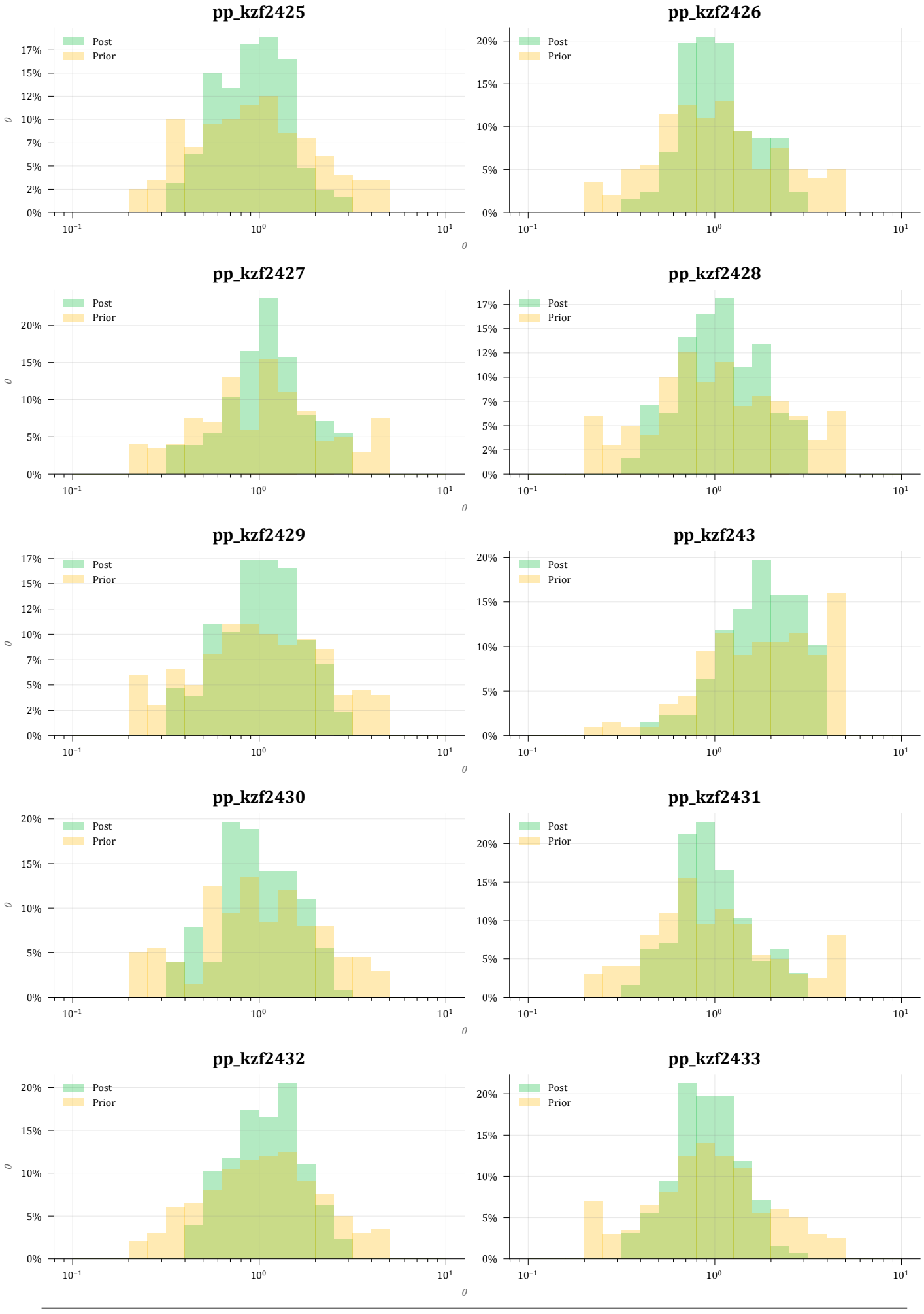

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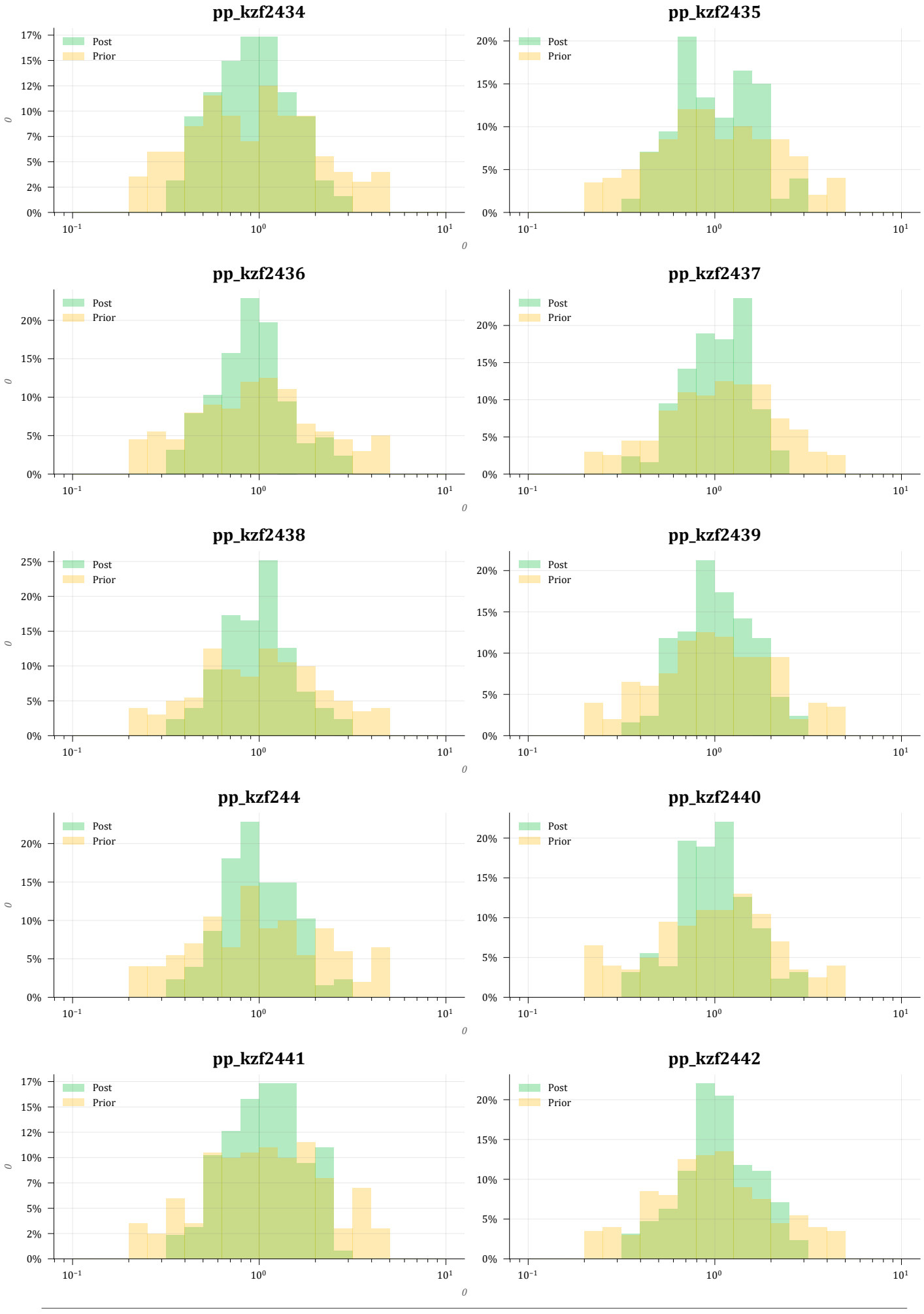

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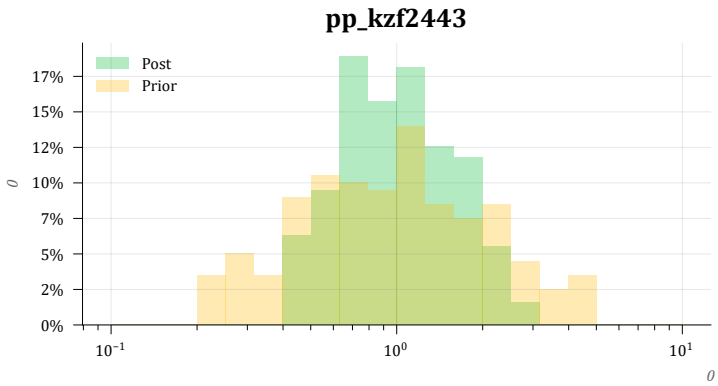

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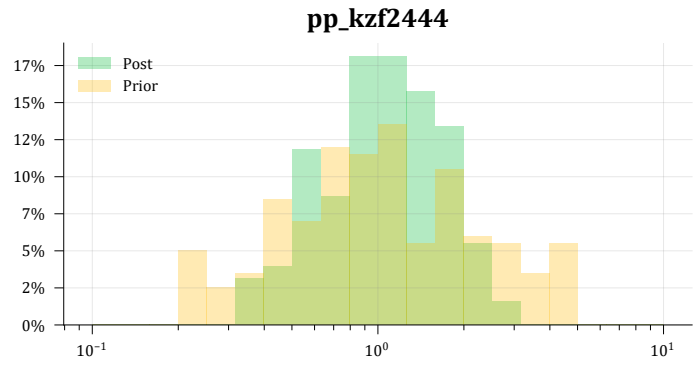

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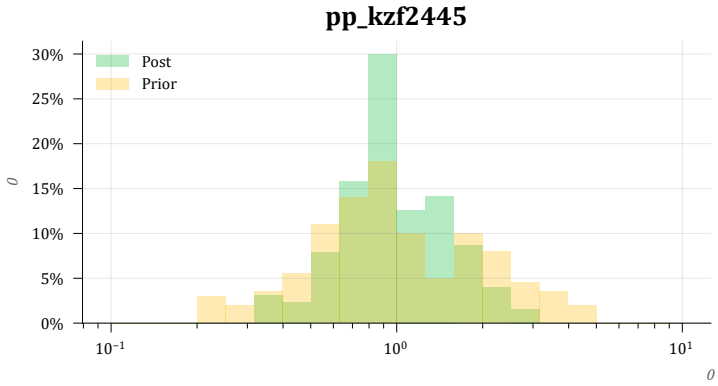

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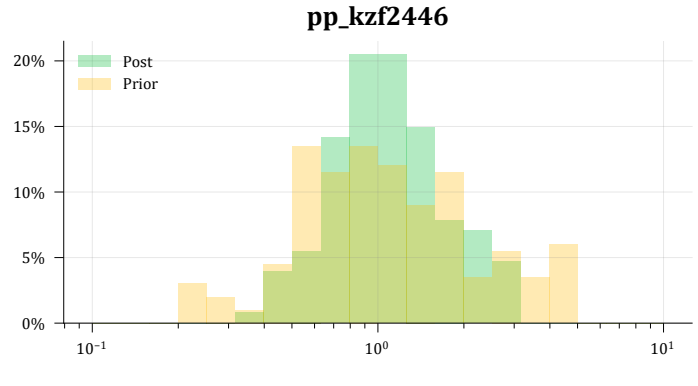

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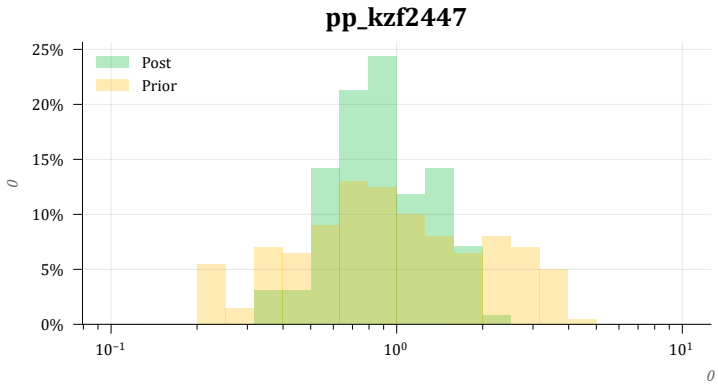

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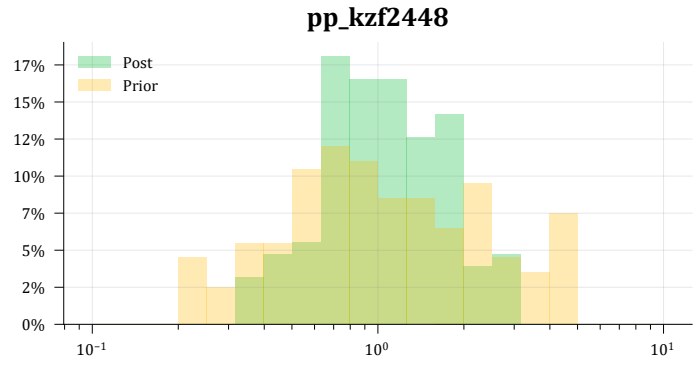

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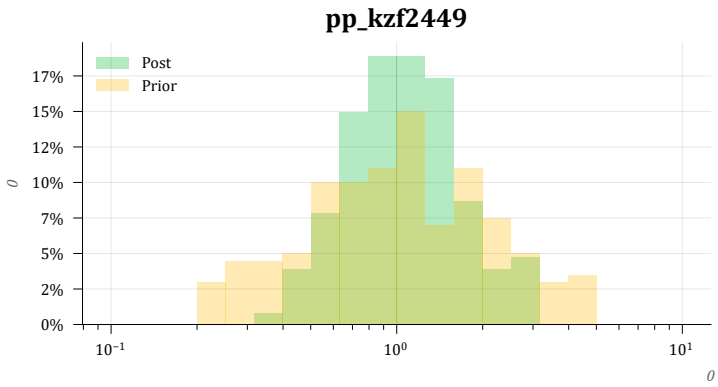

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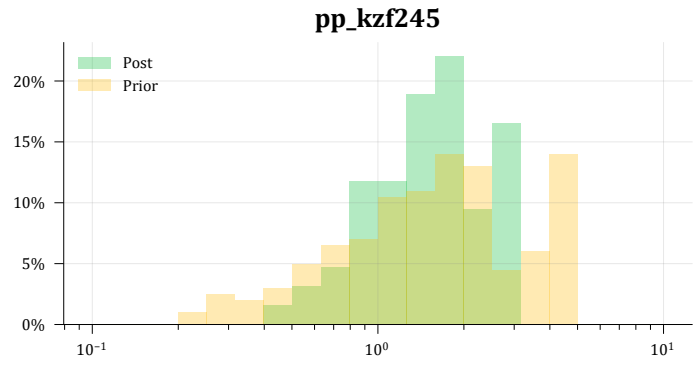

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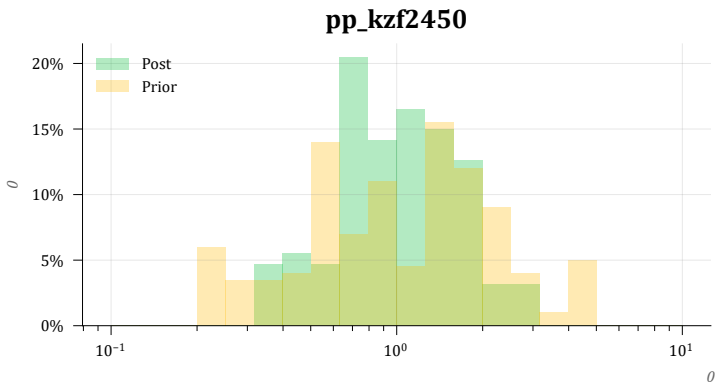

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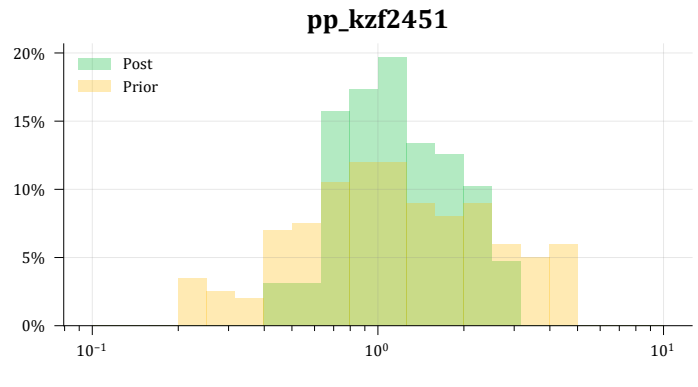

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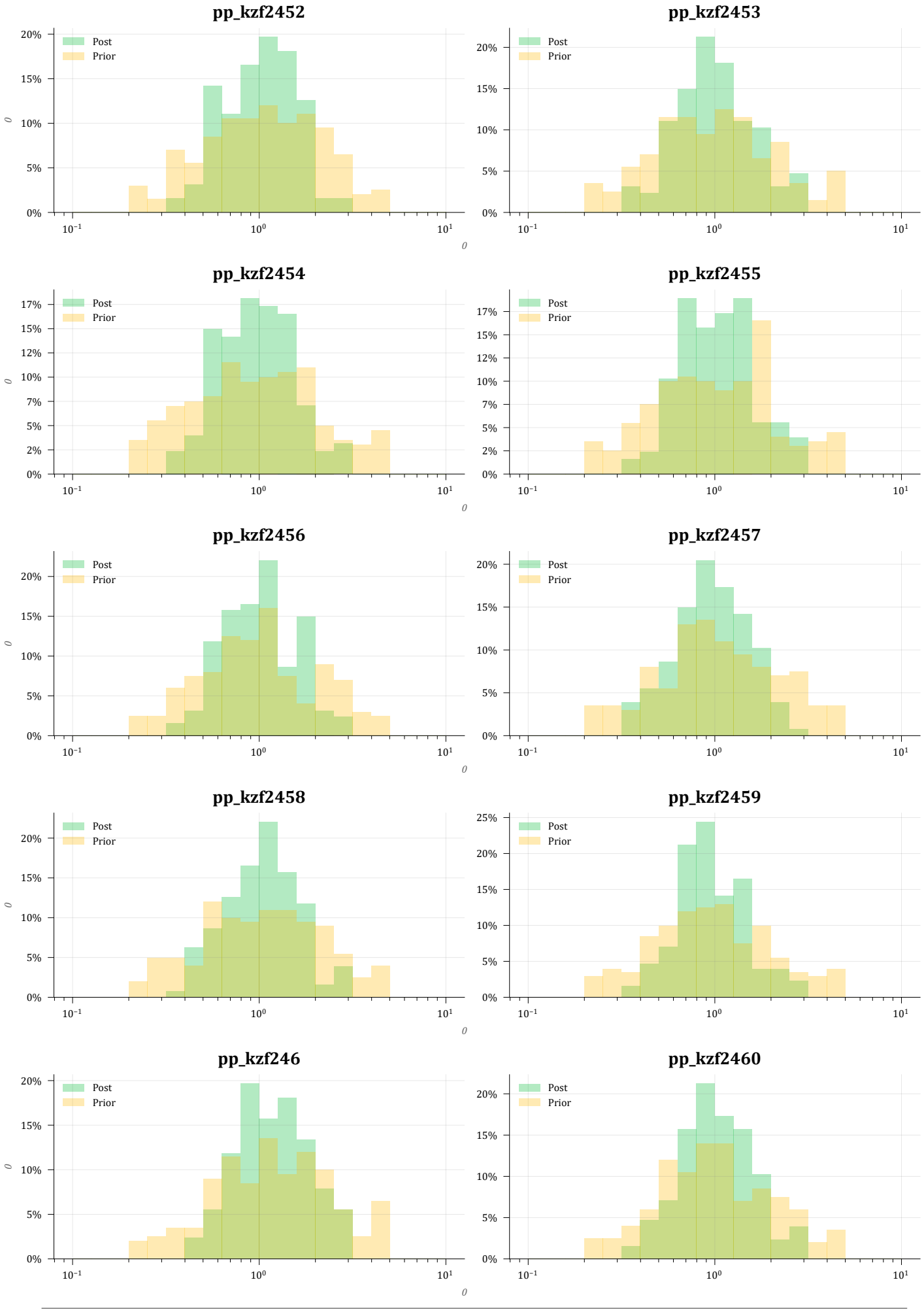

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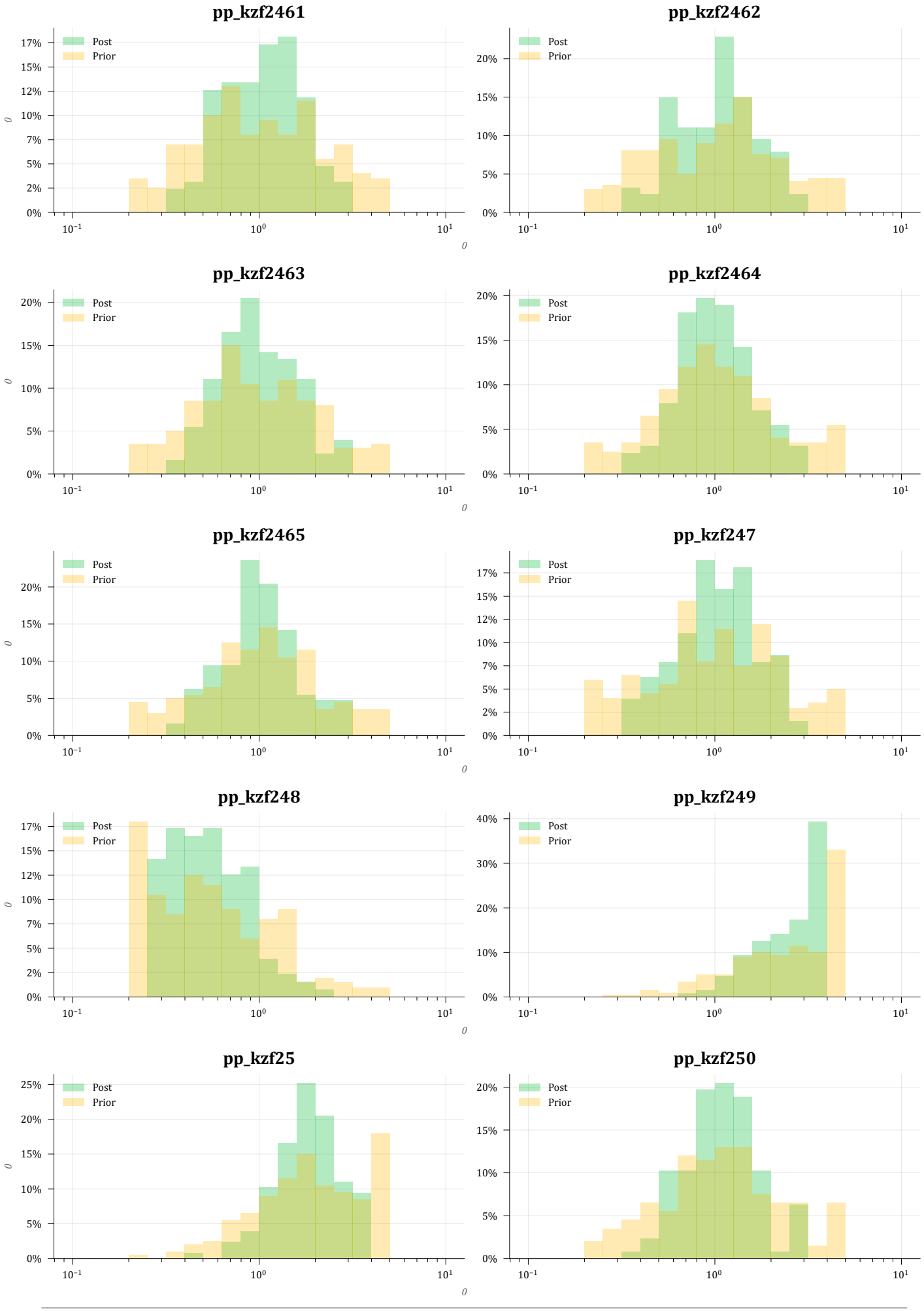

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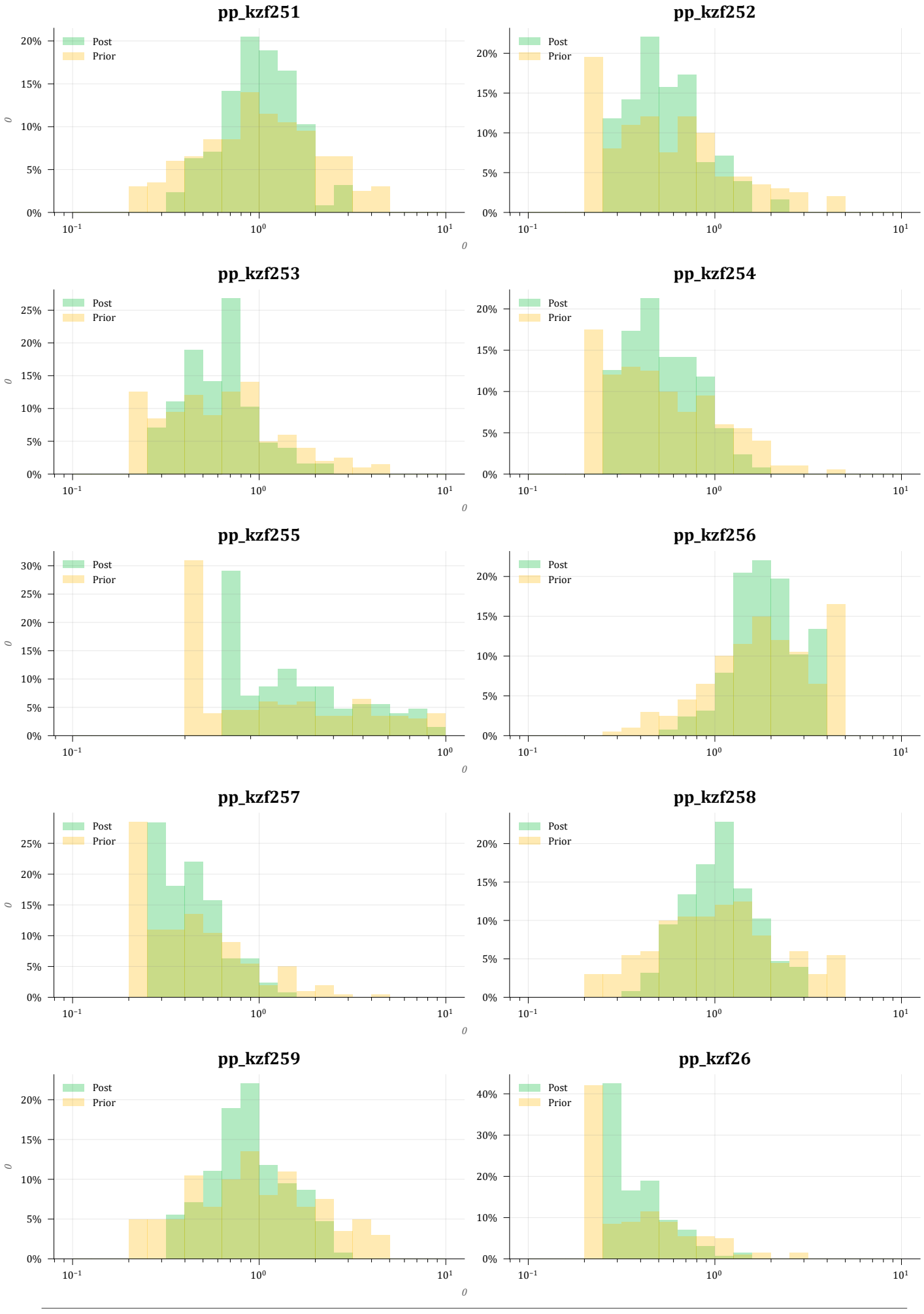

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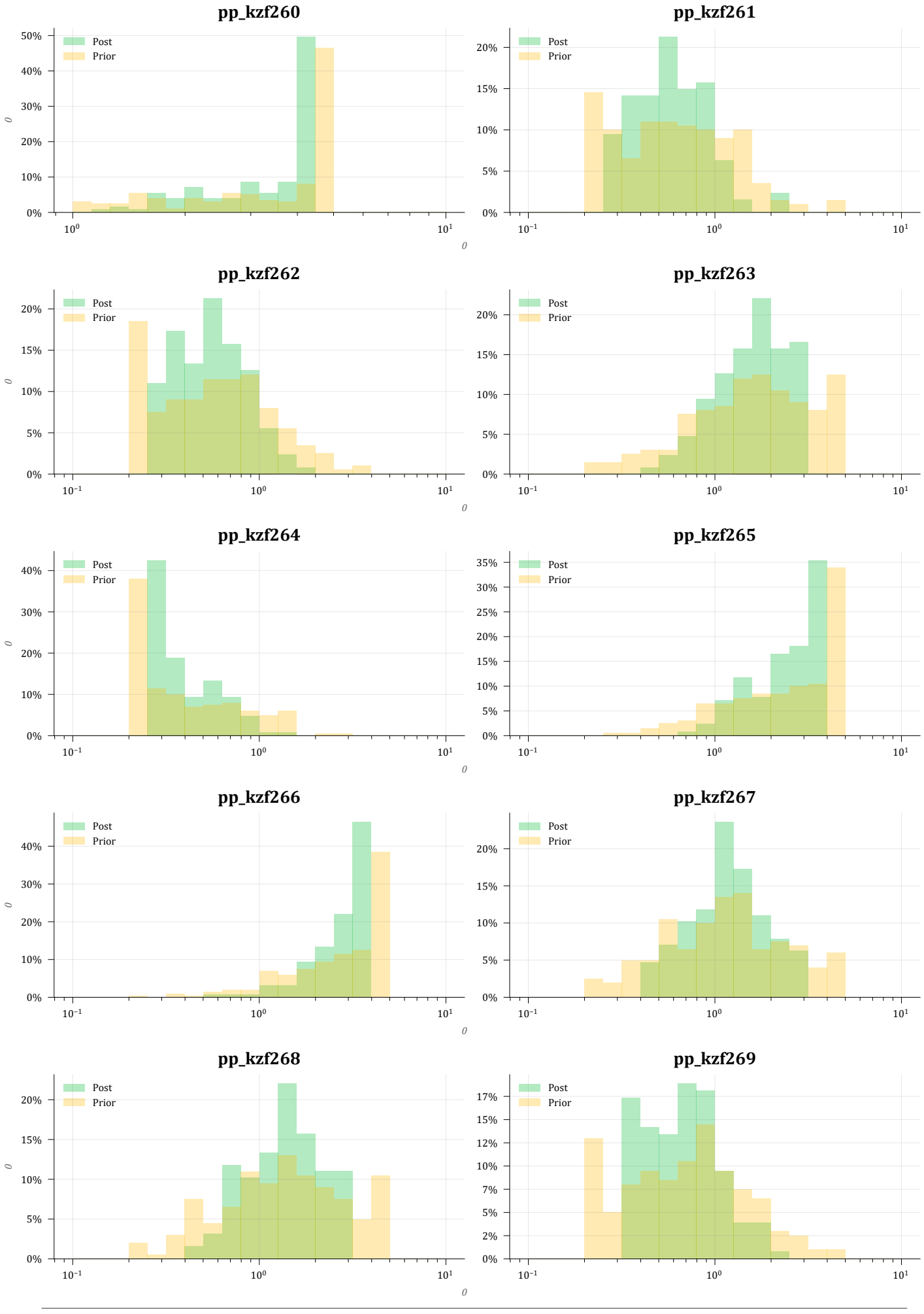

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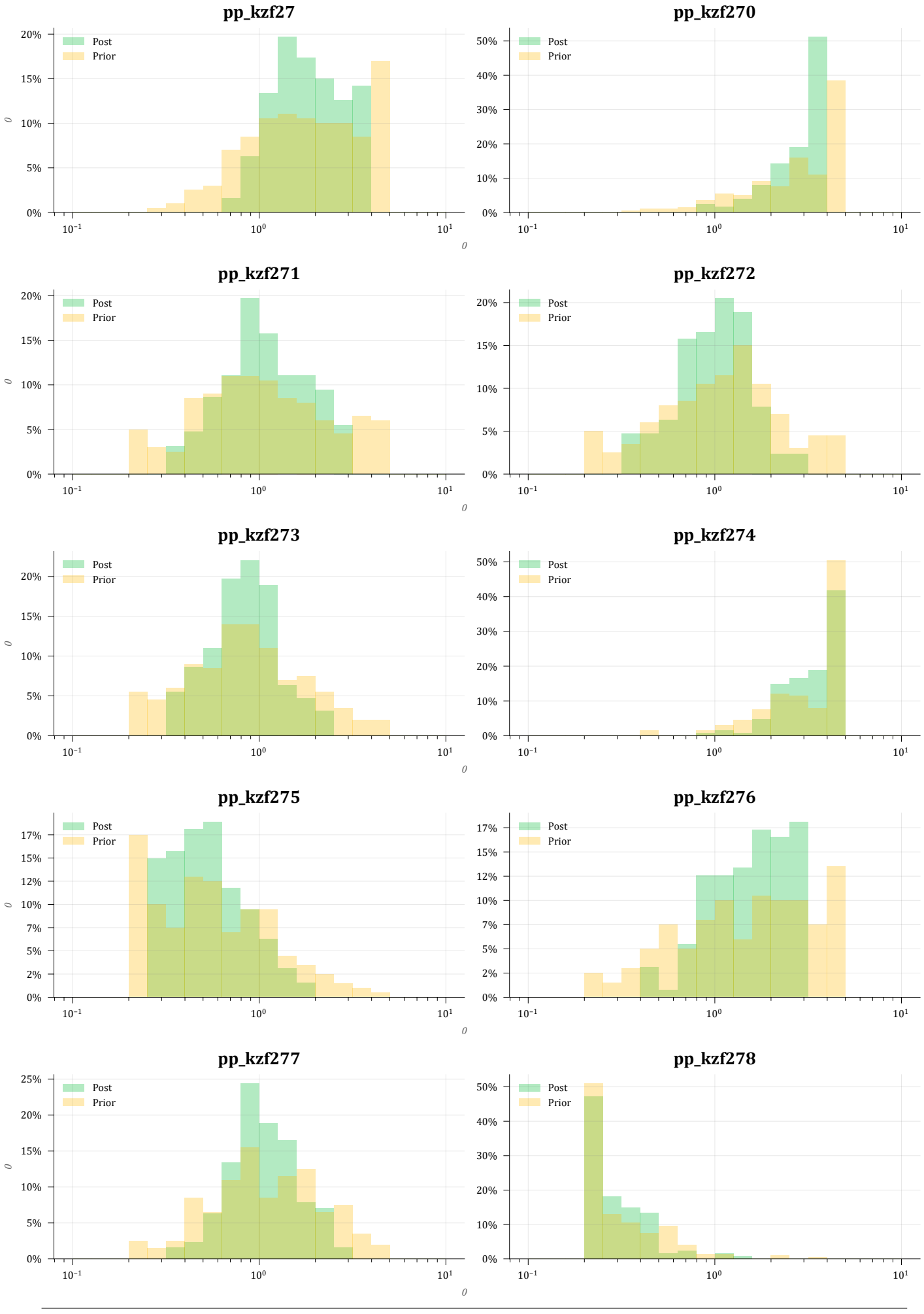

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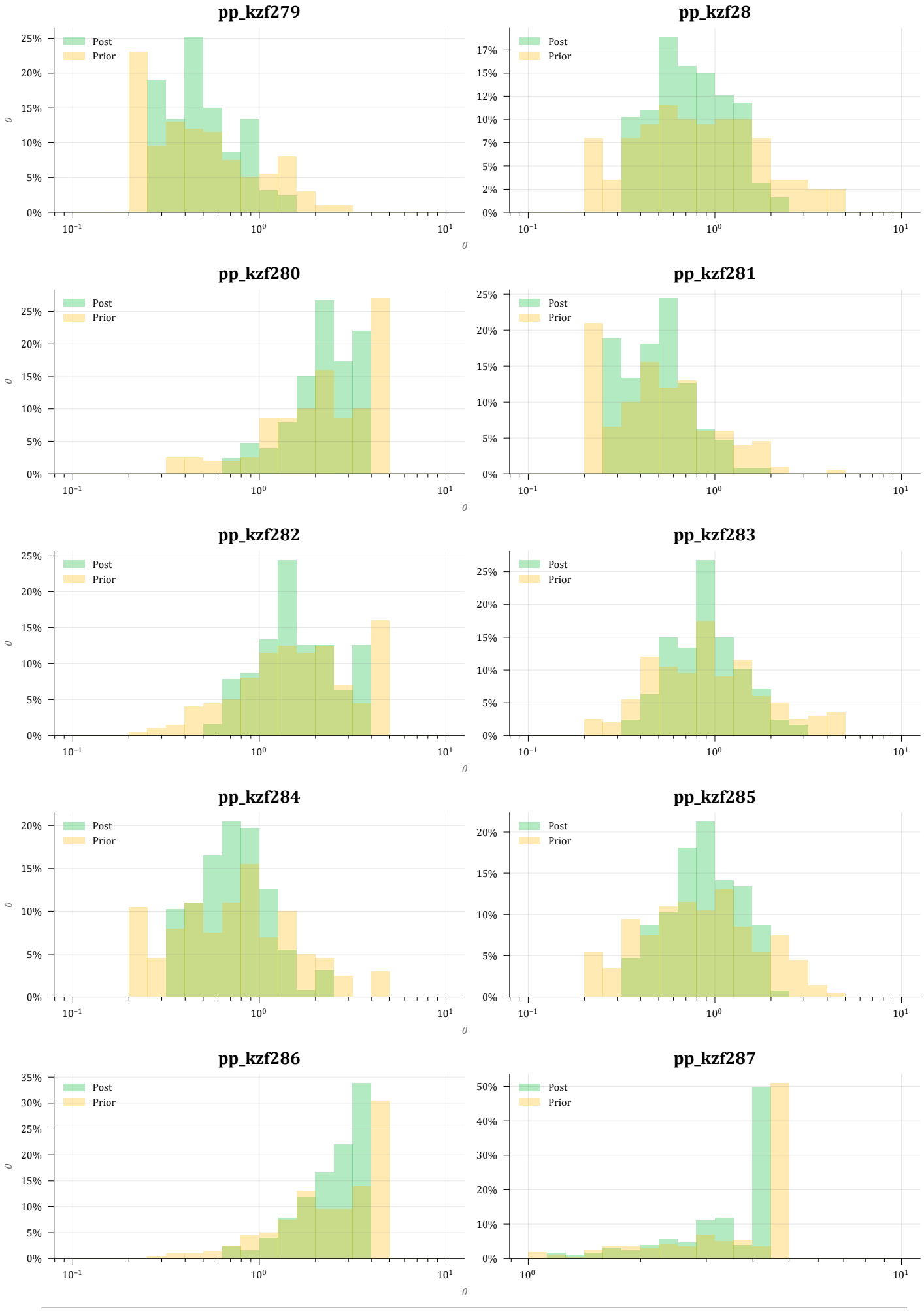

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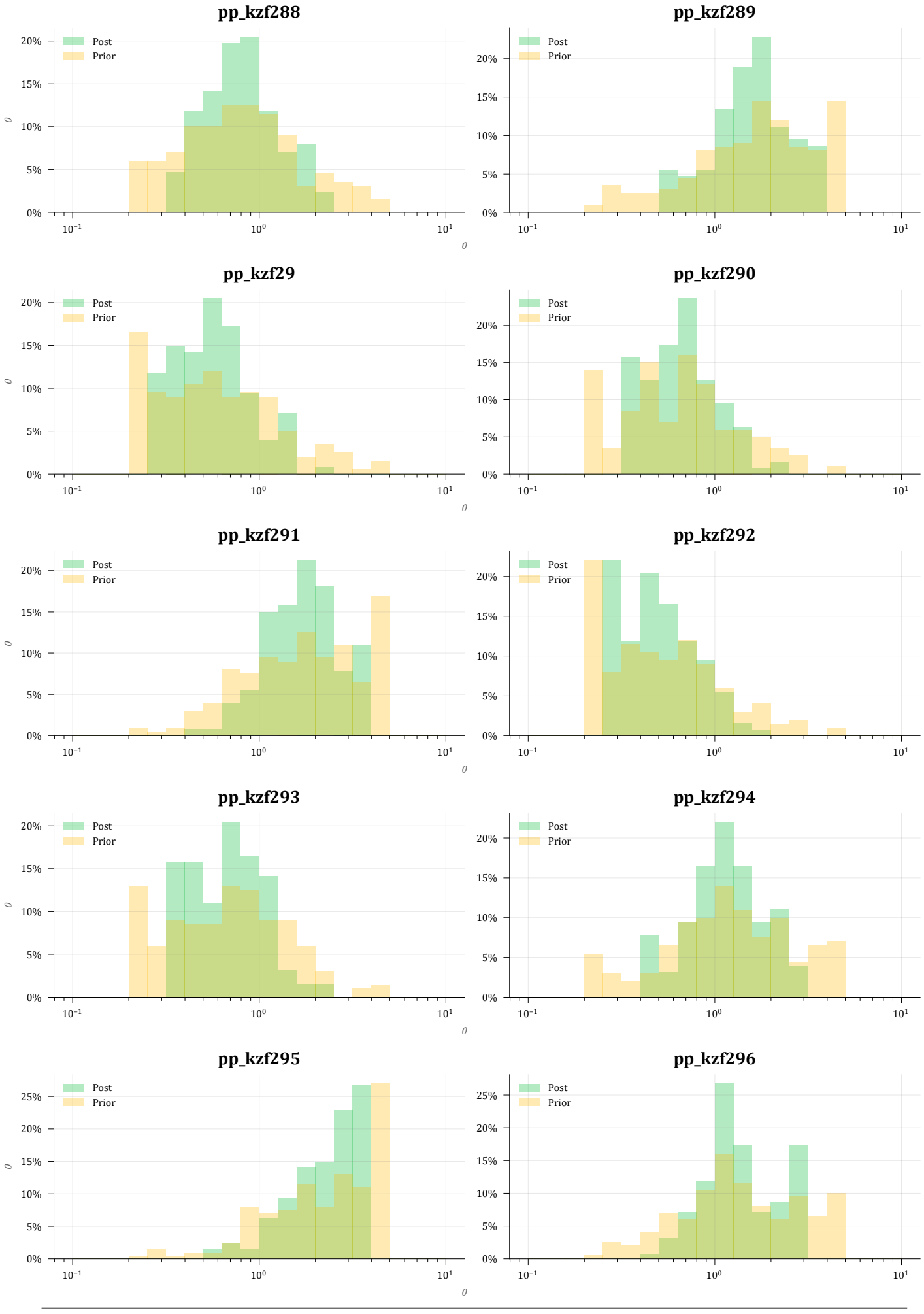

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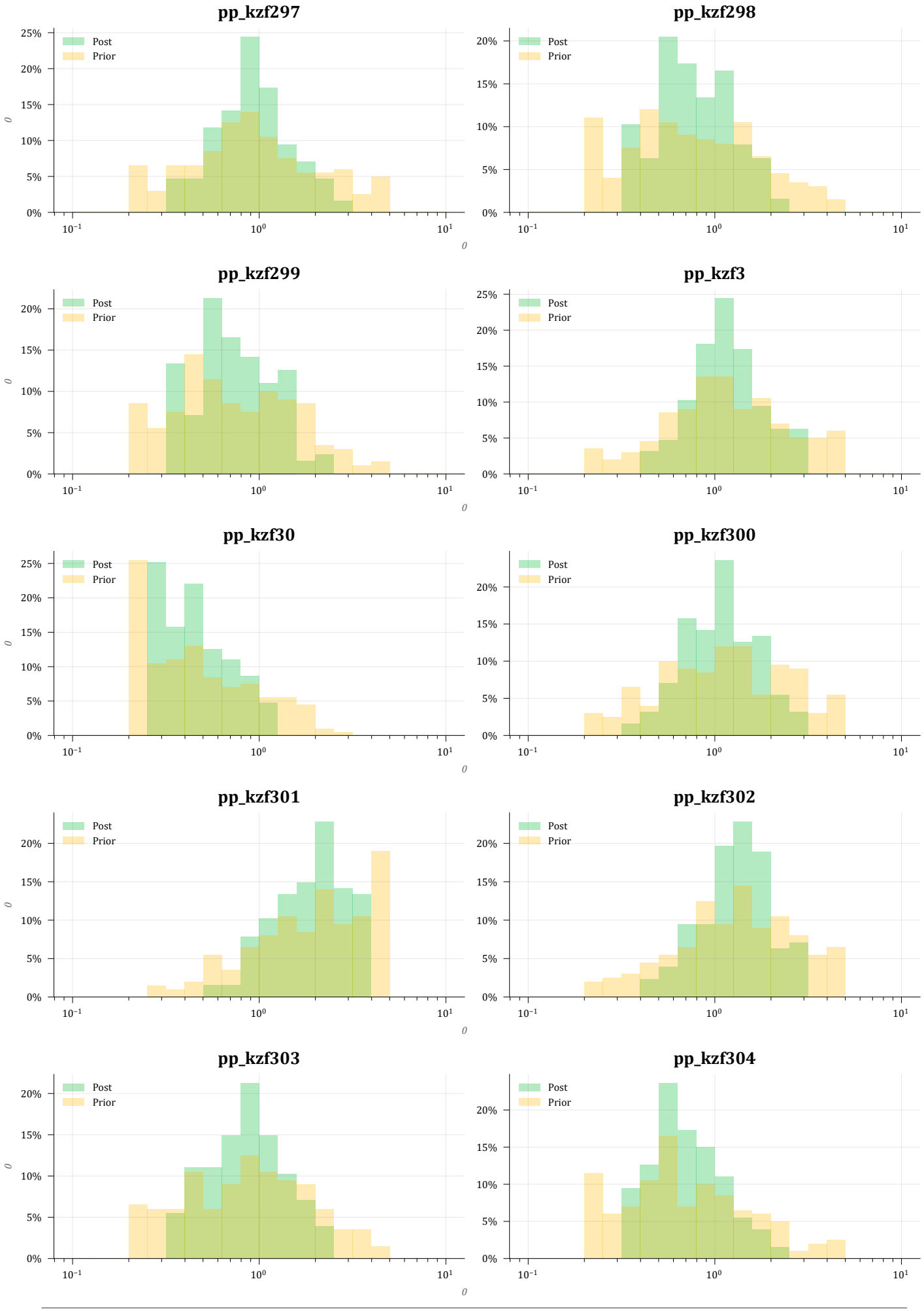

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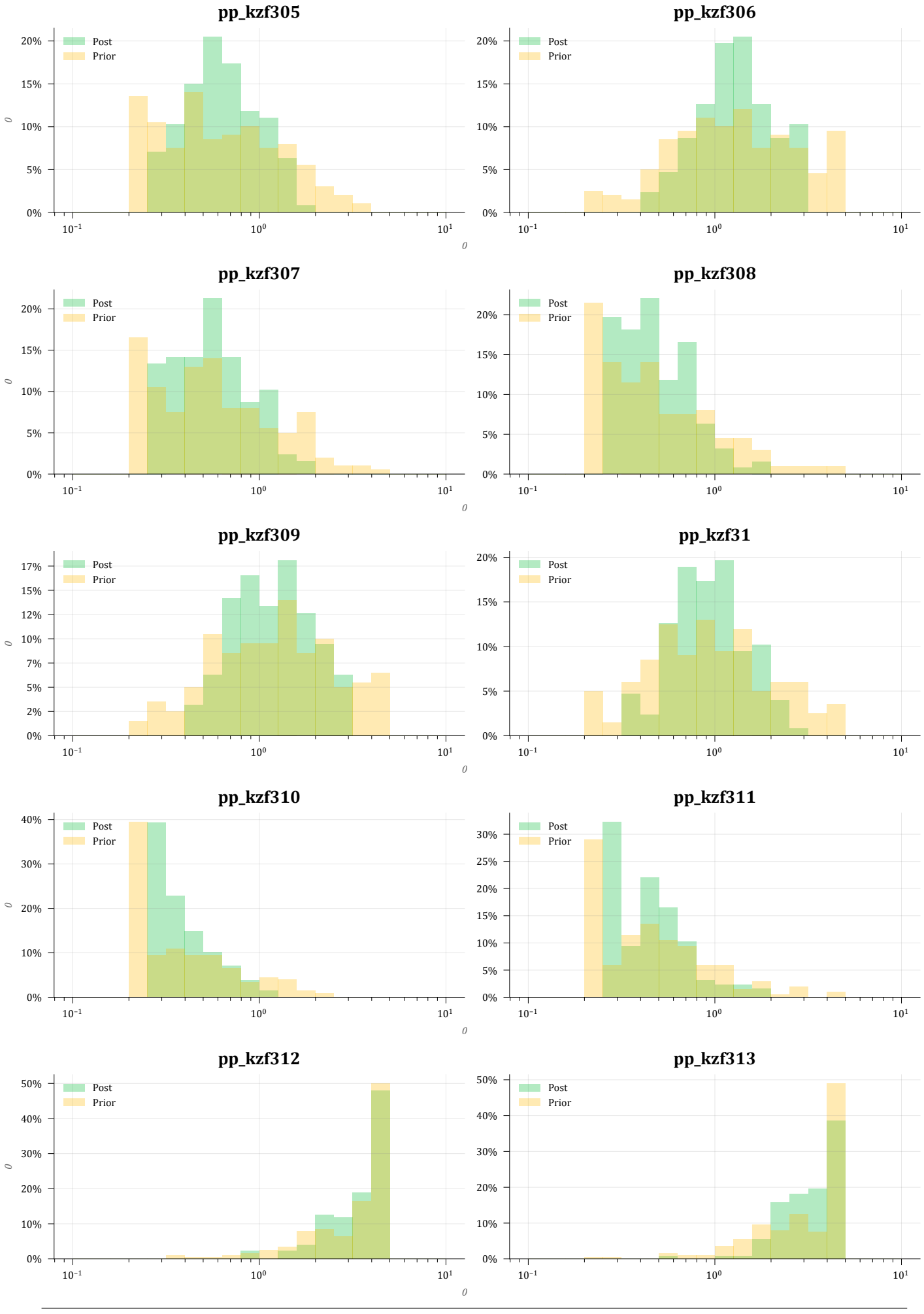

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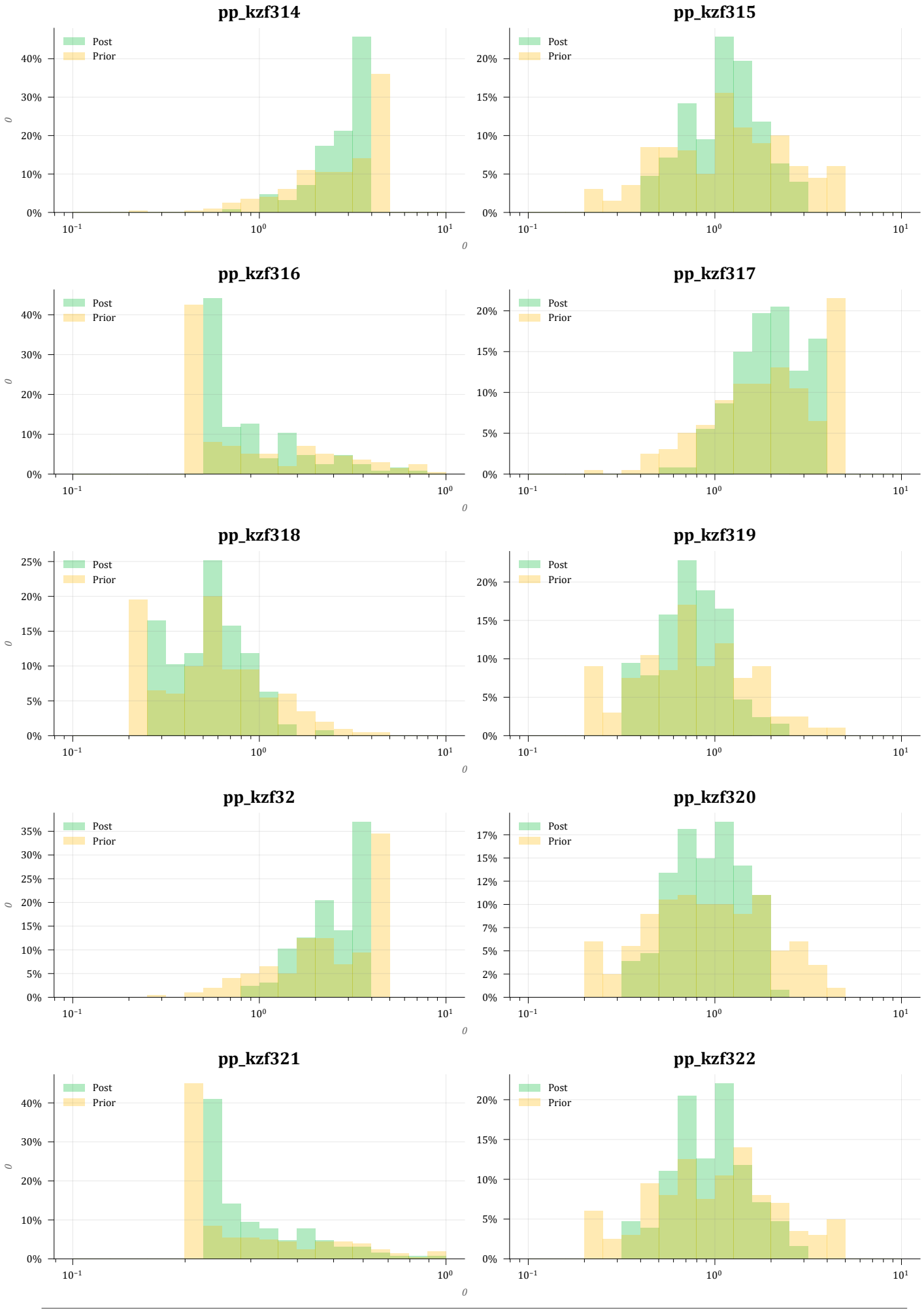

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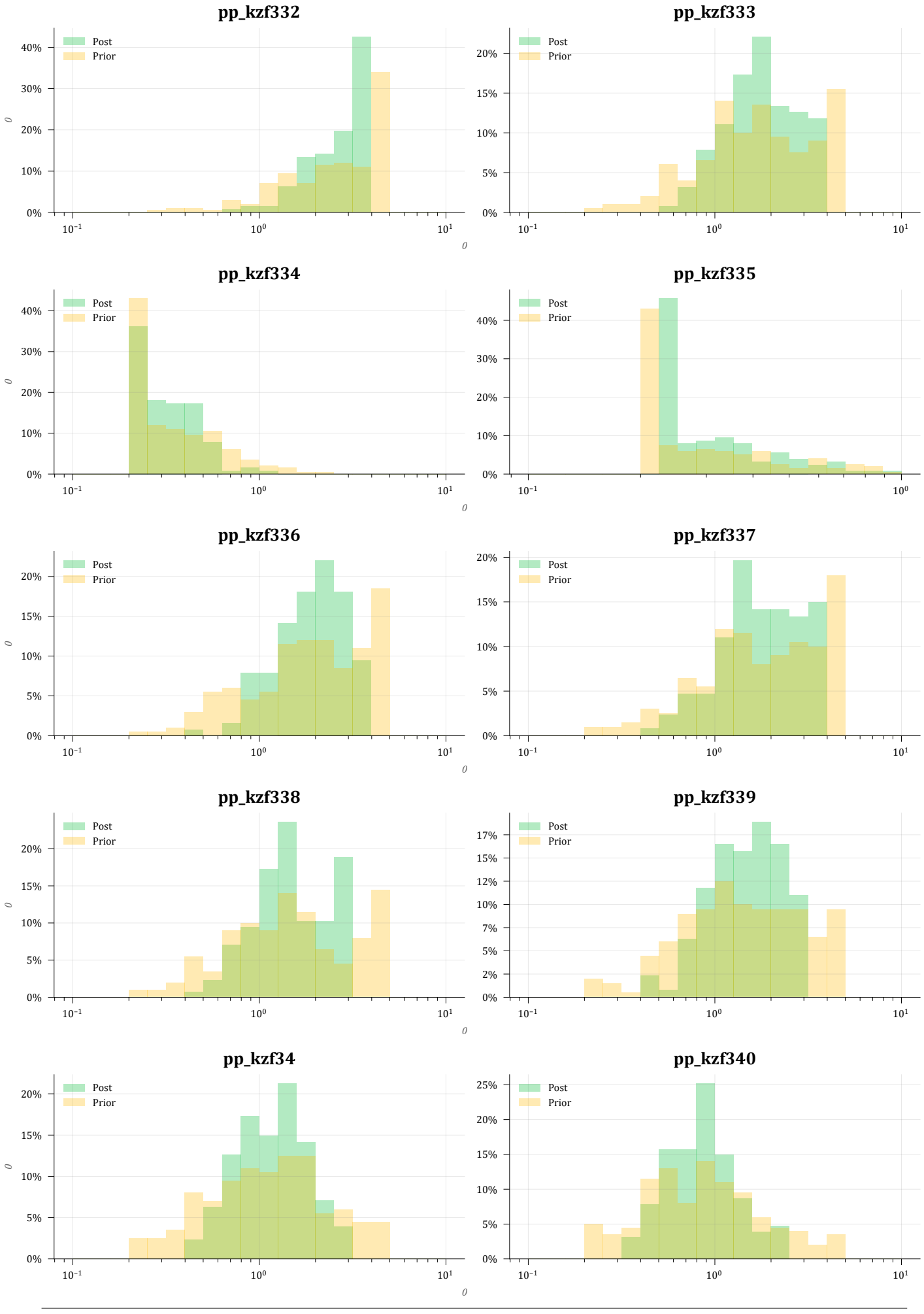

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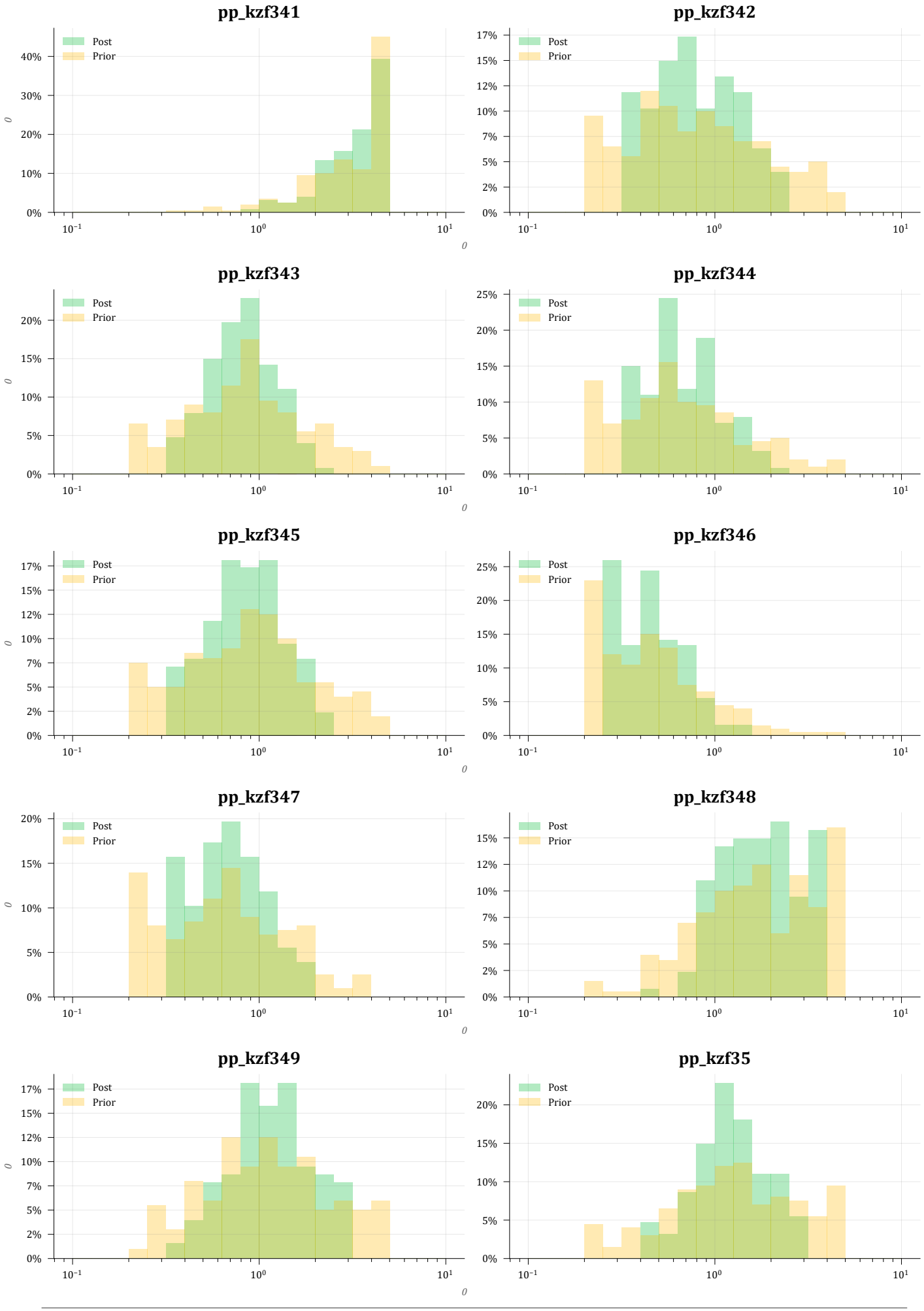

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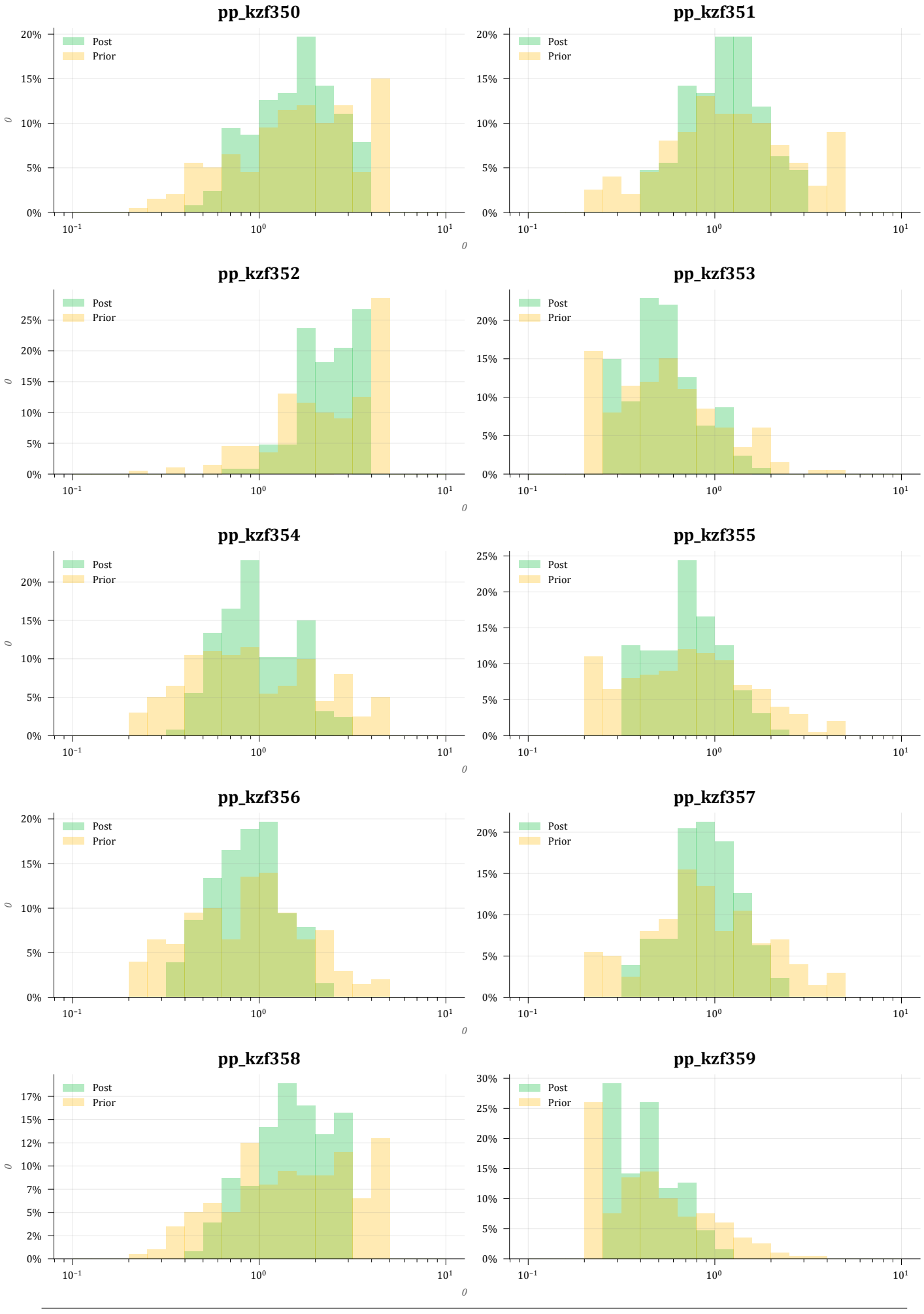

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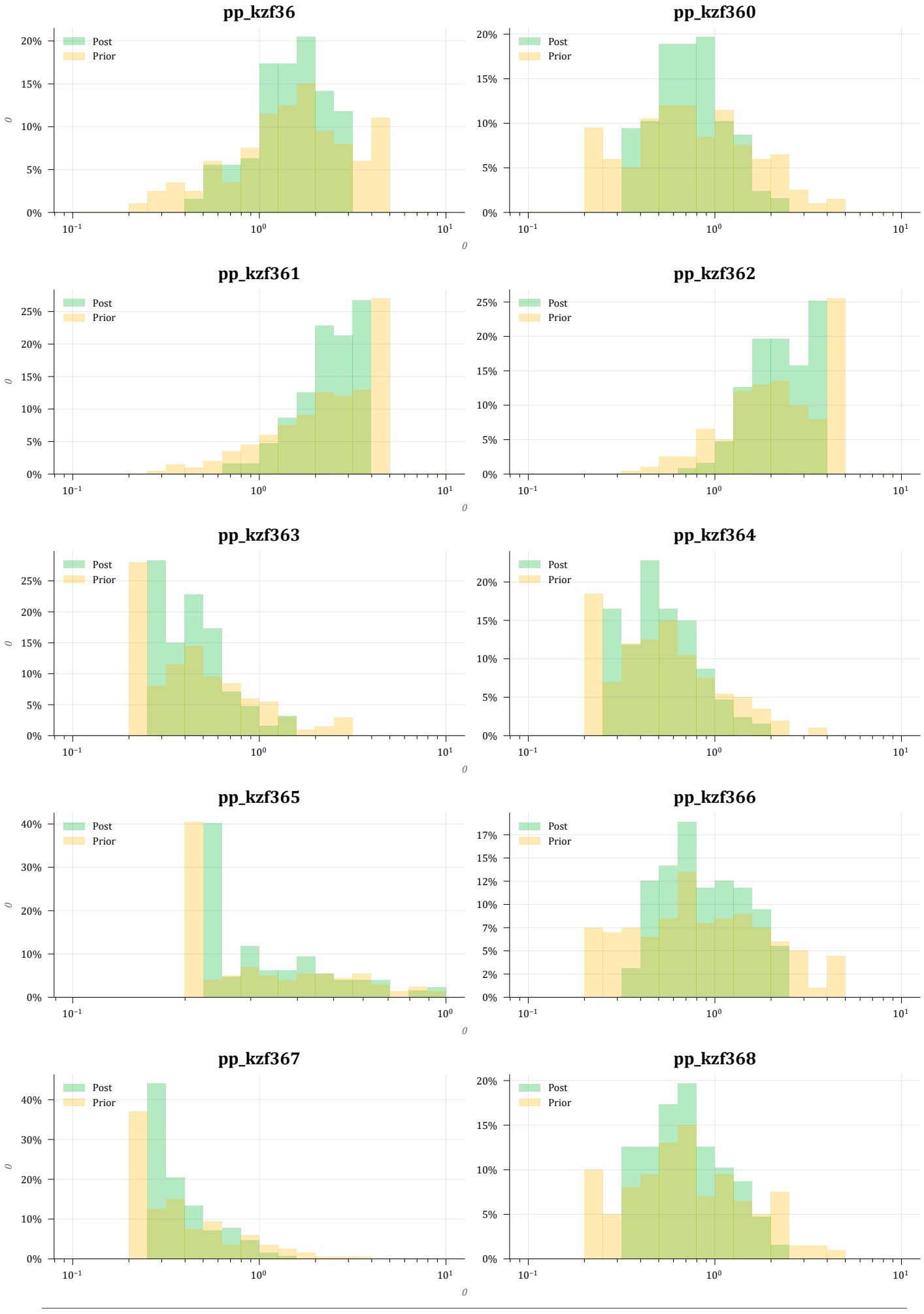

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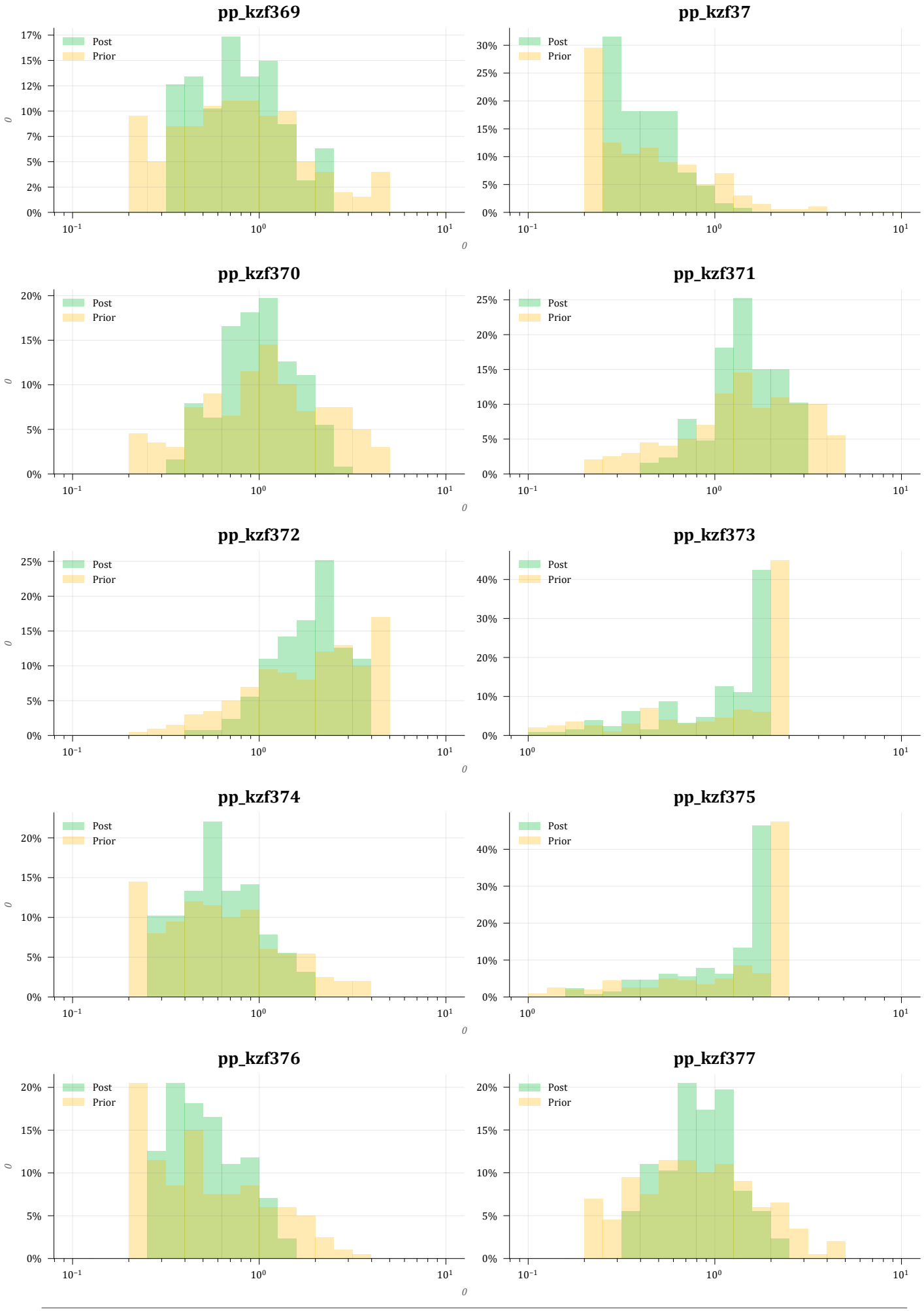

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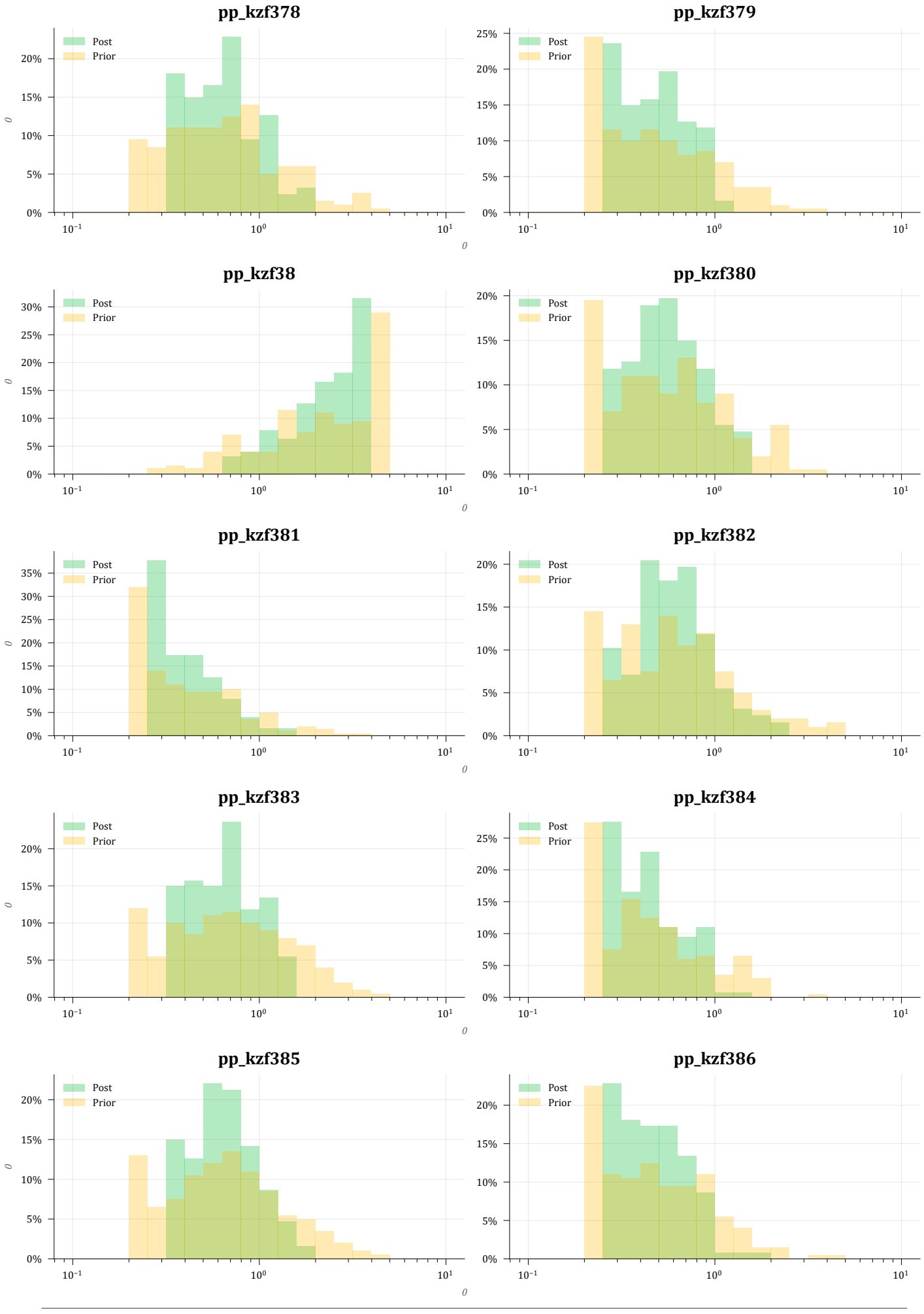

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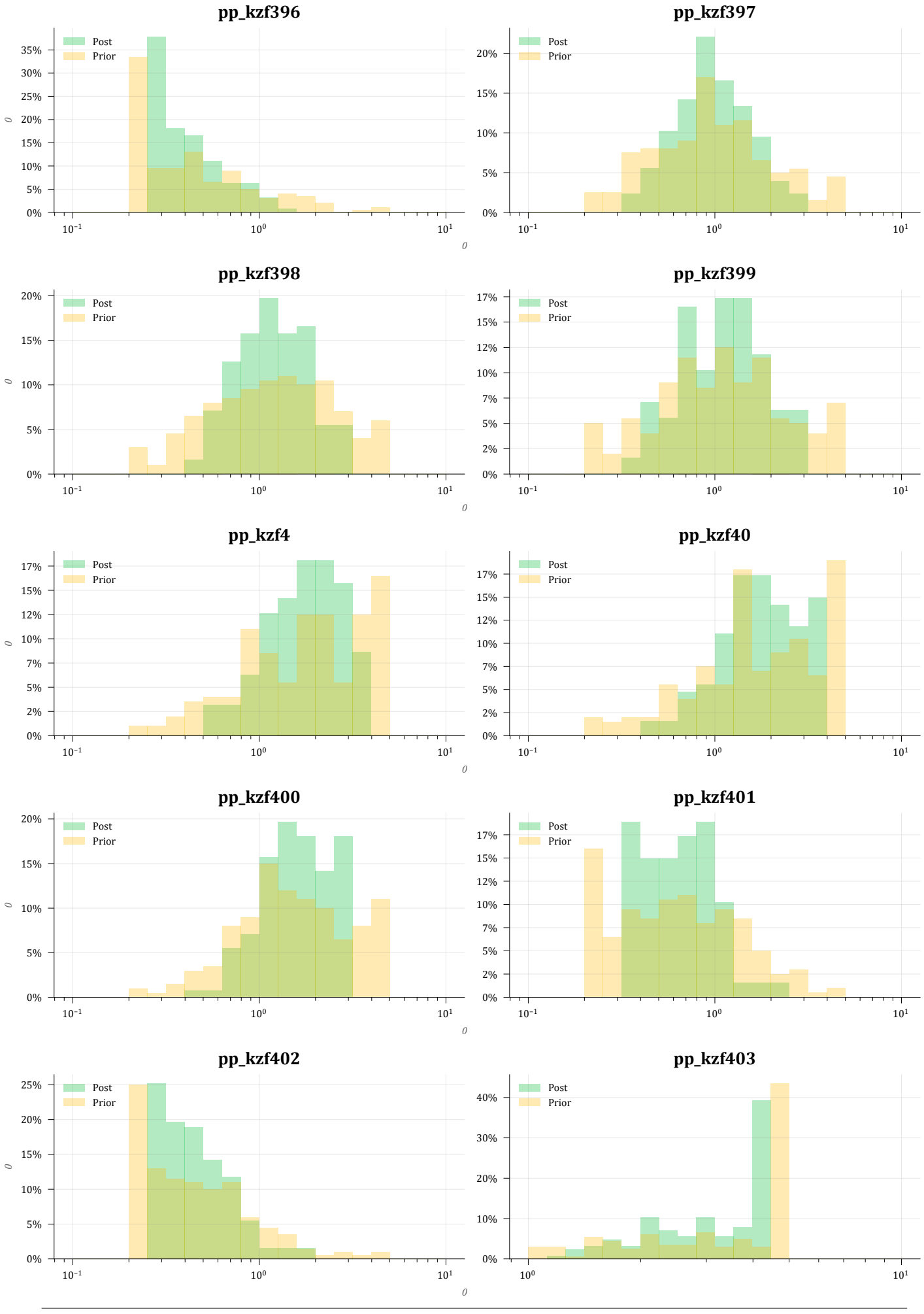

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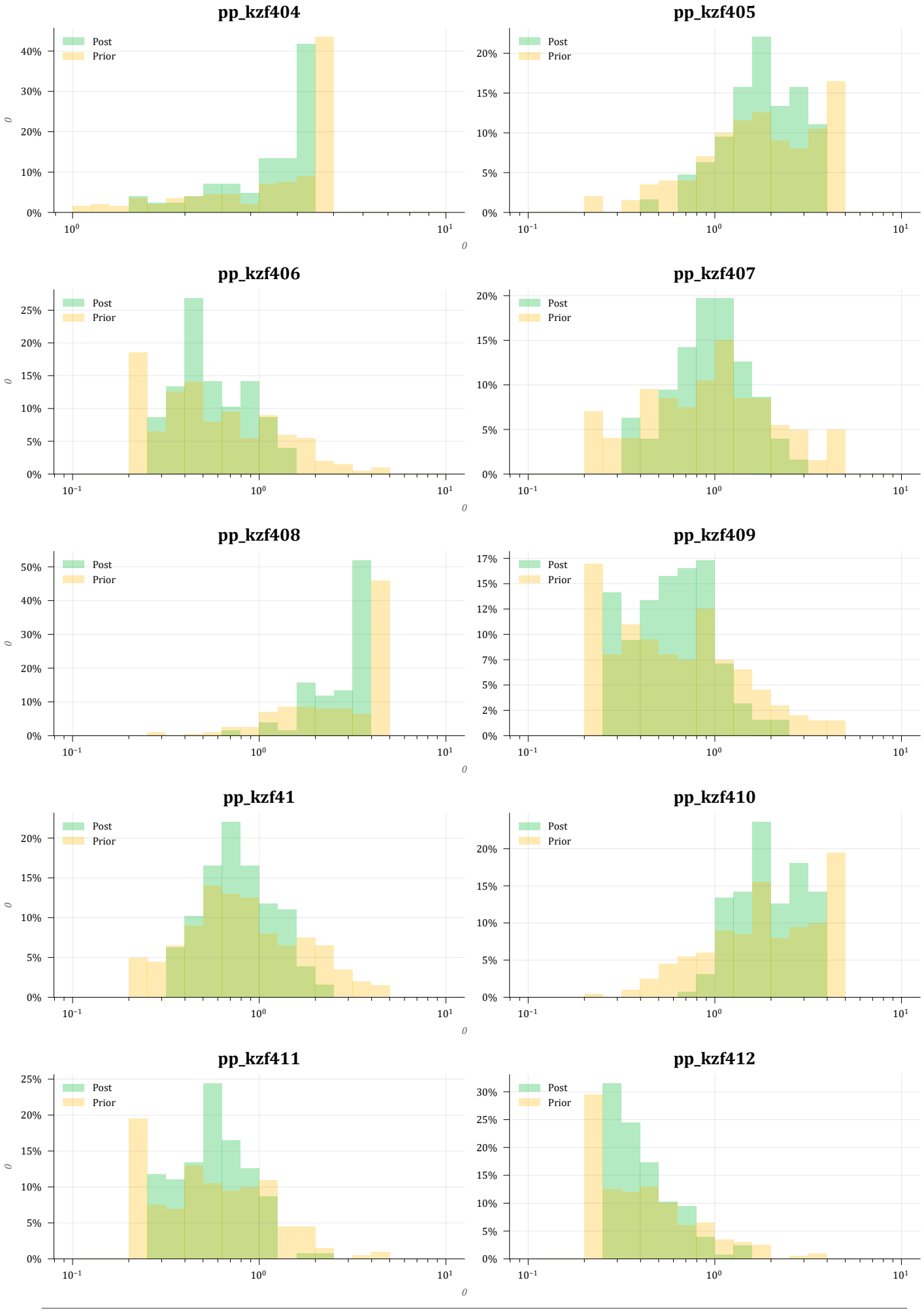

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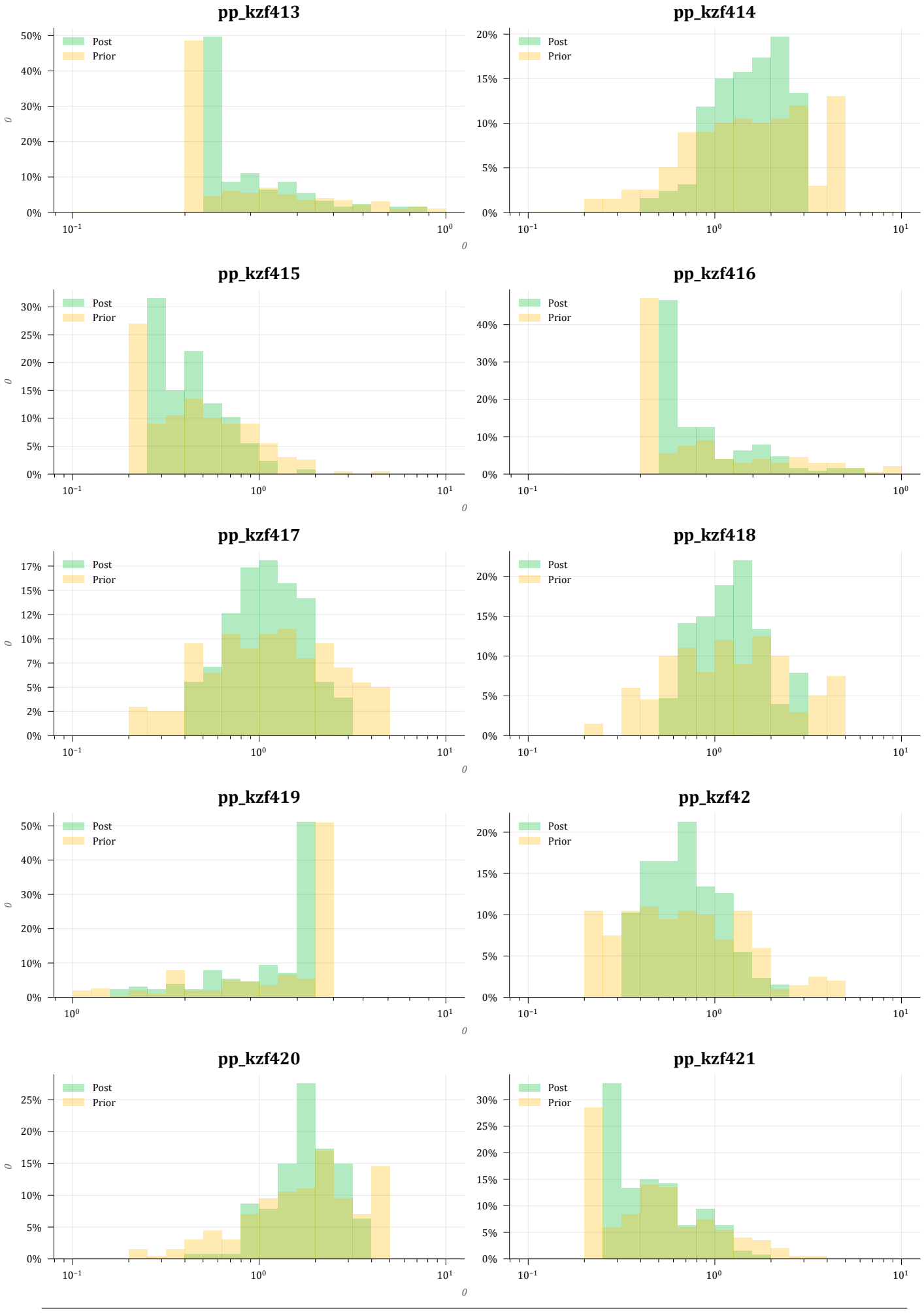

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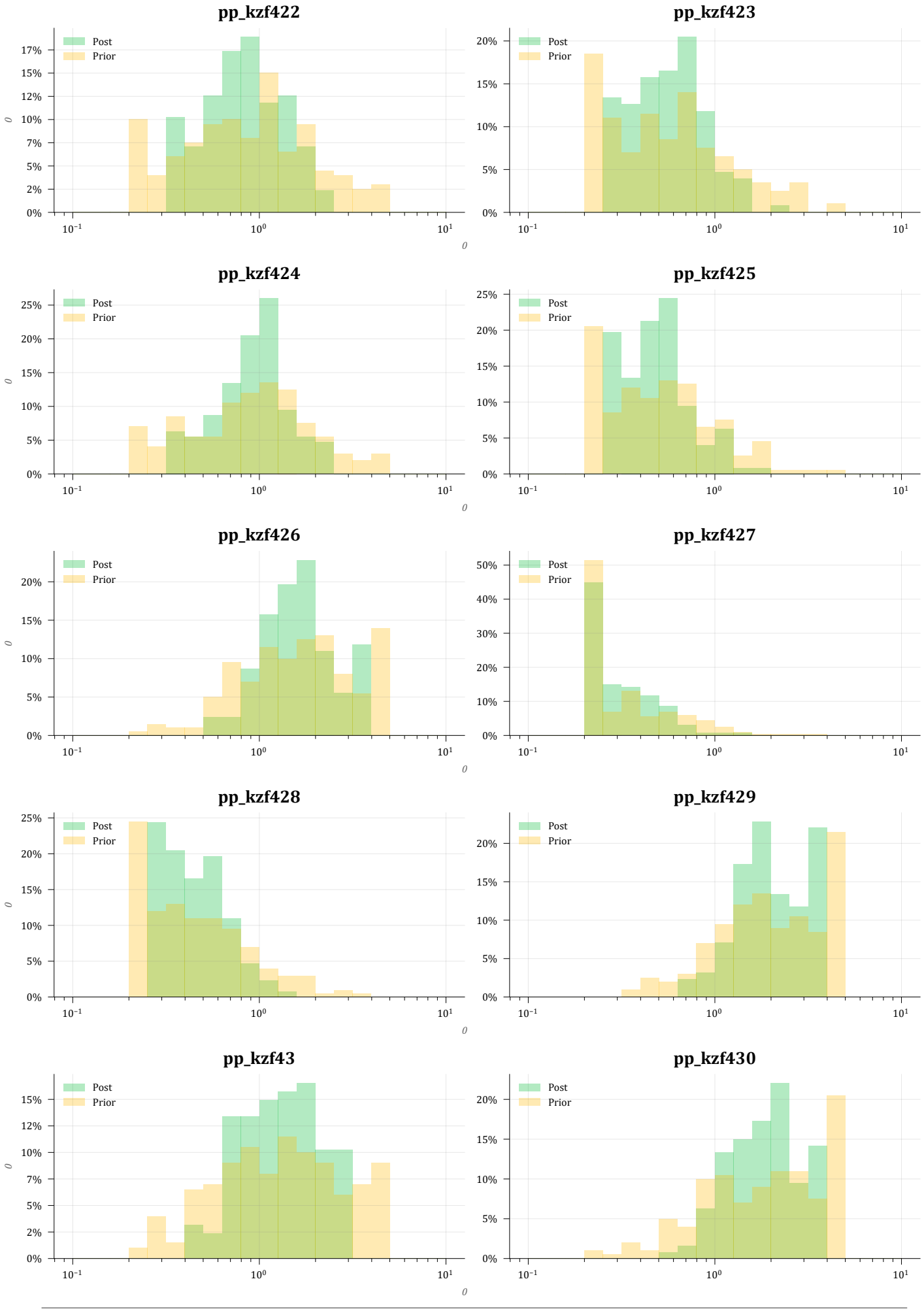

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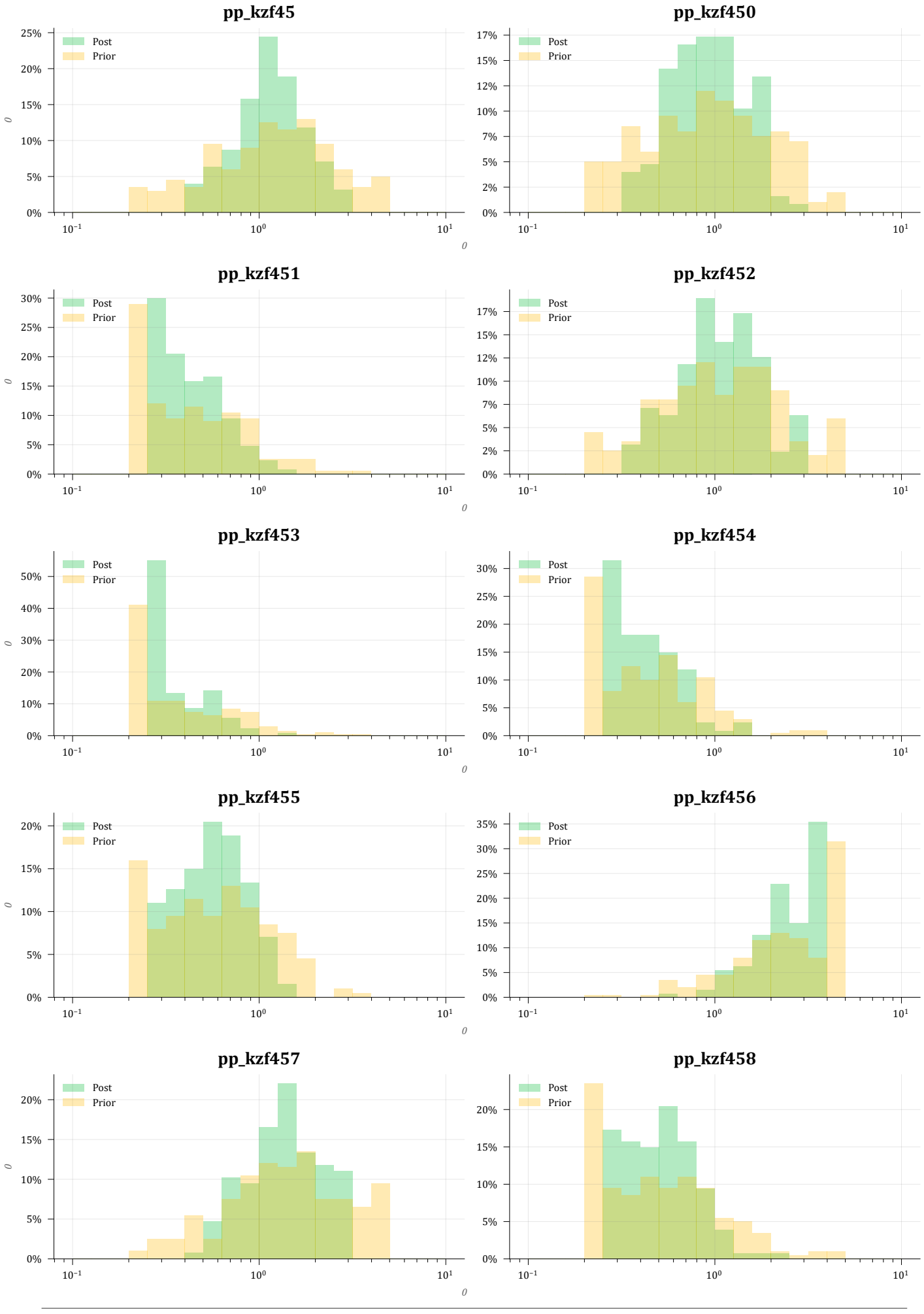

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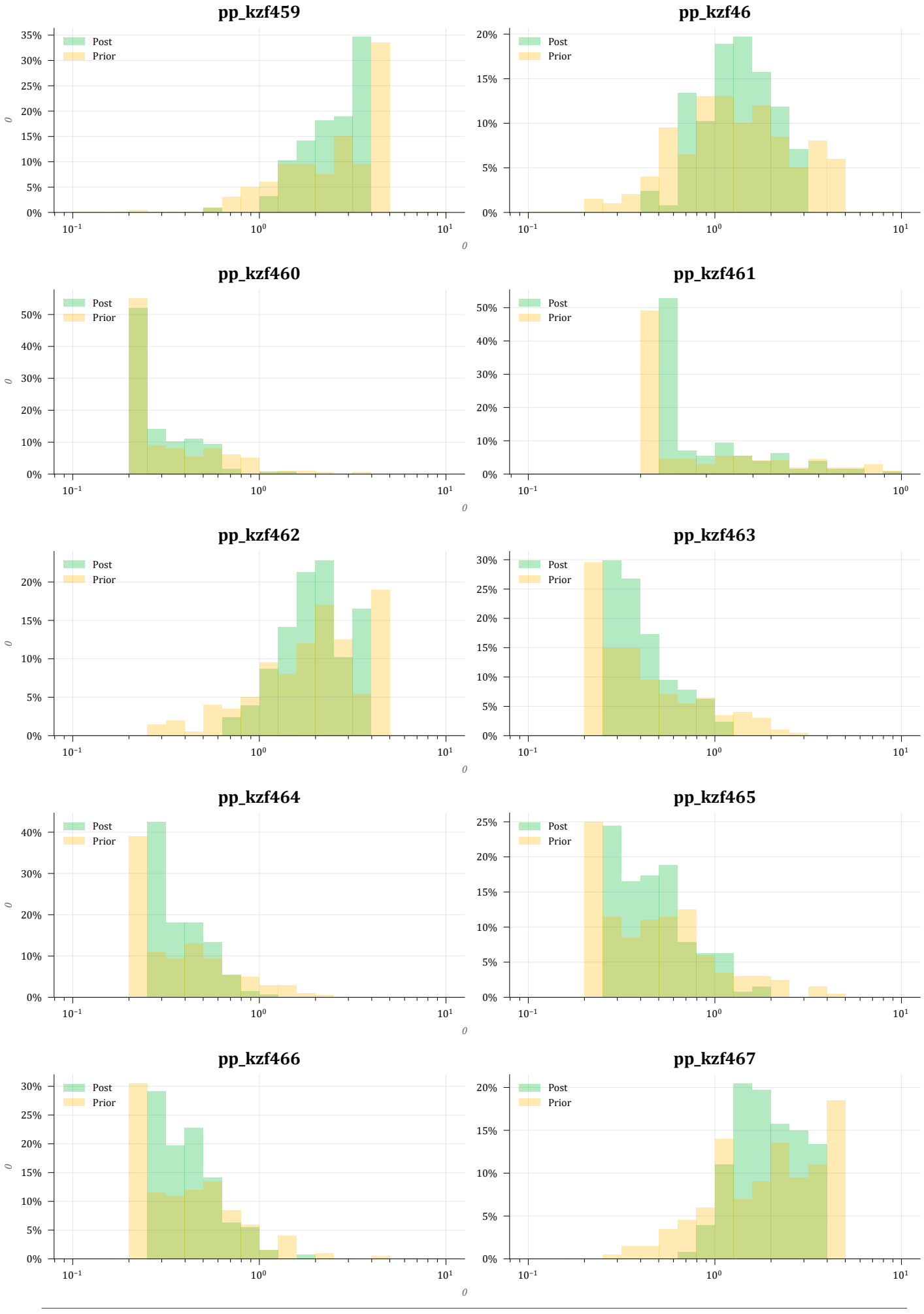

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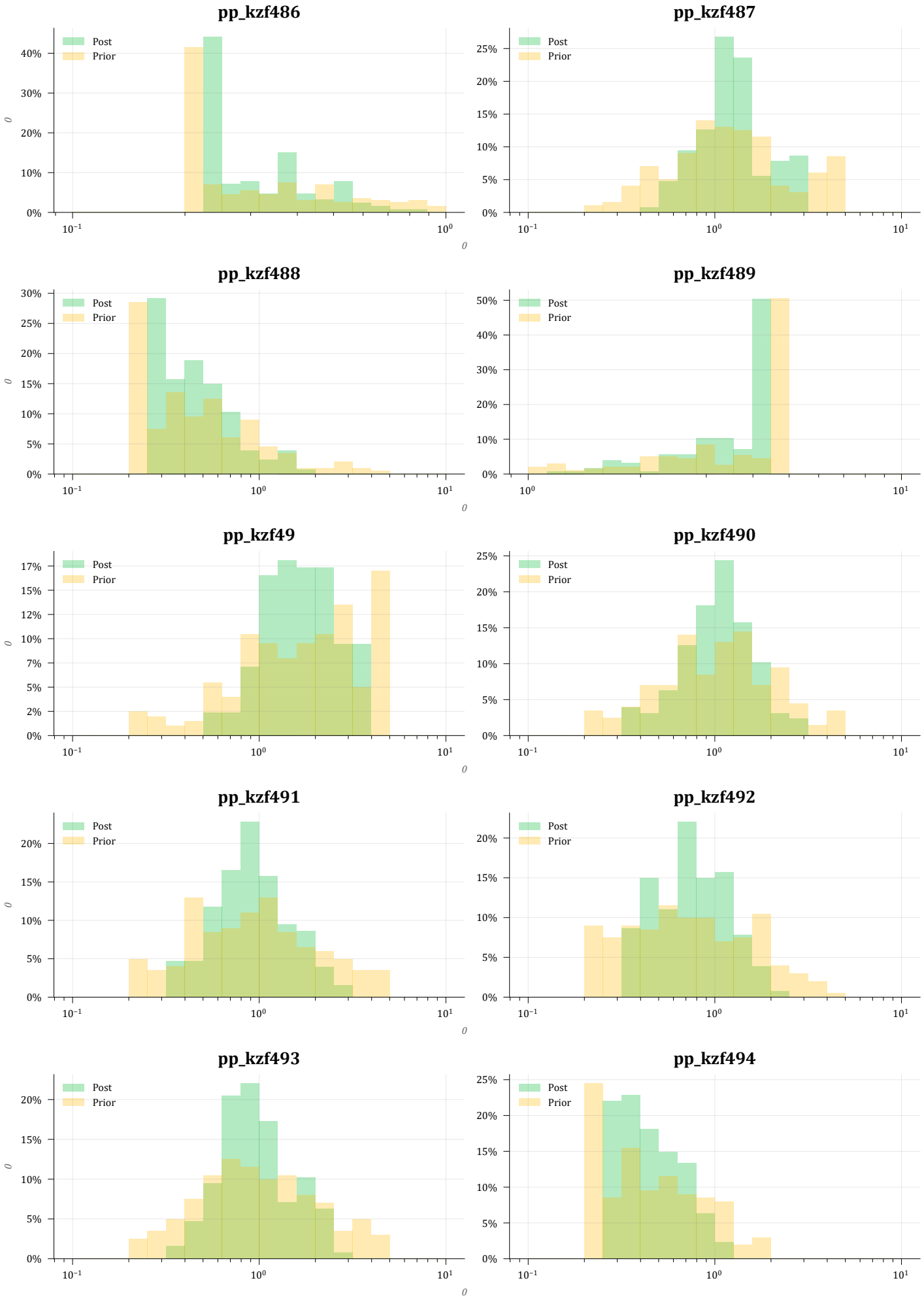

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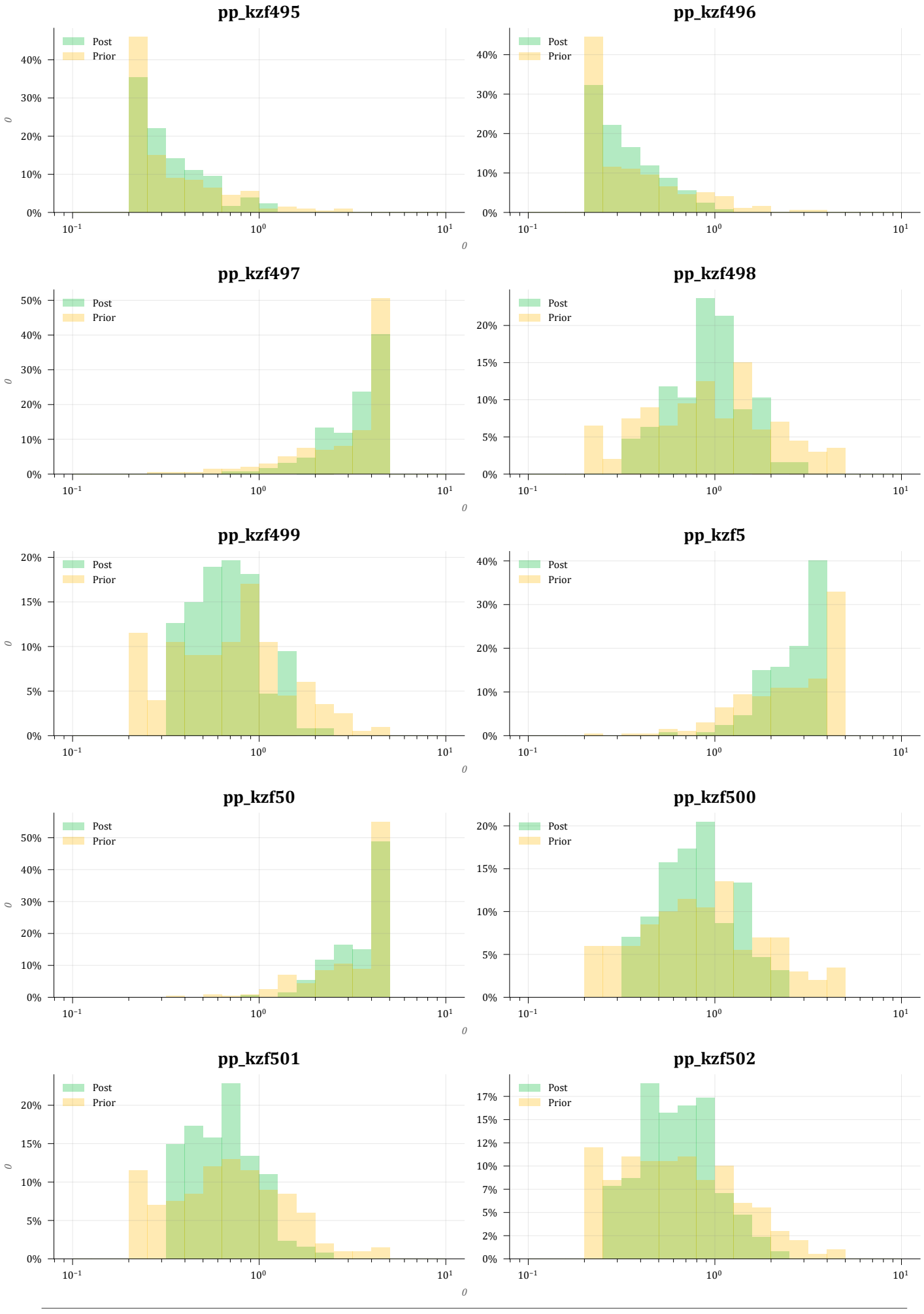

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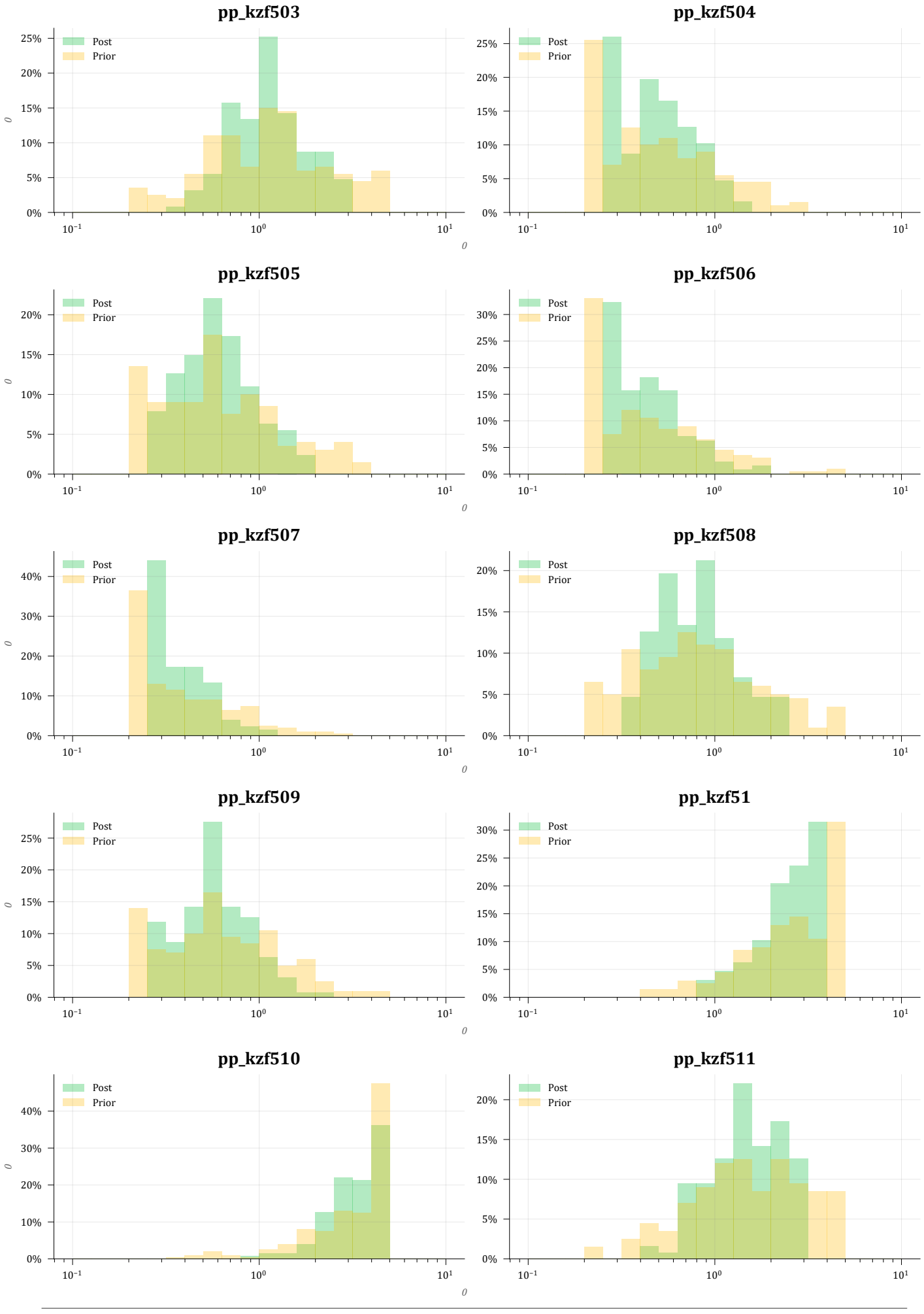

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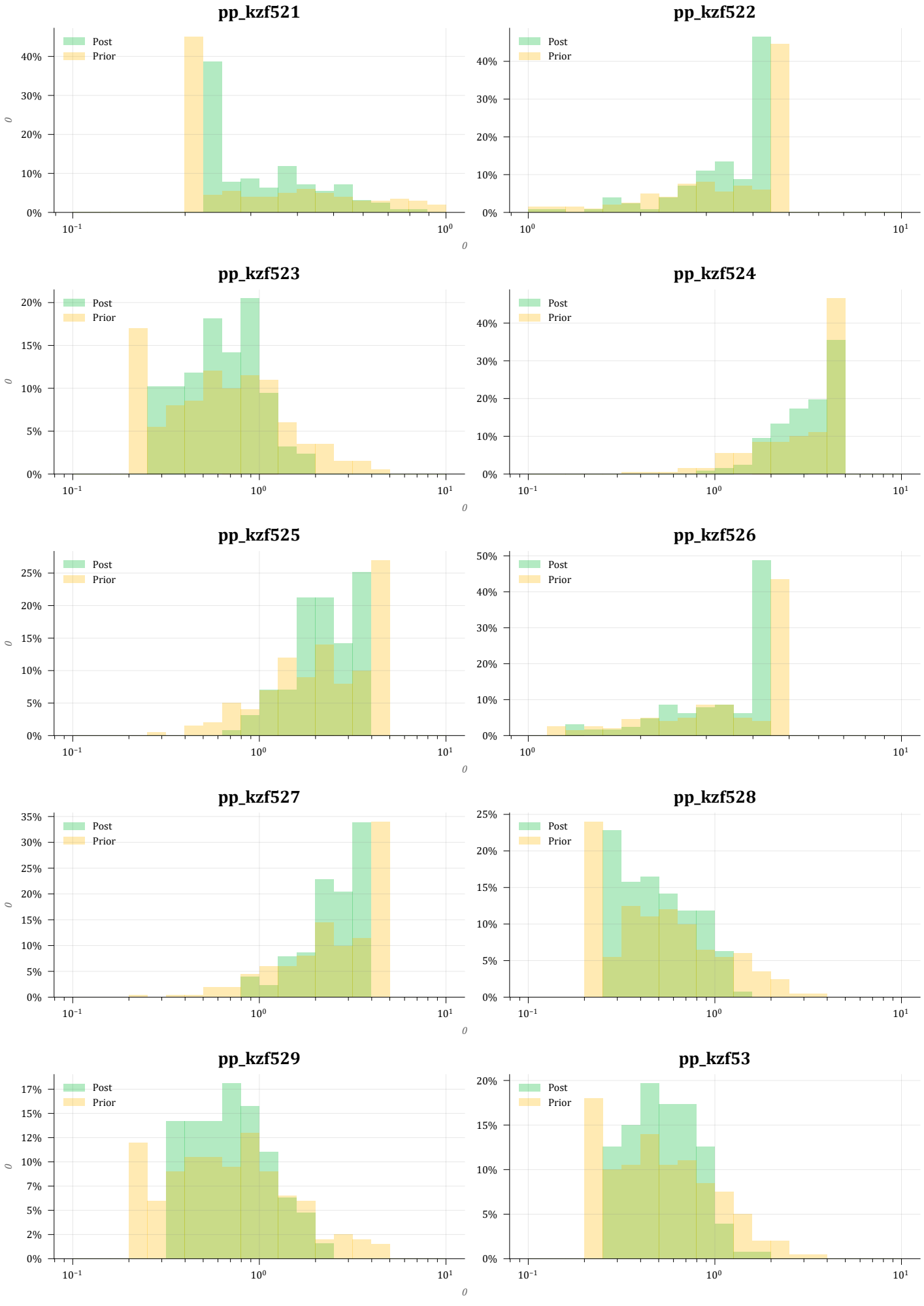

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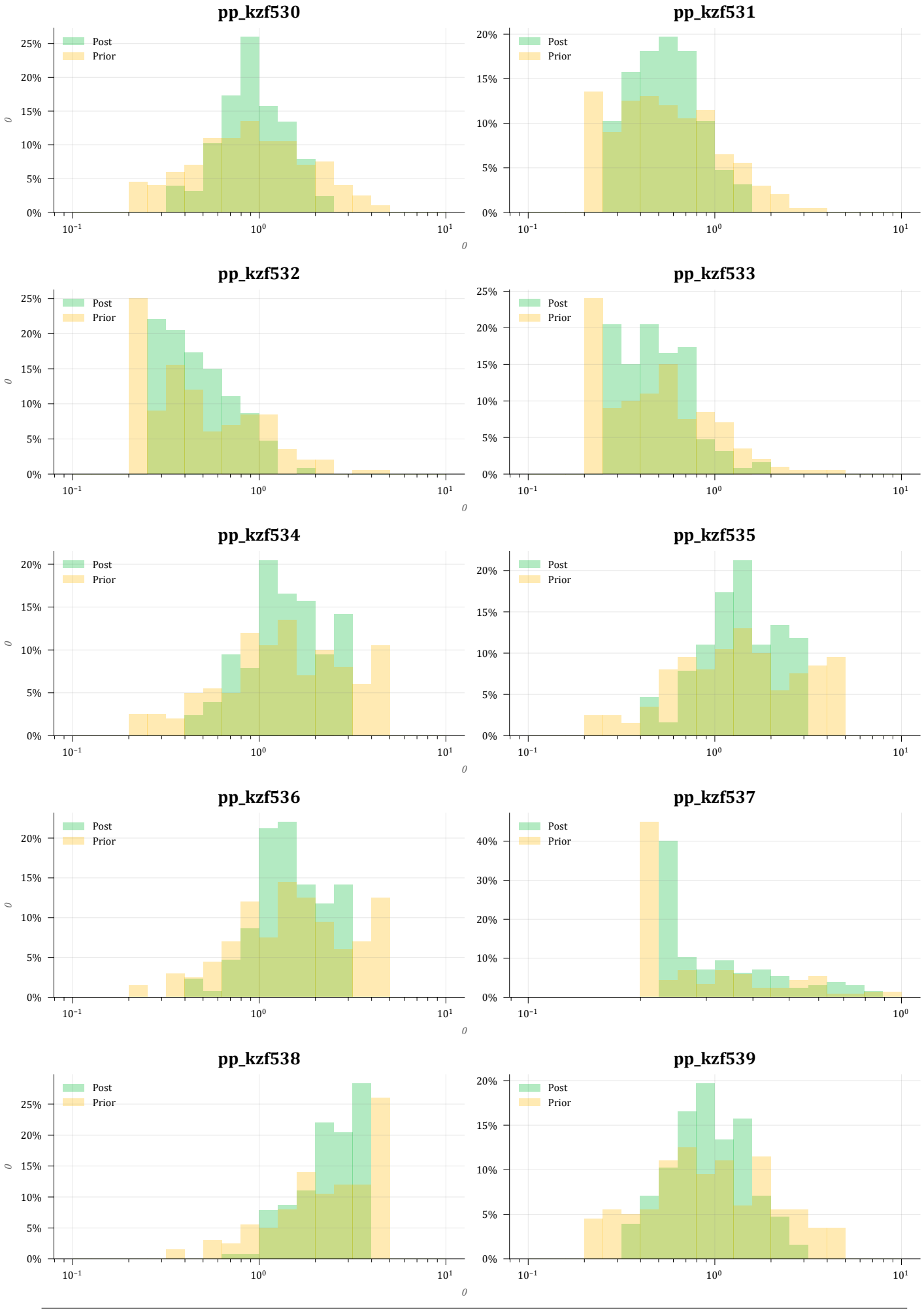

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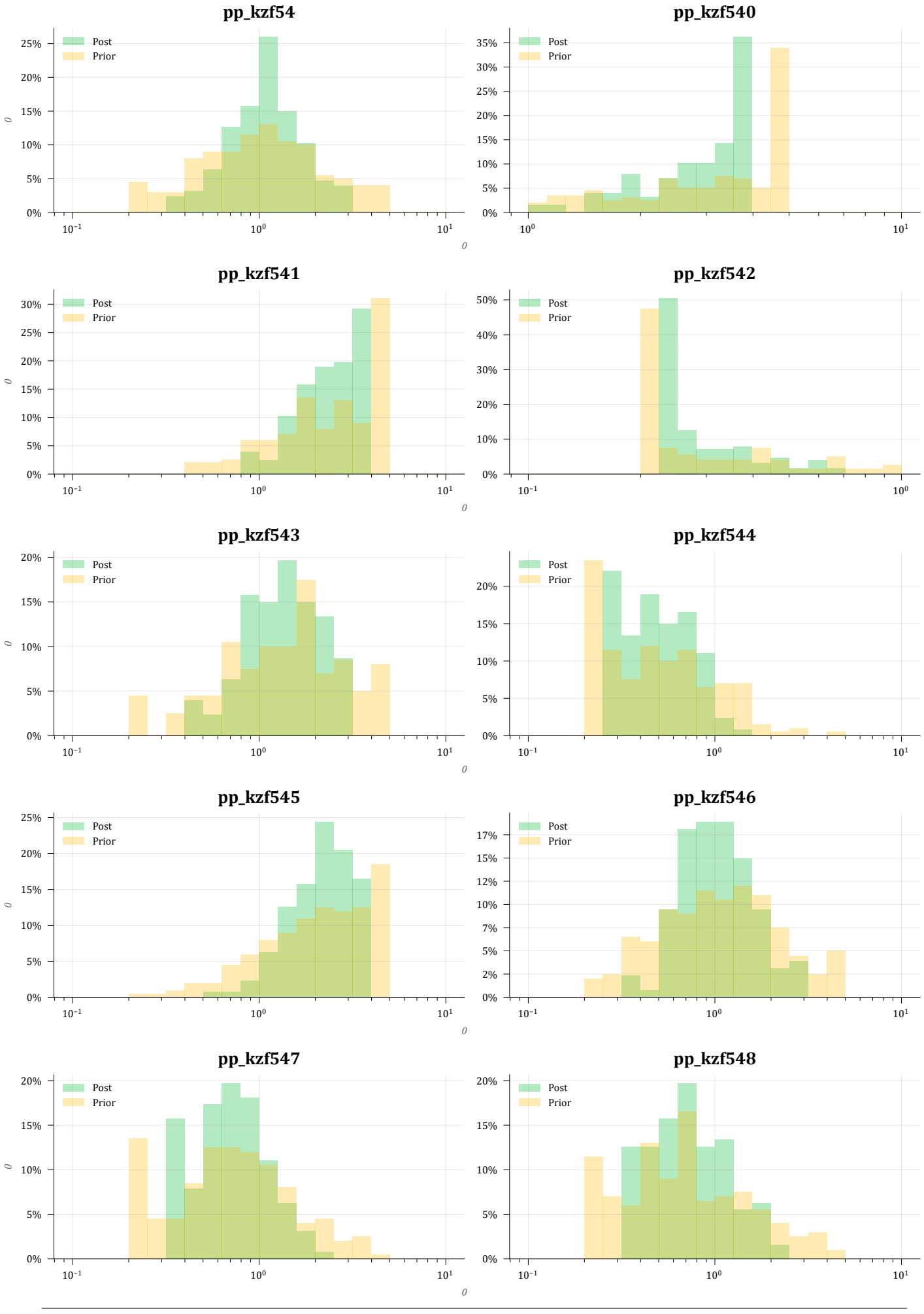

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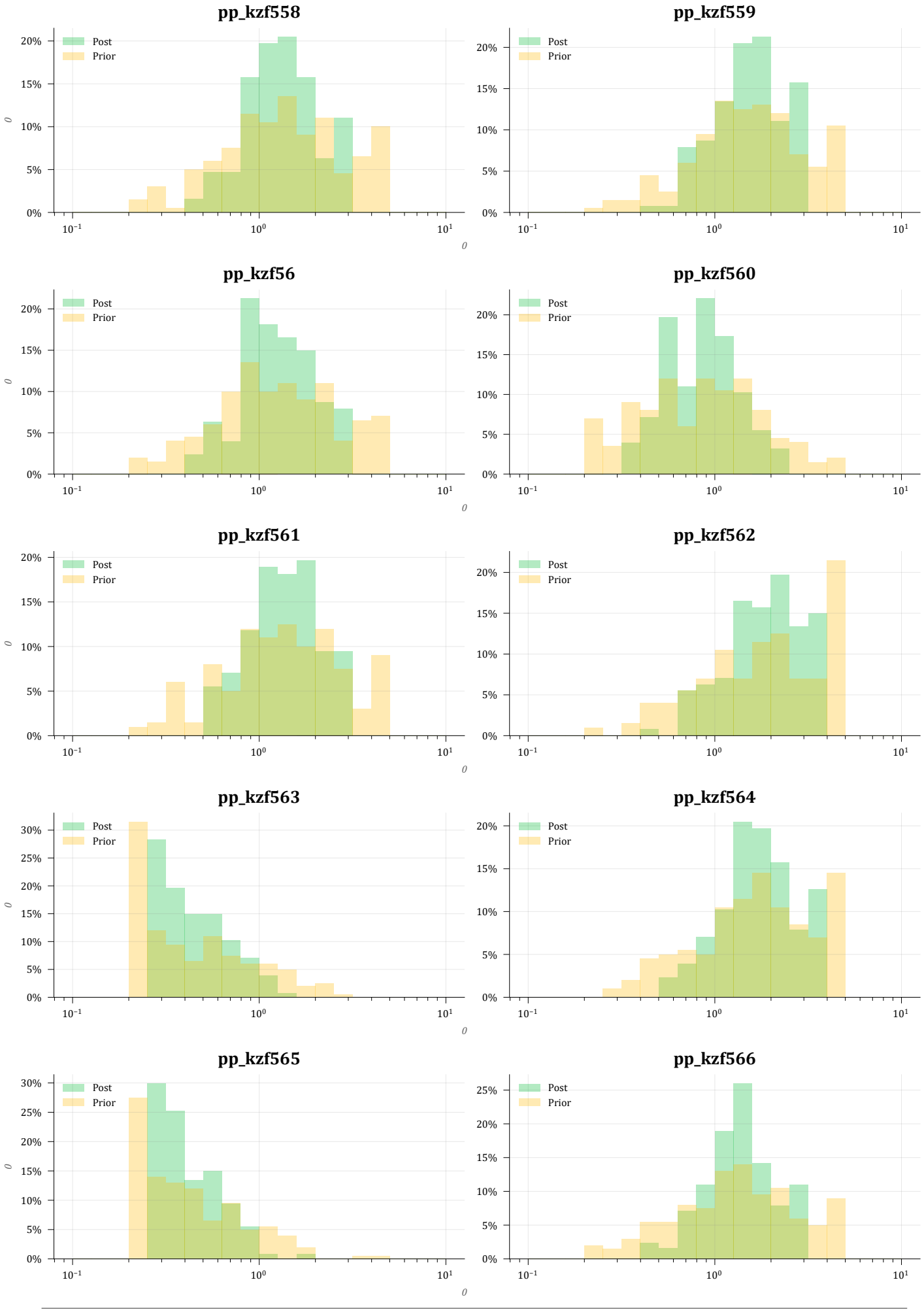

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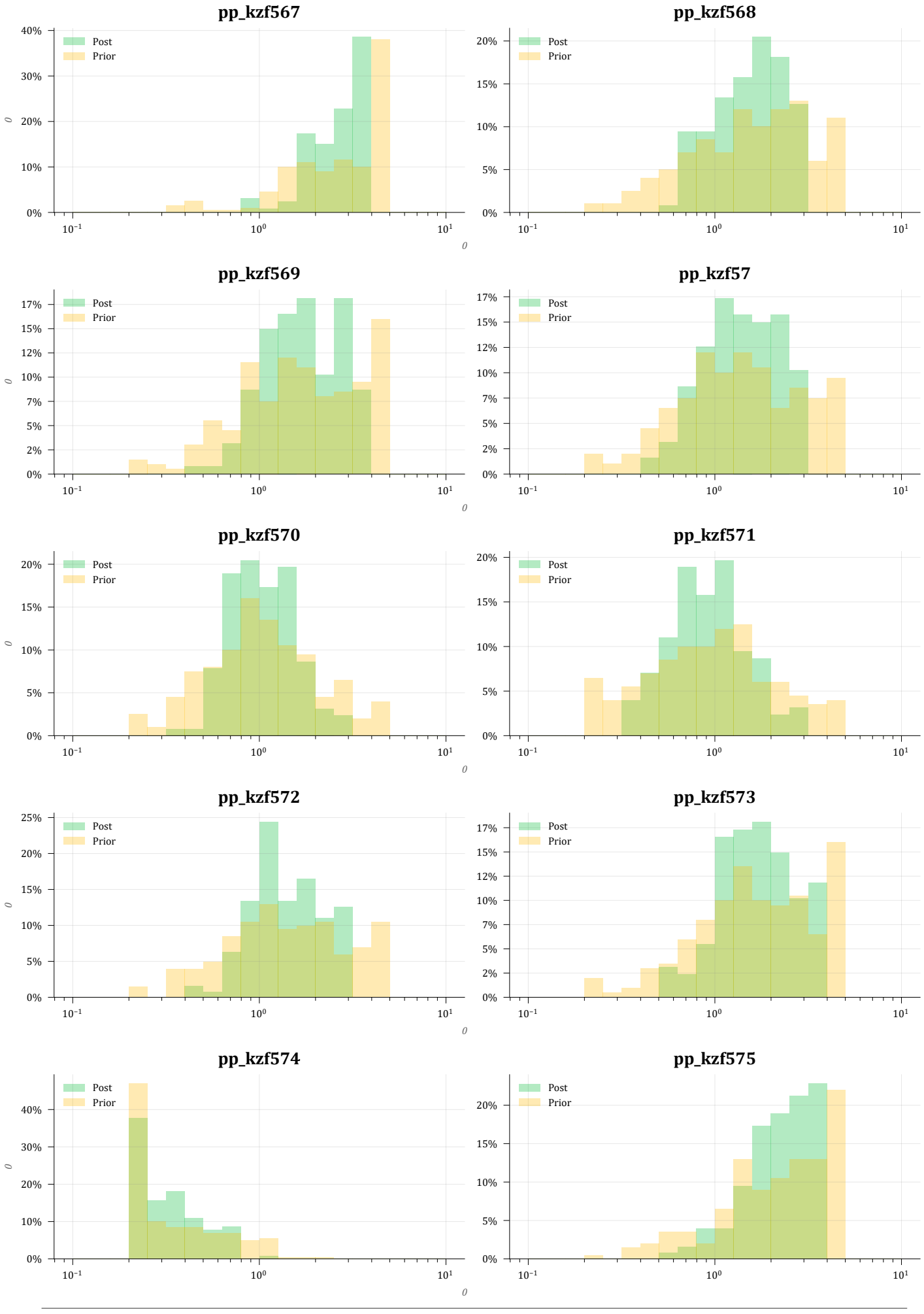

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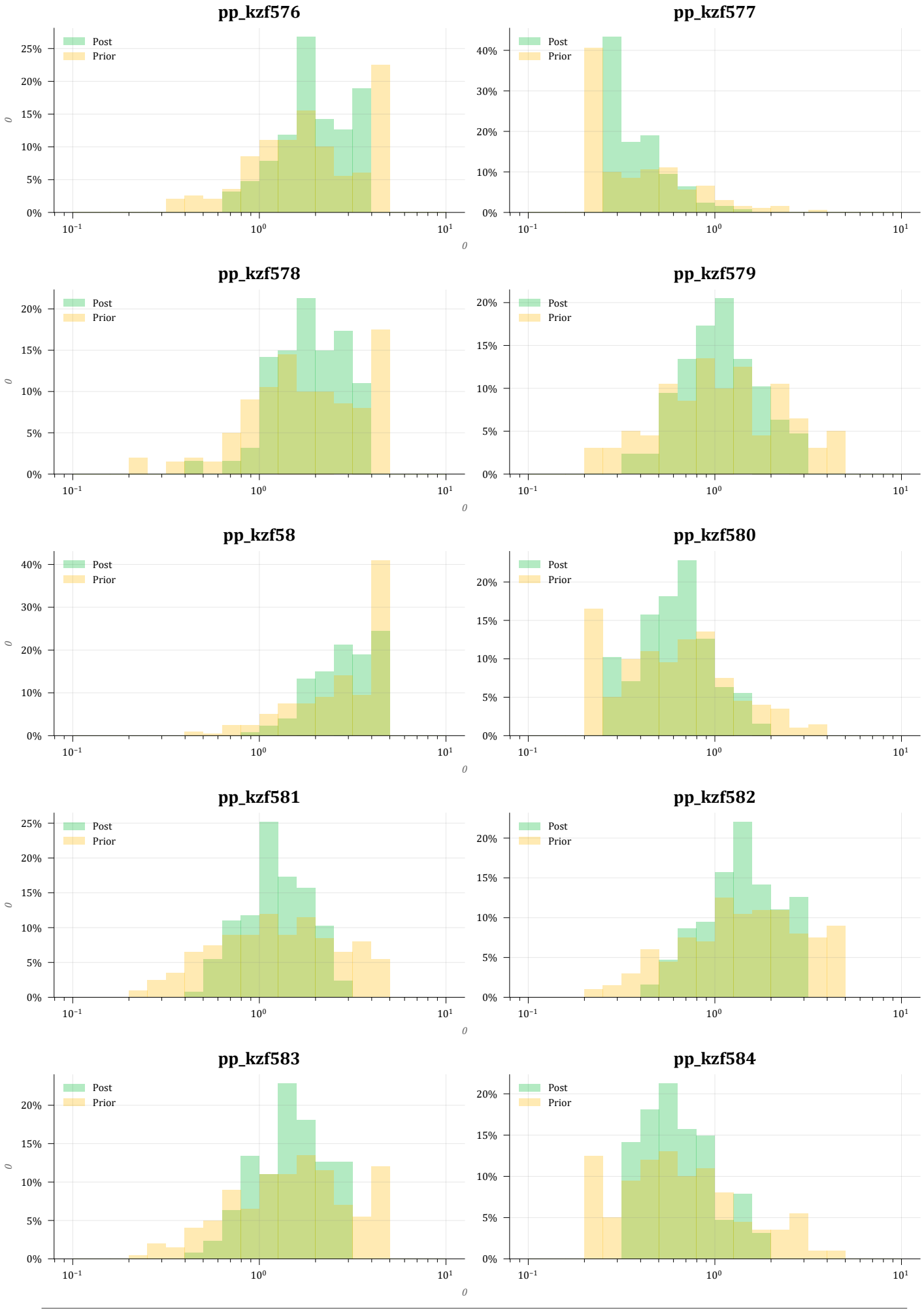

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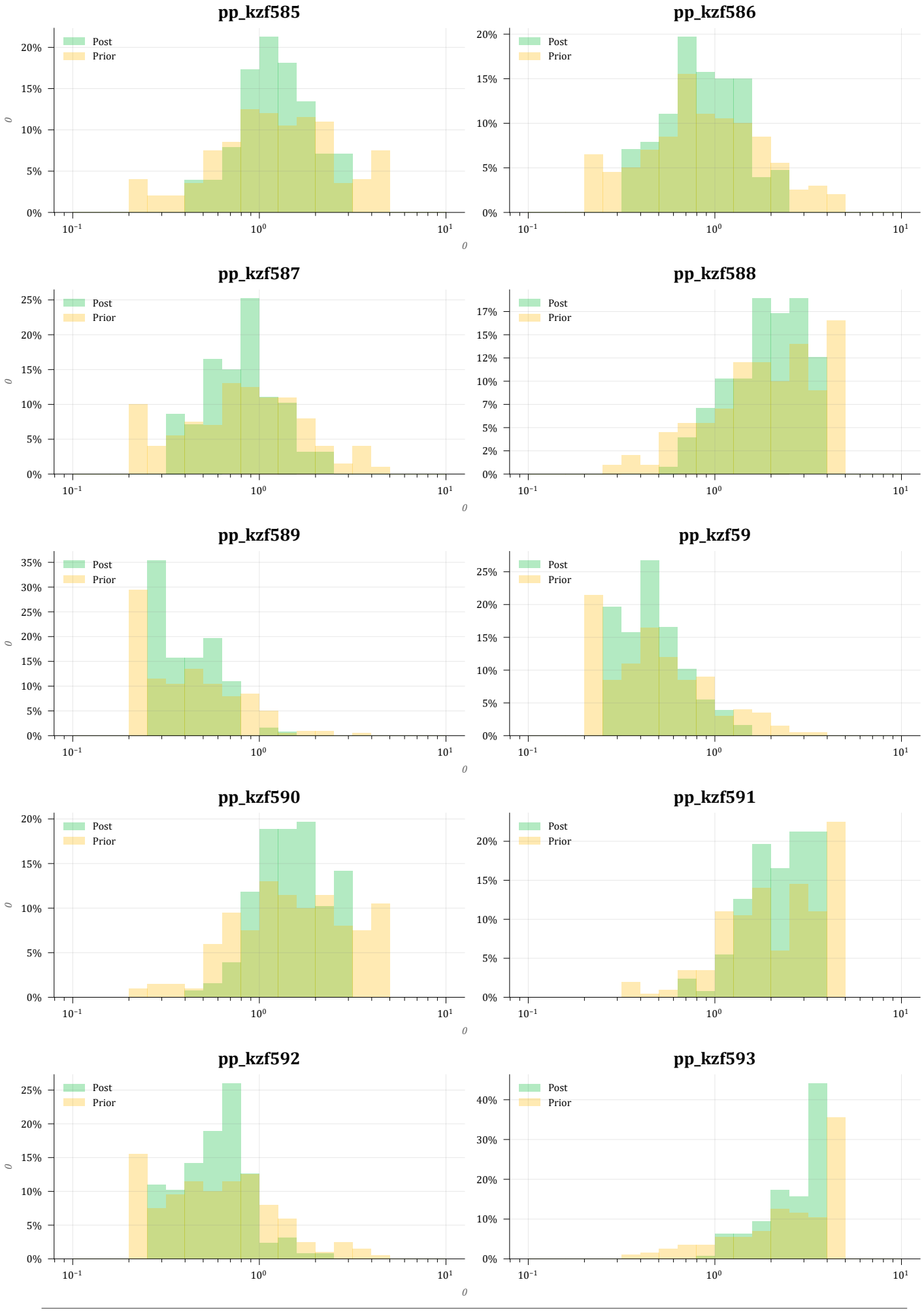

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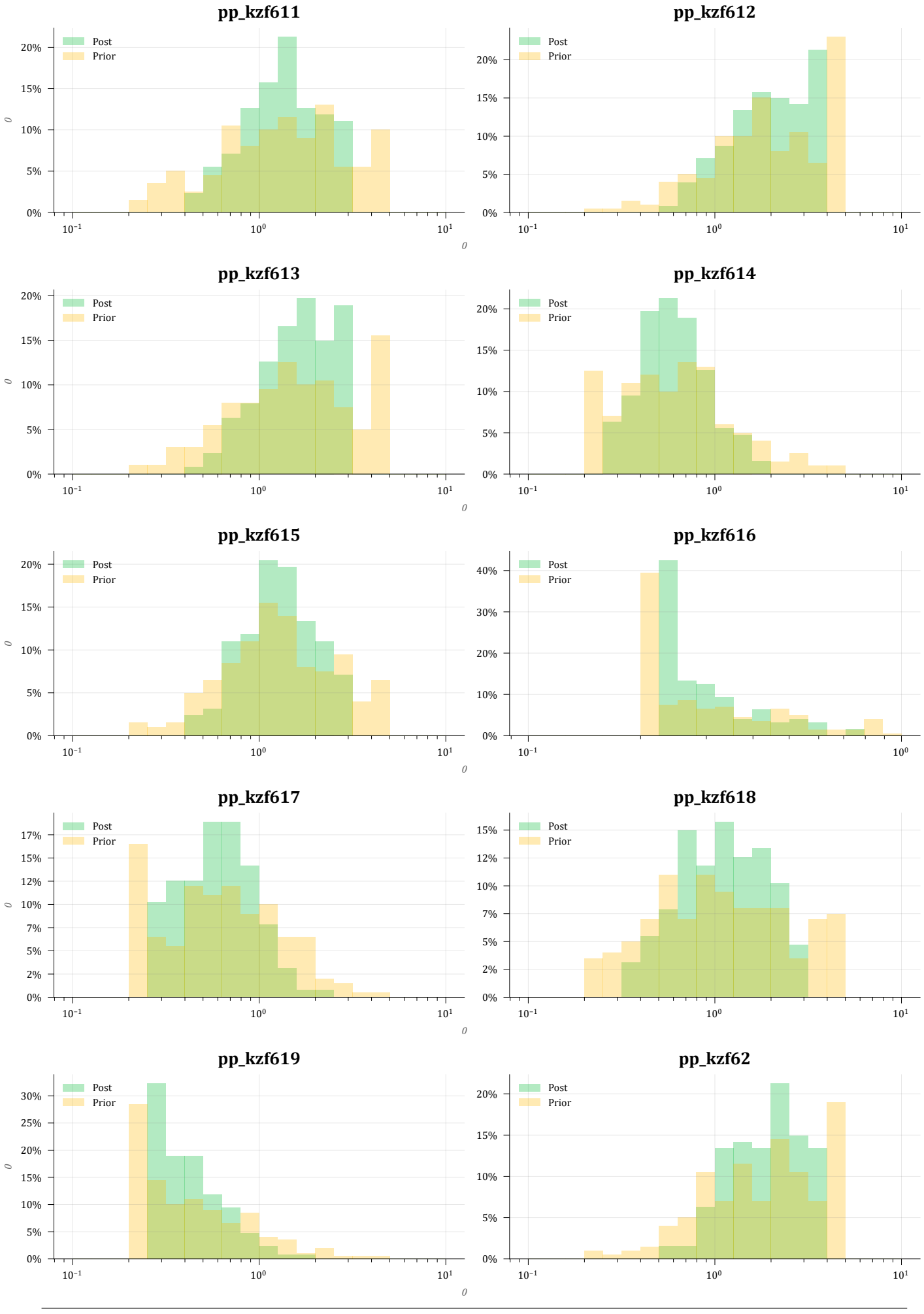

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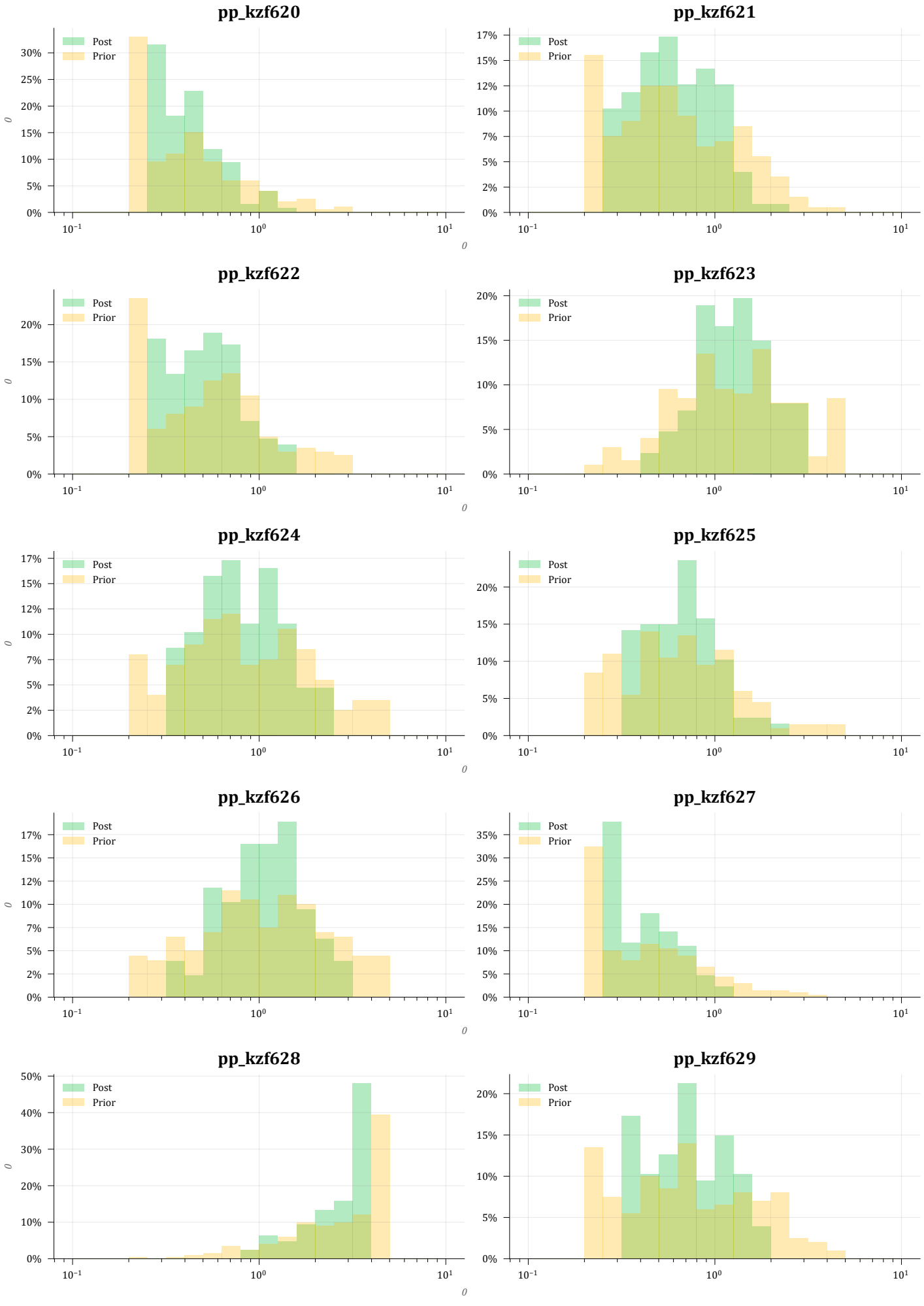

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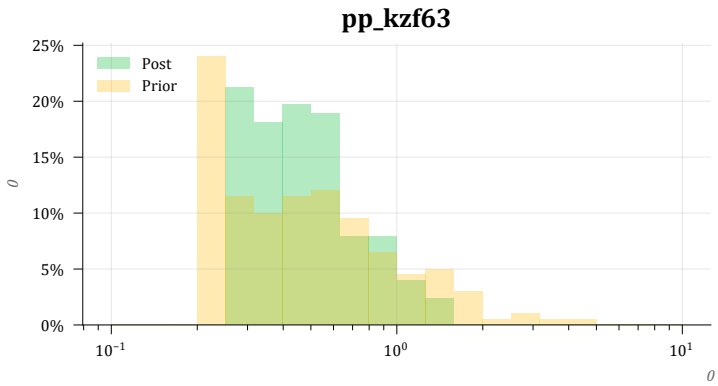

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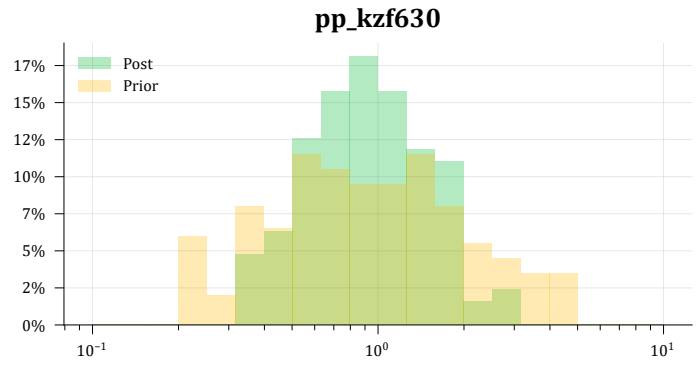

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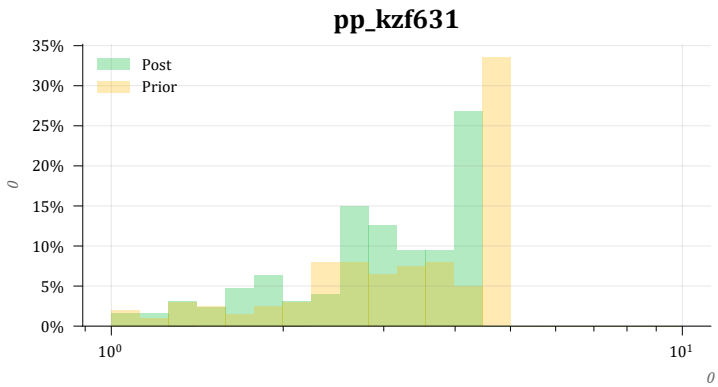

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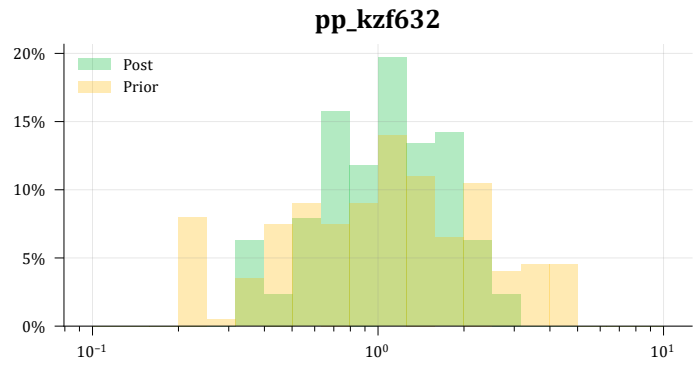

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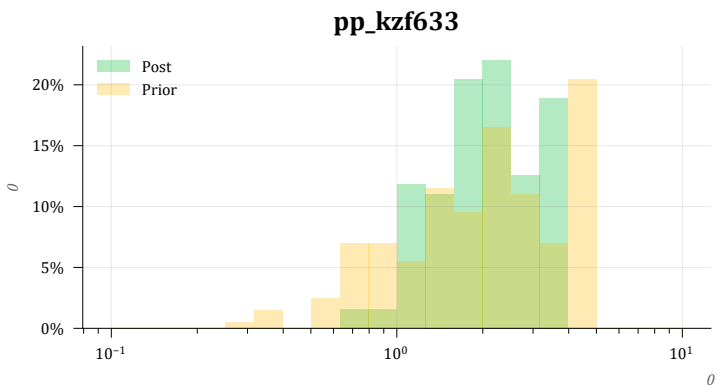

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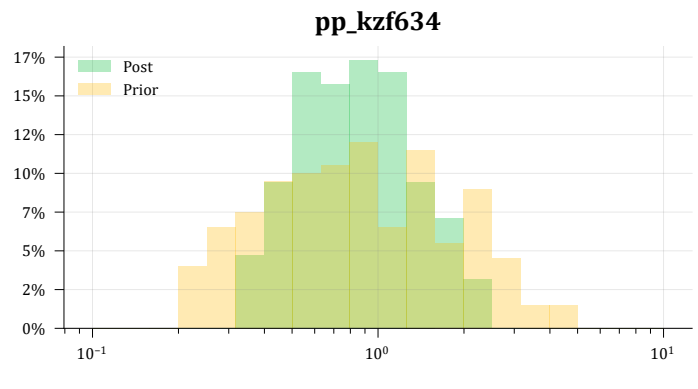

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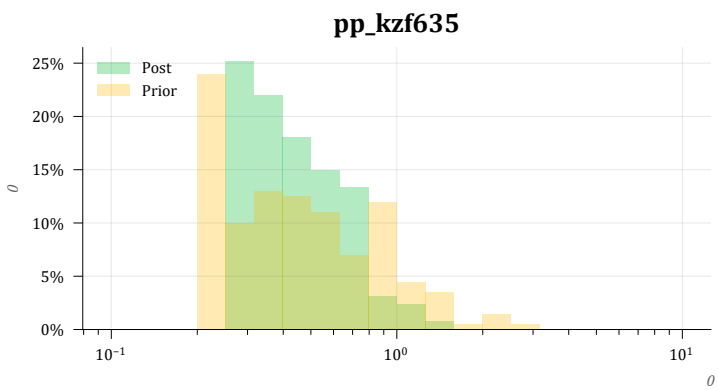

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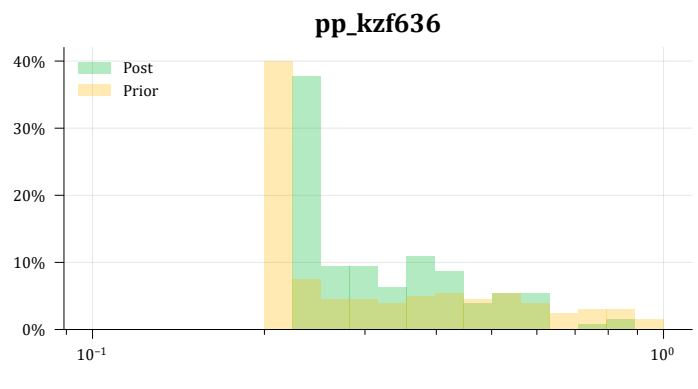

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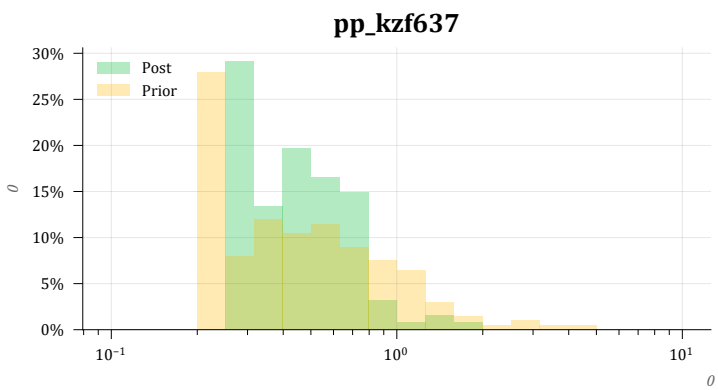

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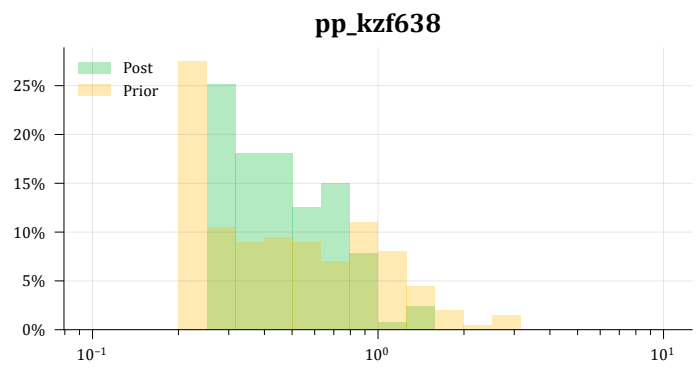

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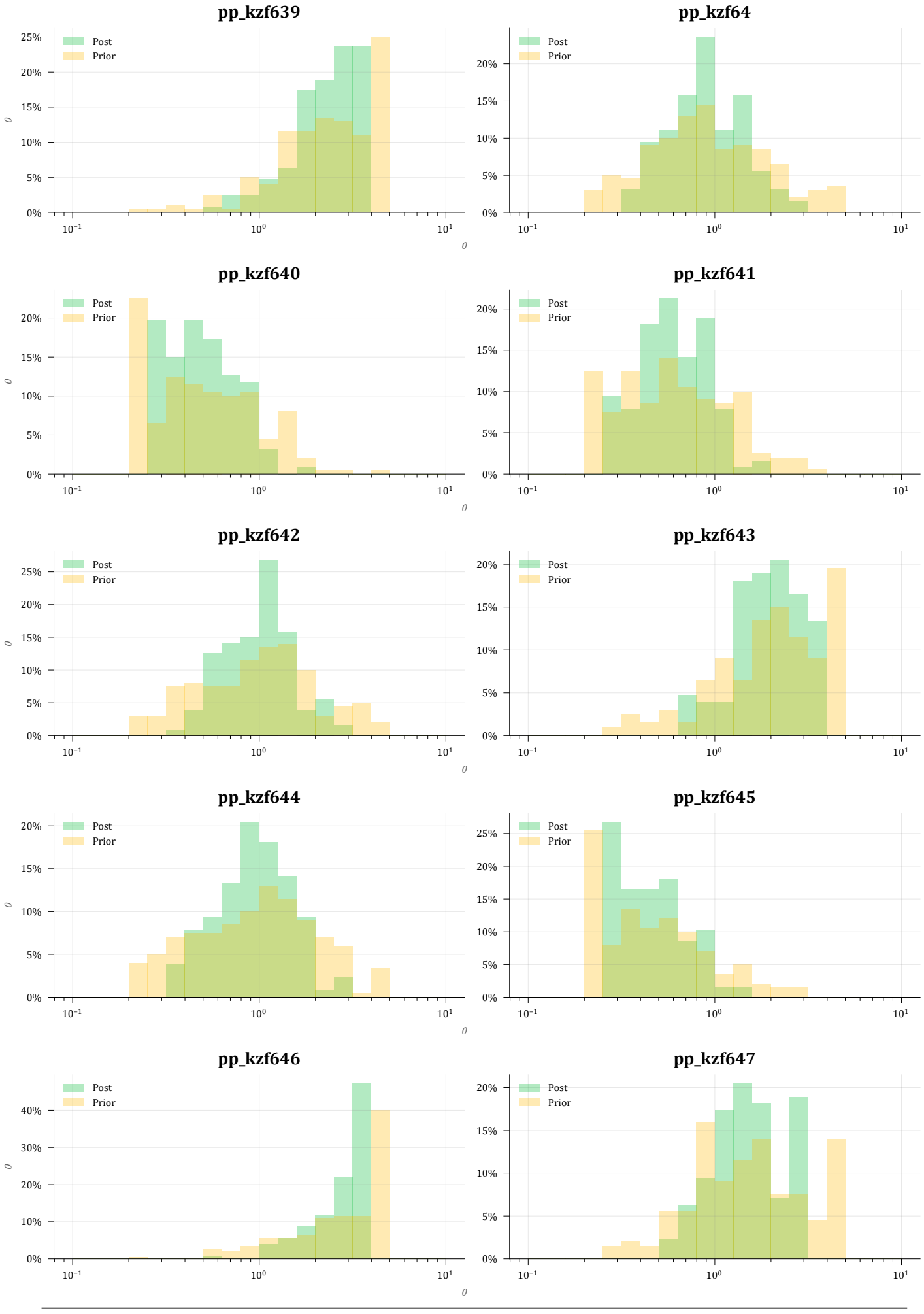

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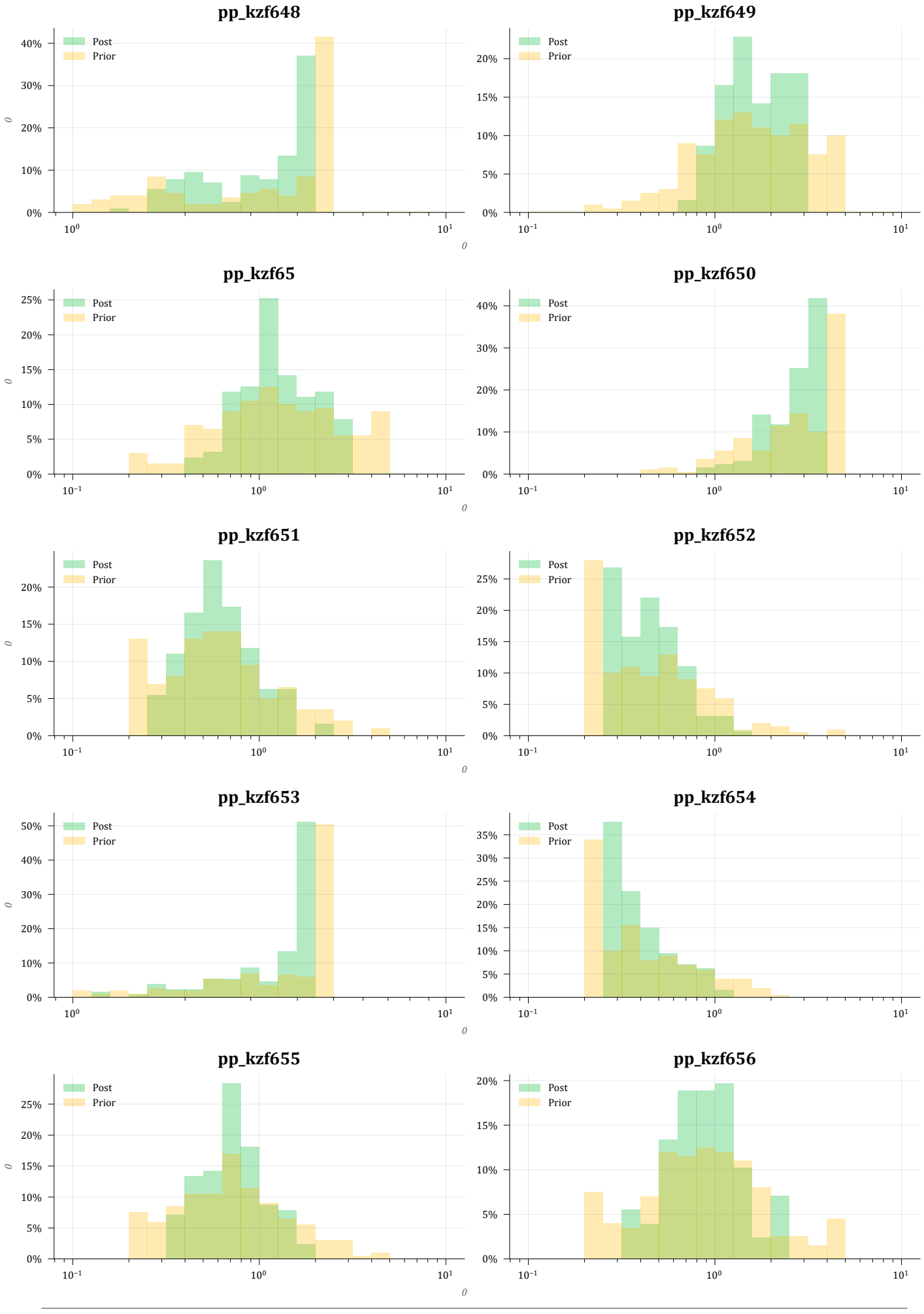

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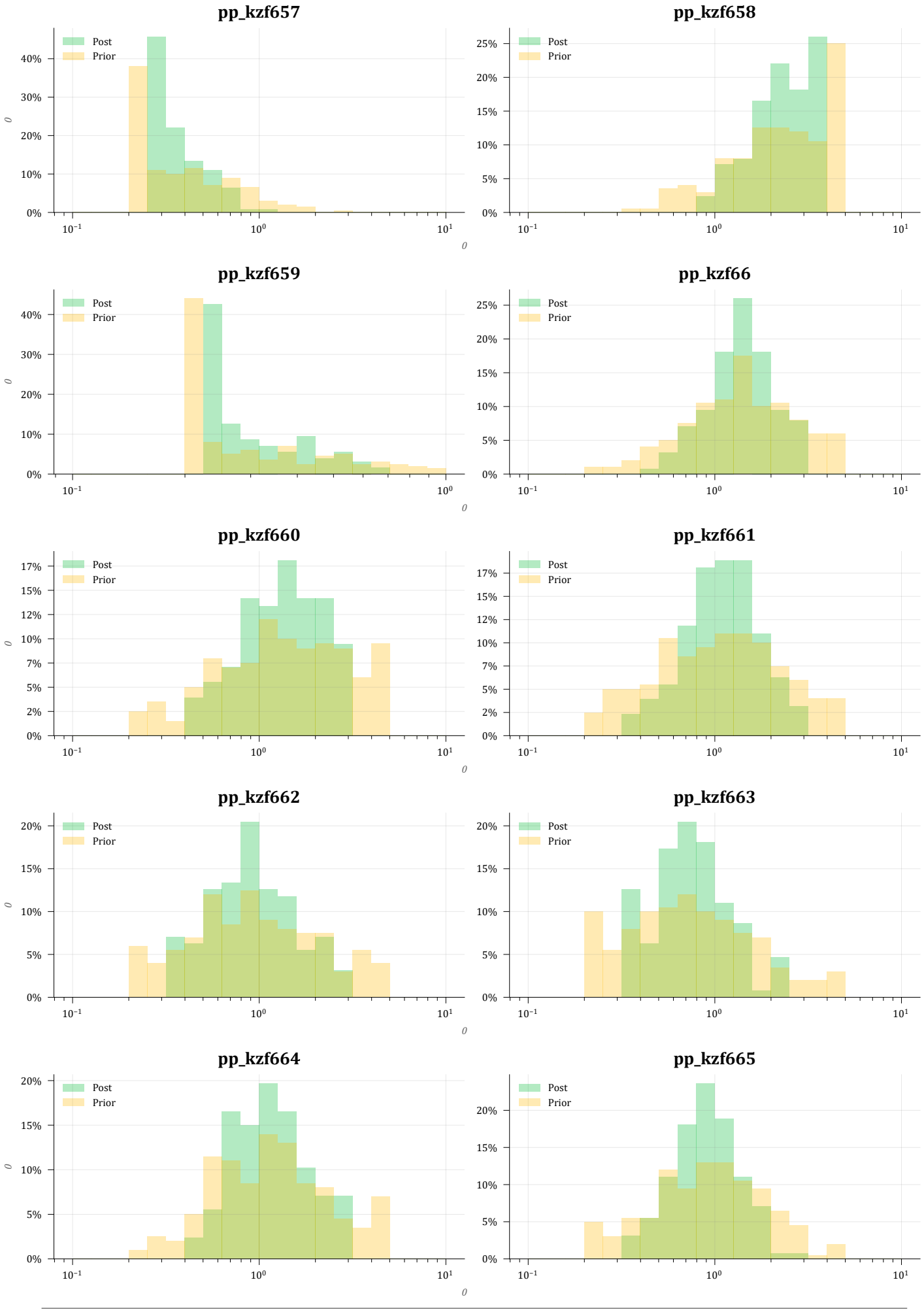

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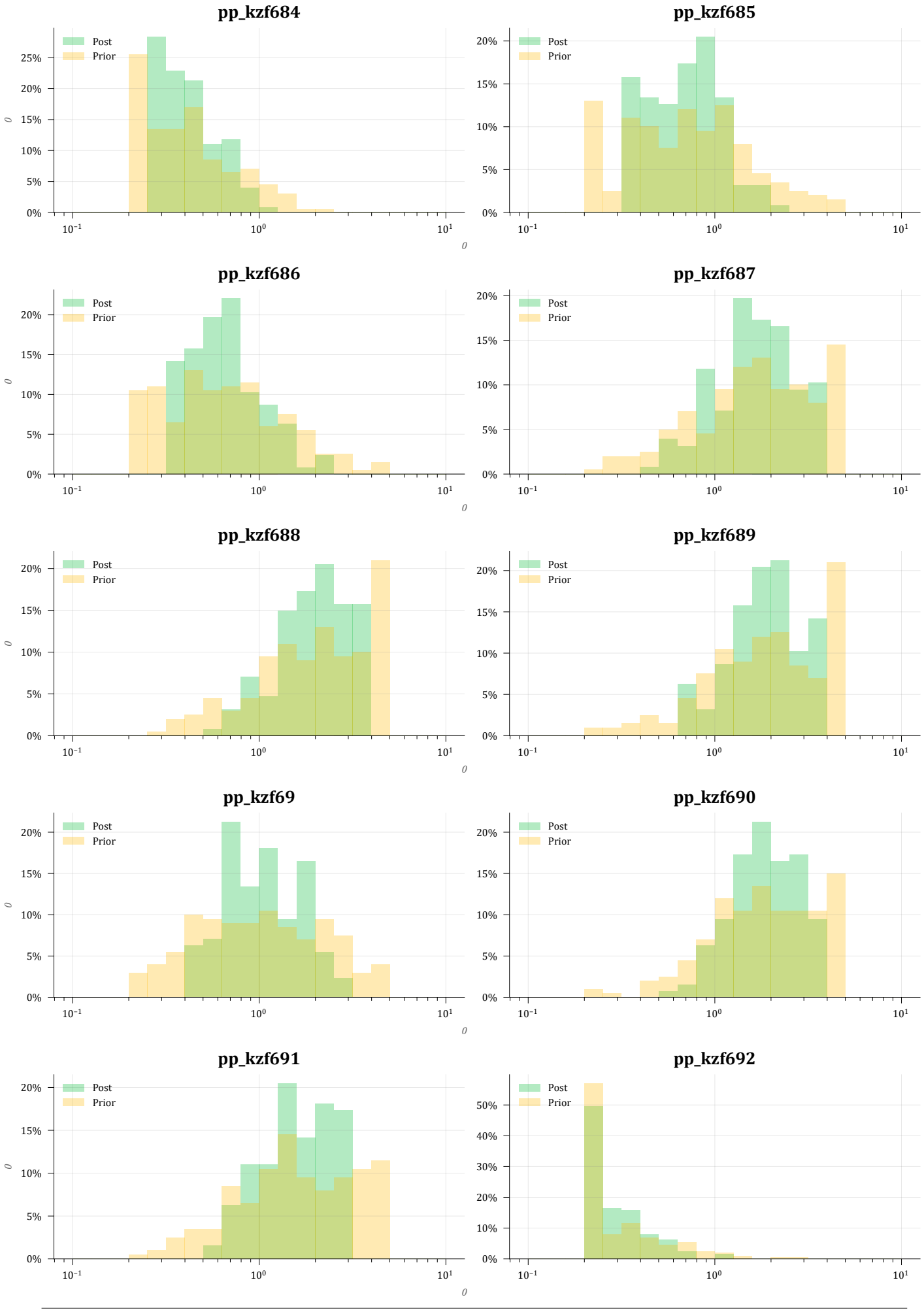

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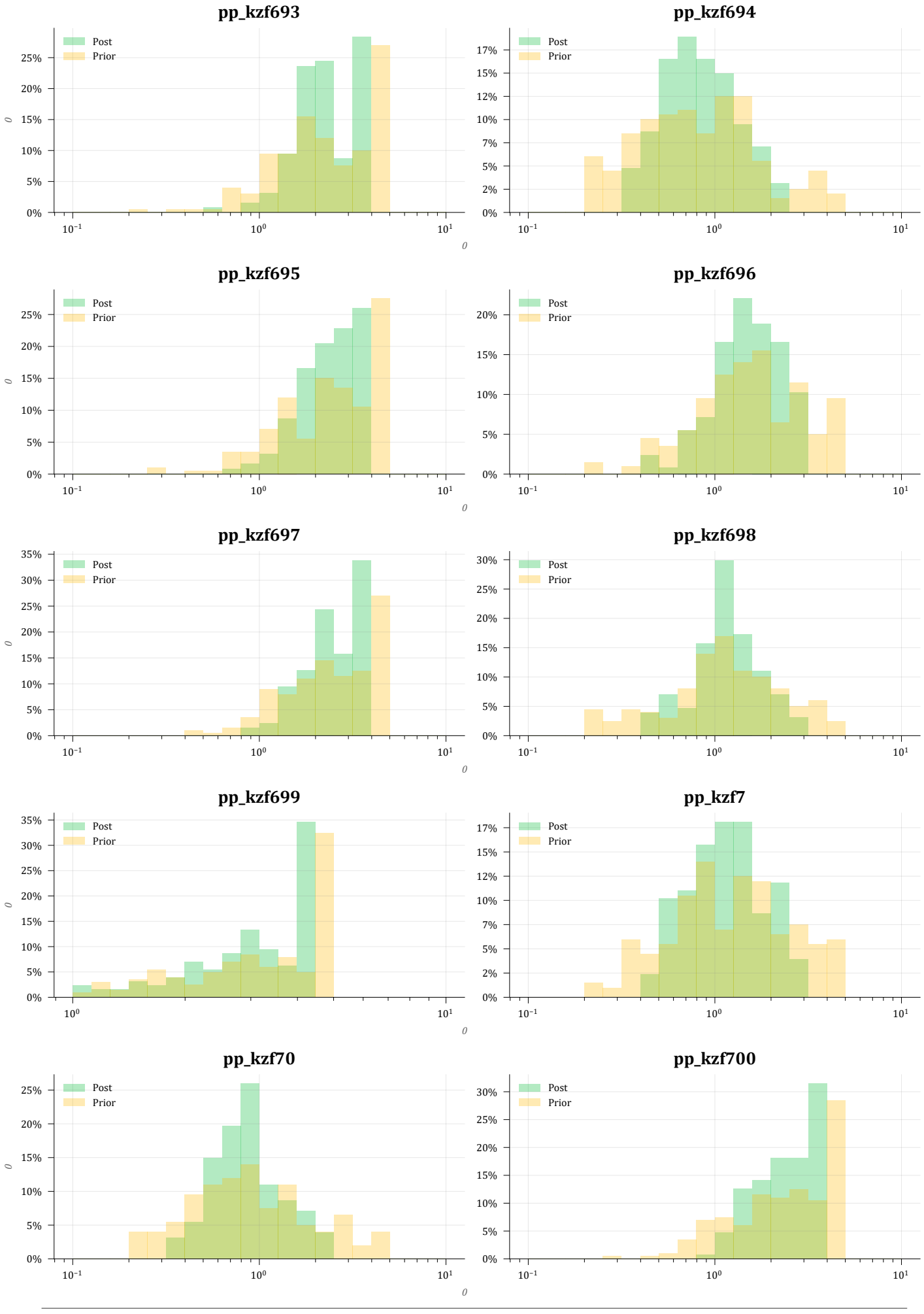

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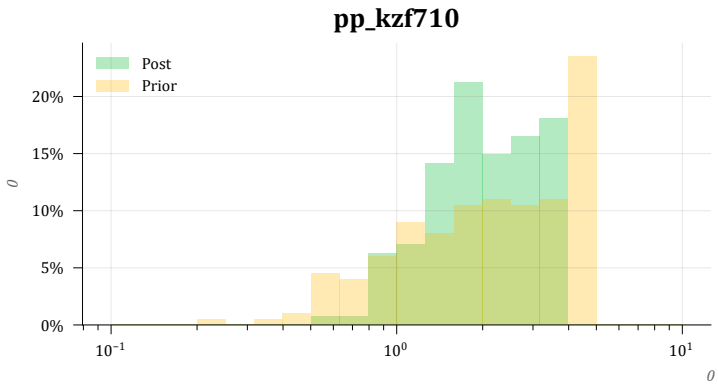

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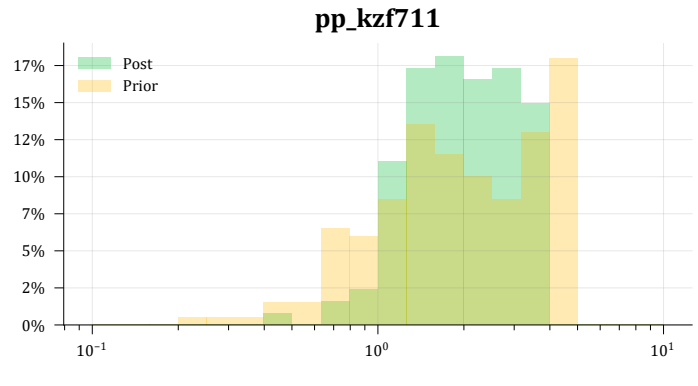

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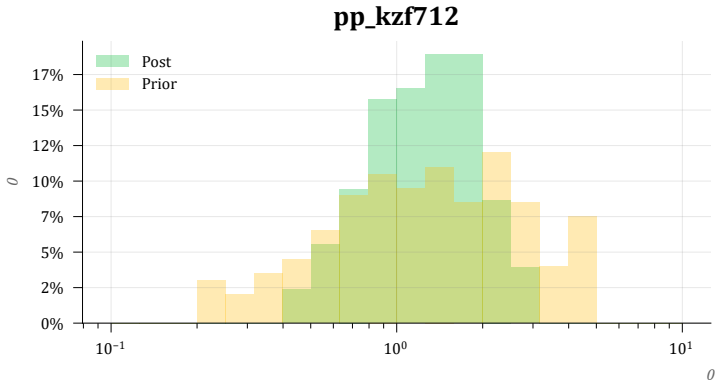

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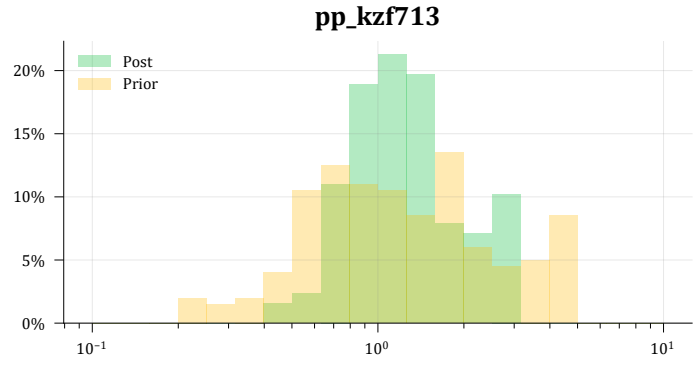

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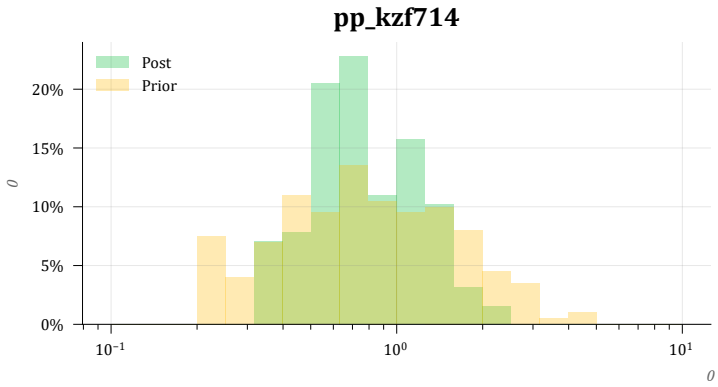

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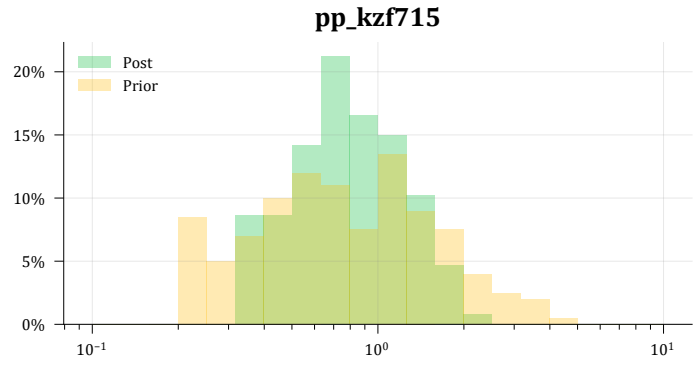

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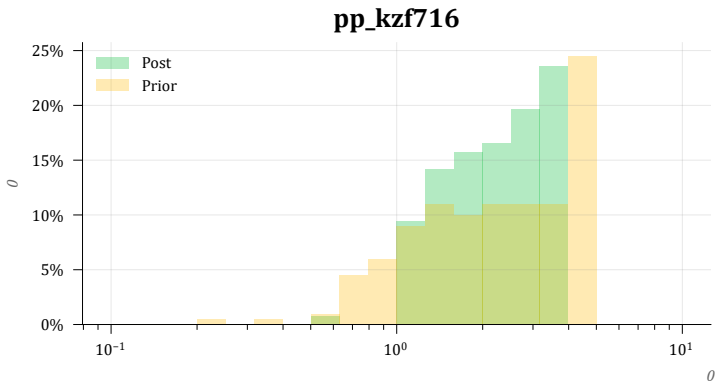

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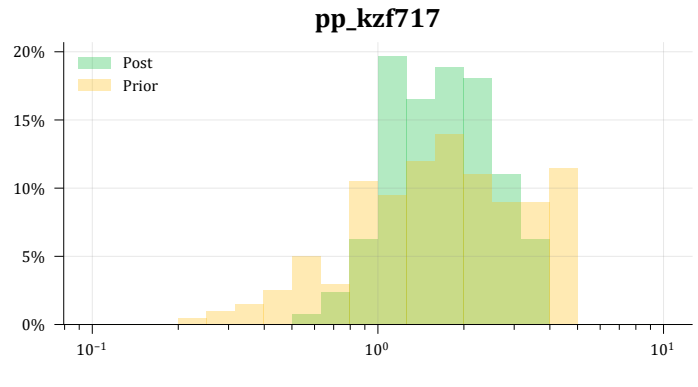

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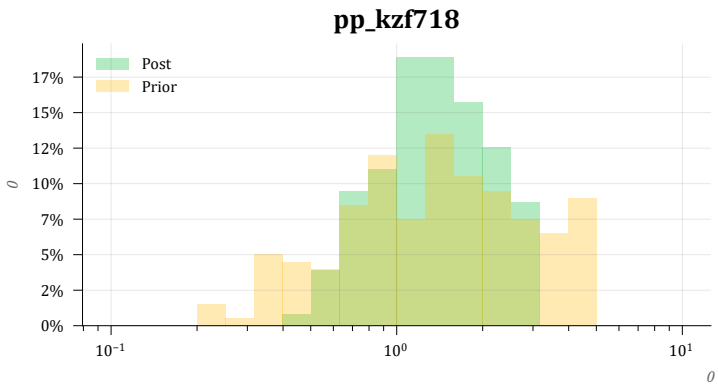

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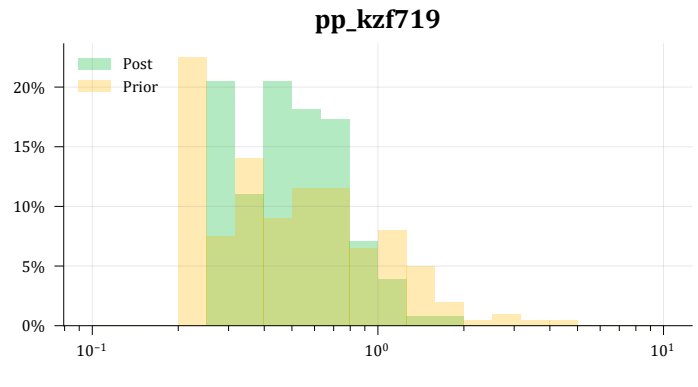

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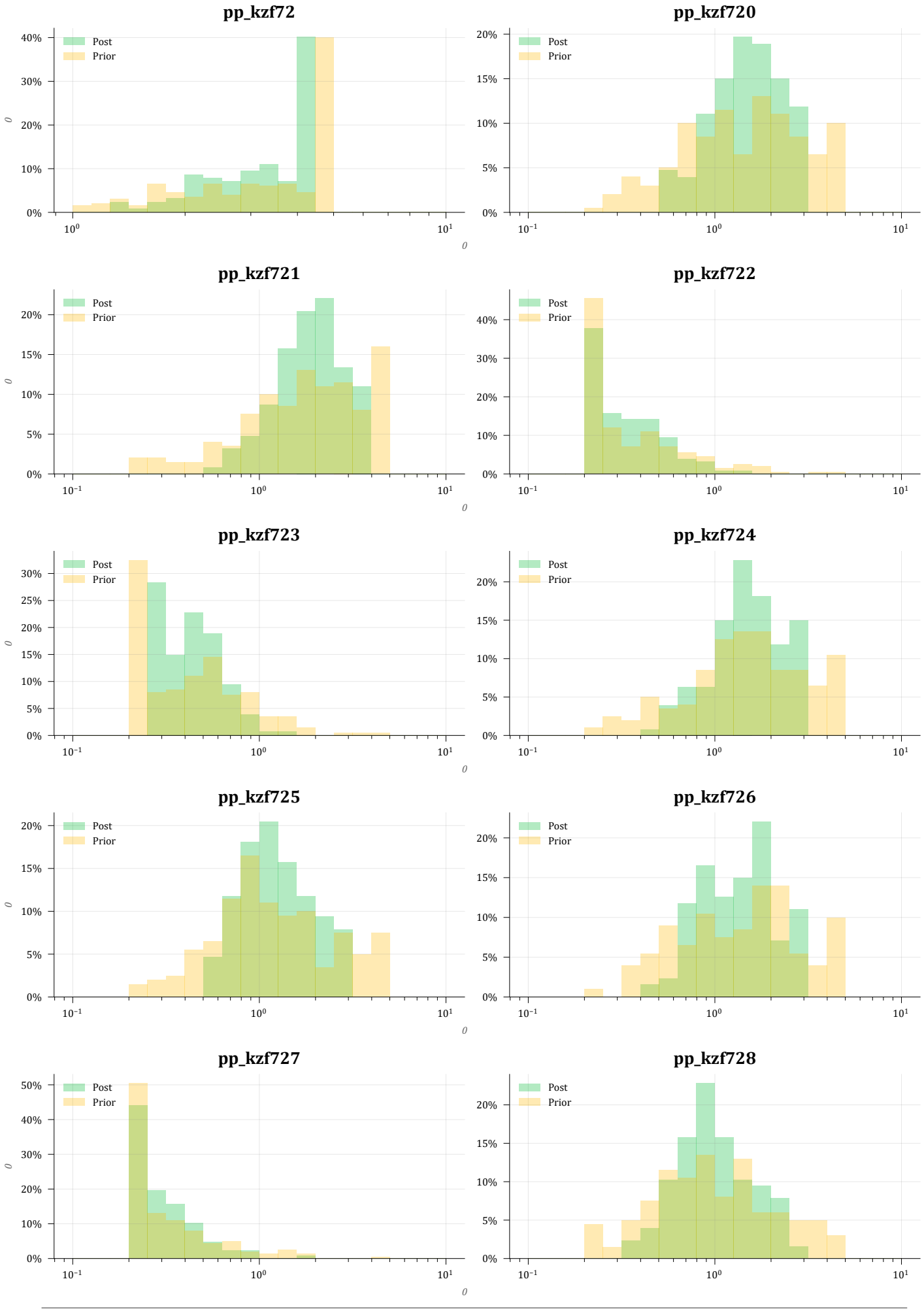

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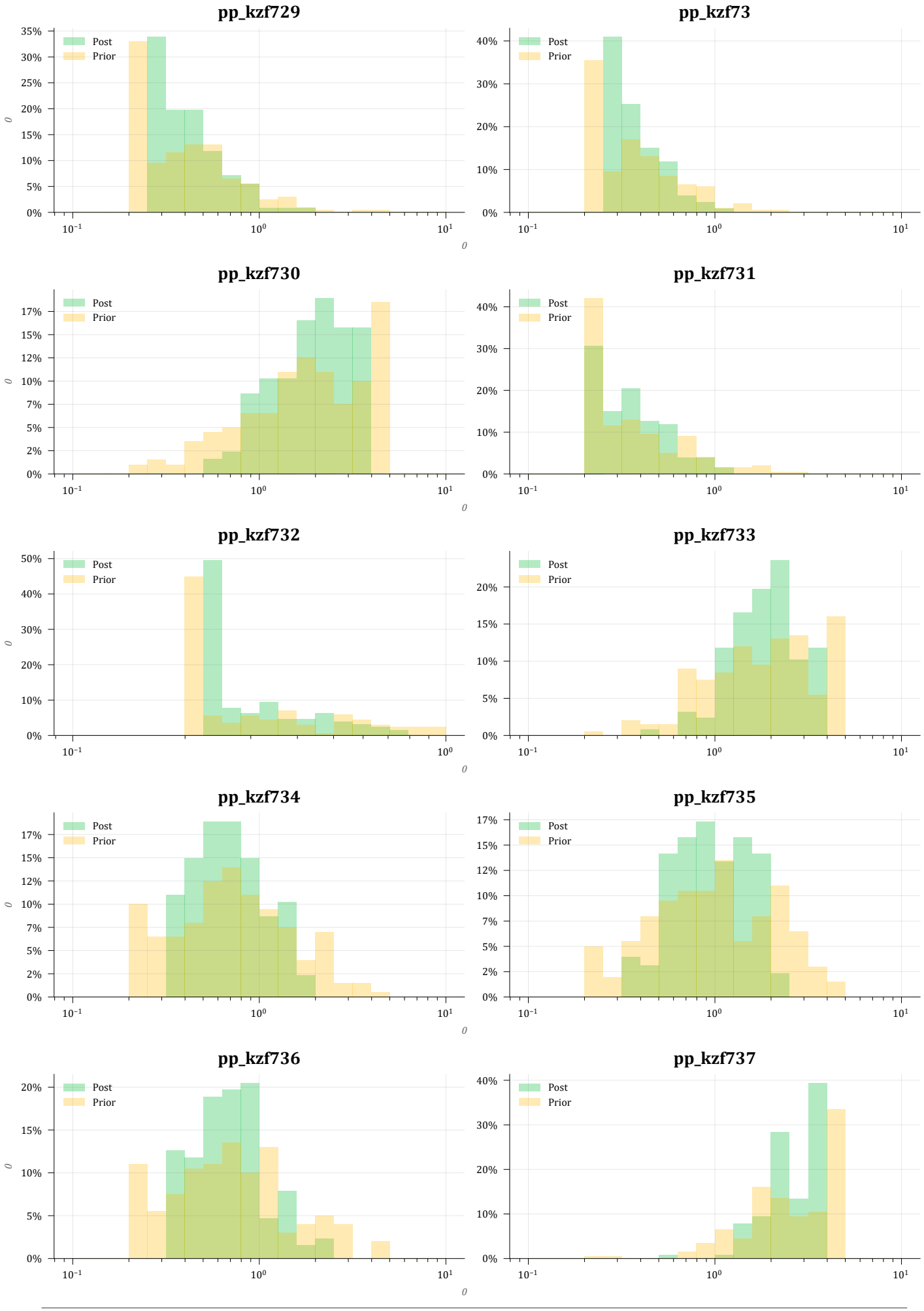

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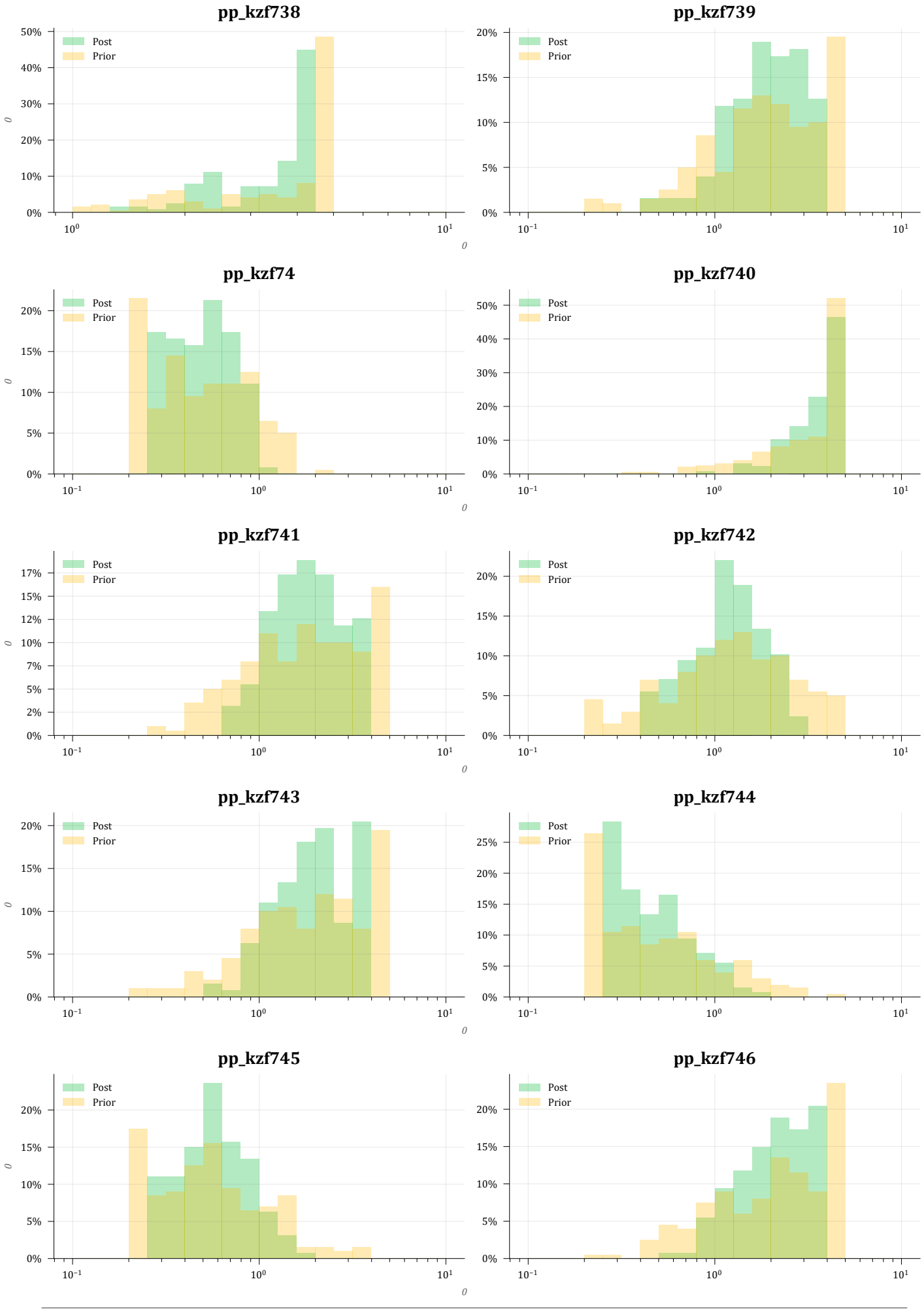

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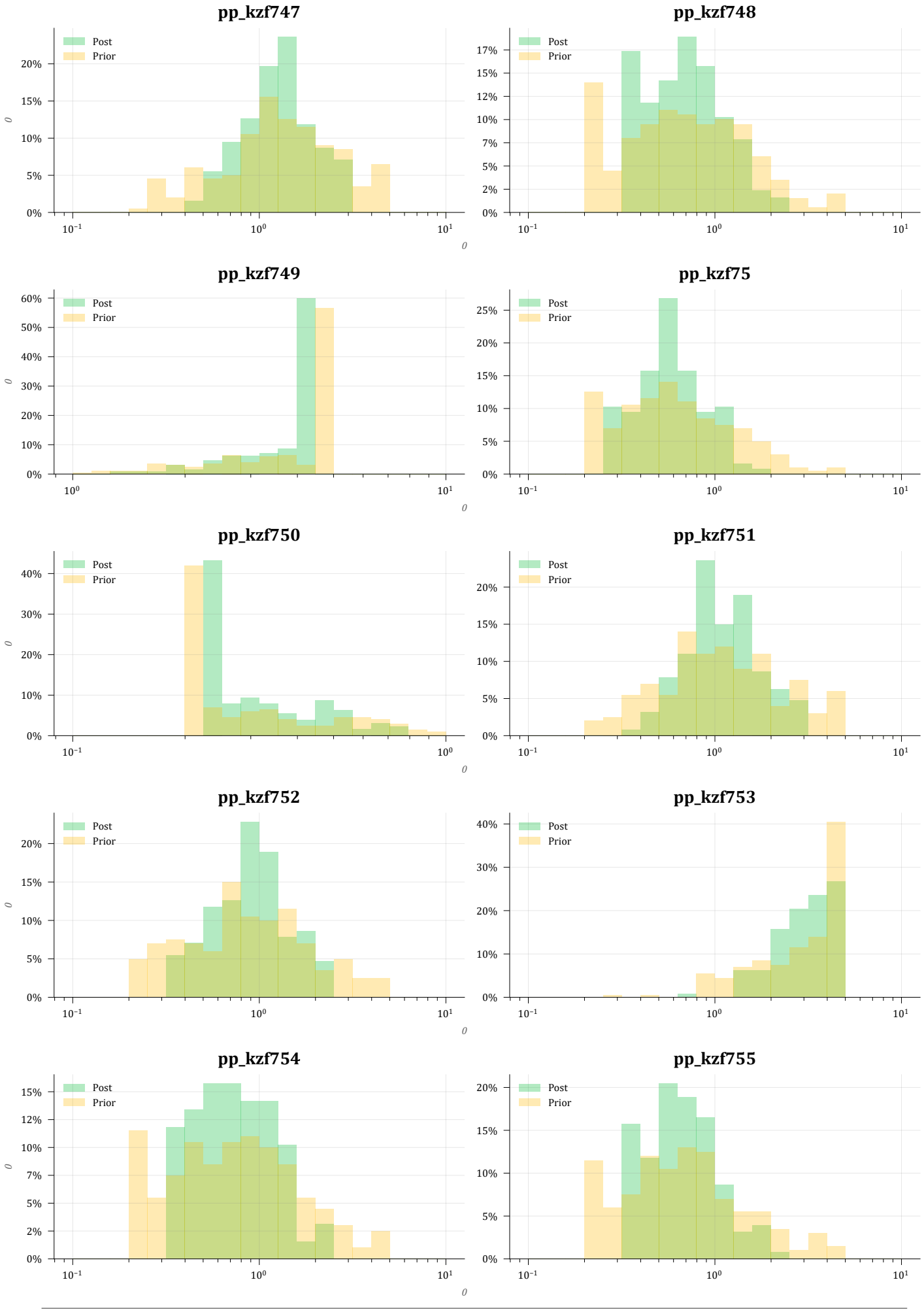

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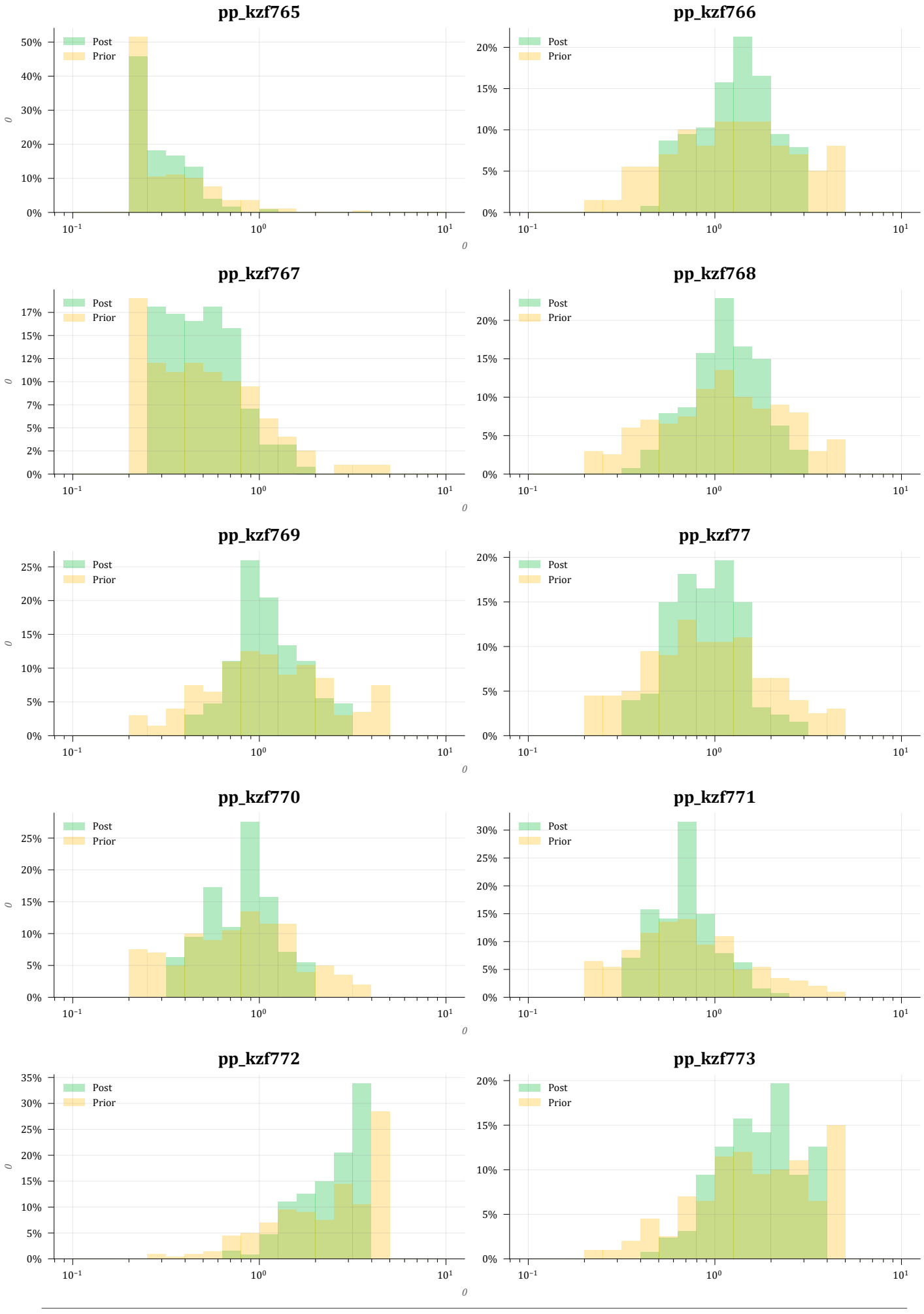

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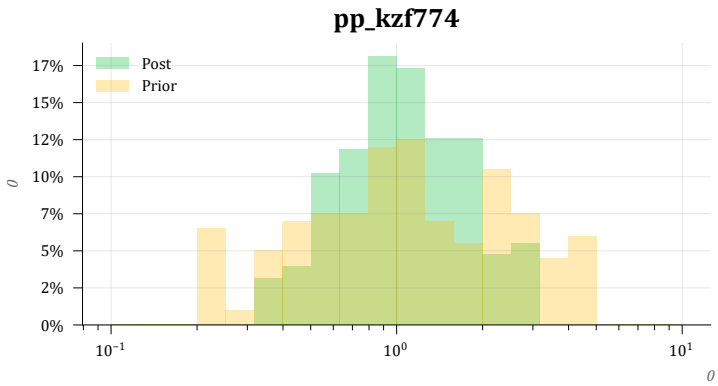

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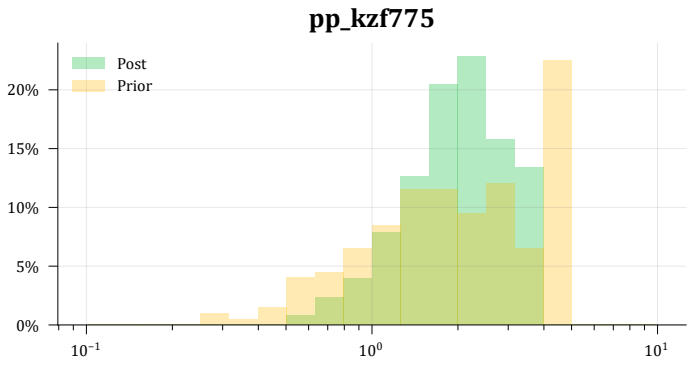

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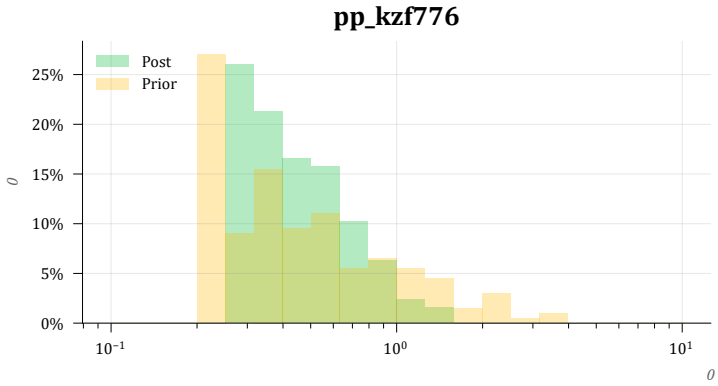

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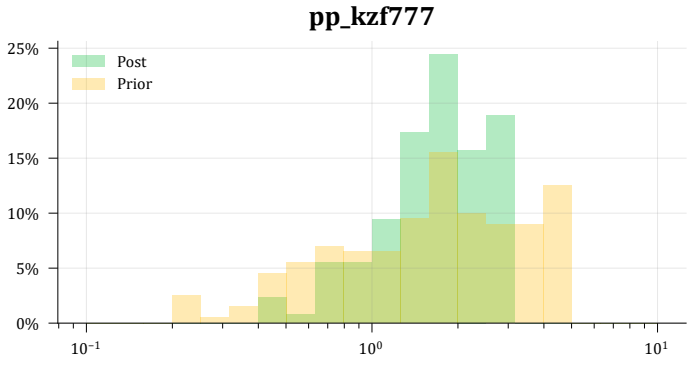

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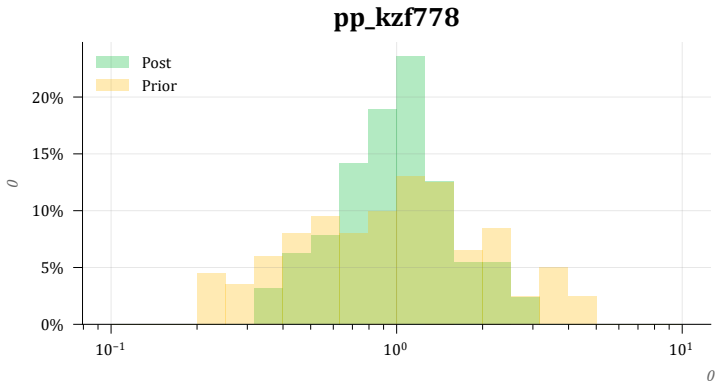

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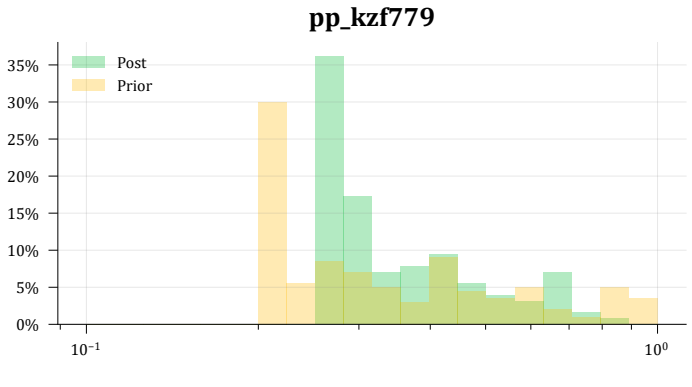

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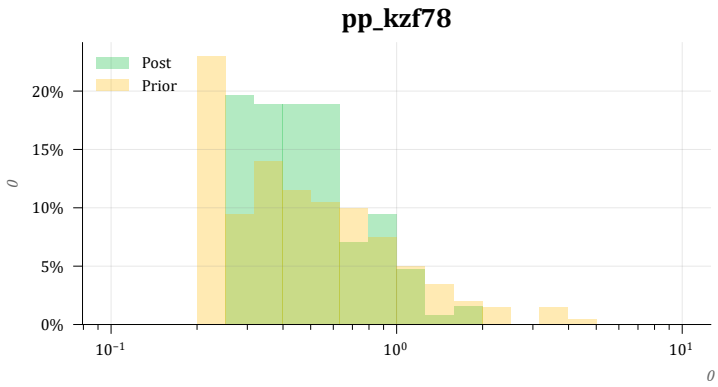

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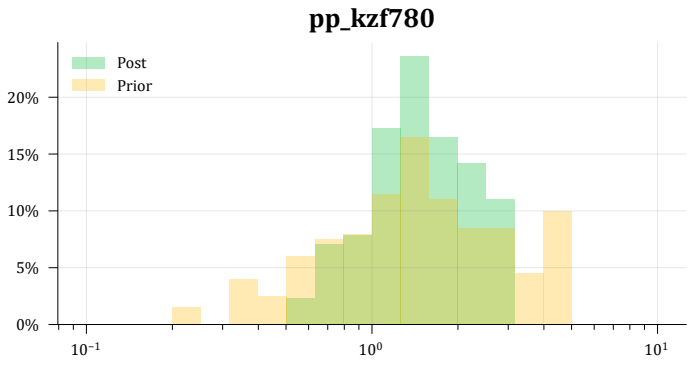

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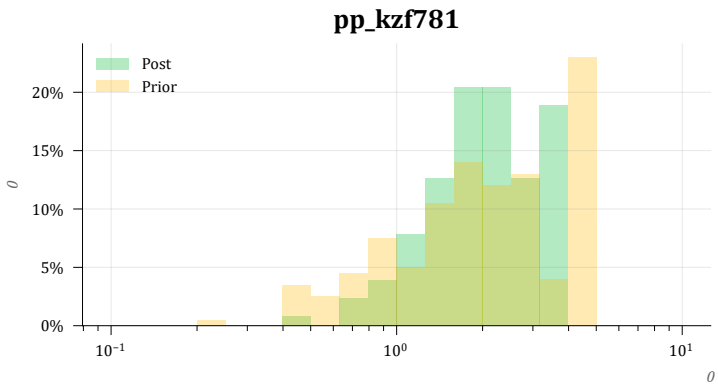

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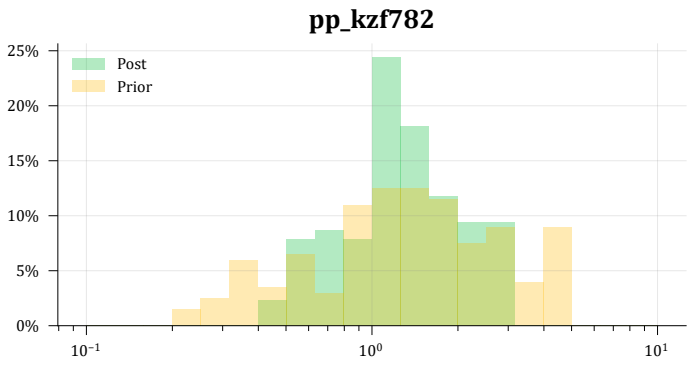

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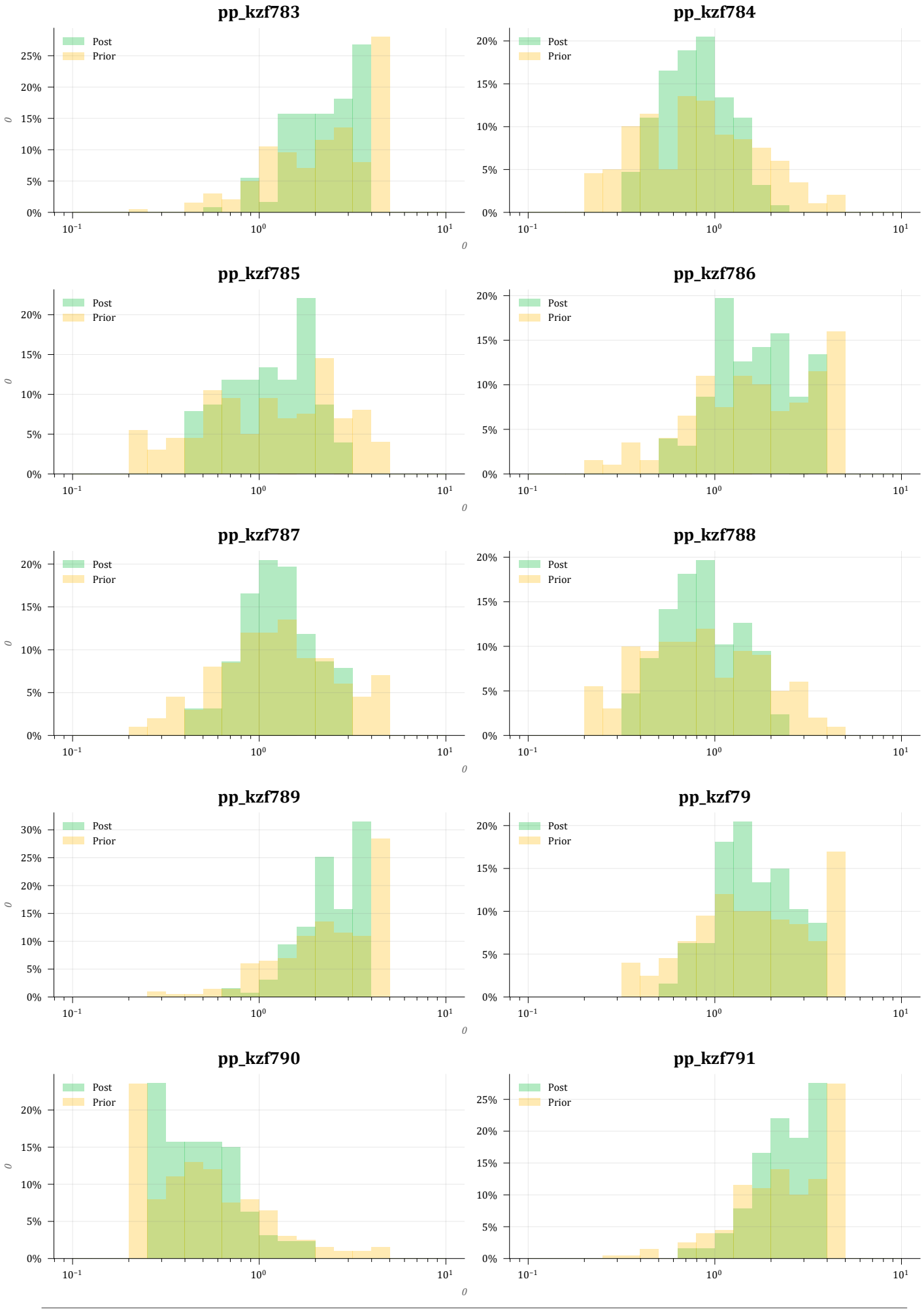

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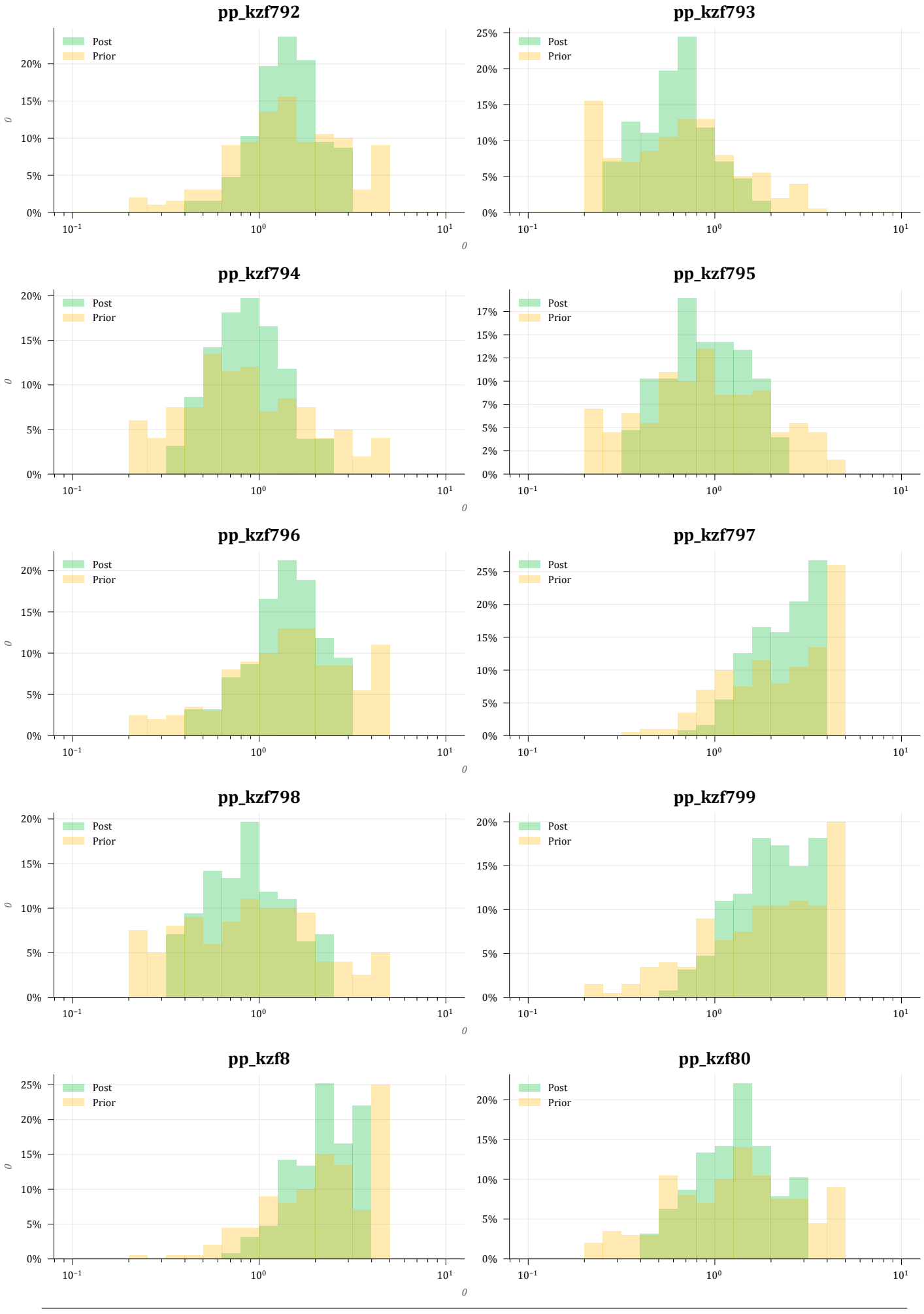

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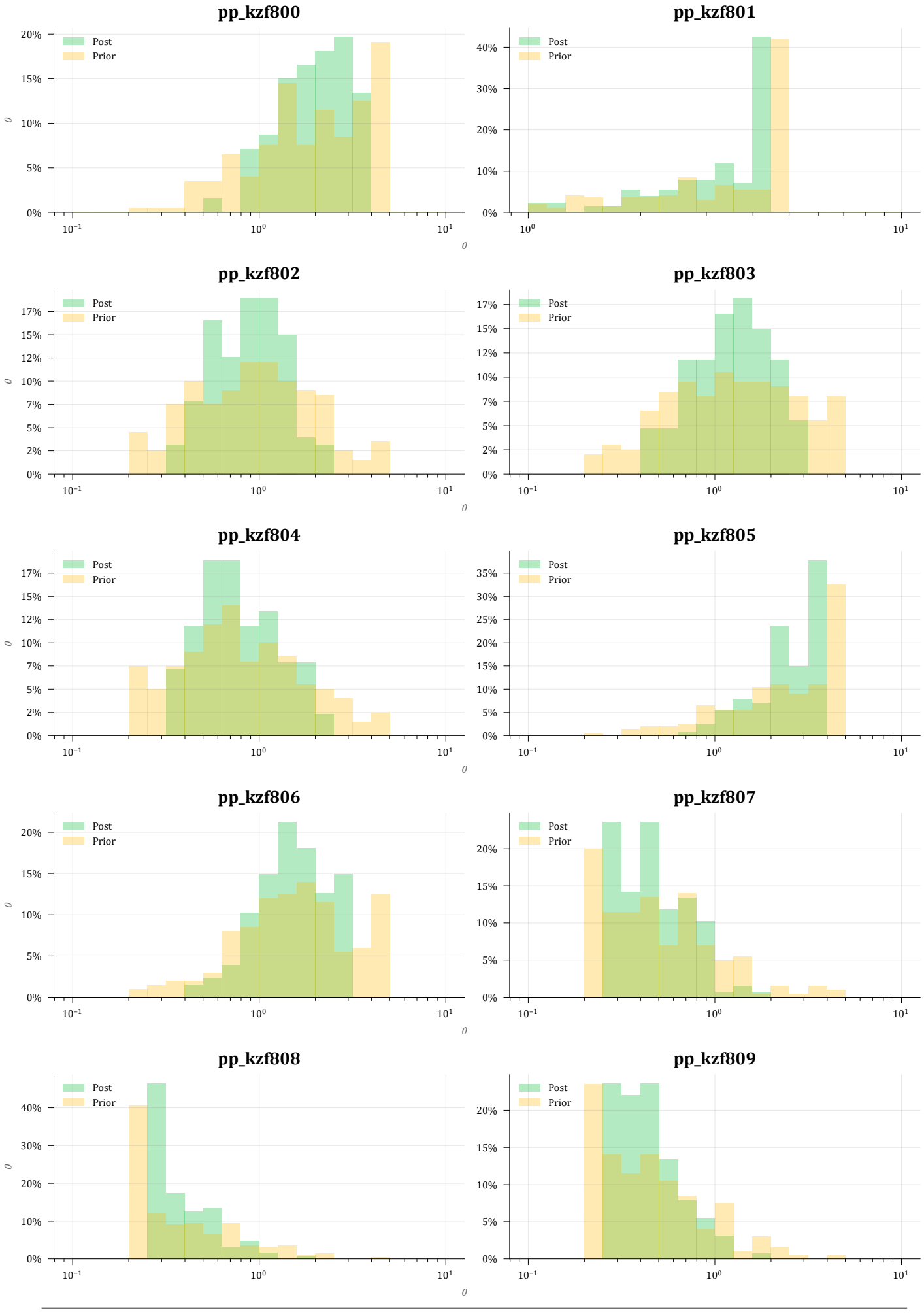

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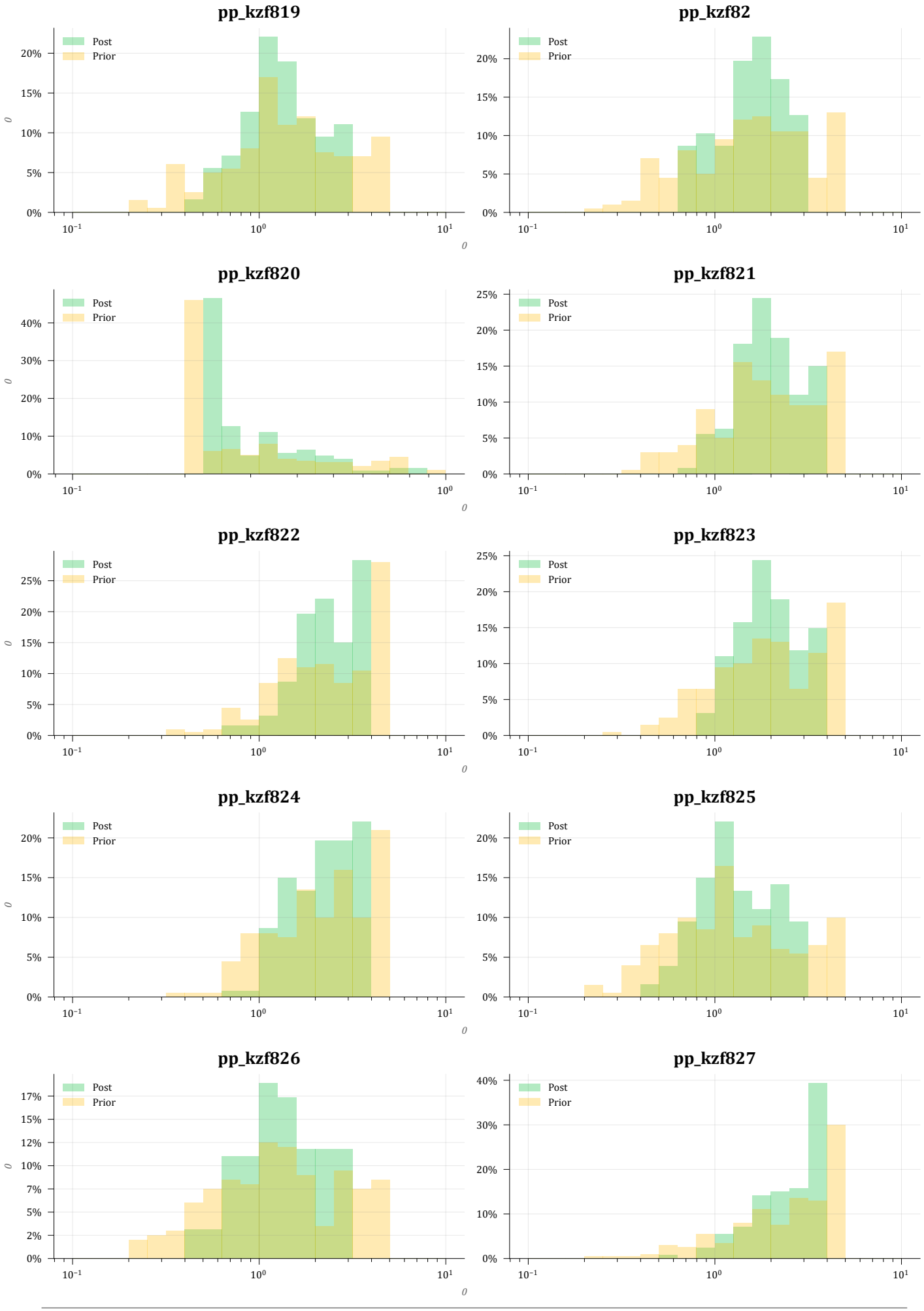

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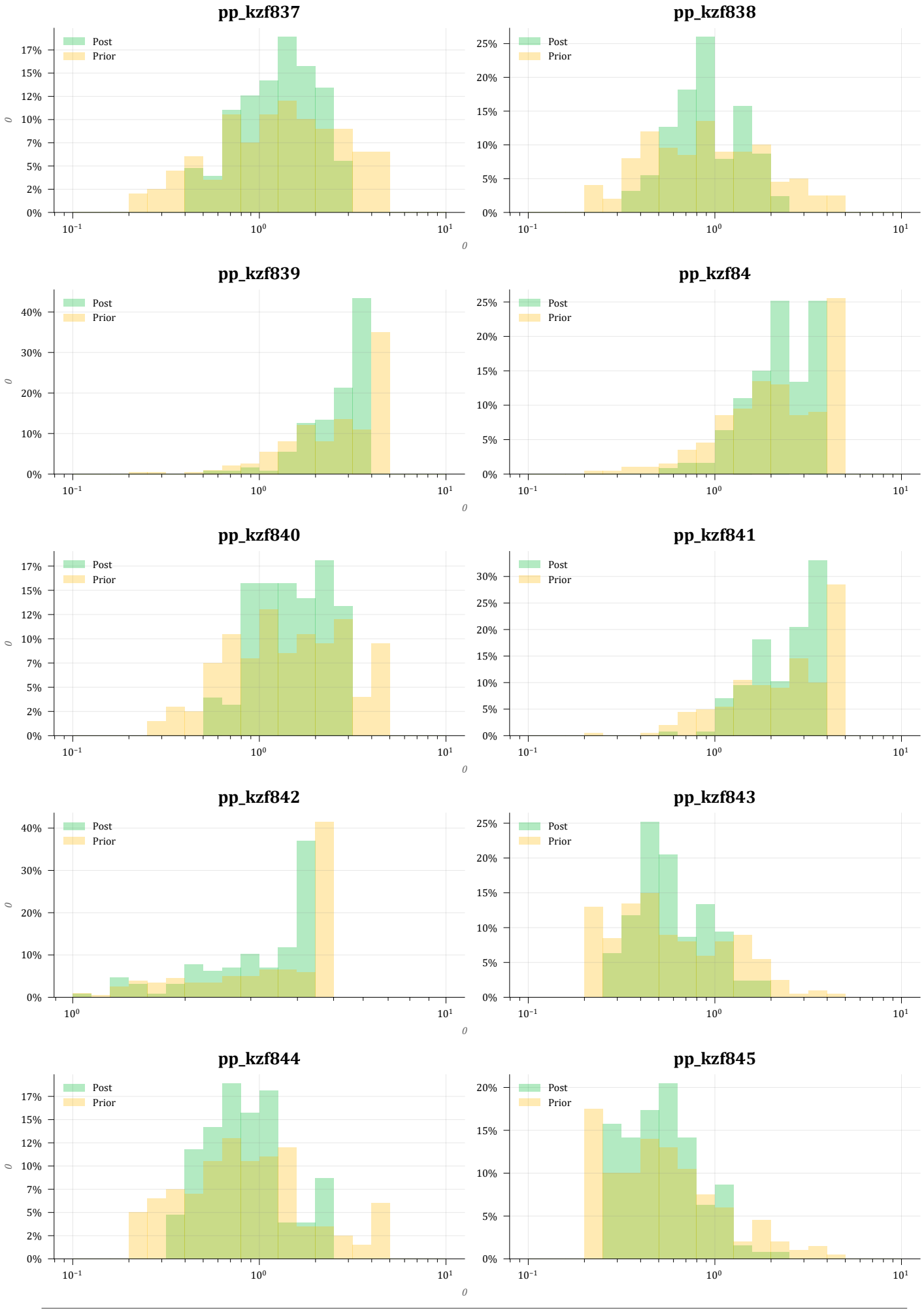

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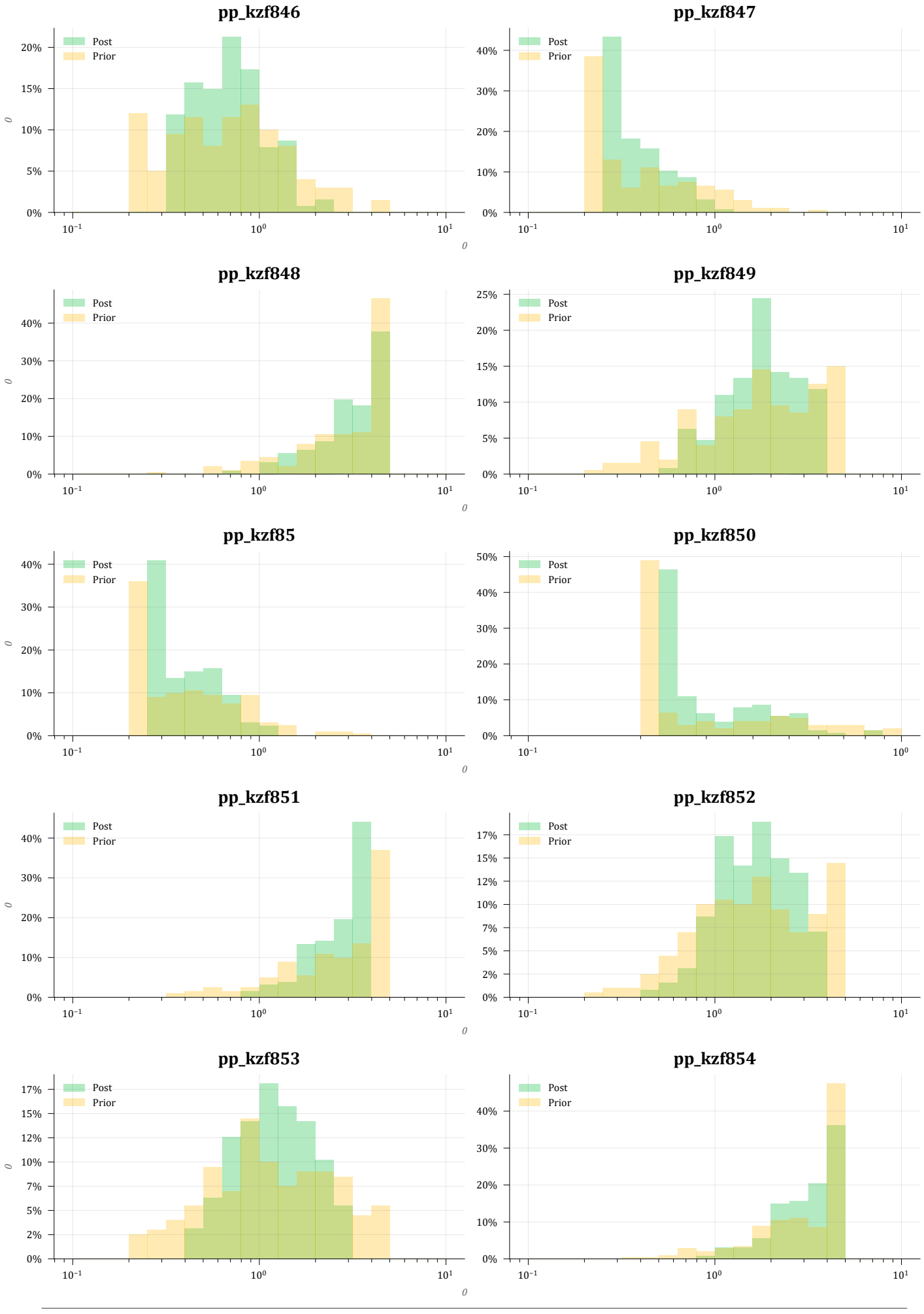

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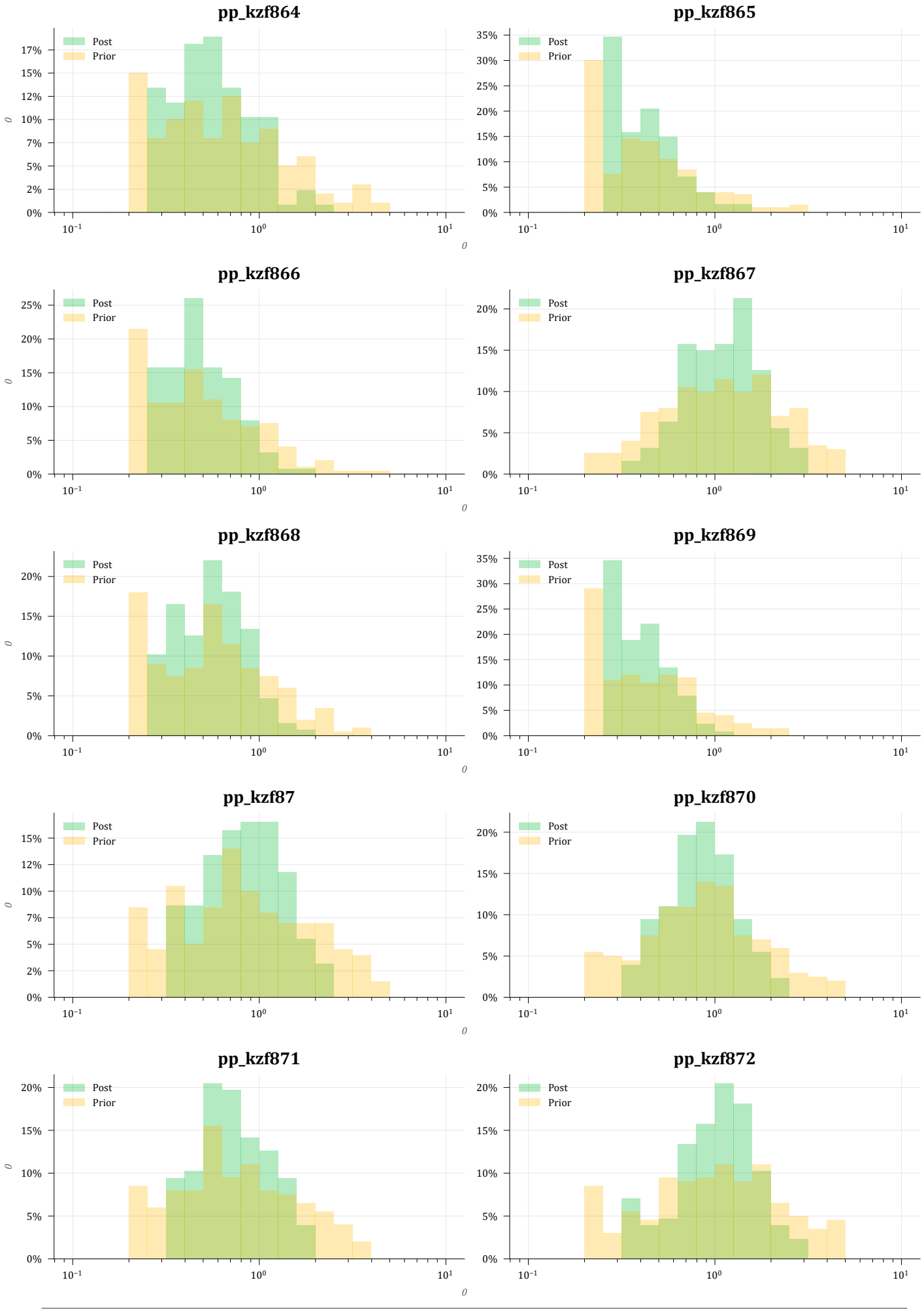

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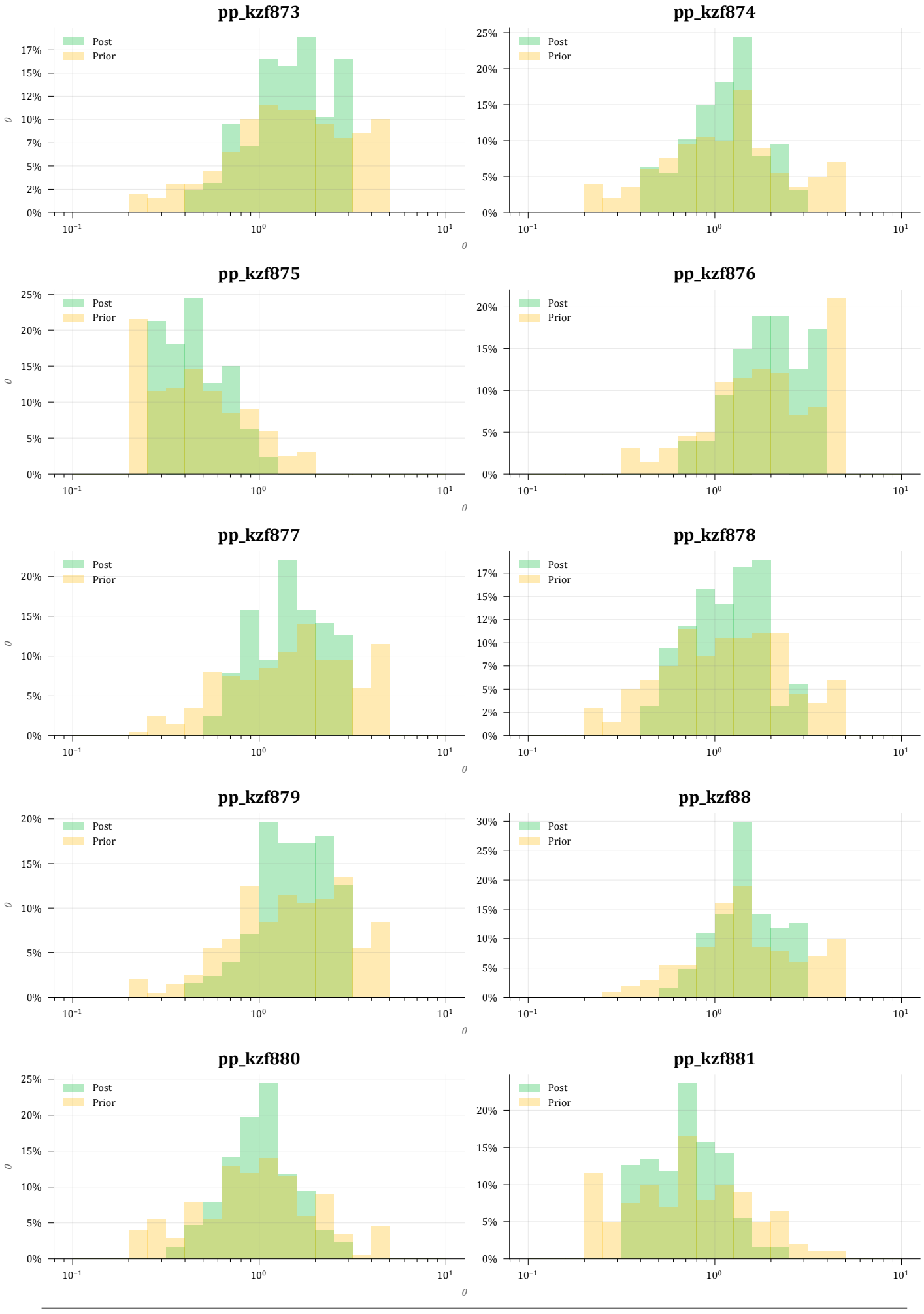

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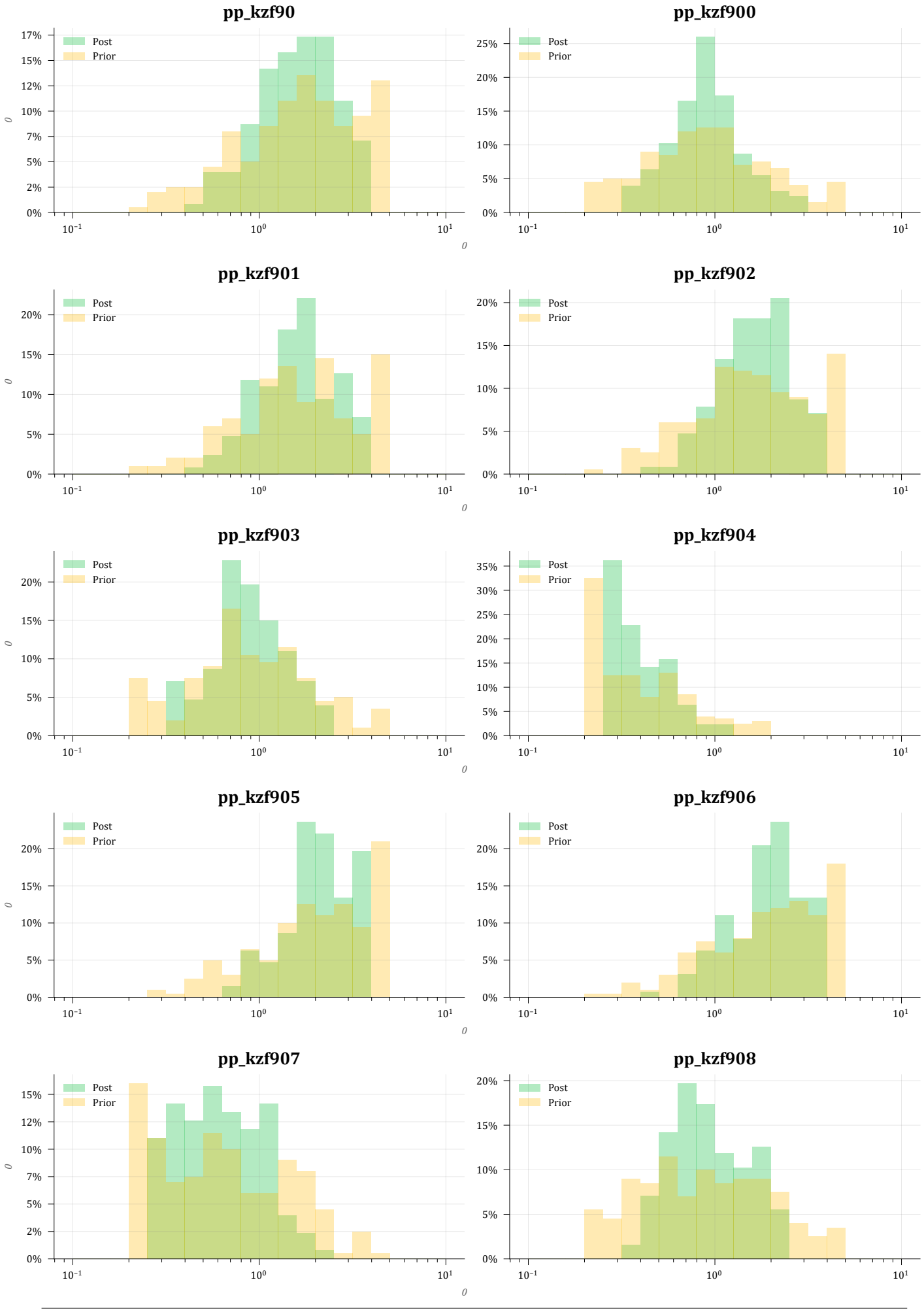

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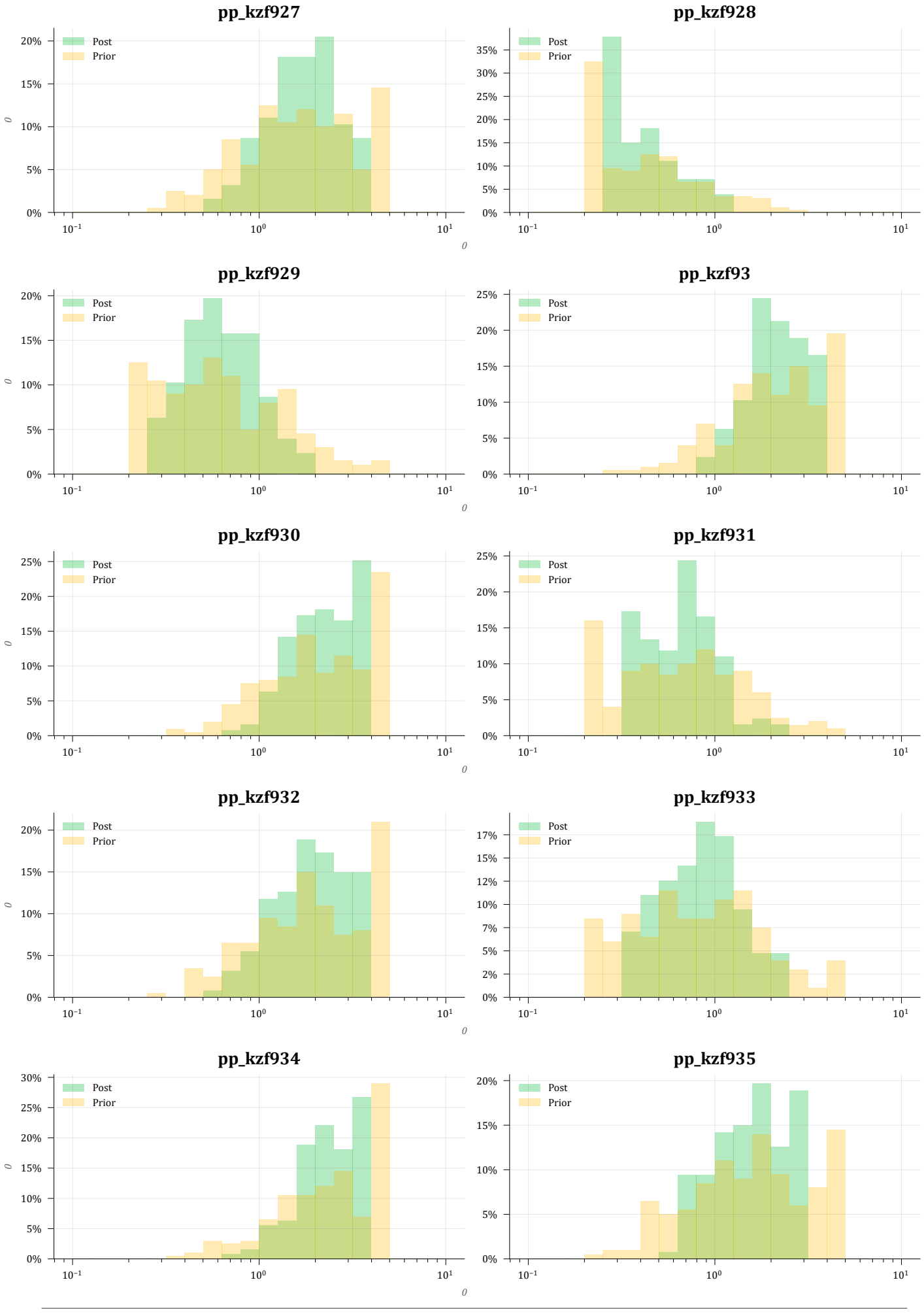

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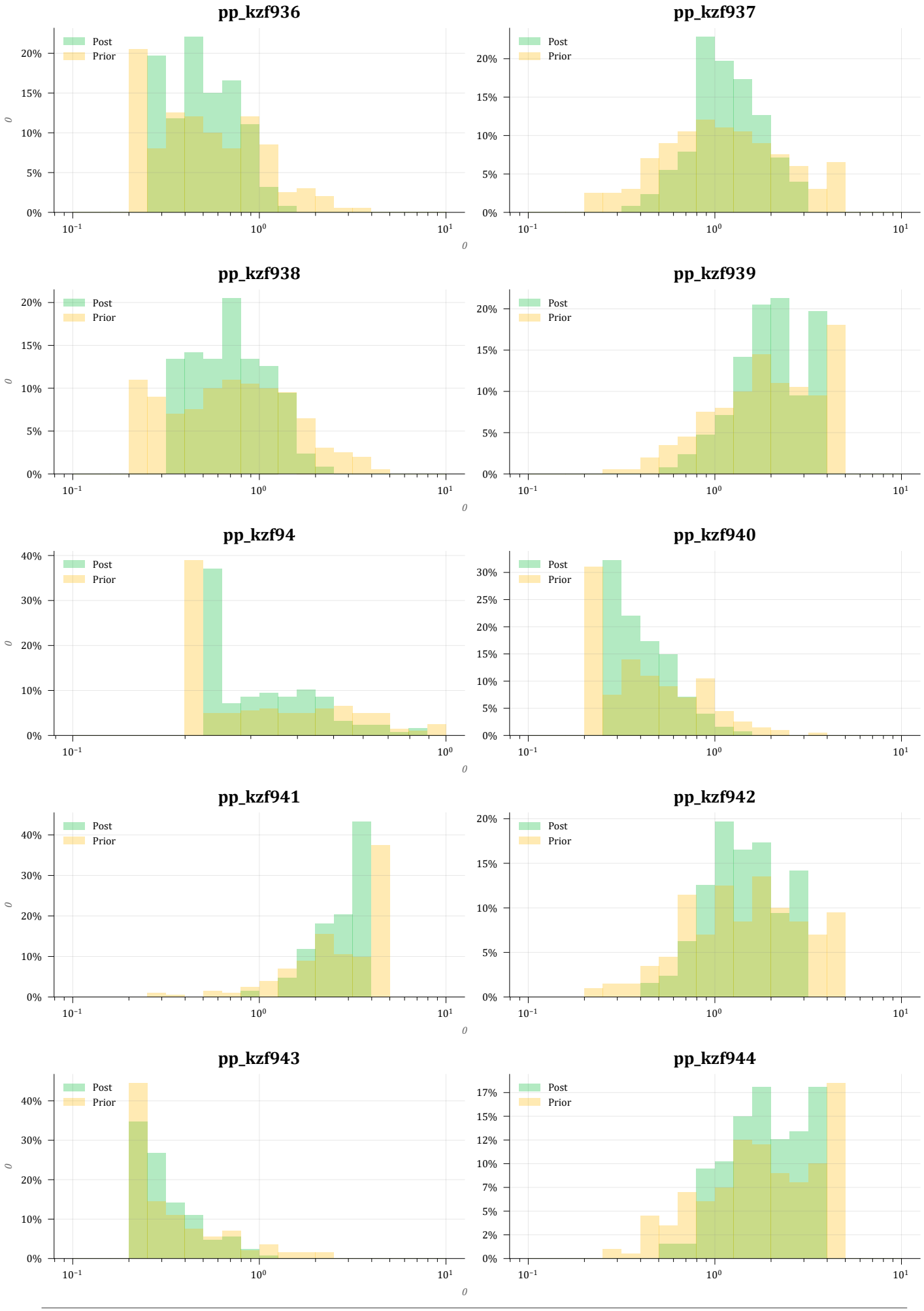

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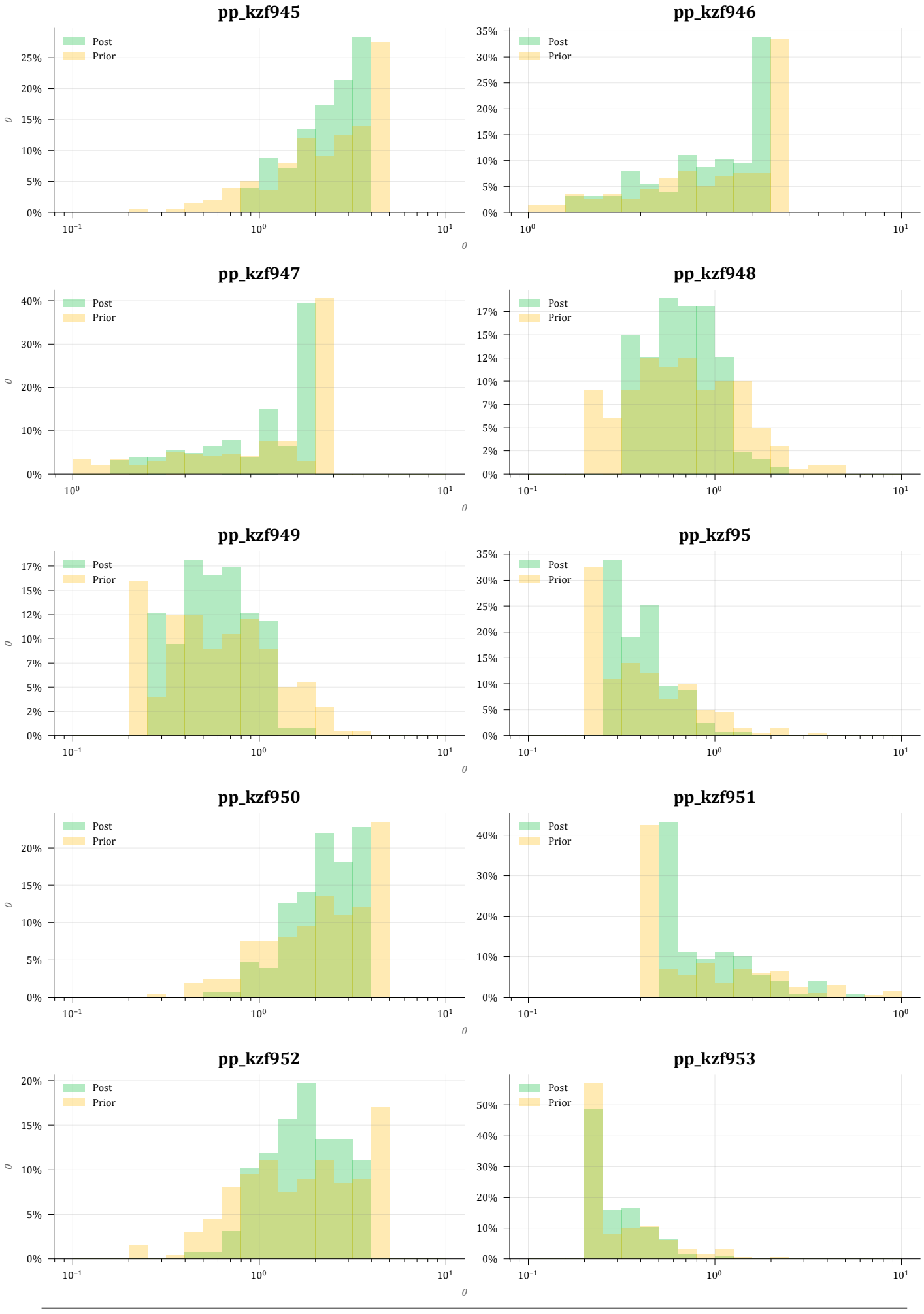

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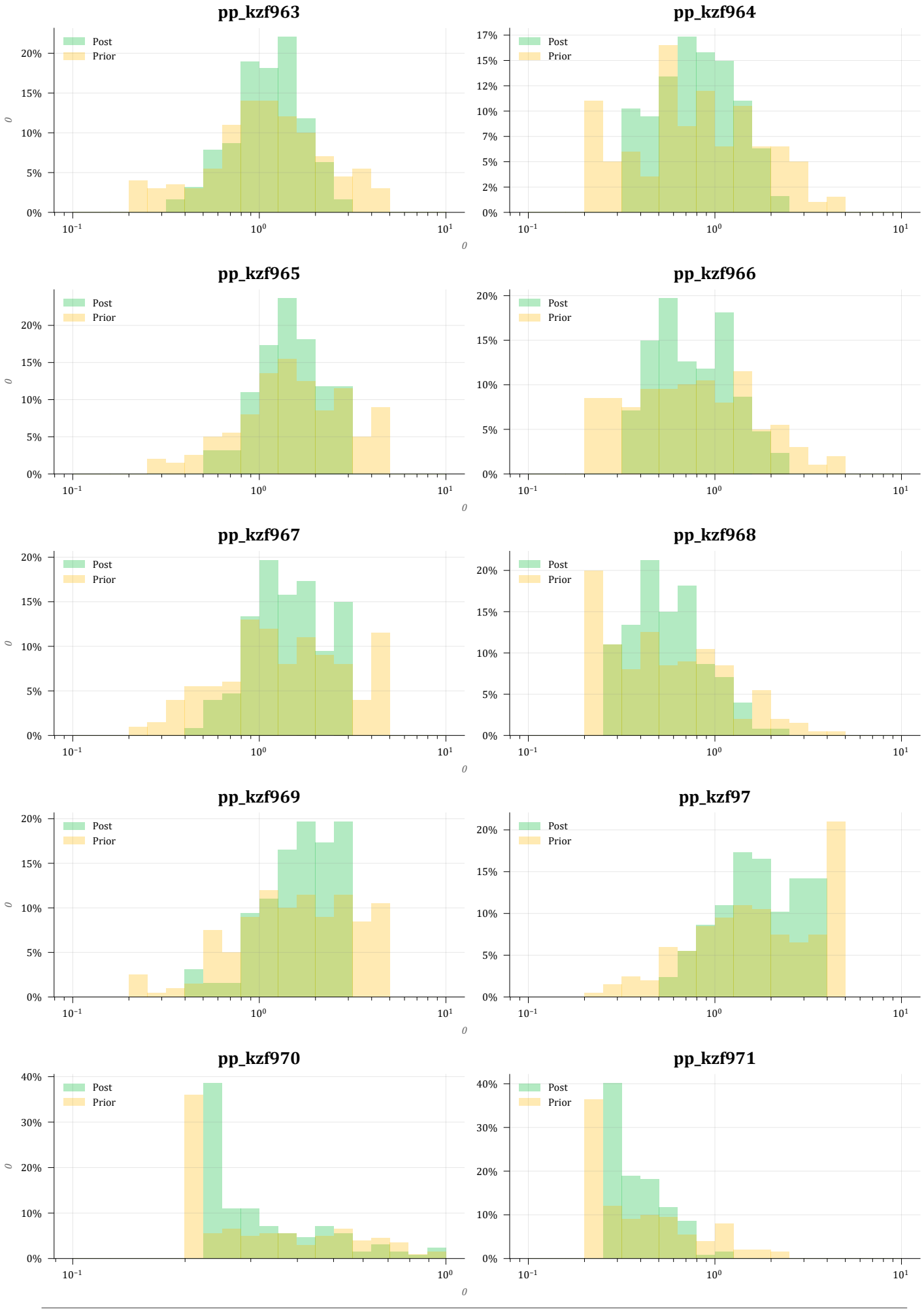

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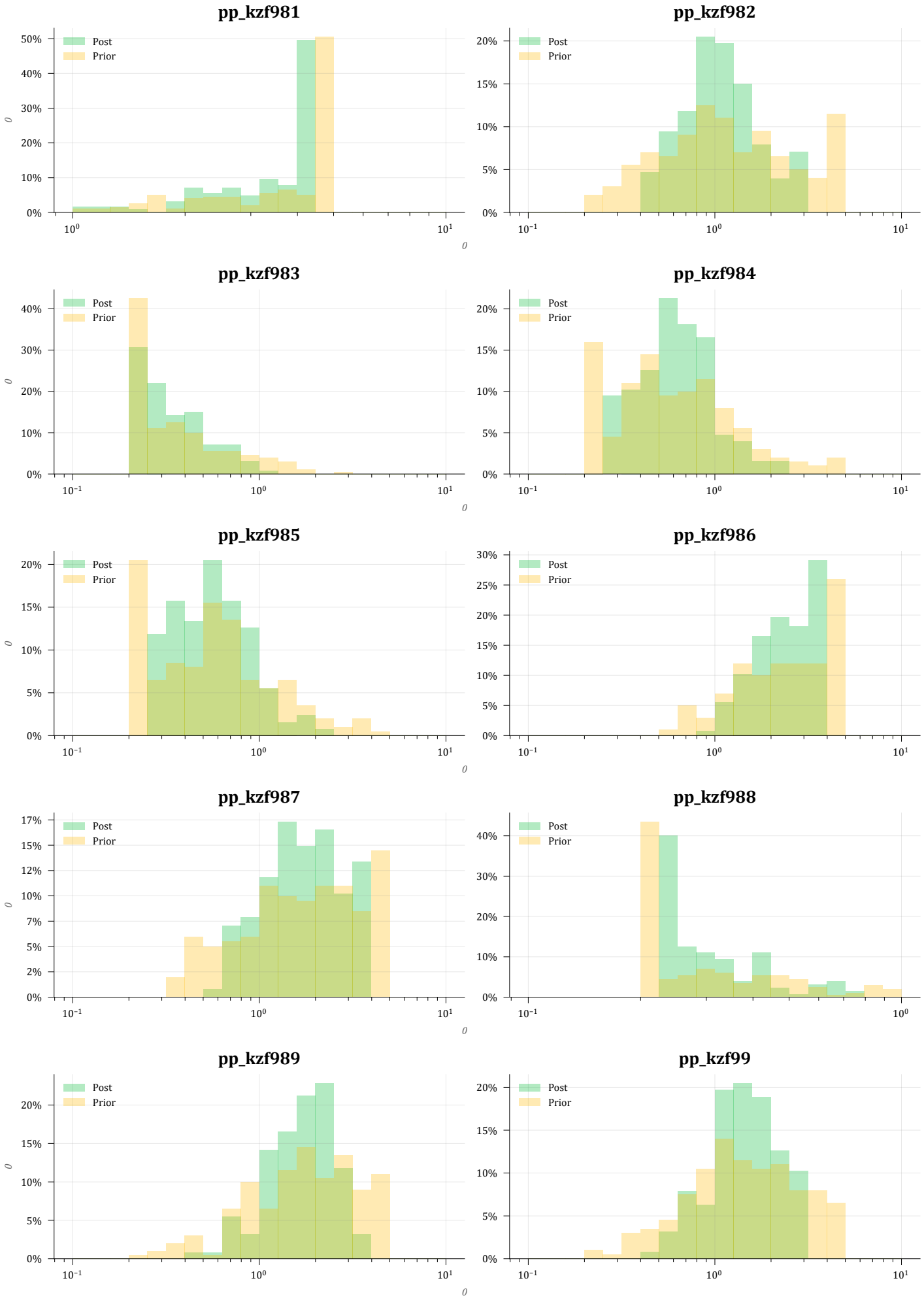

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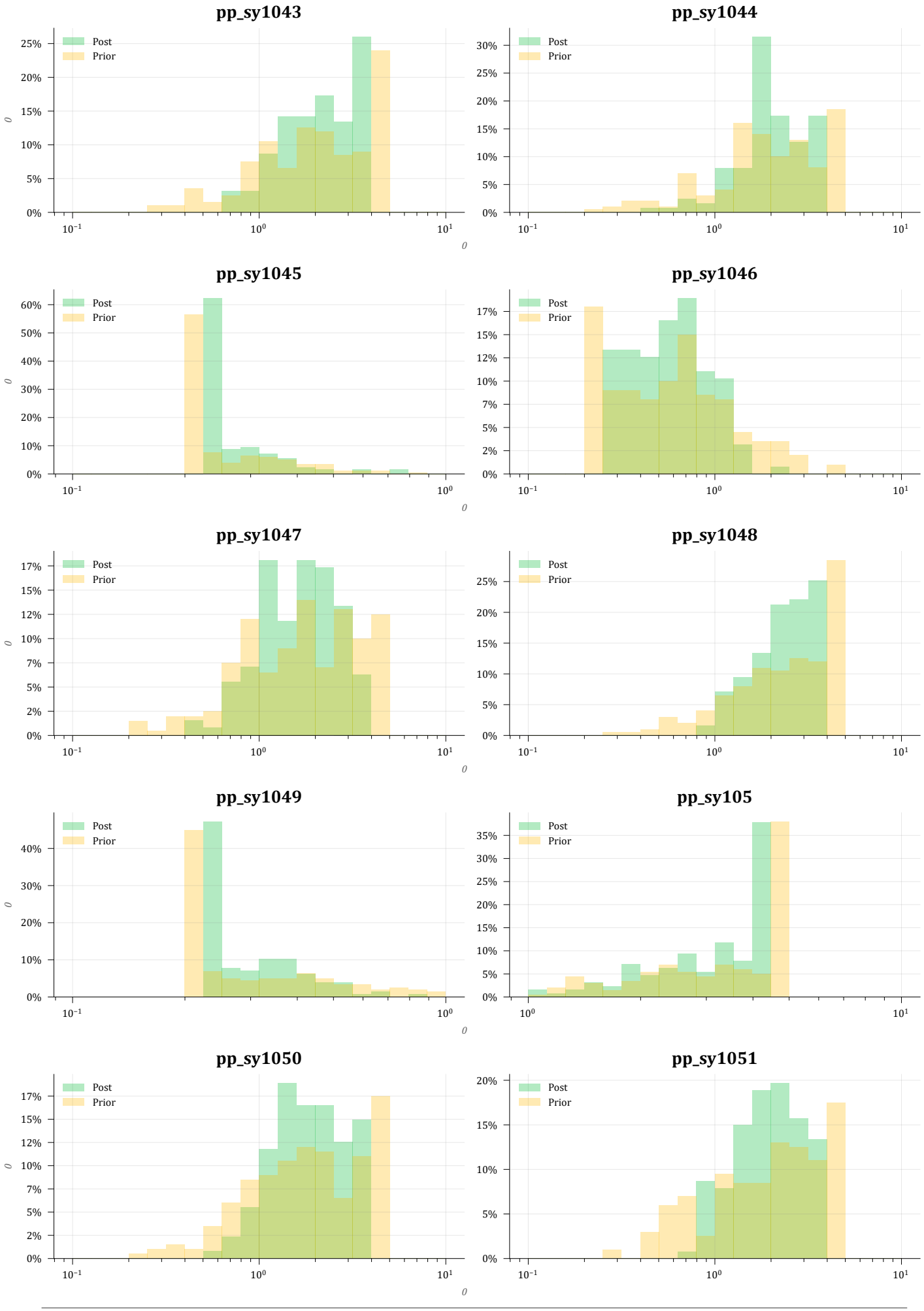

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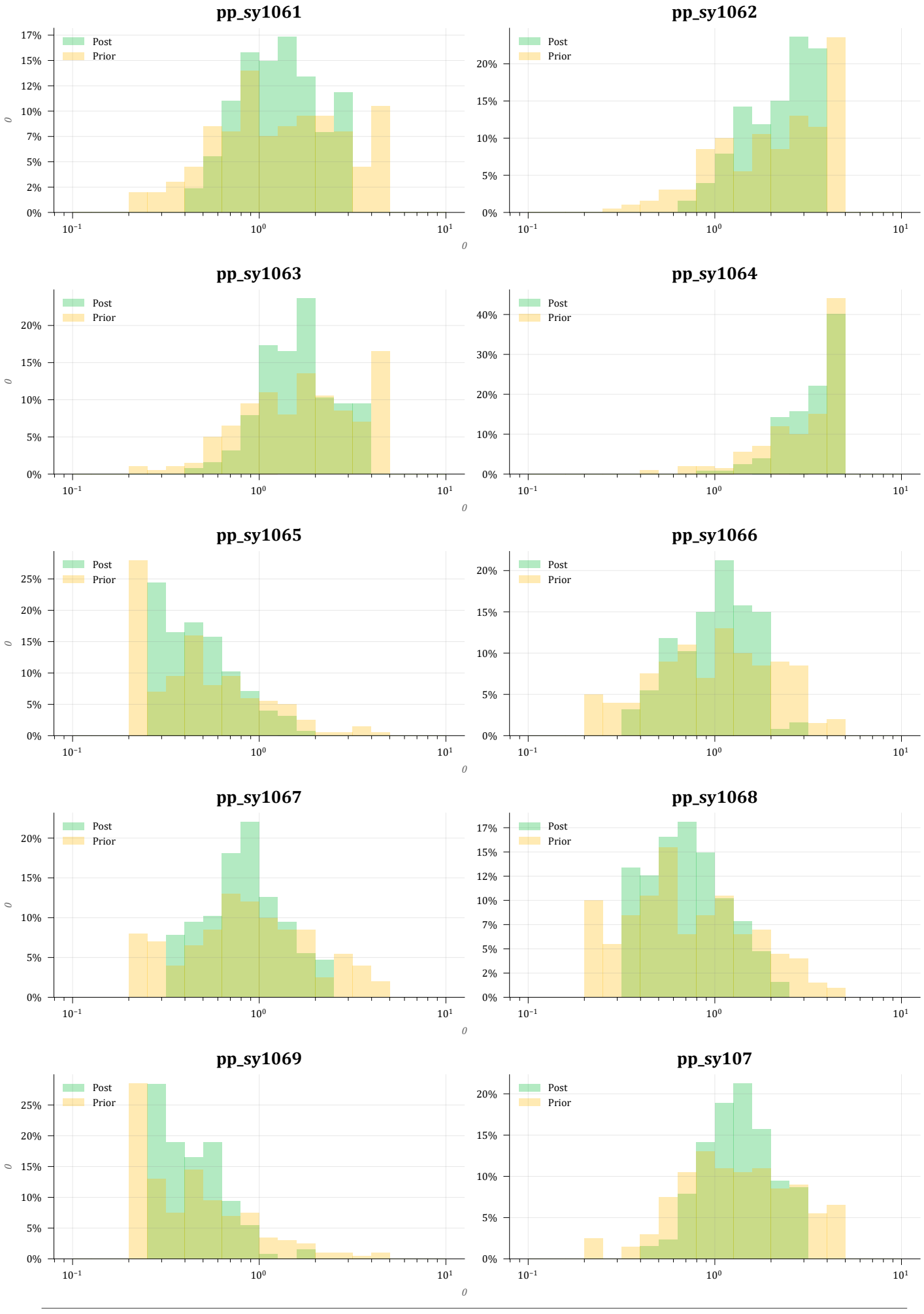

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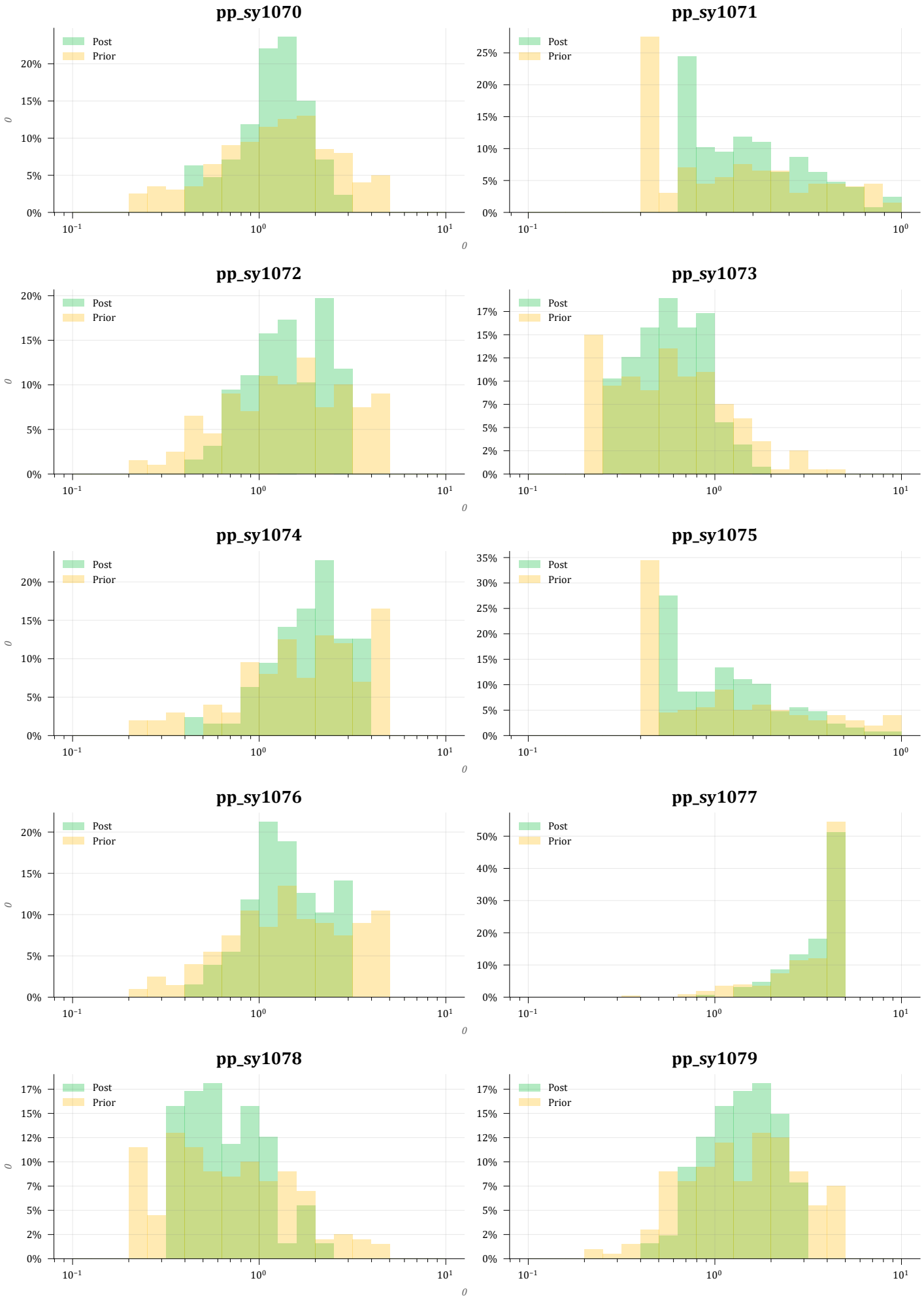

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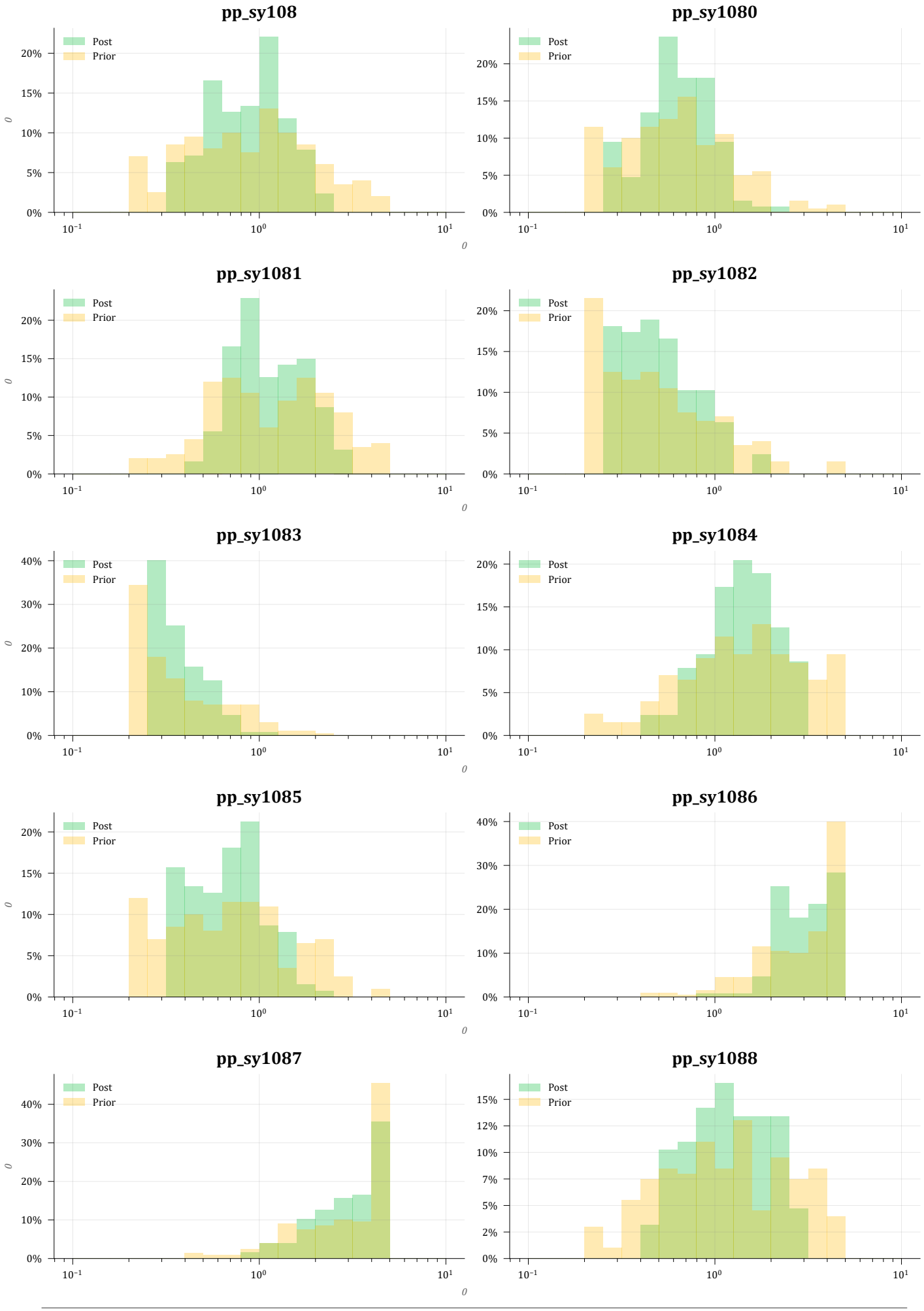

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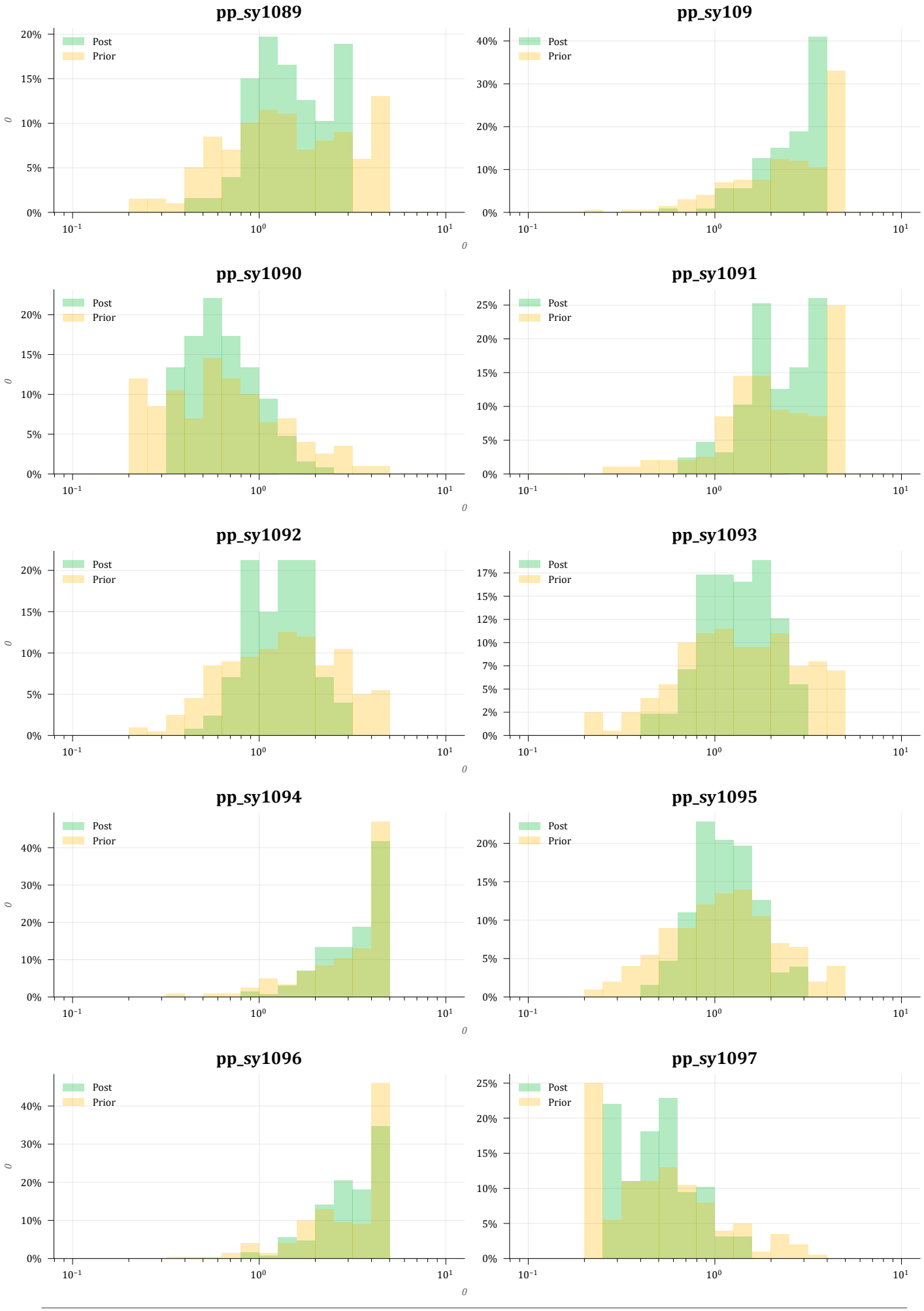

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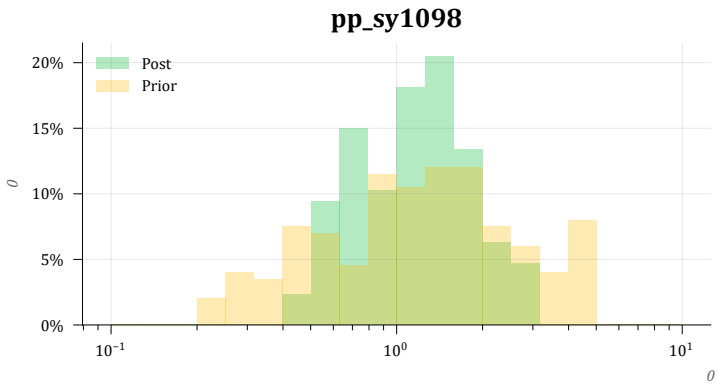

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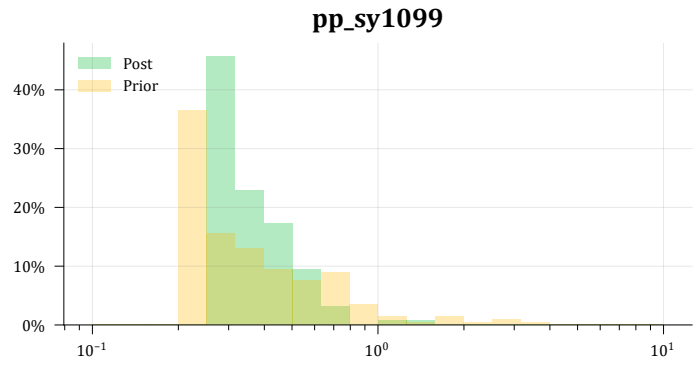

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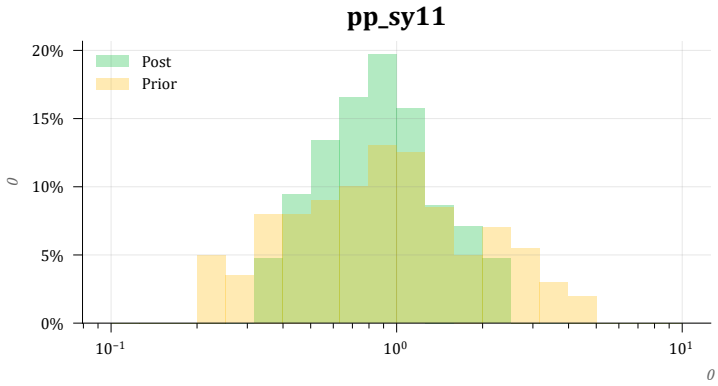

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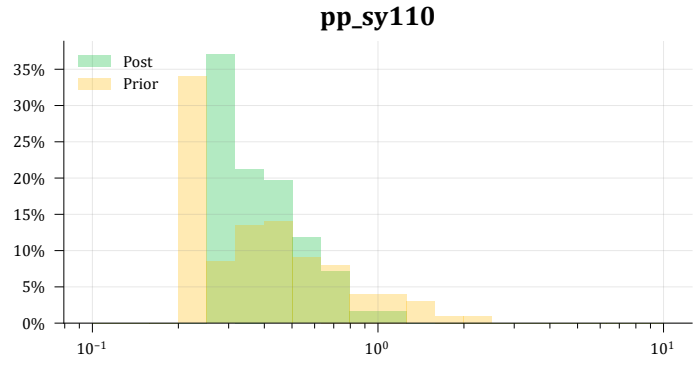

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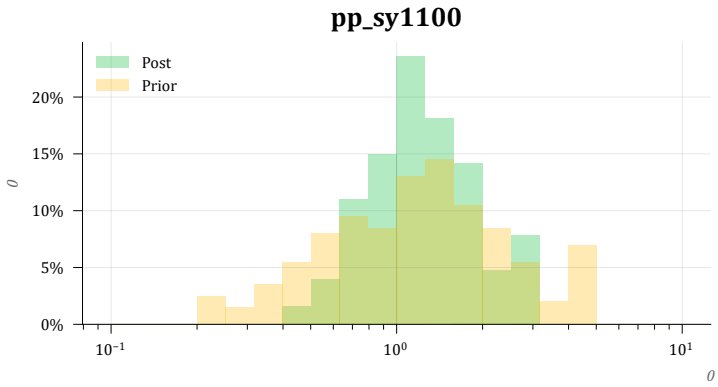

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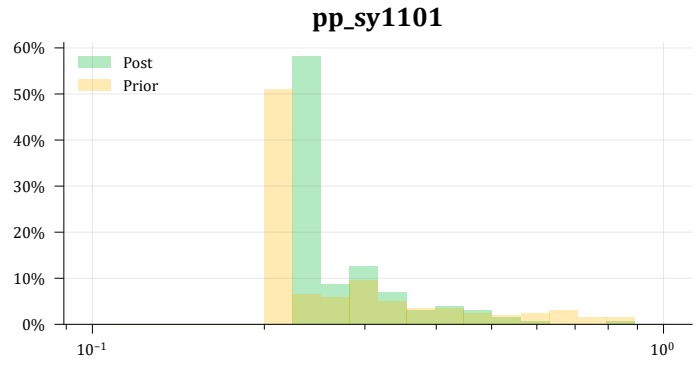

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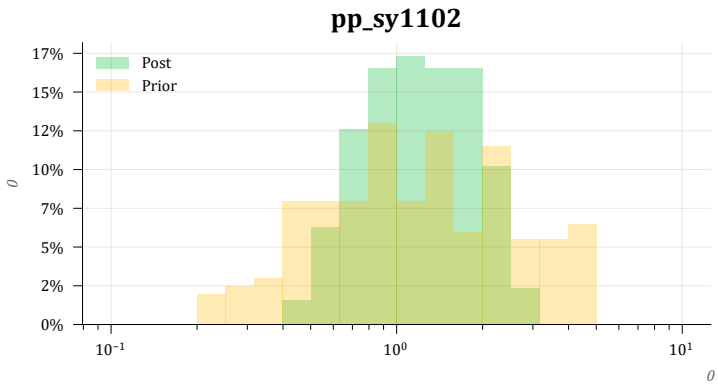

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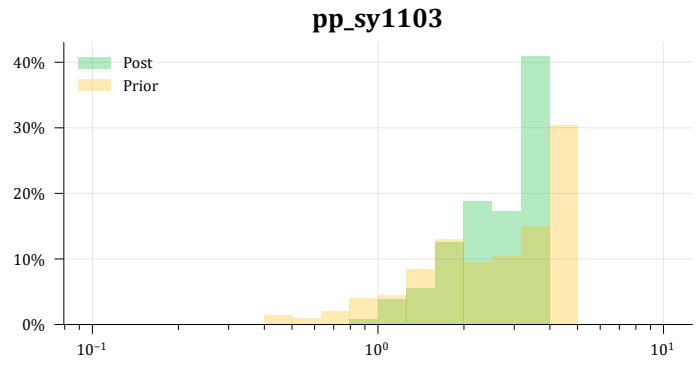

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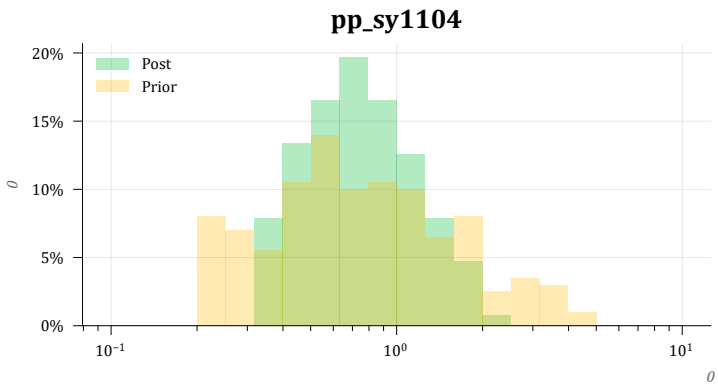

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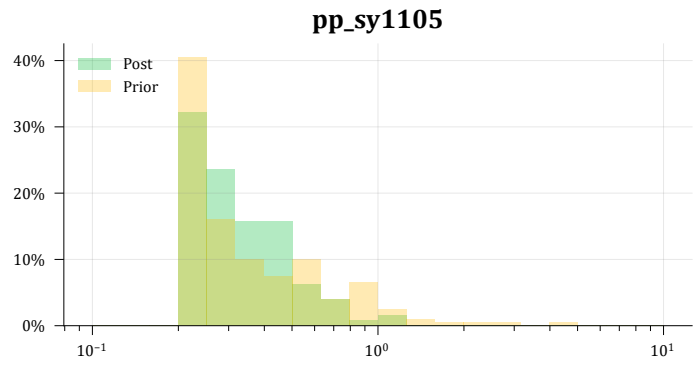

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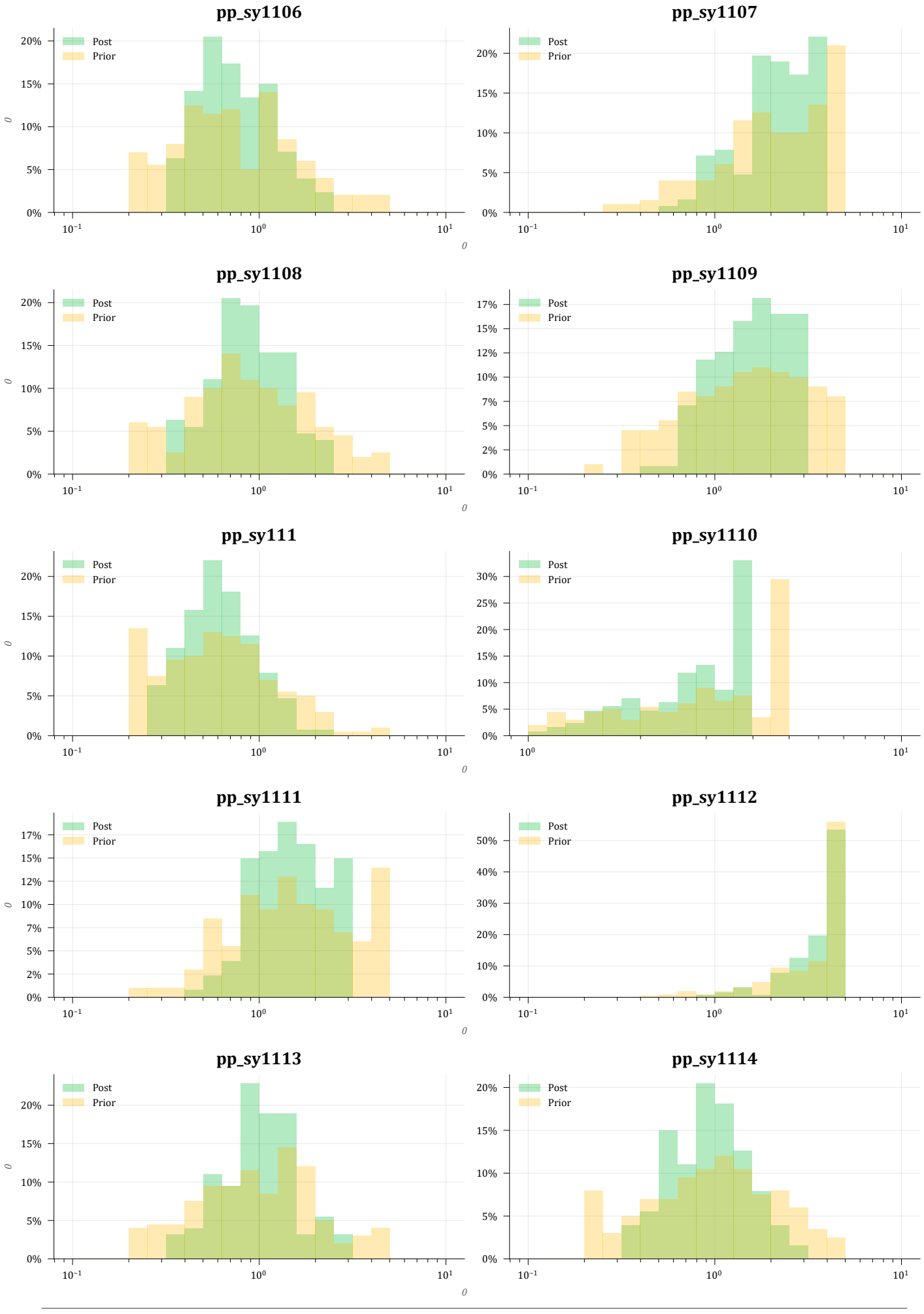

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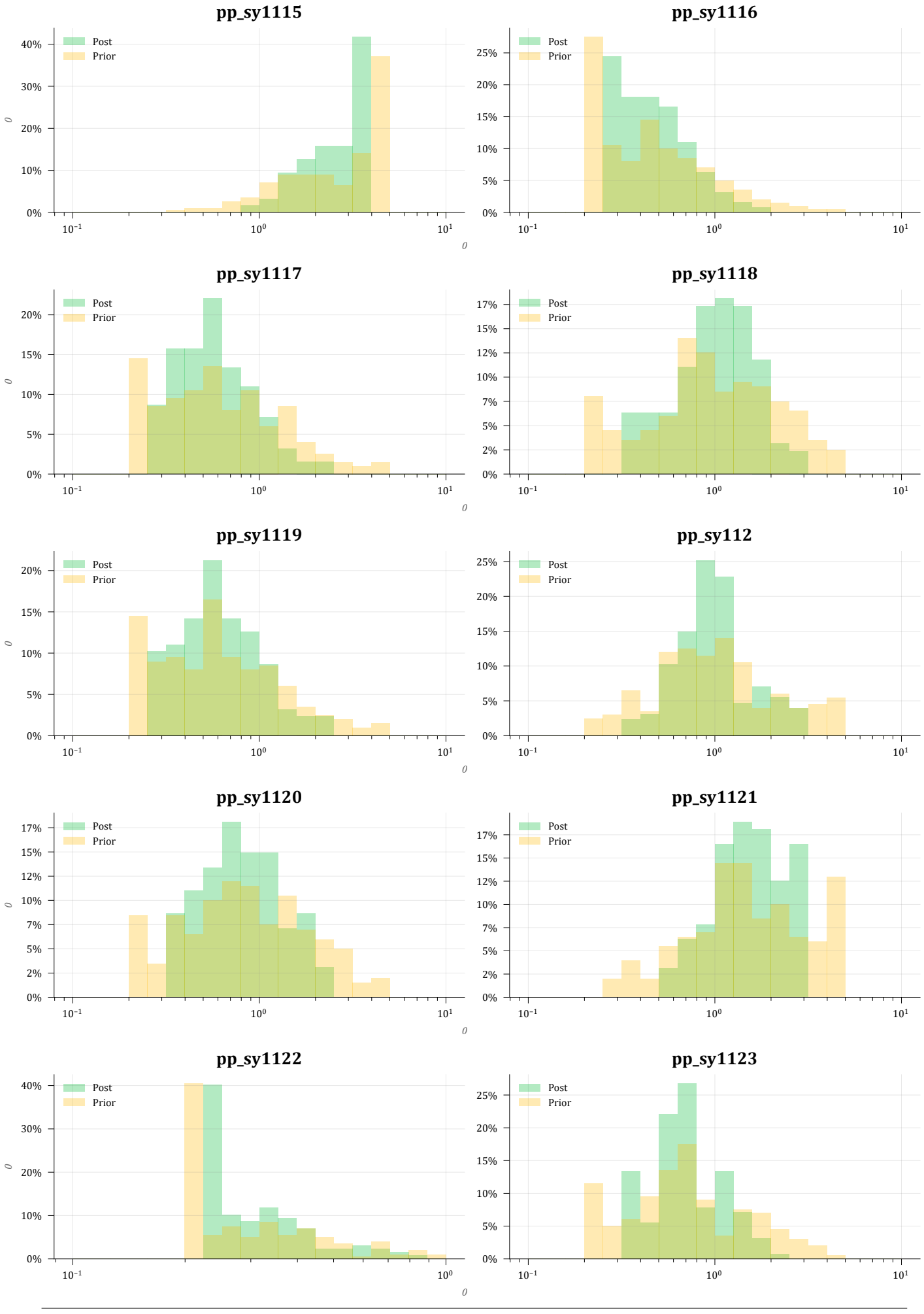

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pp_sy1103
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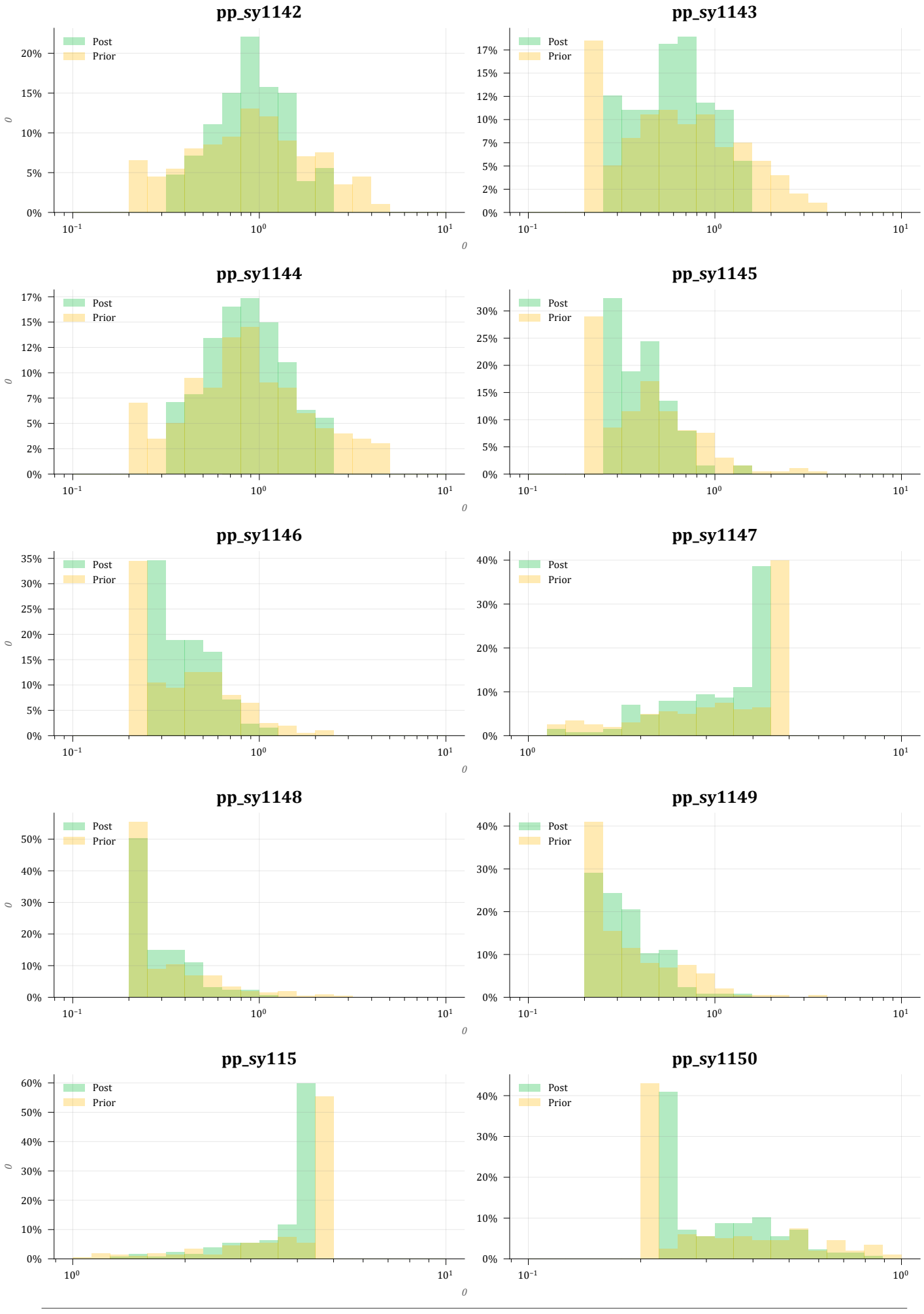

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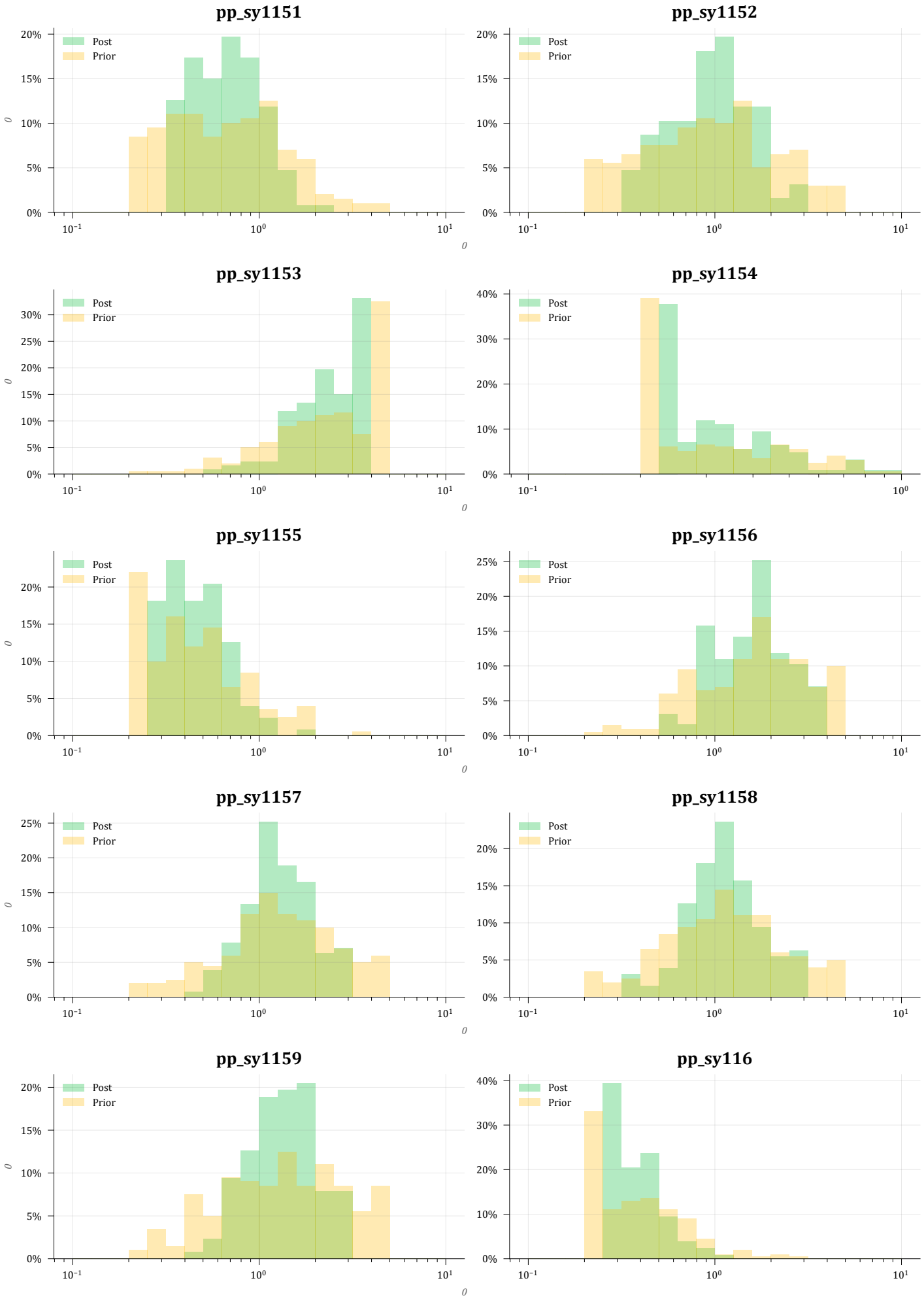

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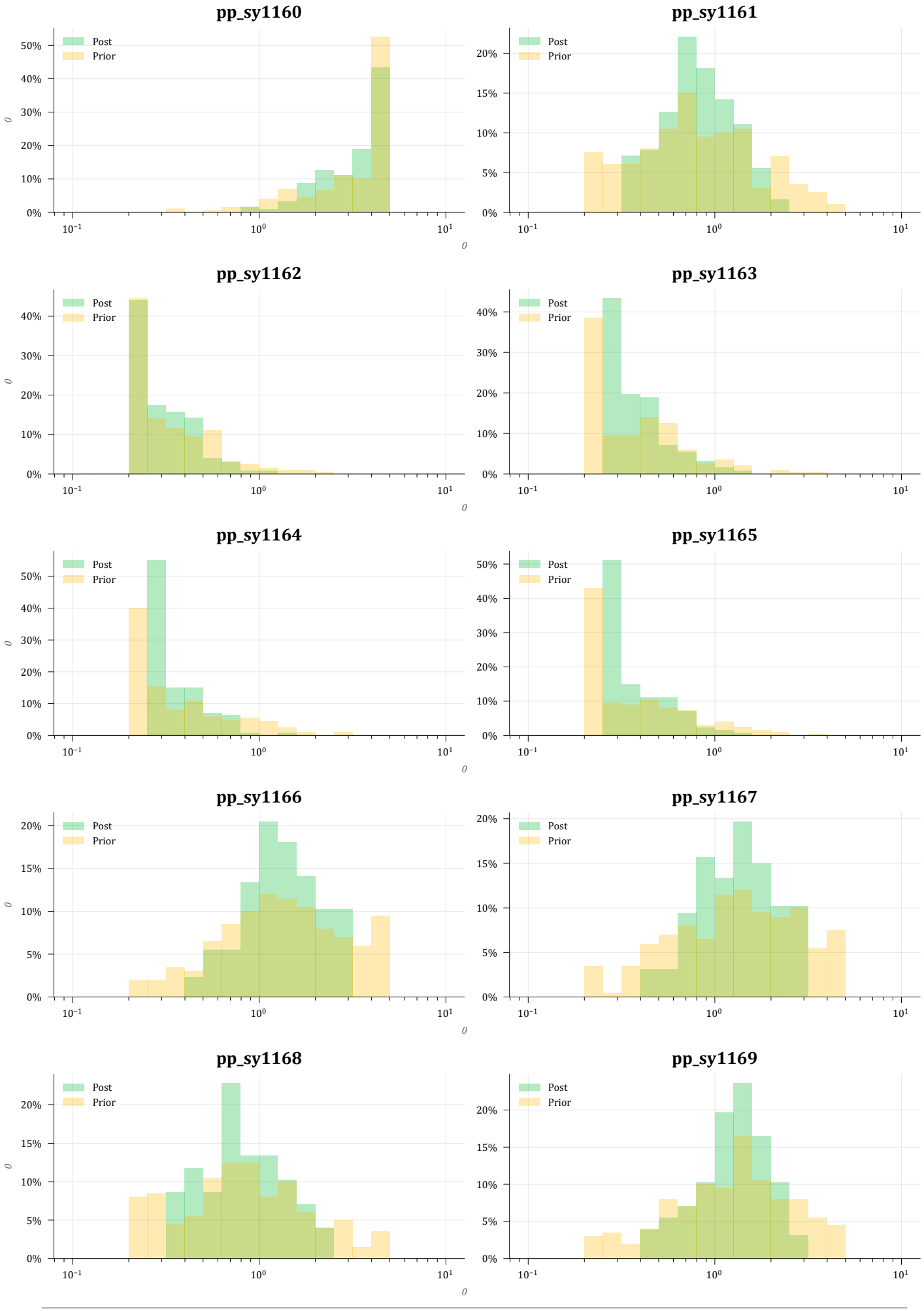

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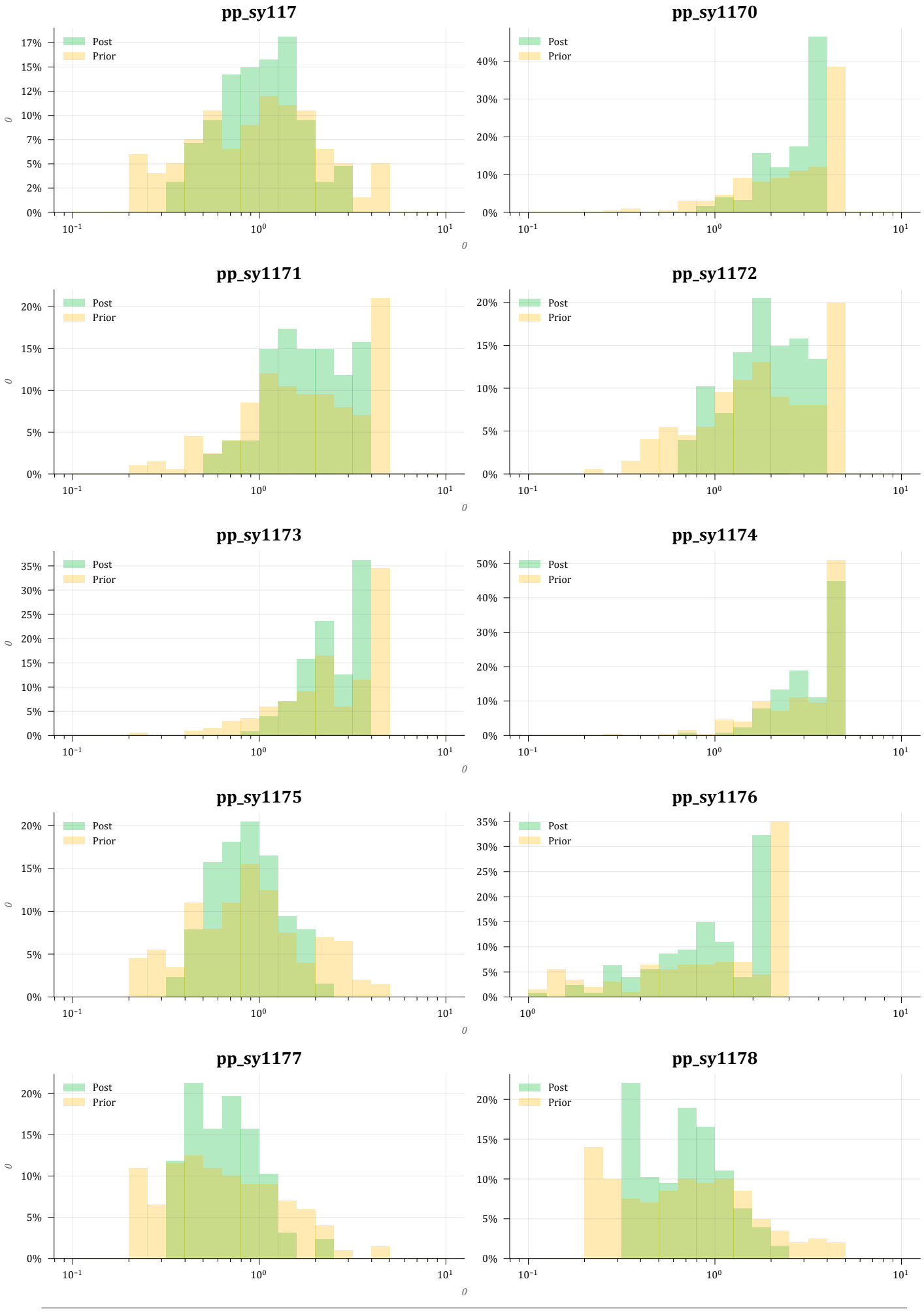

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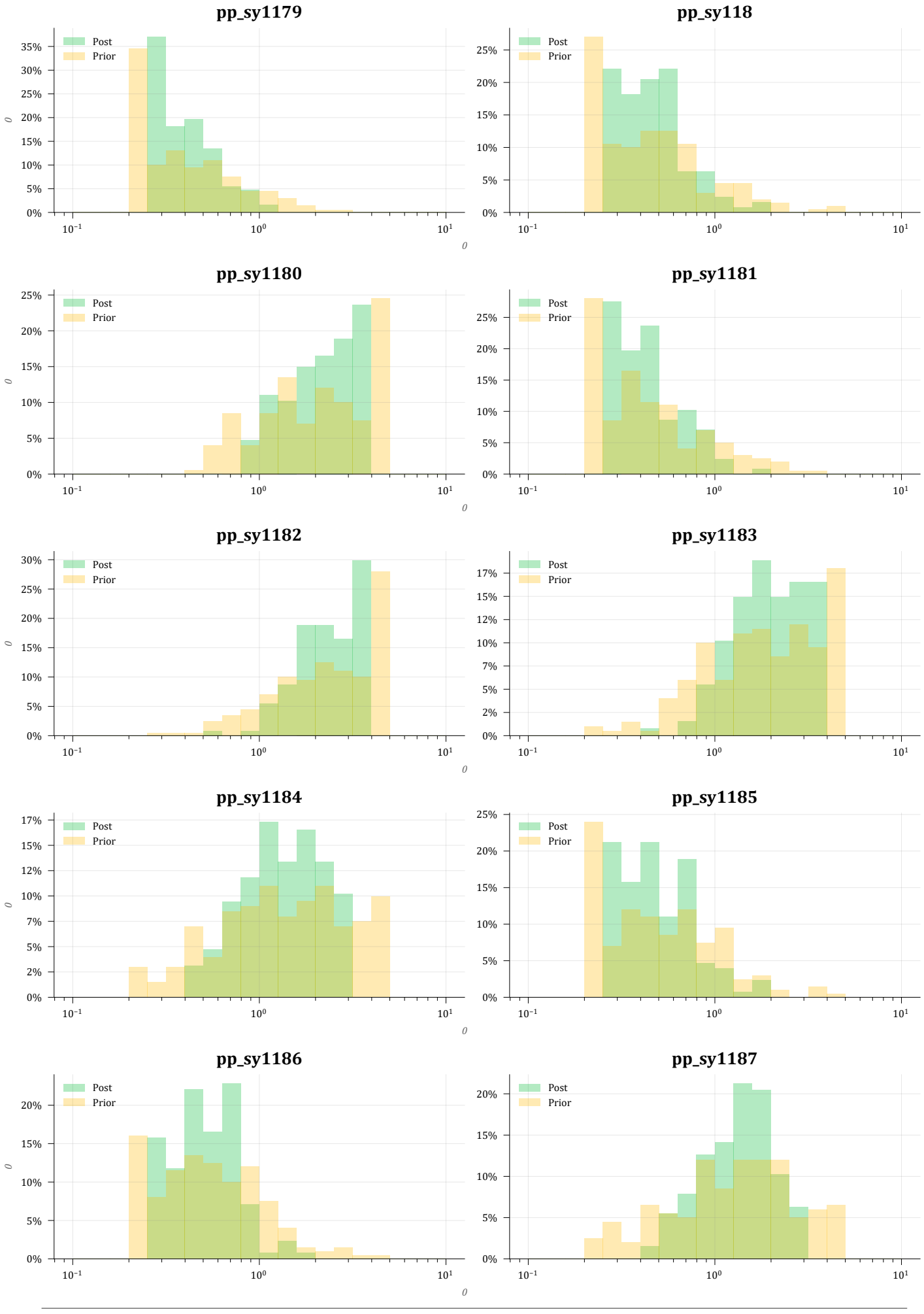

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pp_sy114
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pp_sy1141
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Prior
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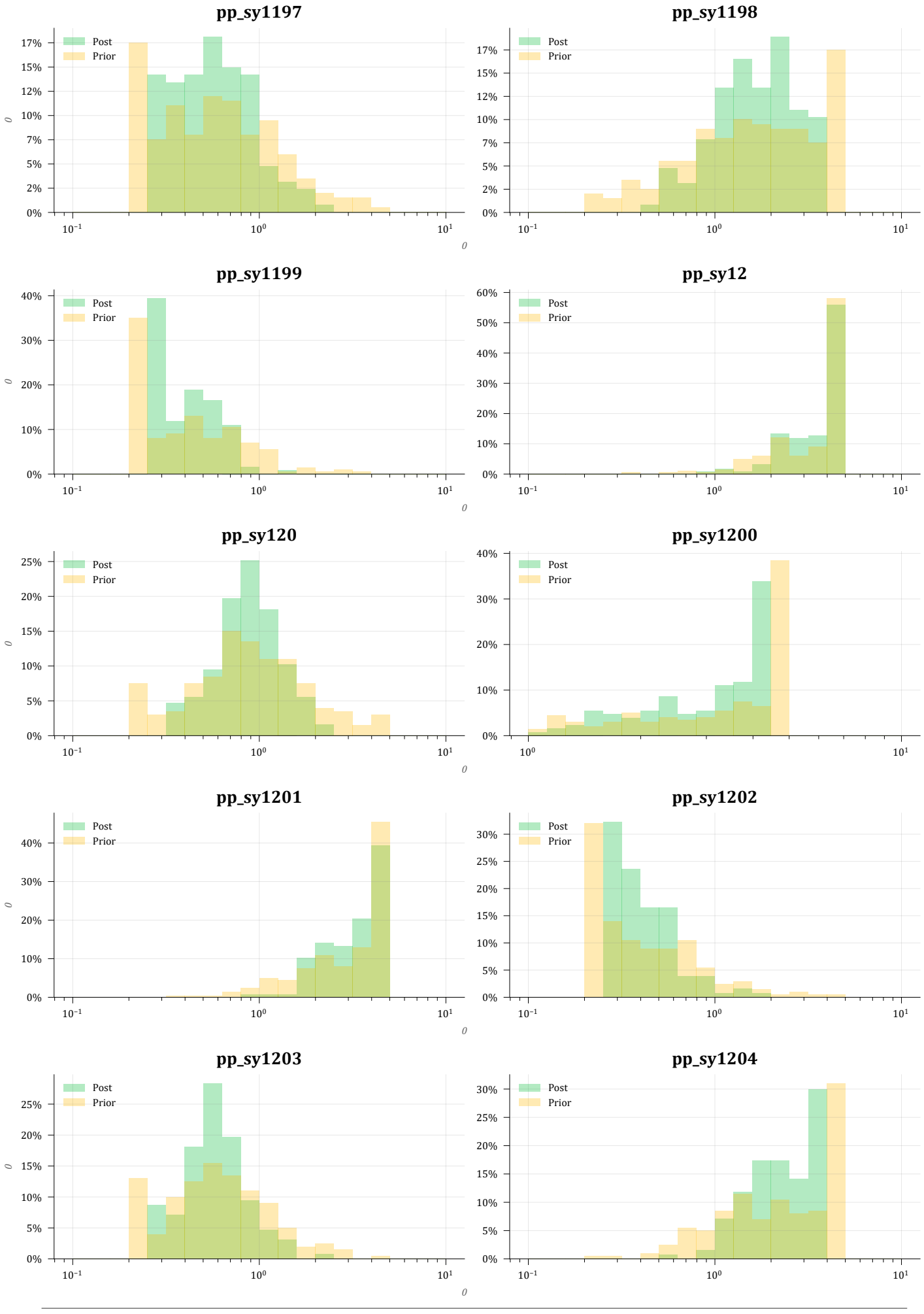

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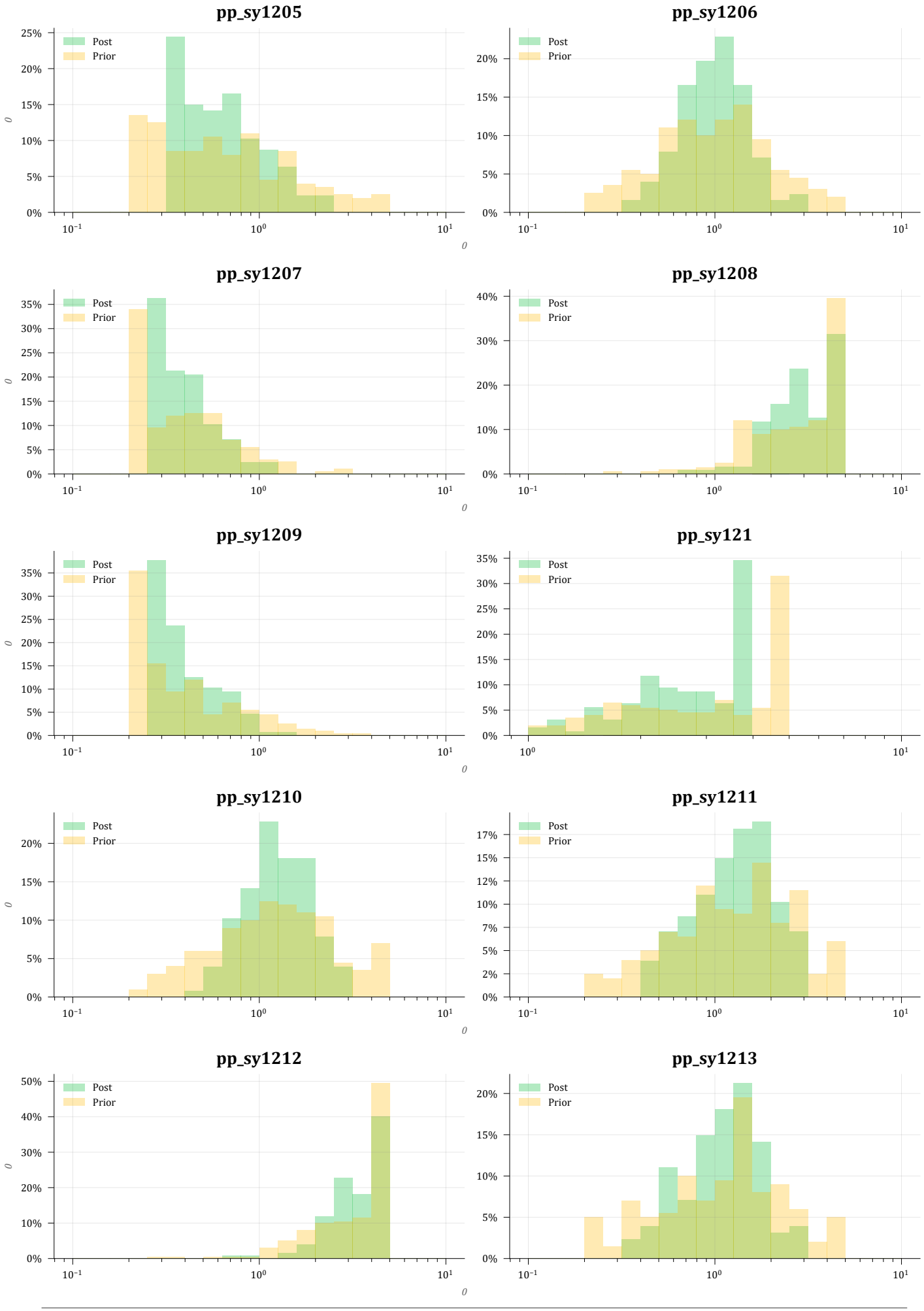

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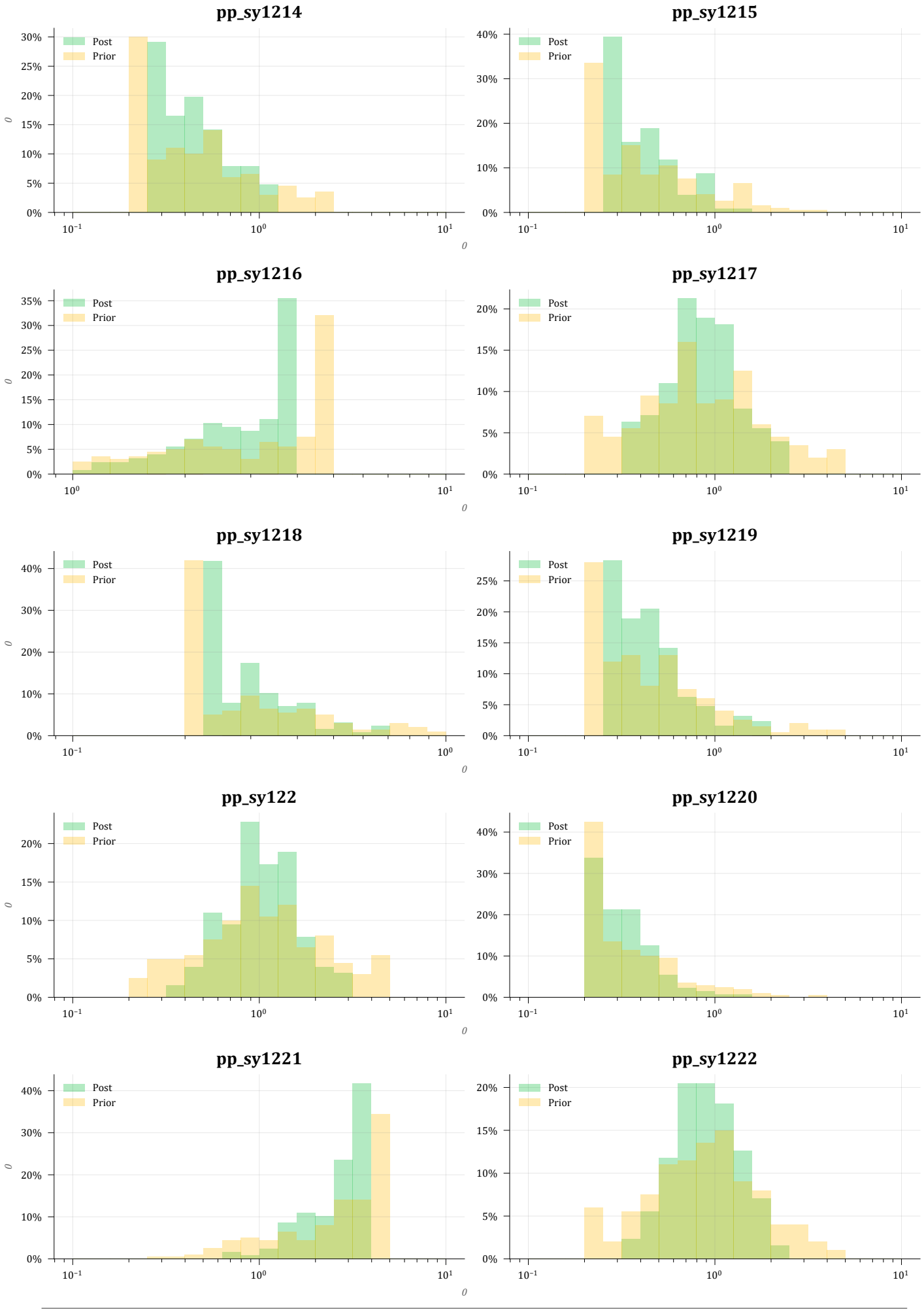

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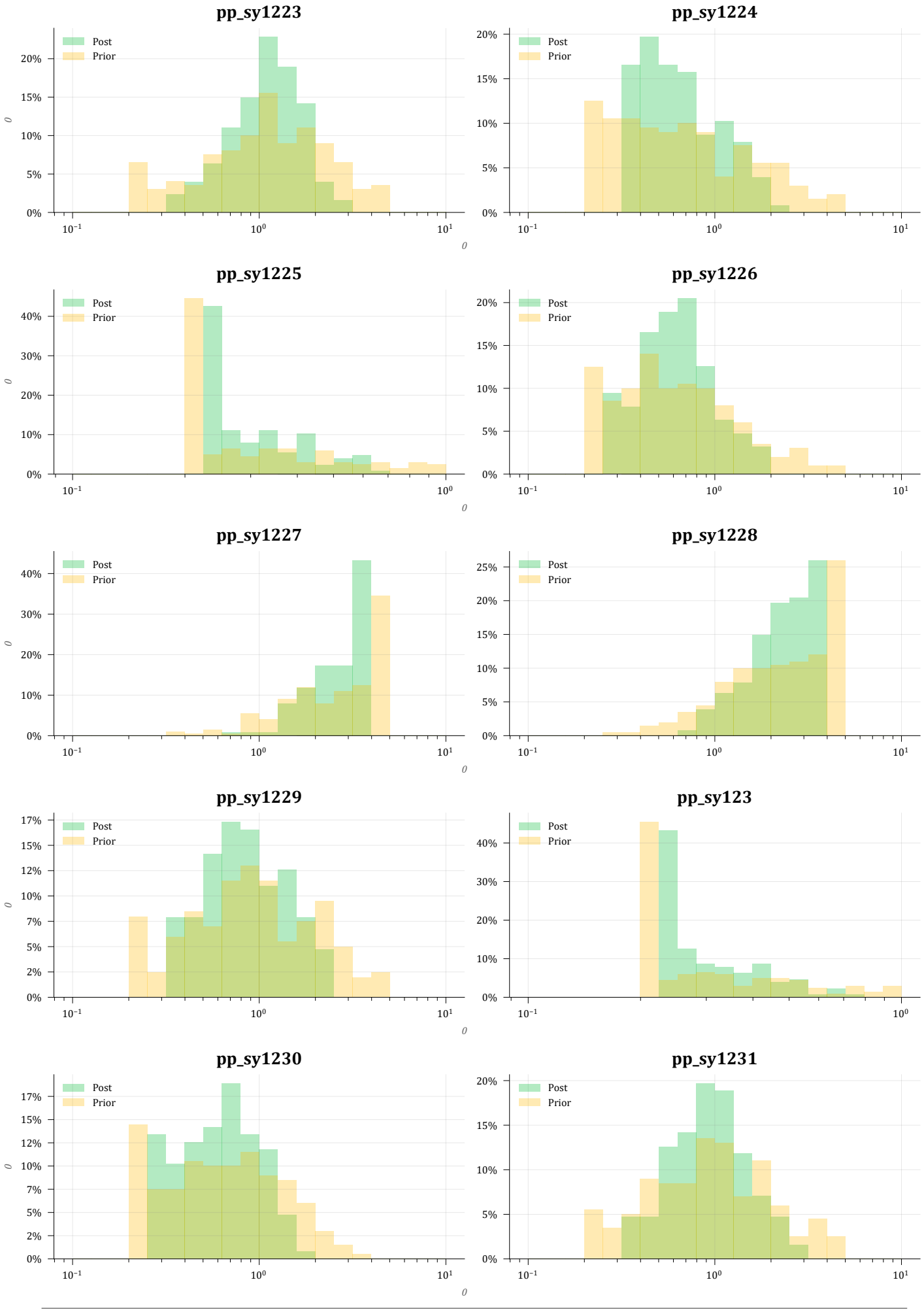

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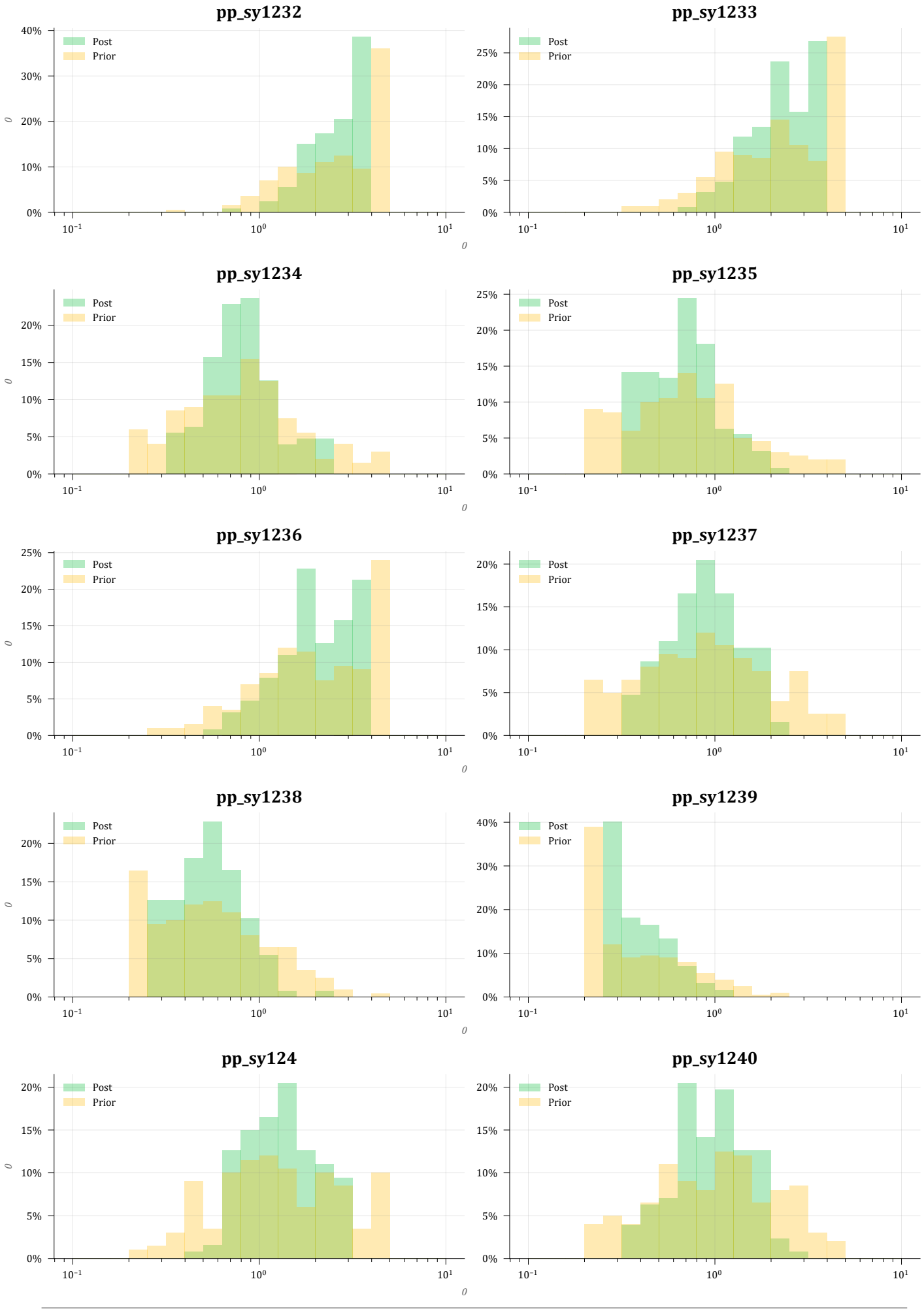

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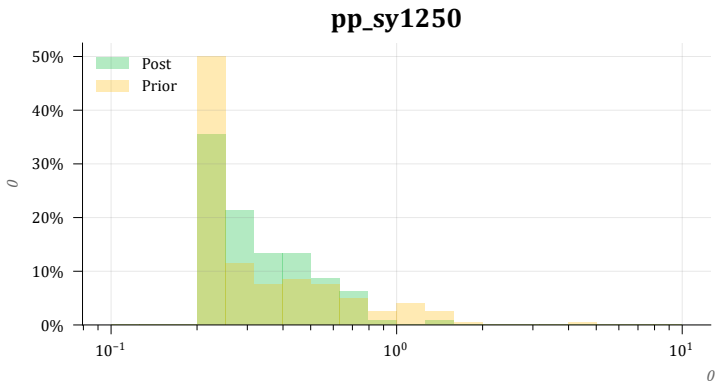

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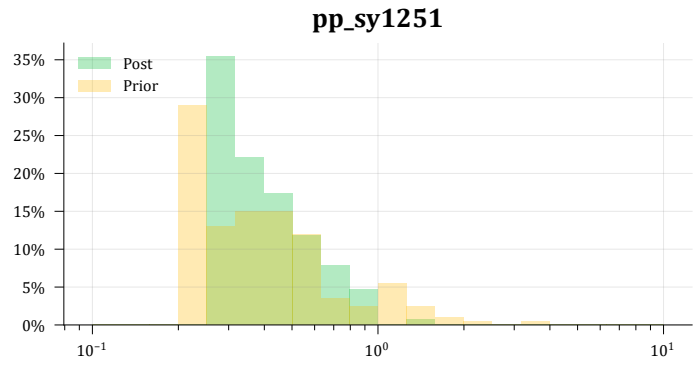

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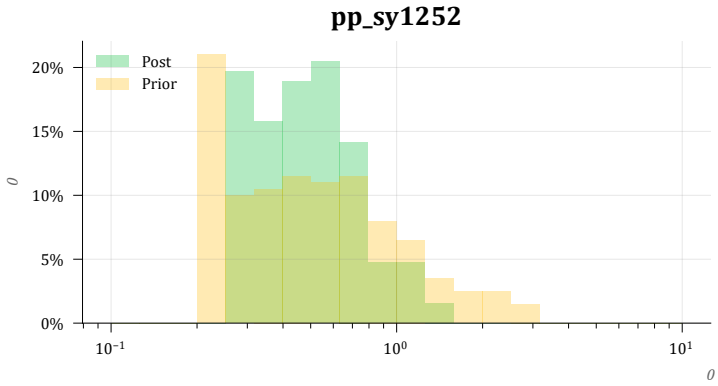

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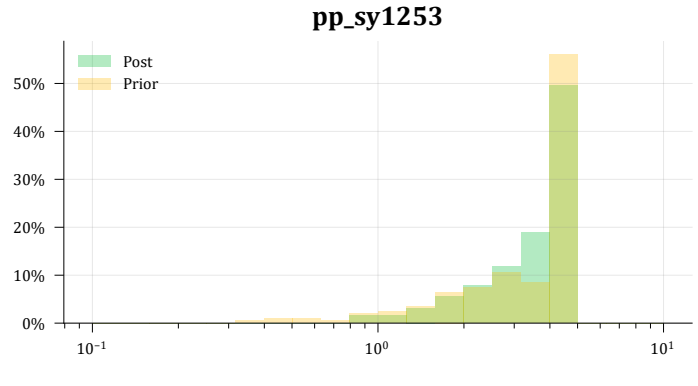

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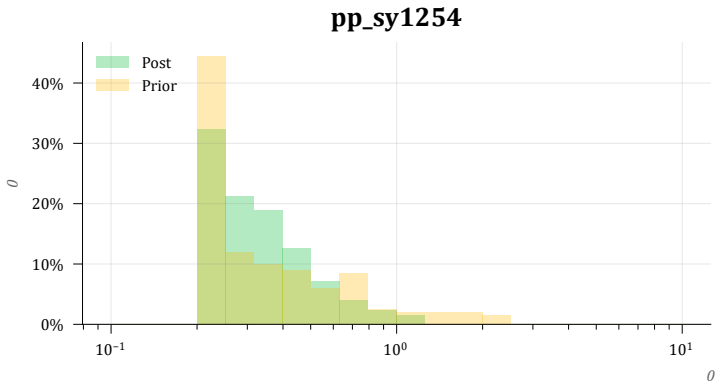

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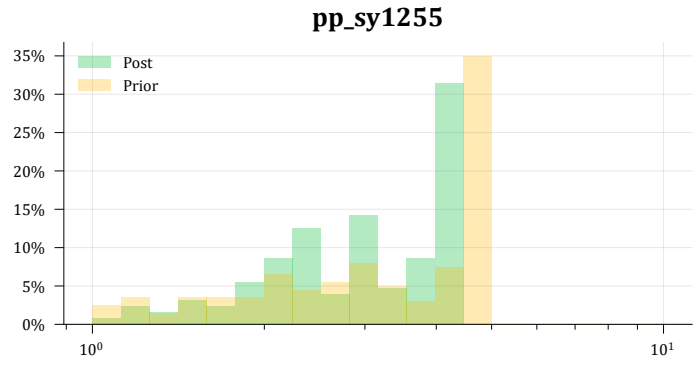

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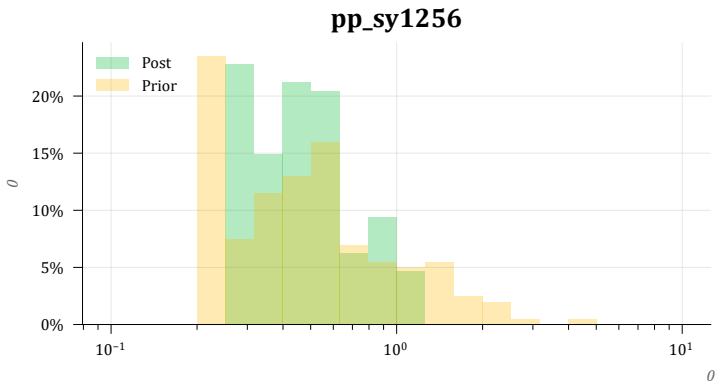

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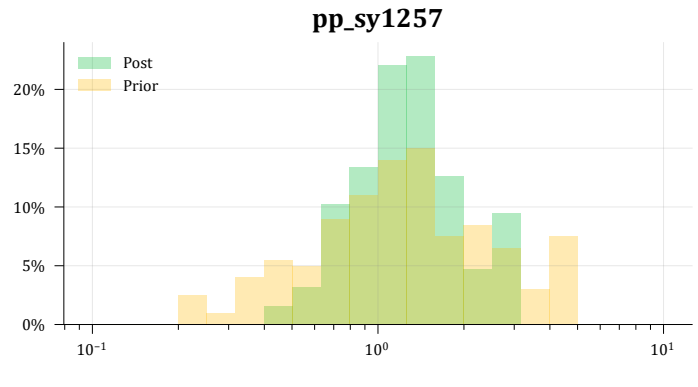

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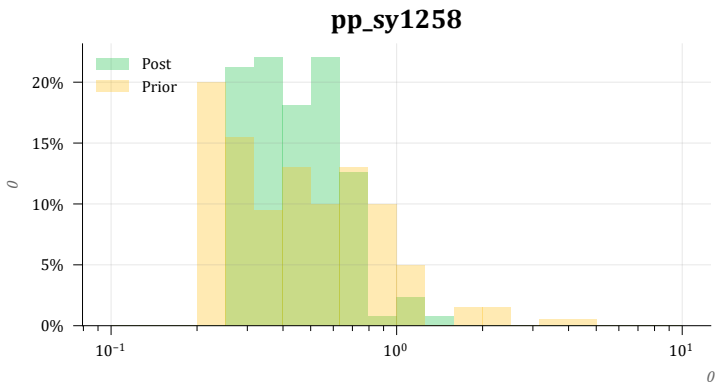

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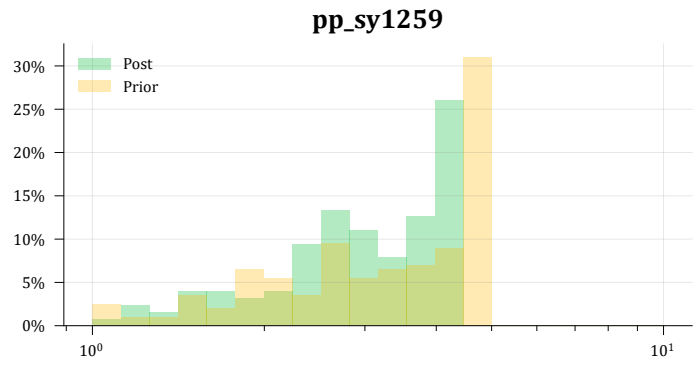

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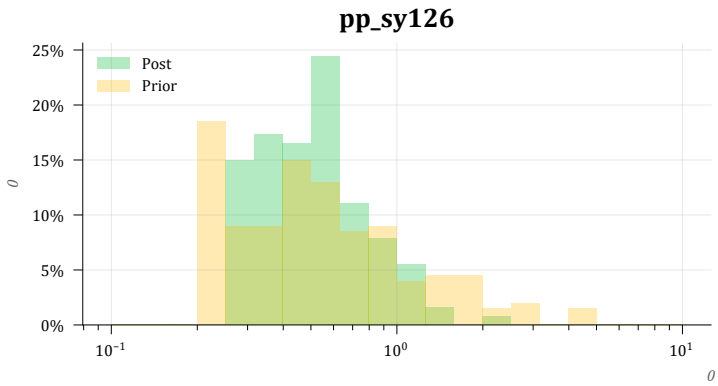

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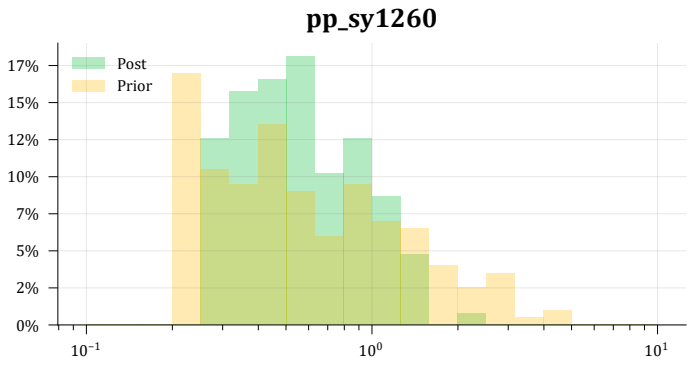

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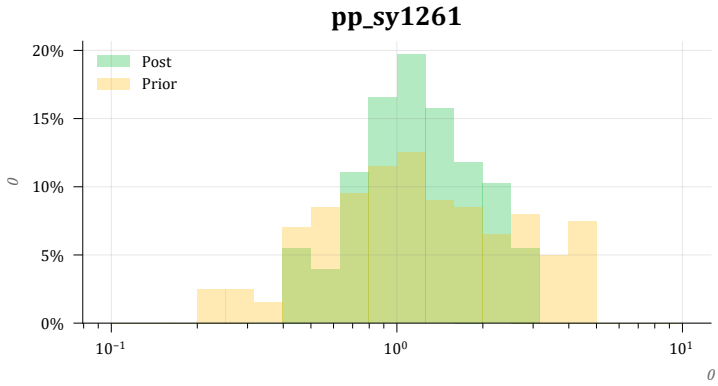

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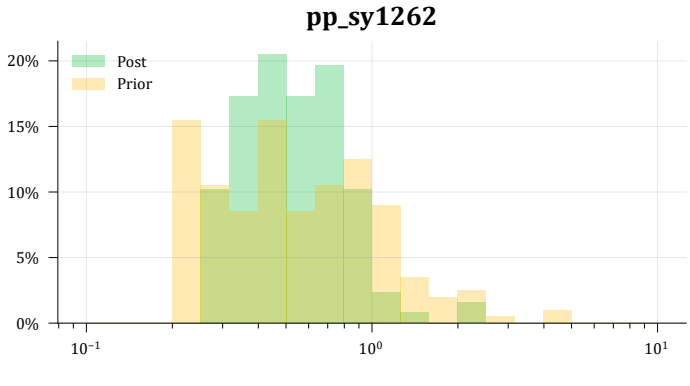

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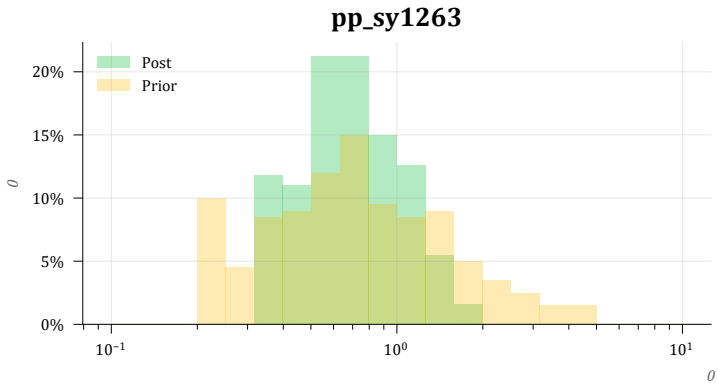

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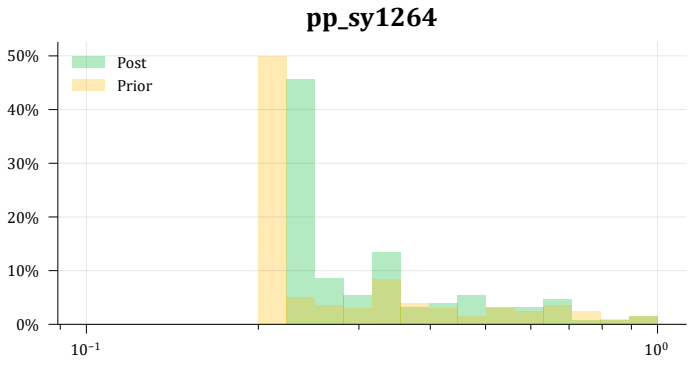

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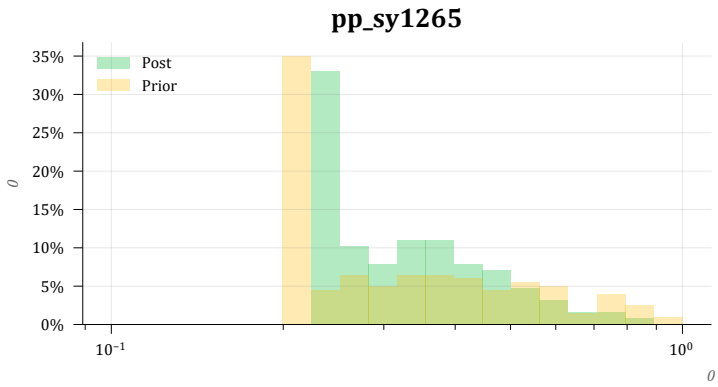

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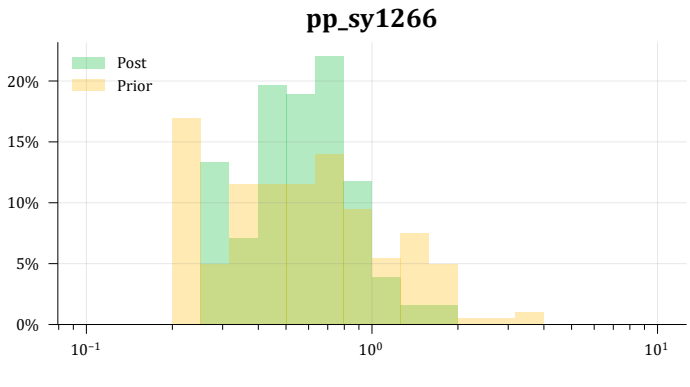

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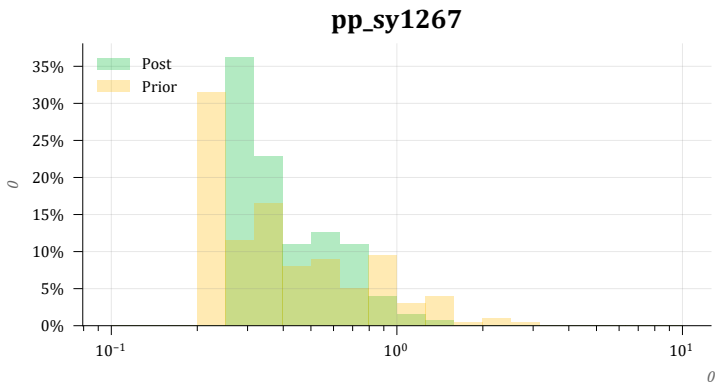

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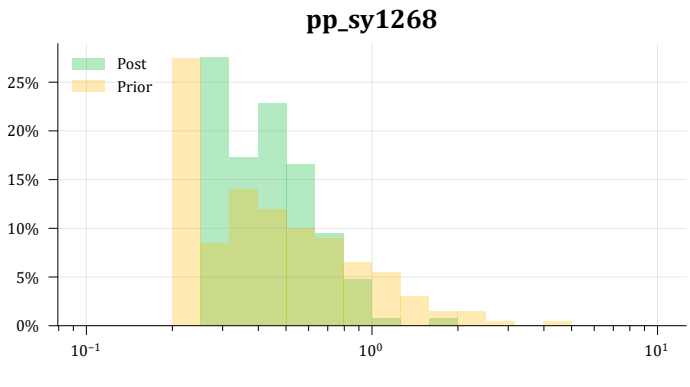

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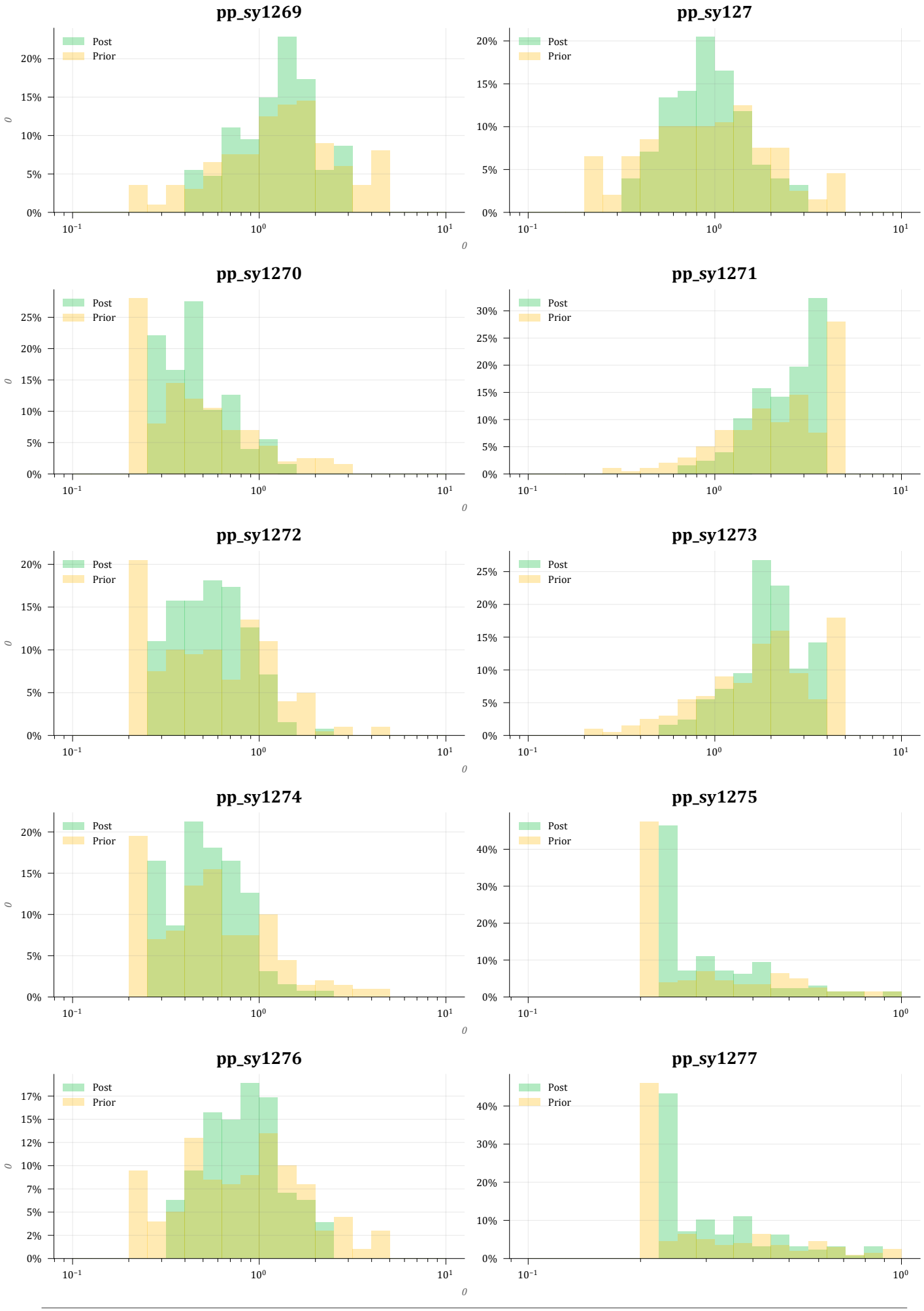

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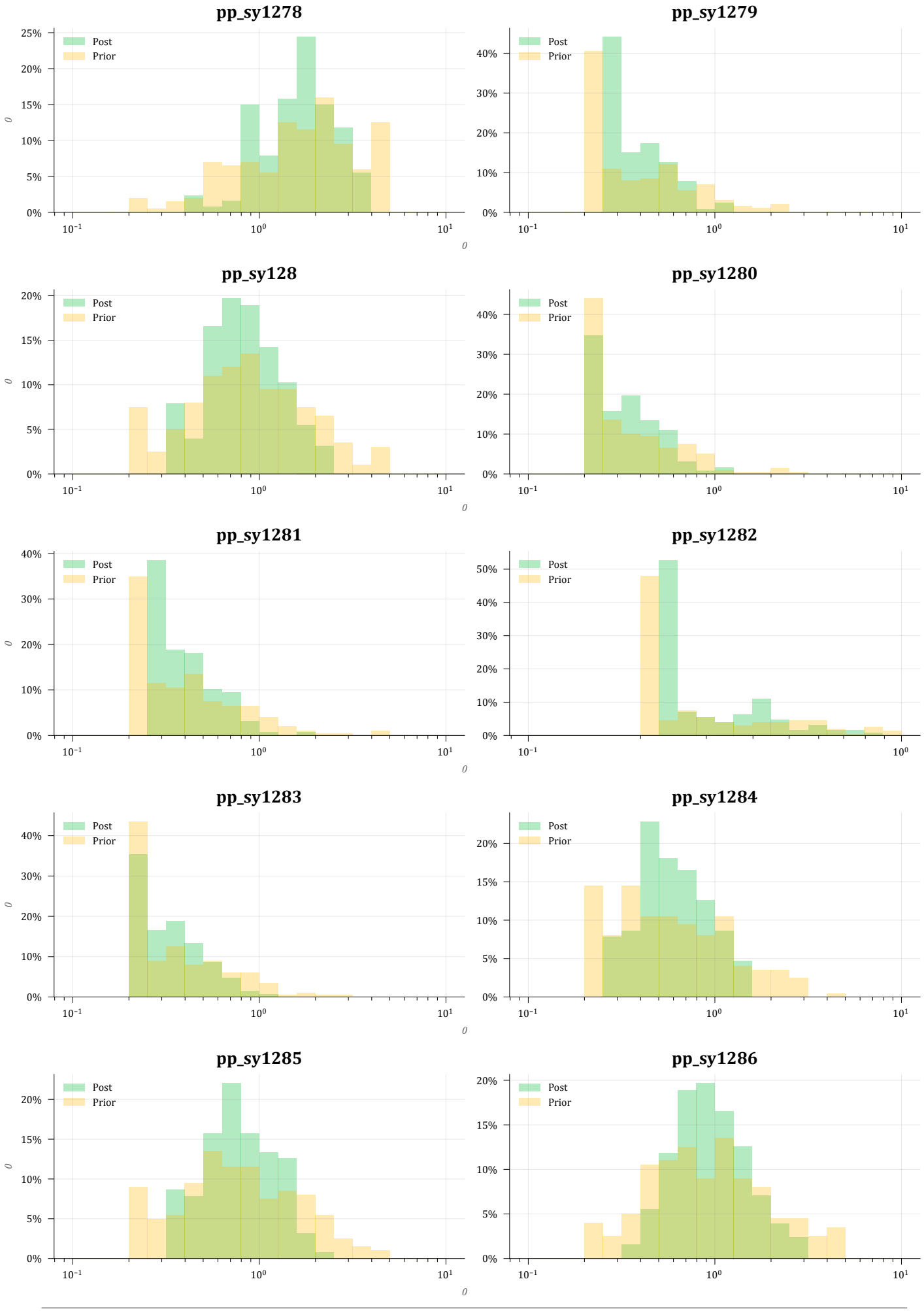

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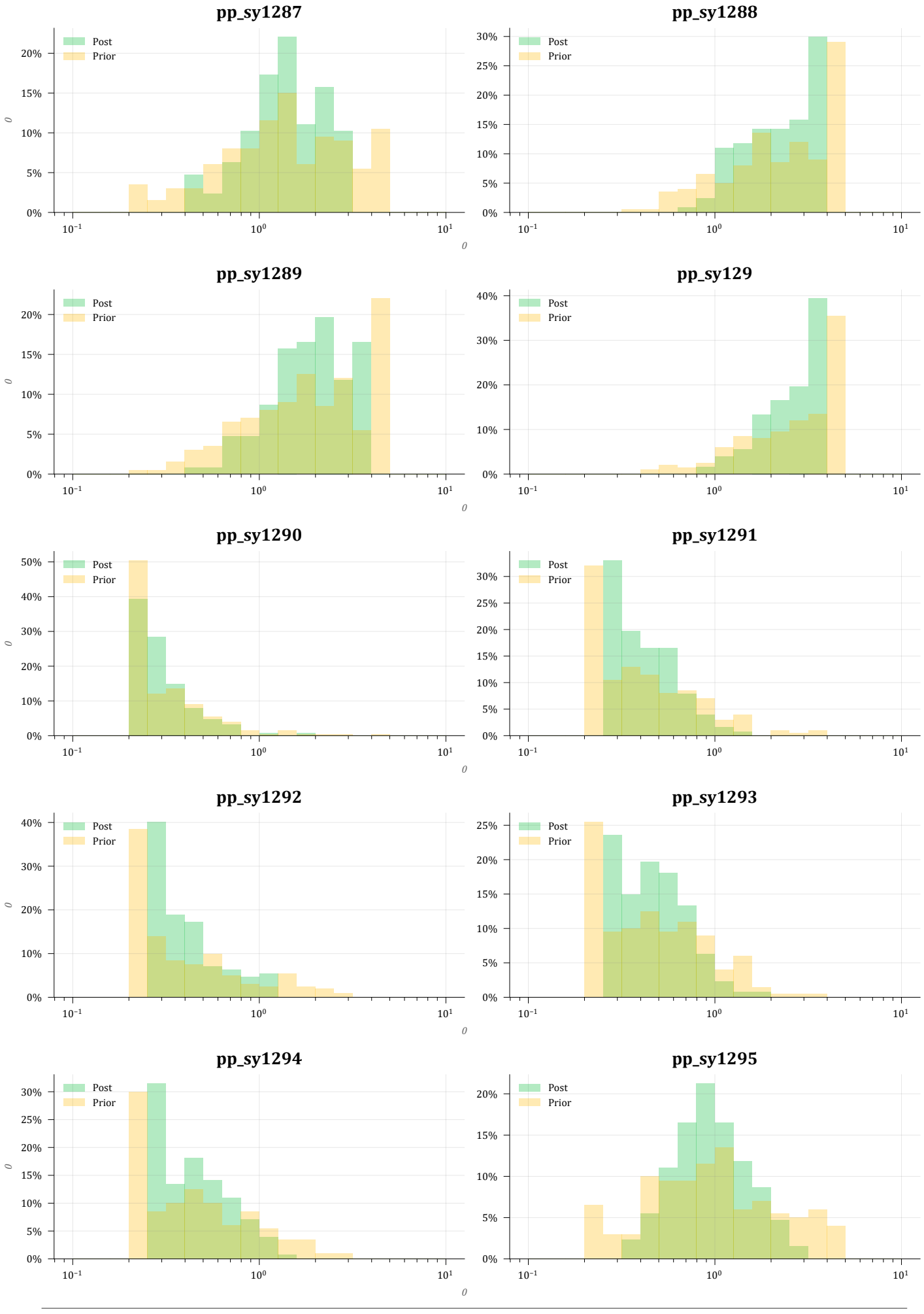

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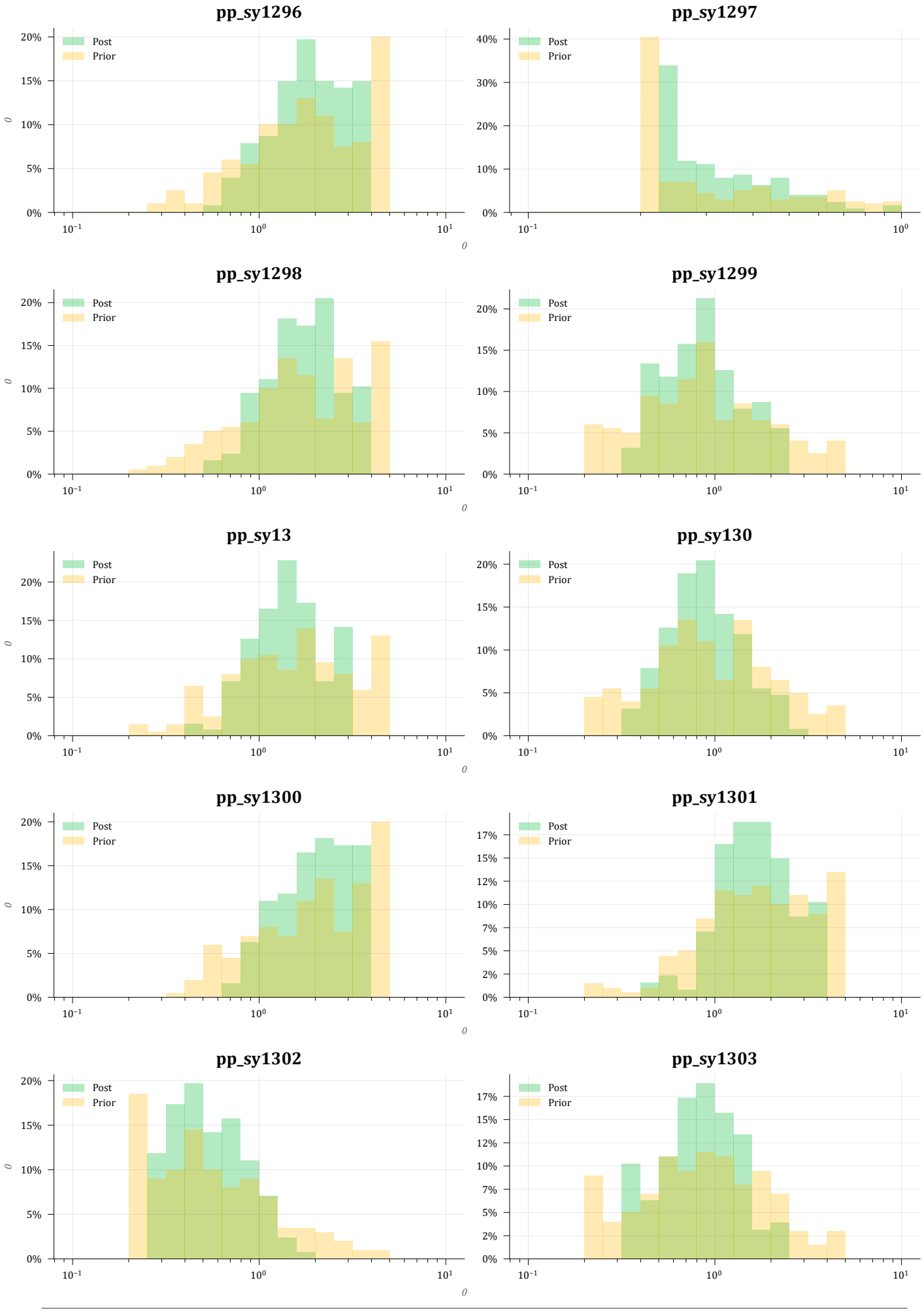

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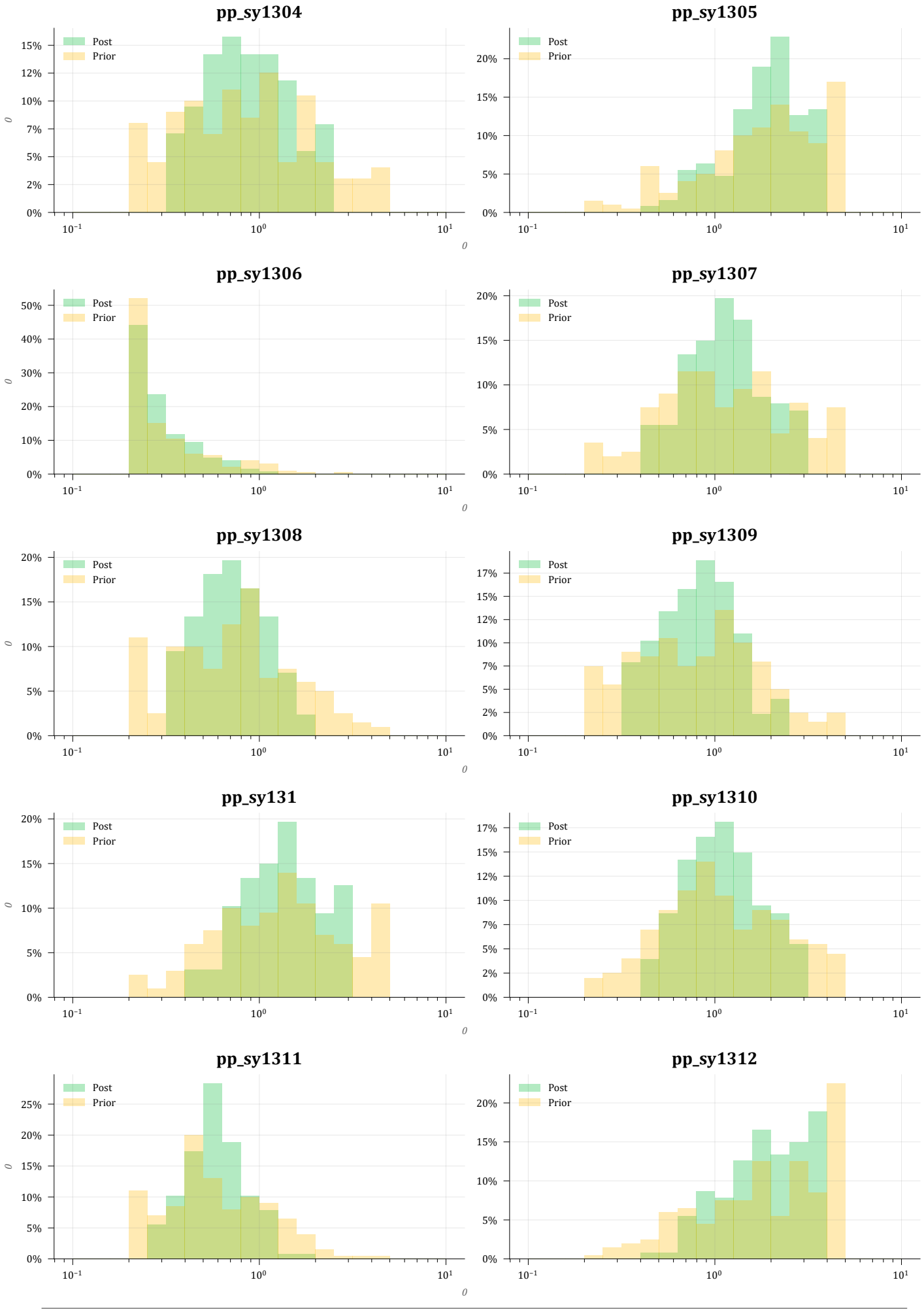

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10^{1}


pp_sy1269
pp_sy127
pp_sy1270
pp_sy1271
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pp_sy1273
pp_sy1274
pp_sy1275
pp_sy1276
pp_sy1277
Post
Prior
0
Parameters


pp_sy1278
pp_sy1279
pp_sy128
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pp_sy1284
pp_sy1285
pp_sy1286
Post
Prior
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pp_sy1287
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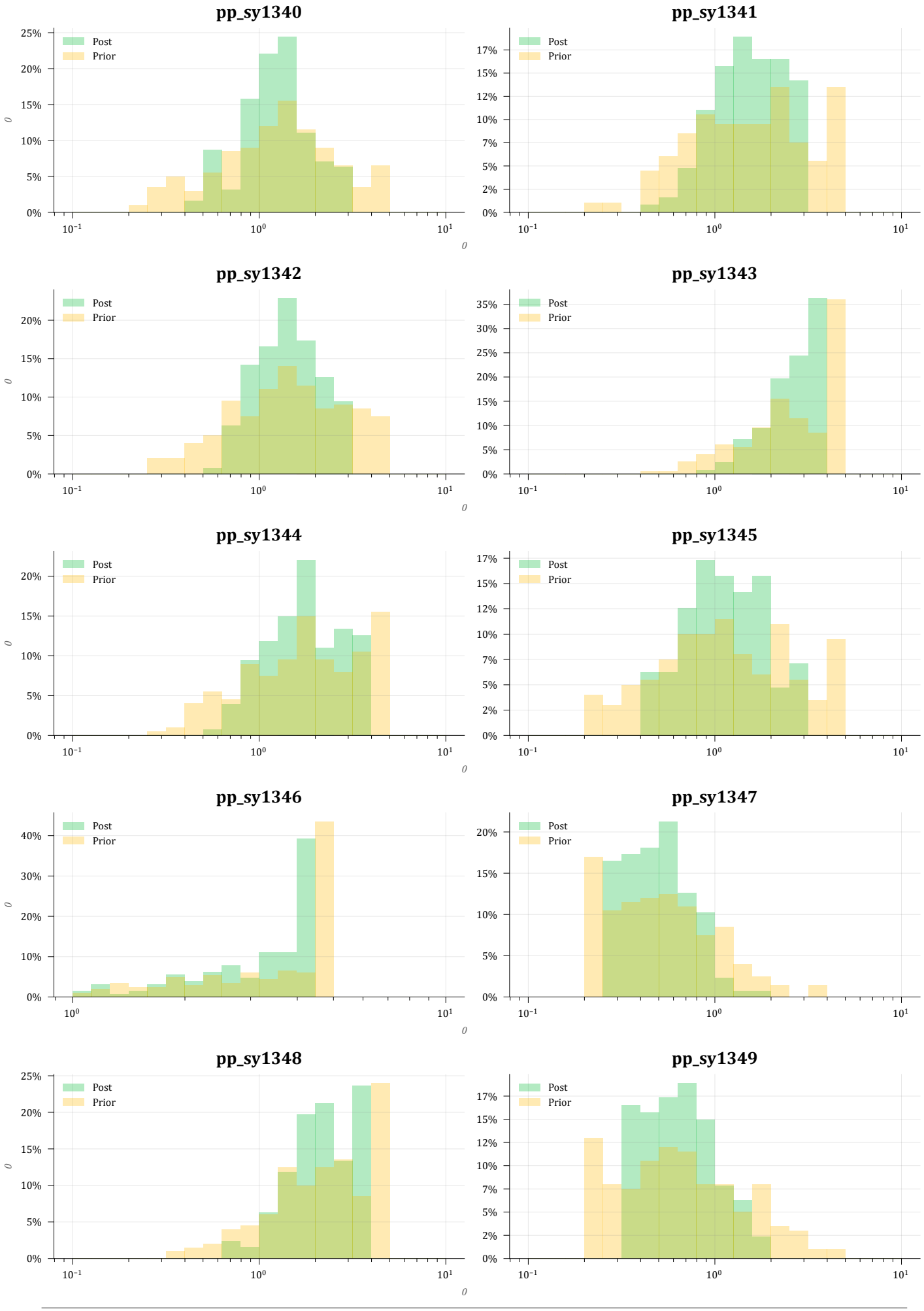

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Post
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Parameters


pp_sy1304
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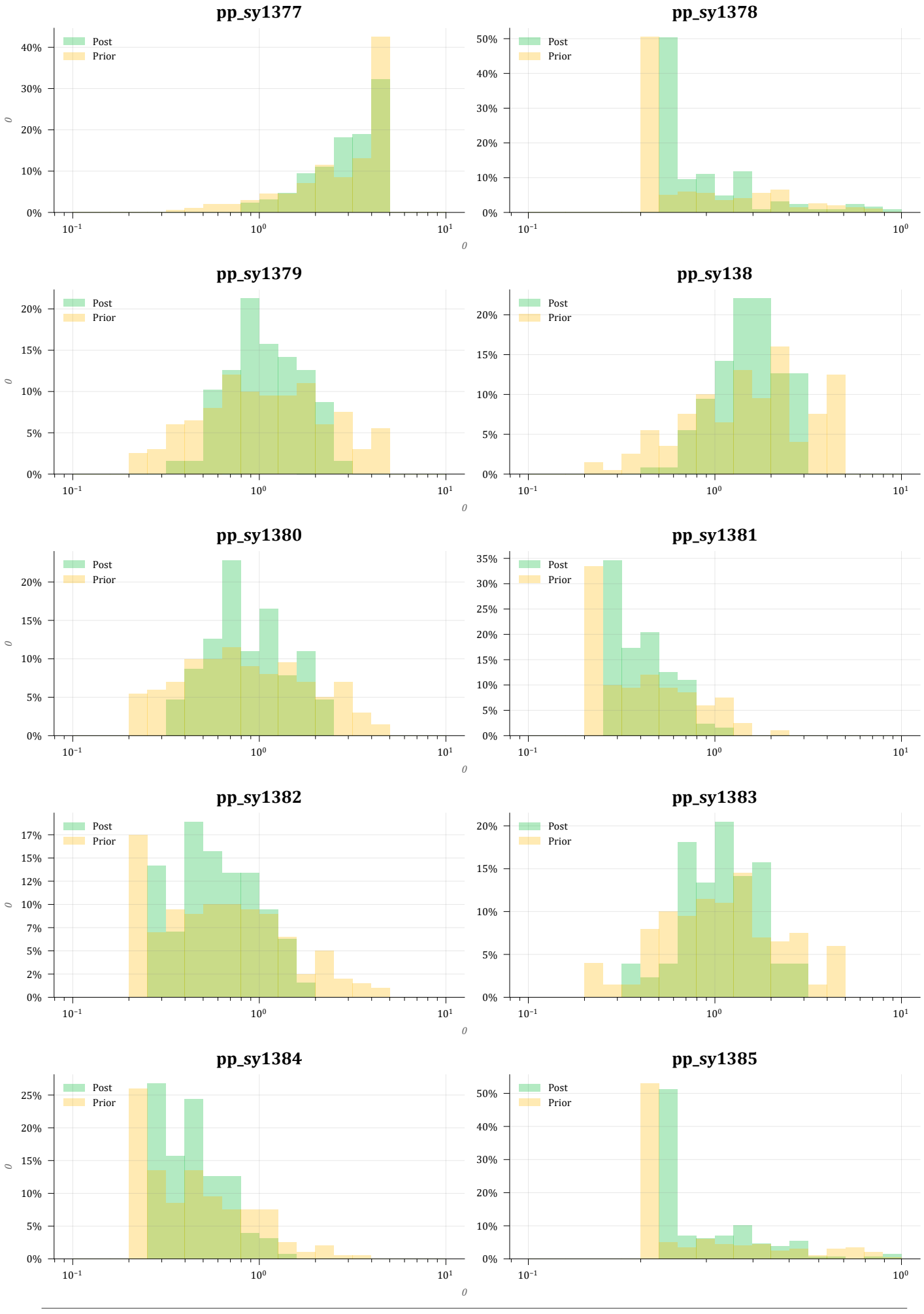

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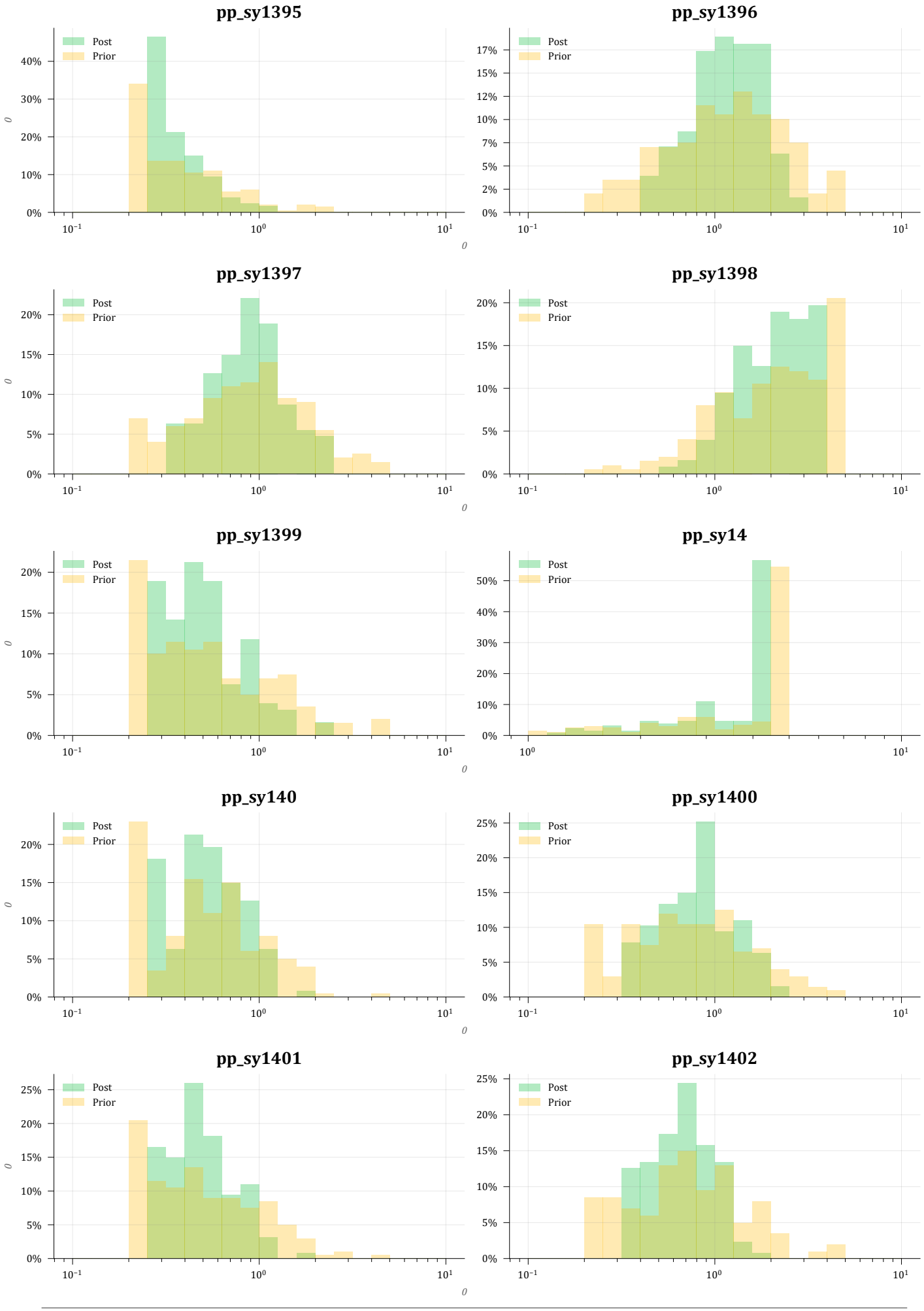

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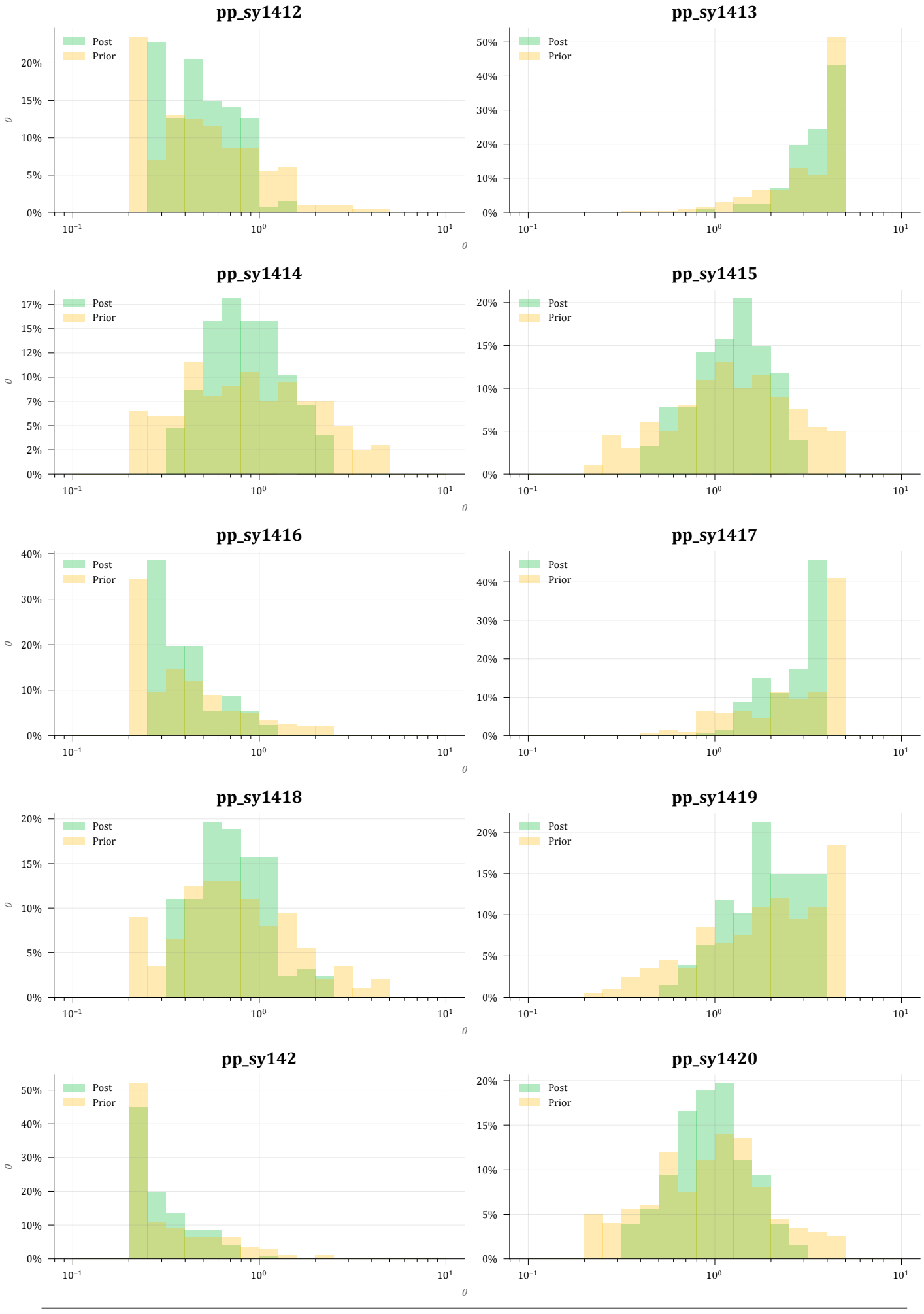

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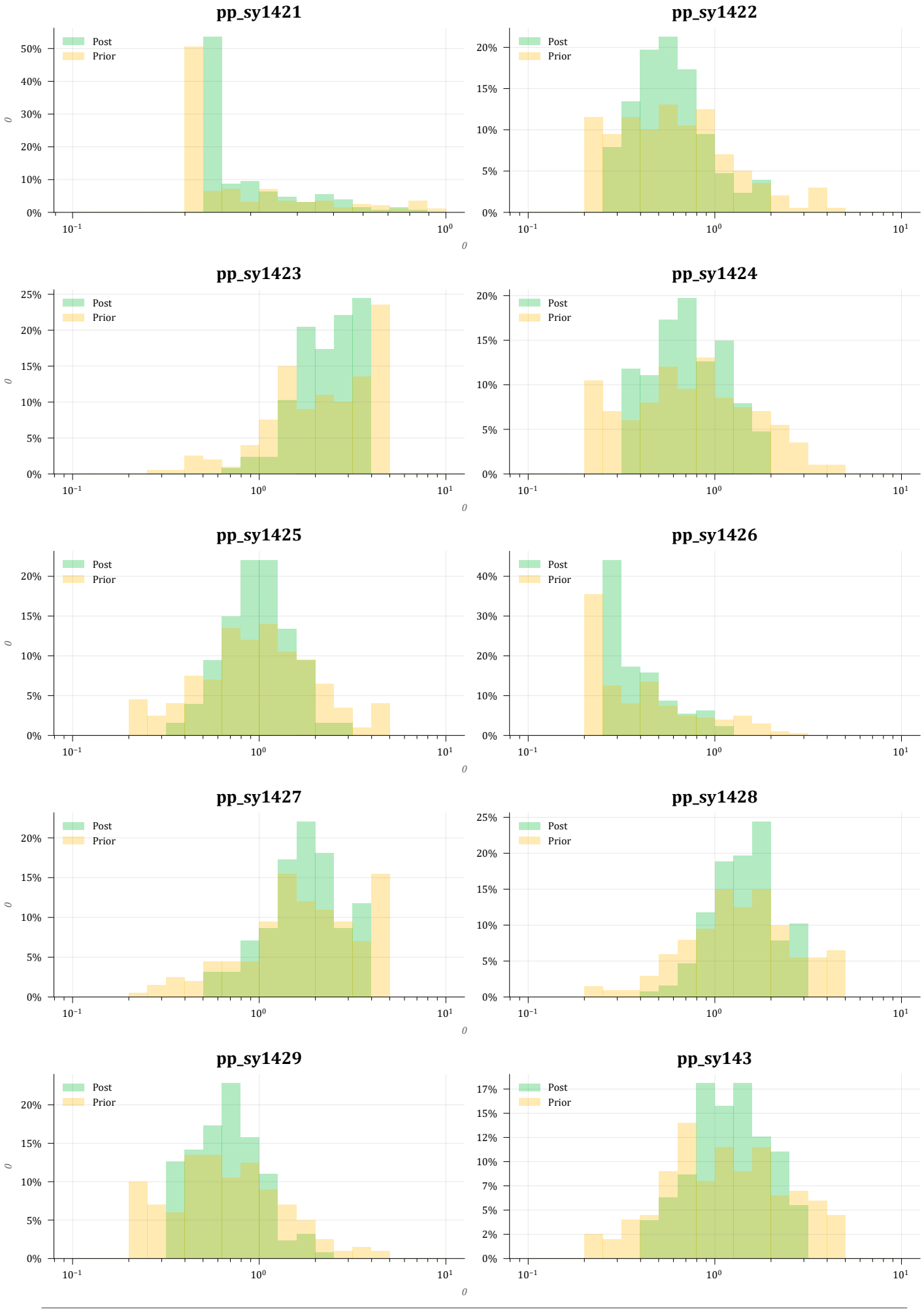

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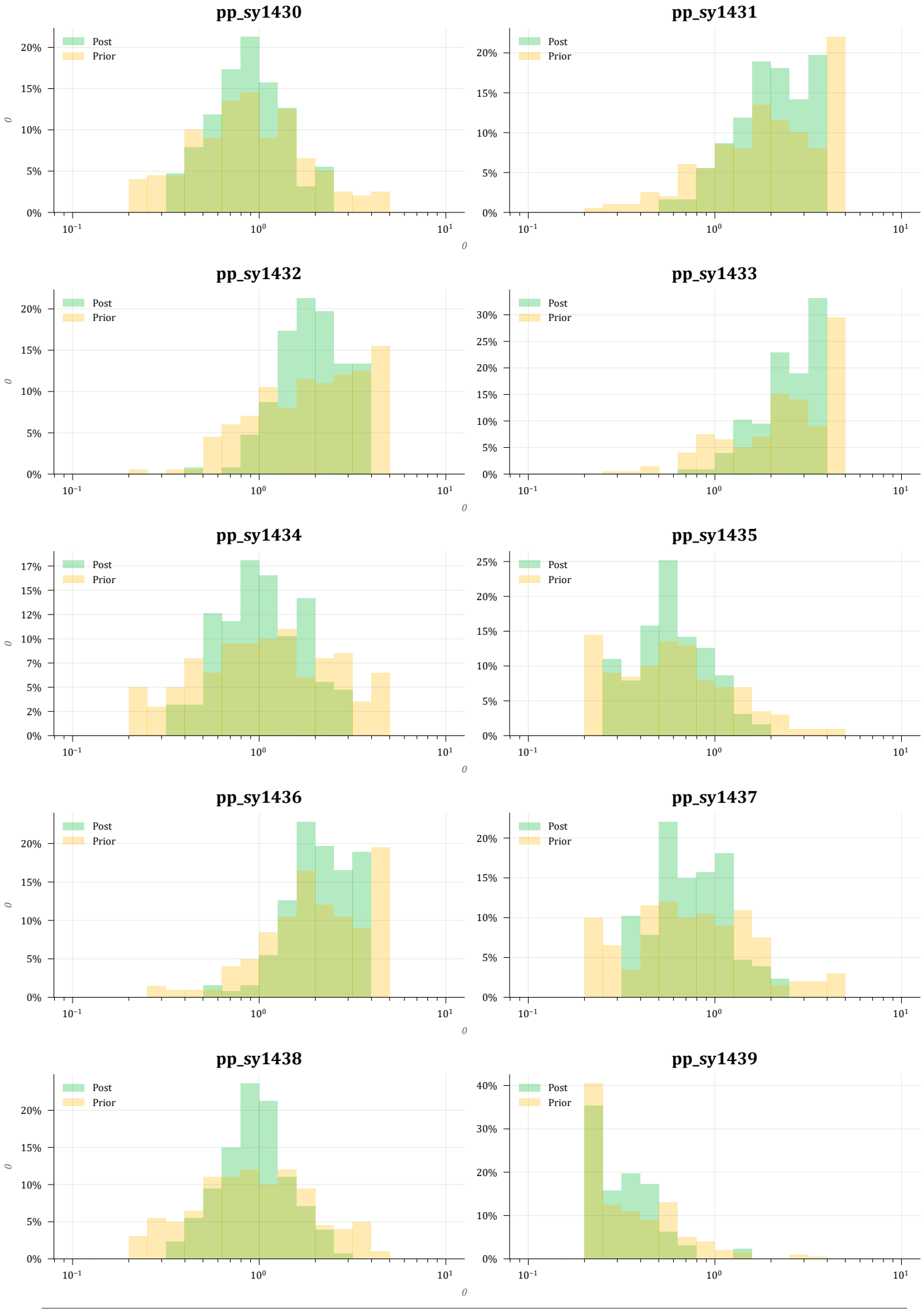

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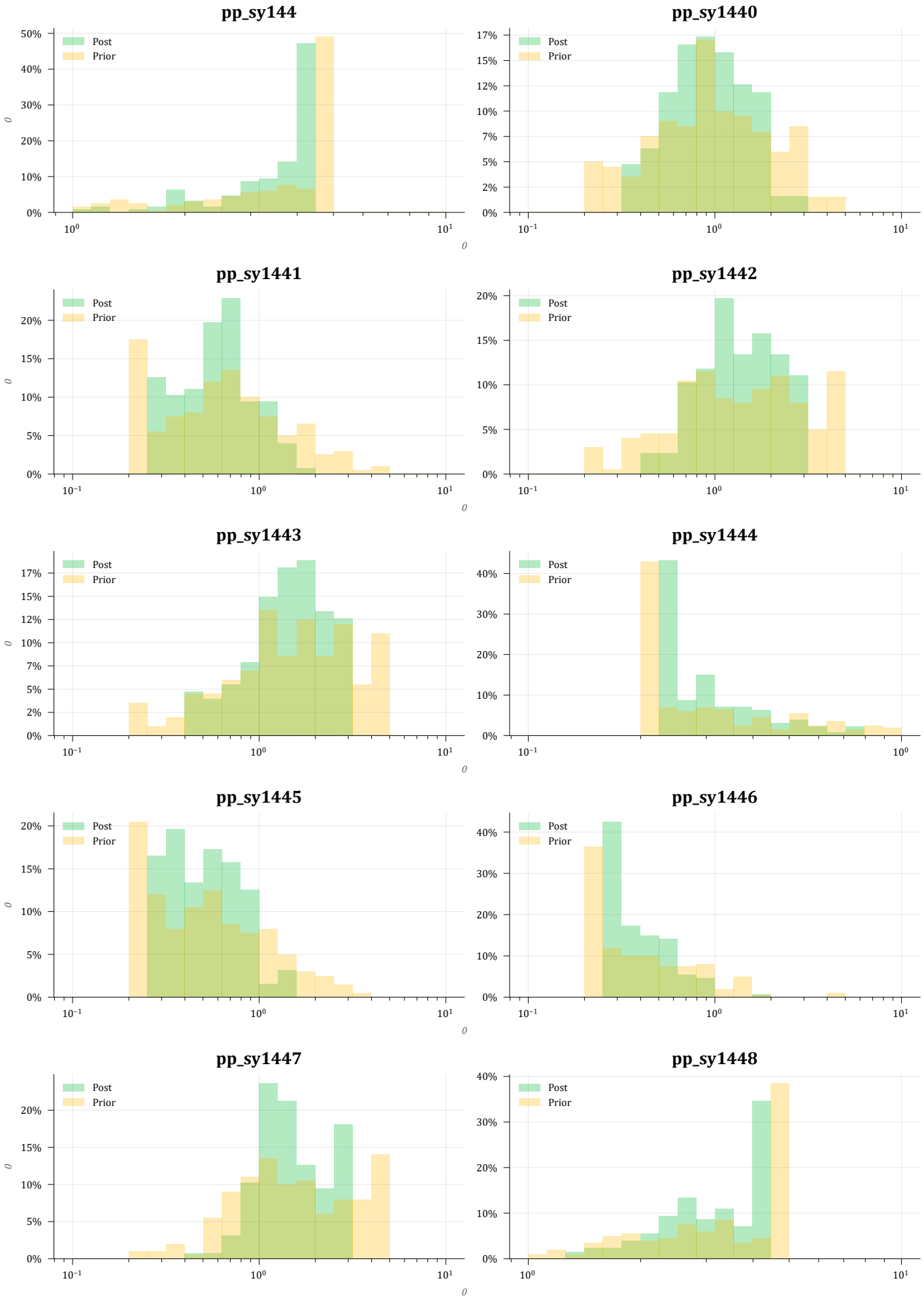

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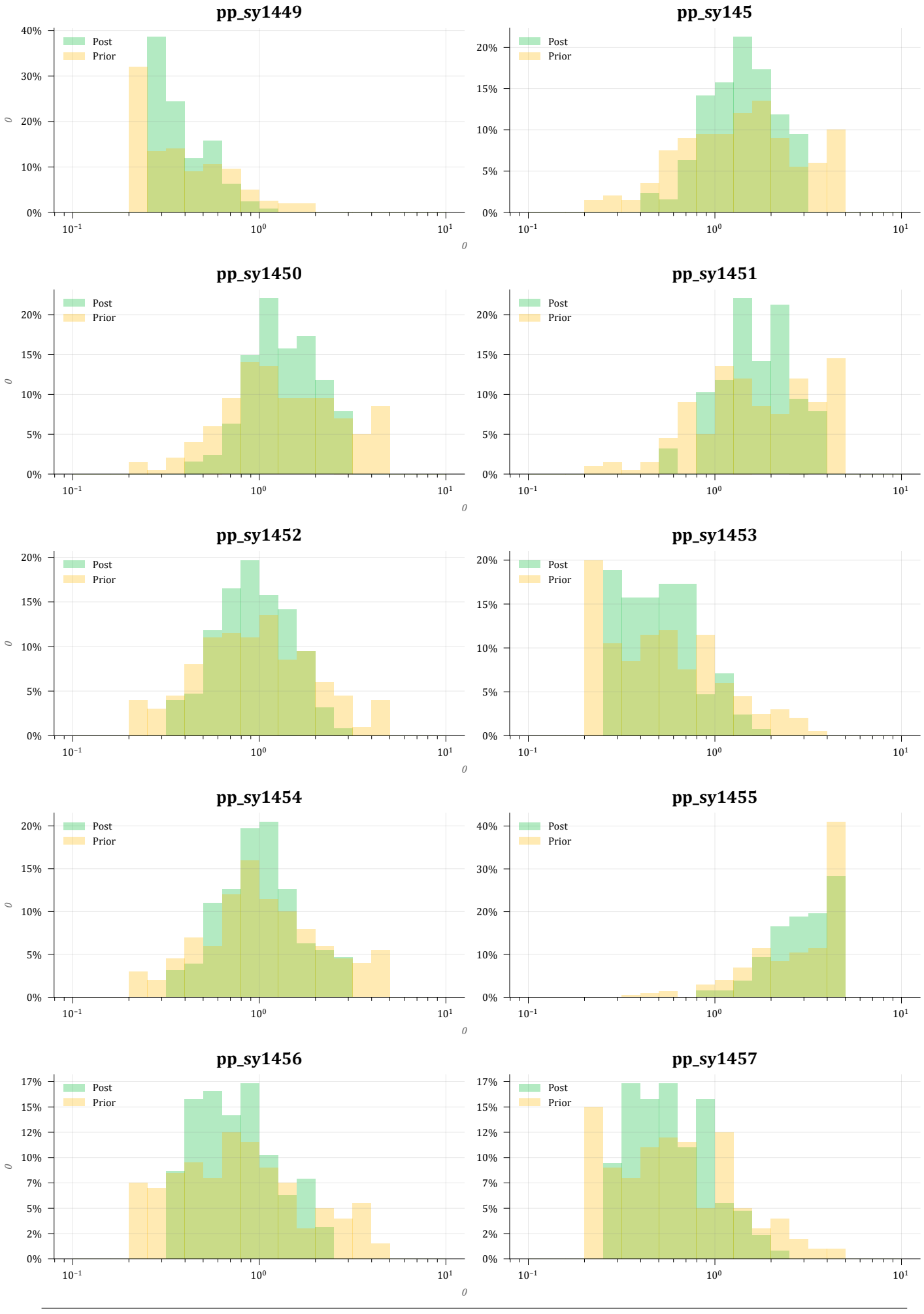

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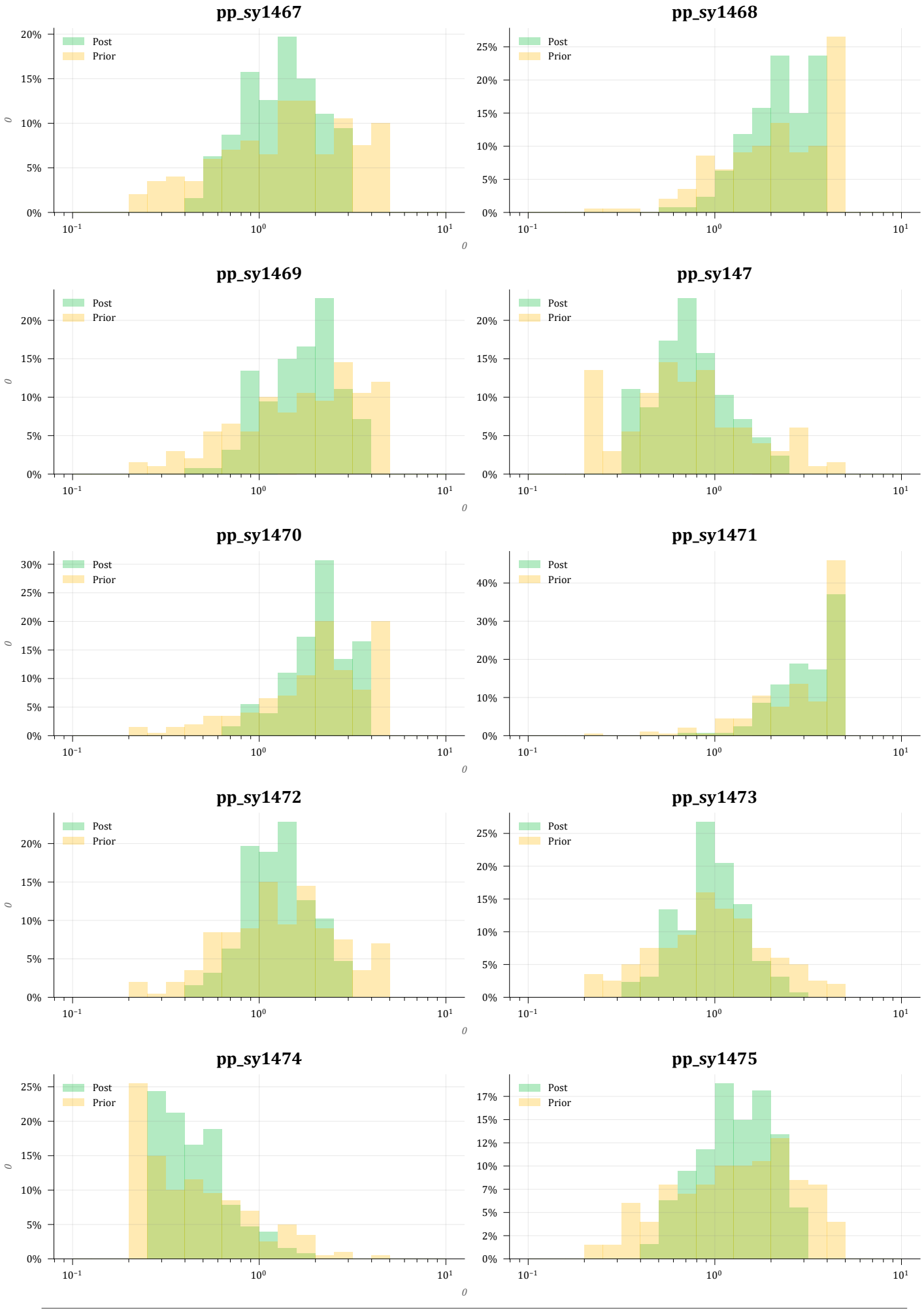

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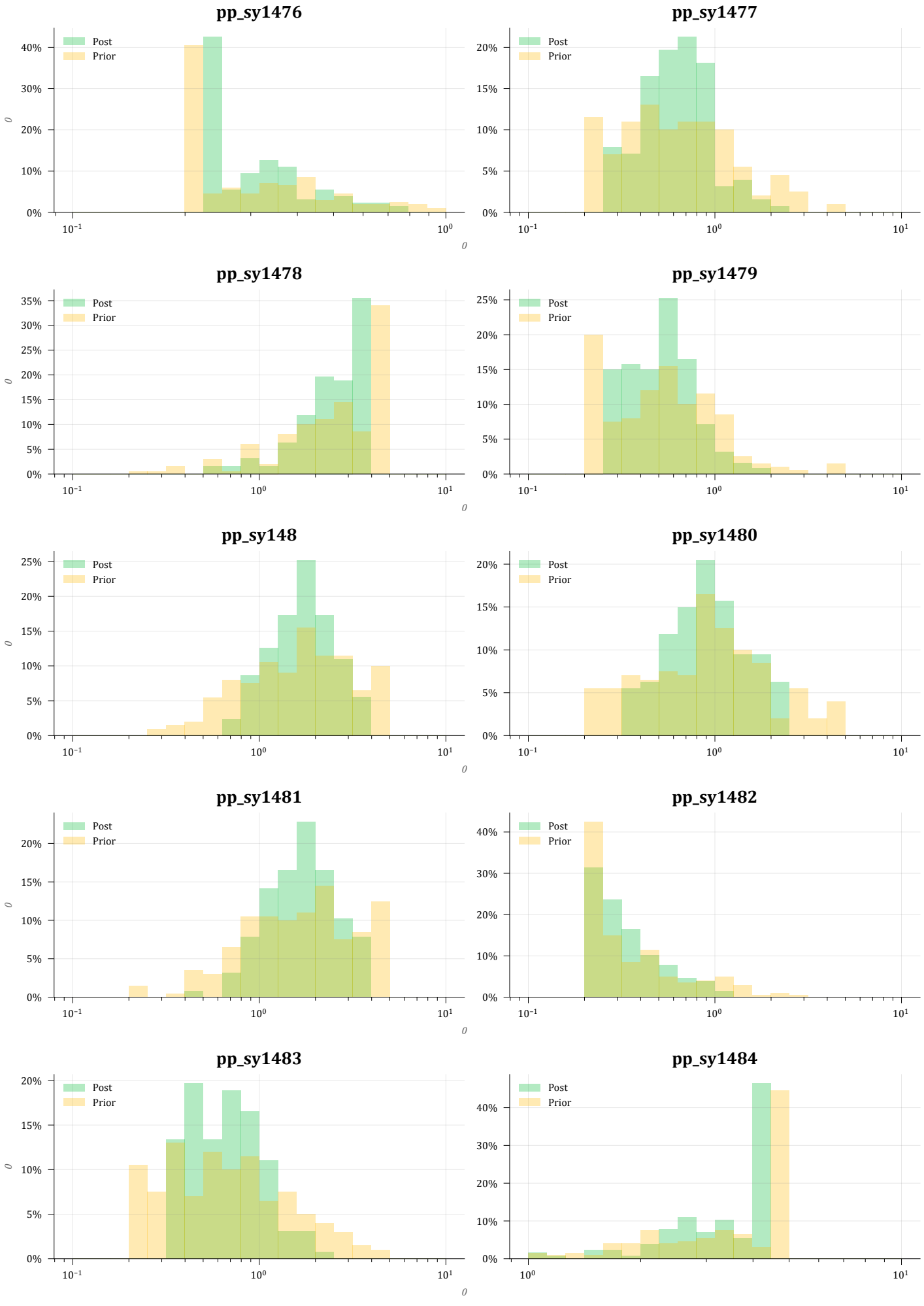

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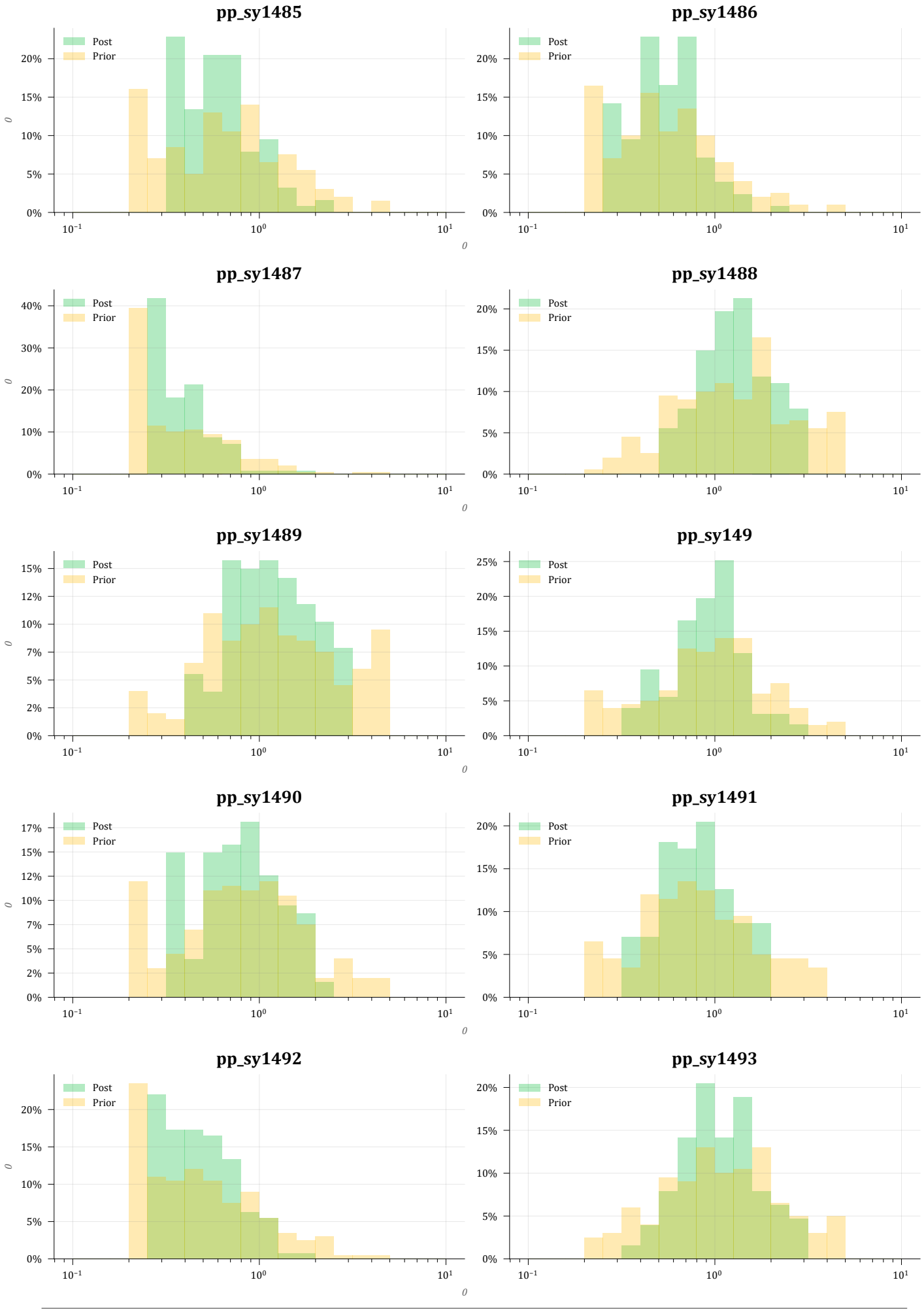

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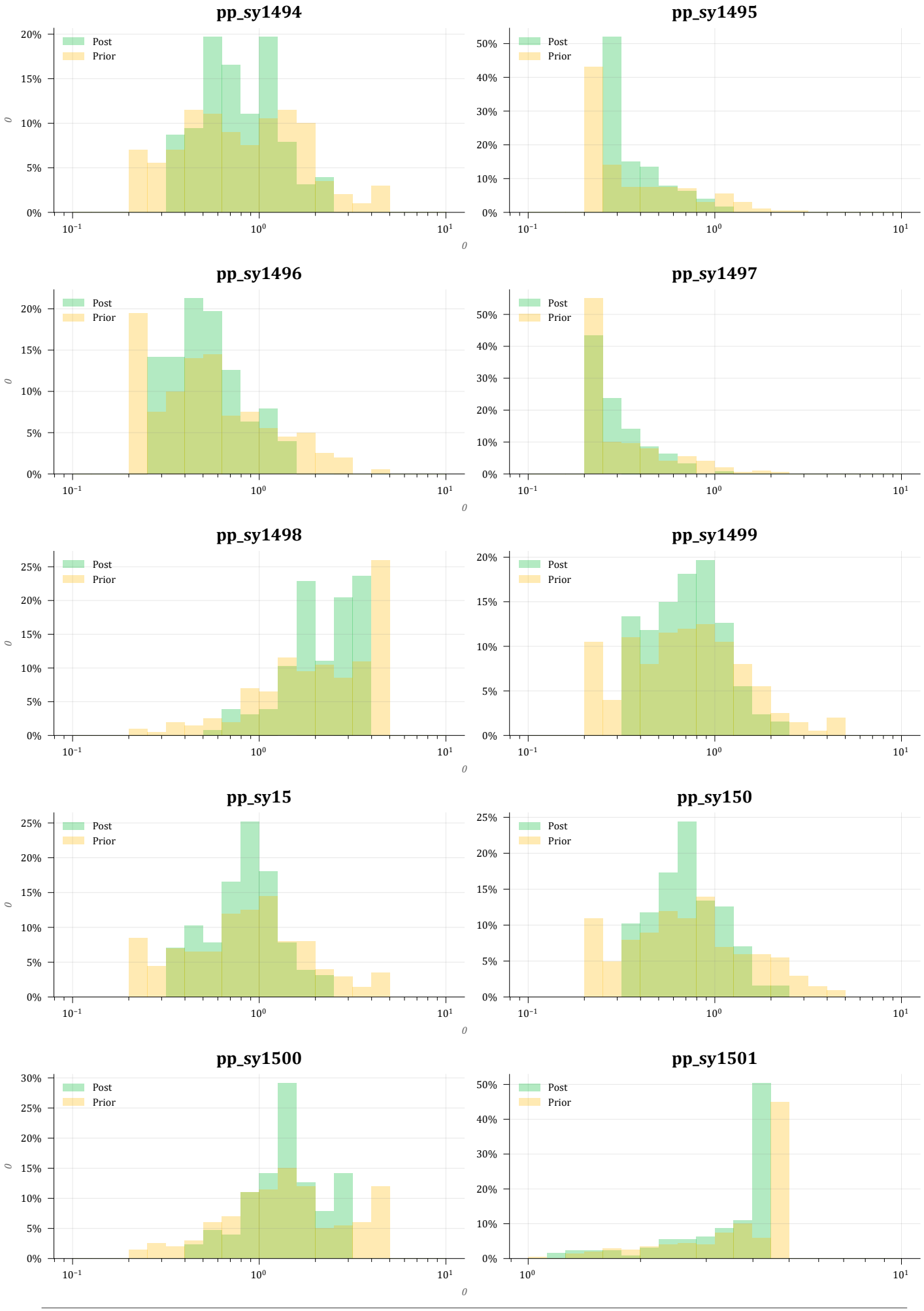

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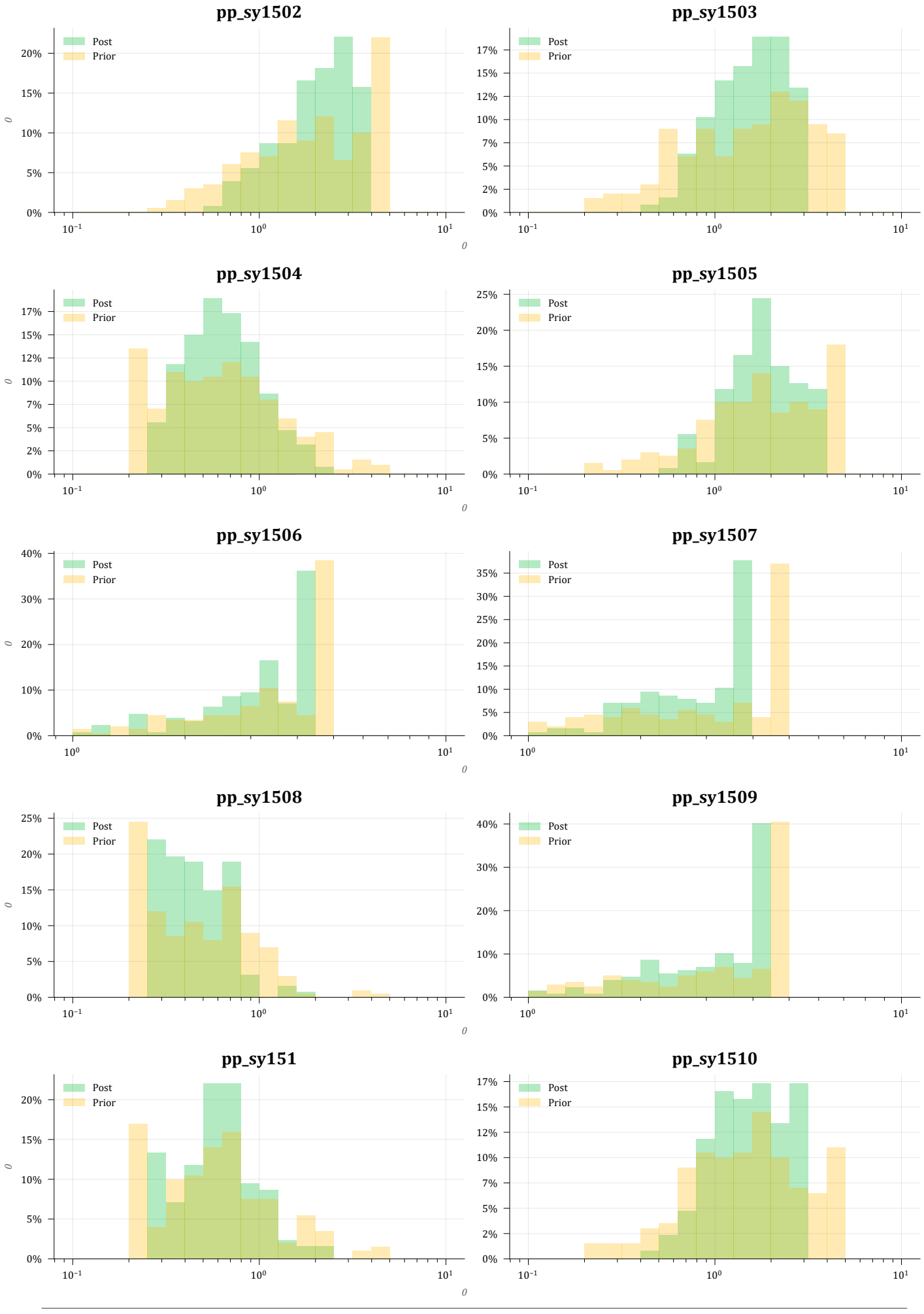

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Post
Prior
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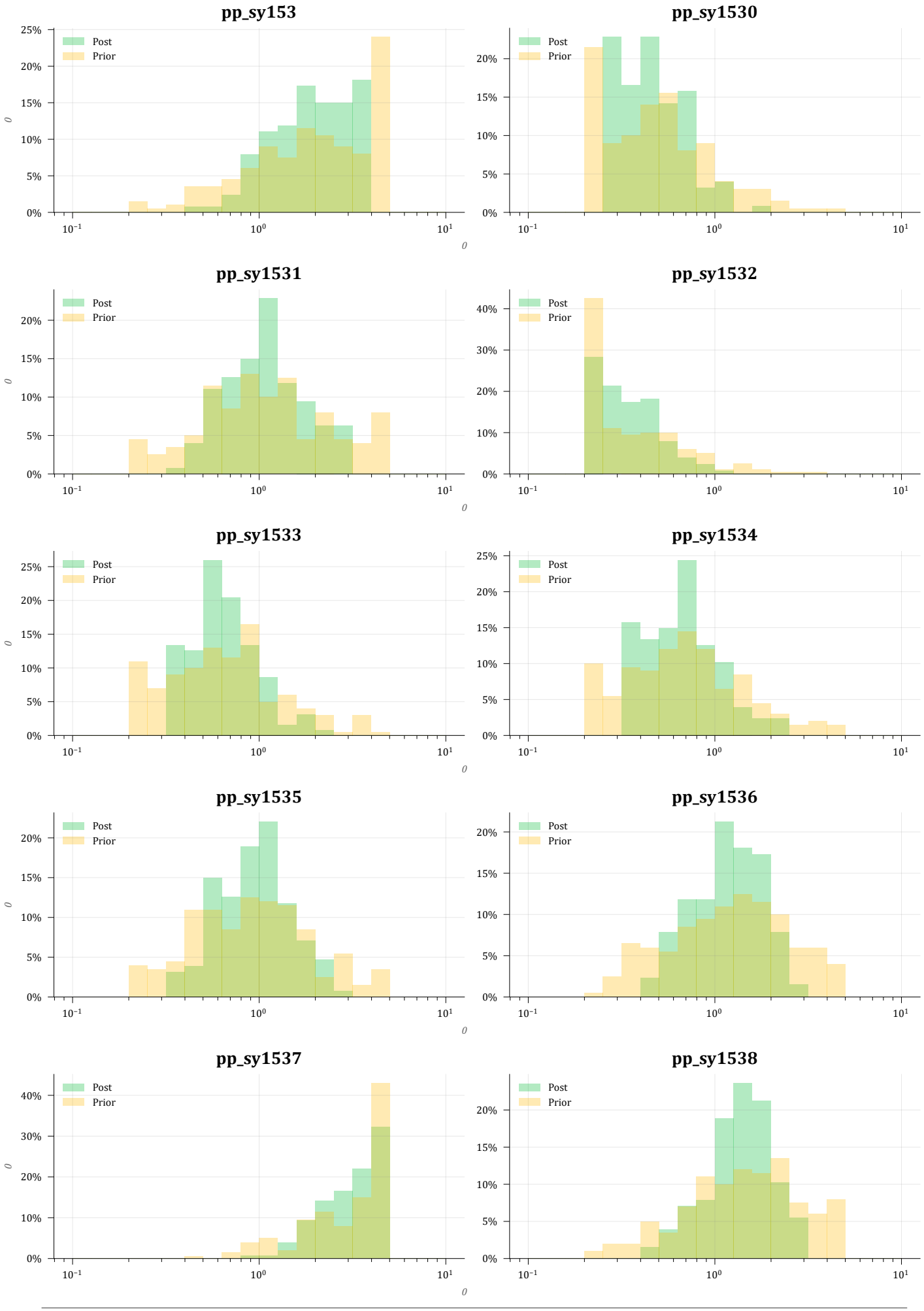

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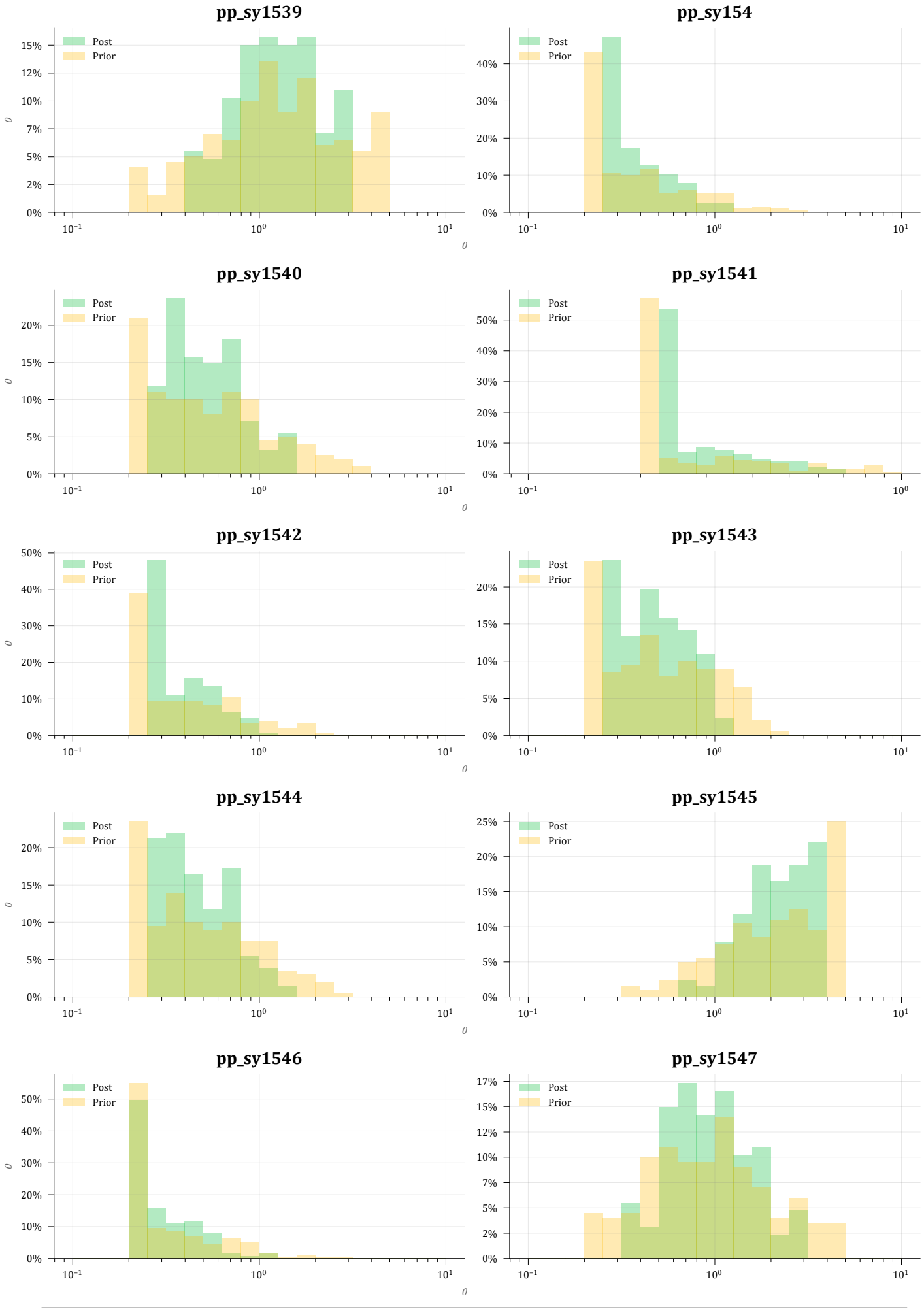

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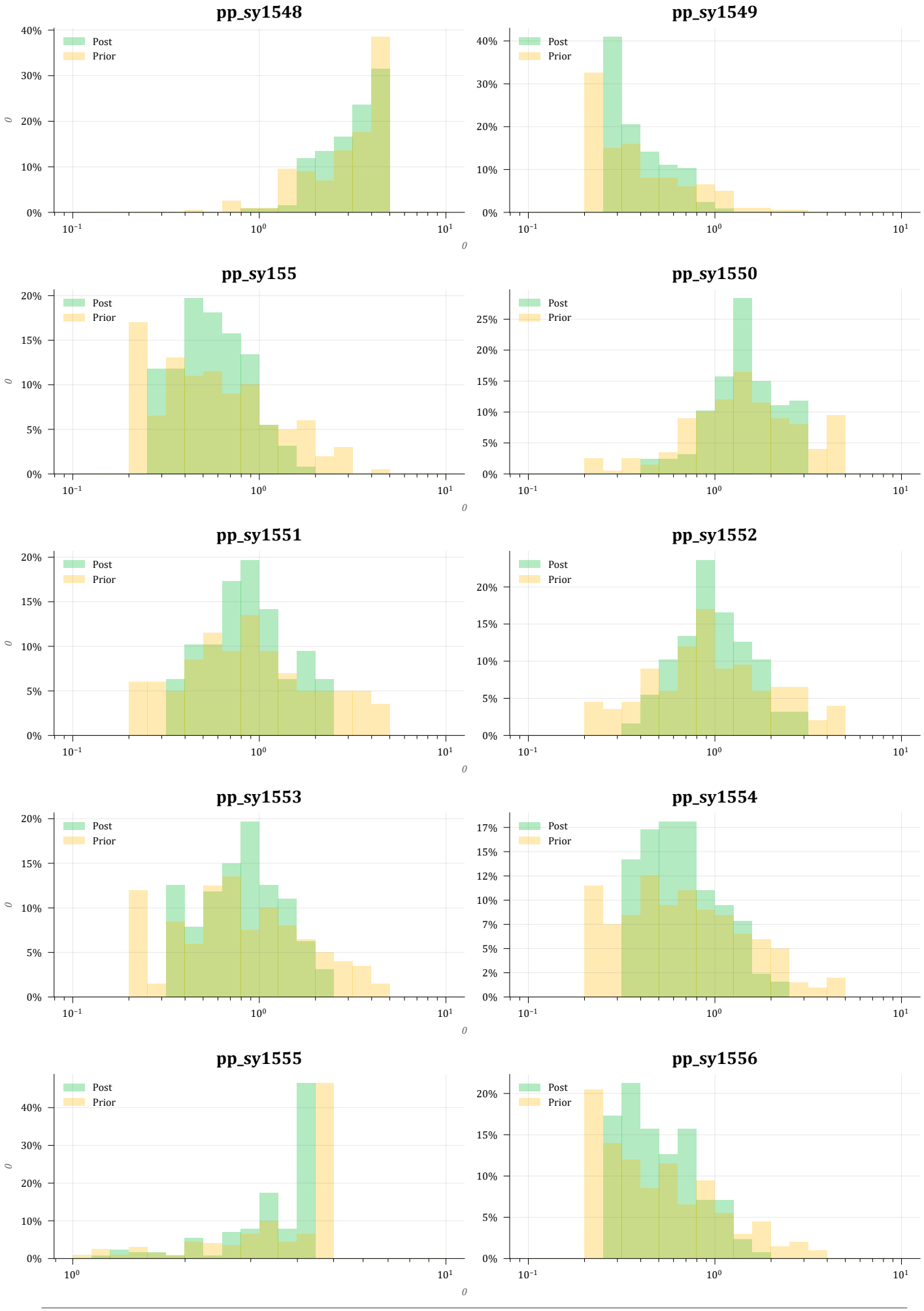

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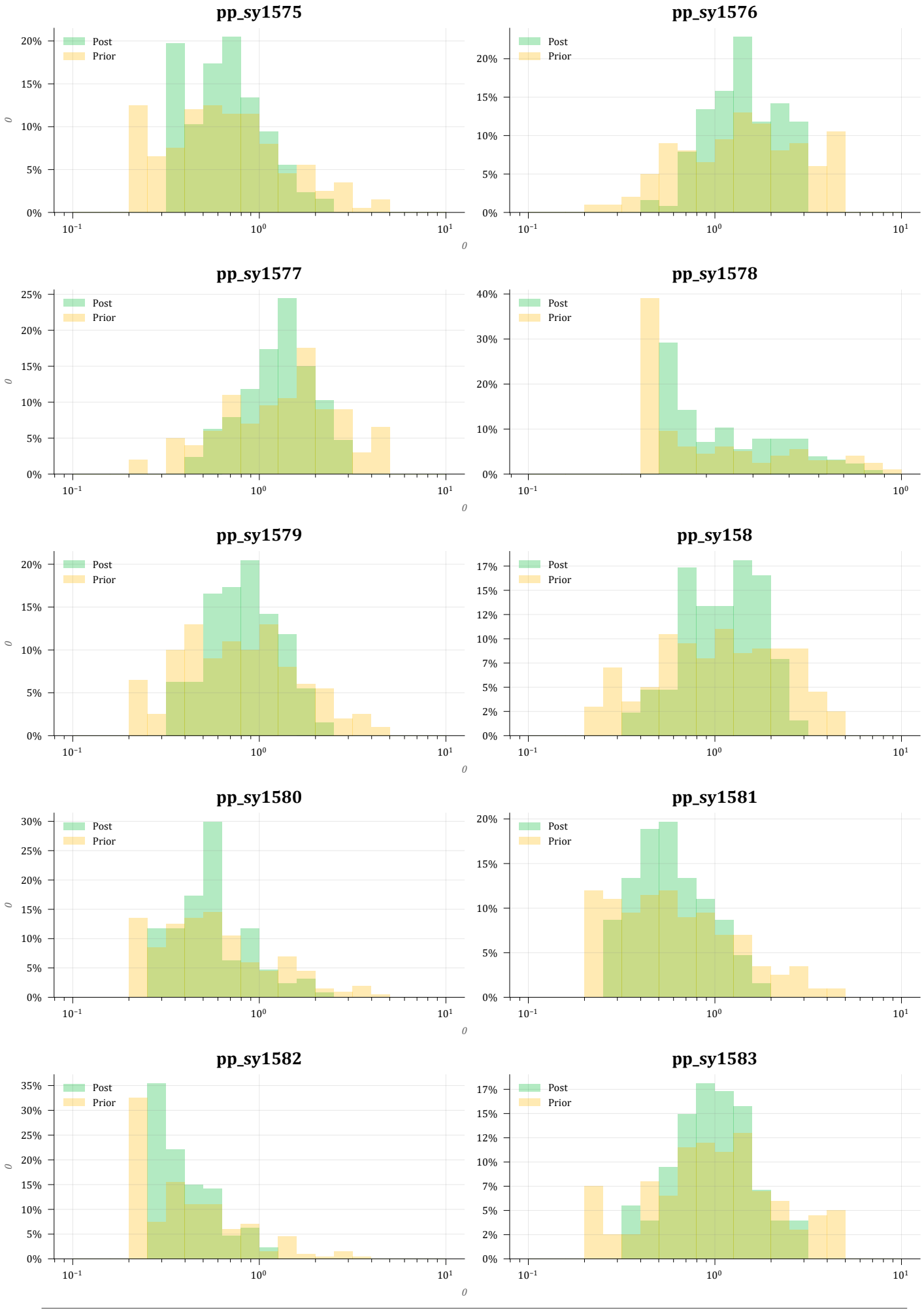

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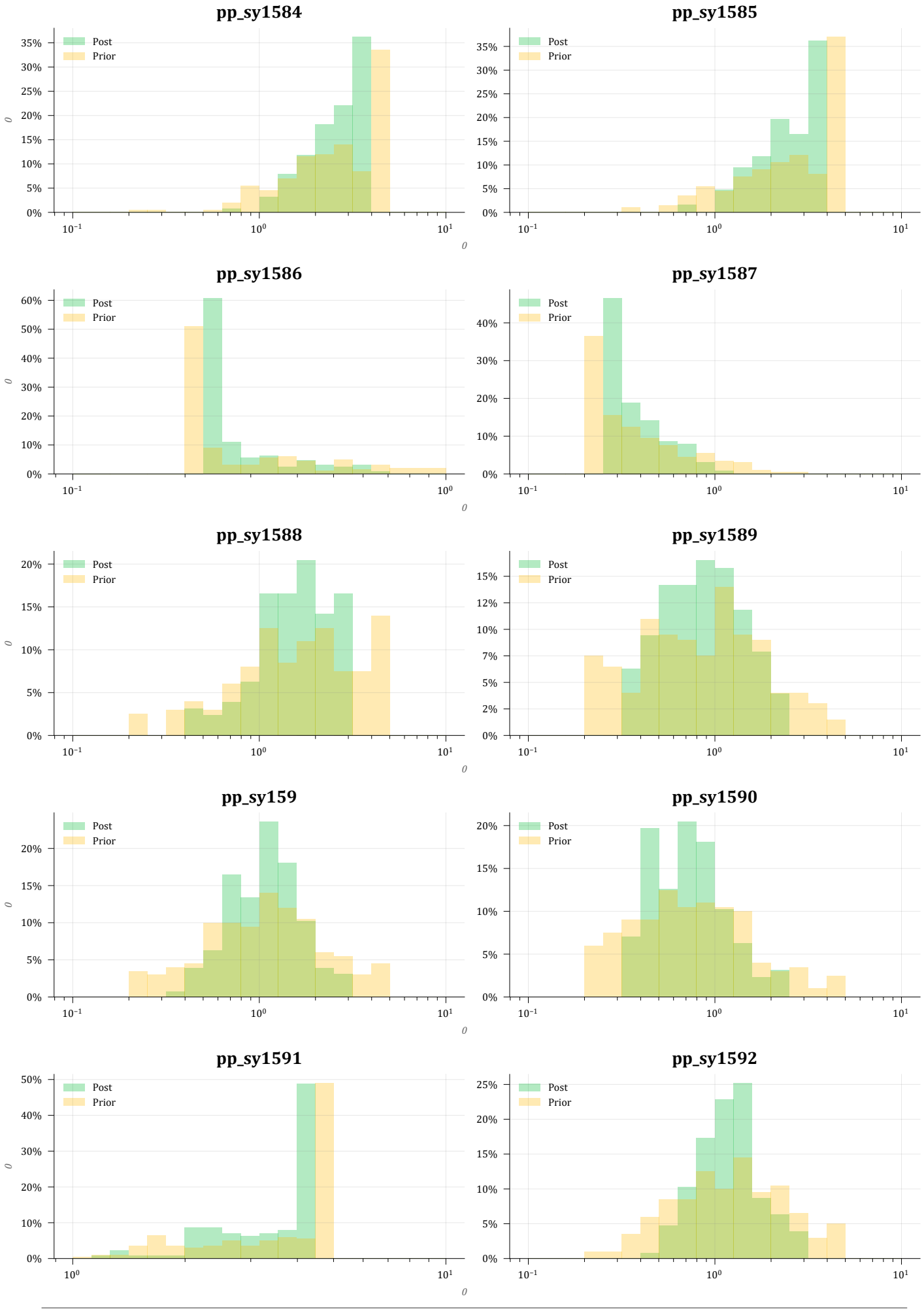

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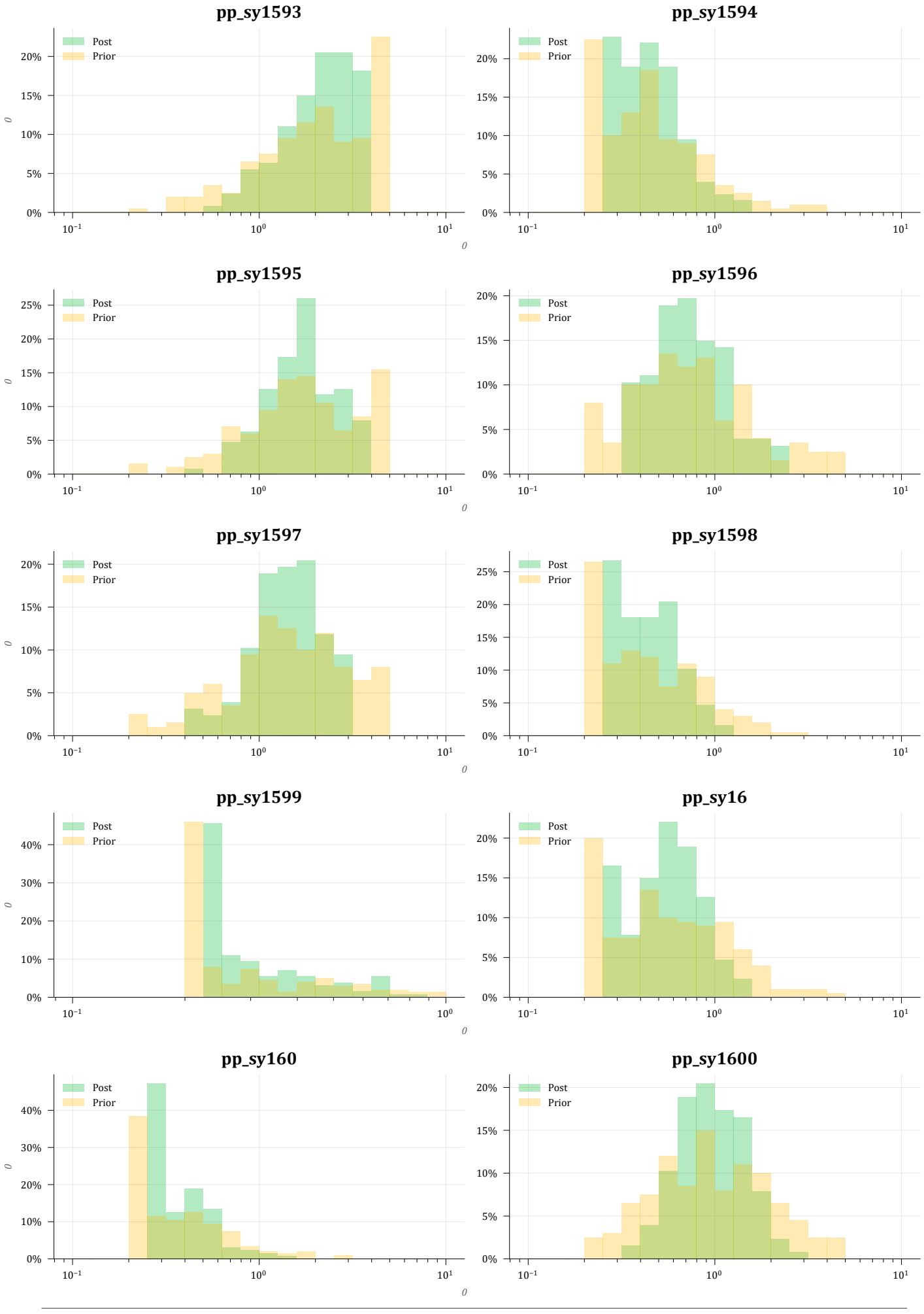

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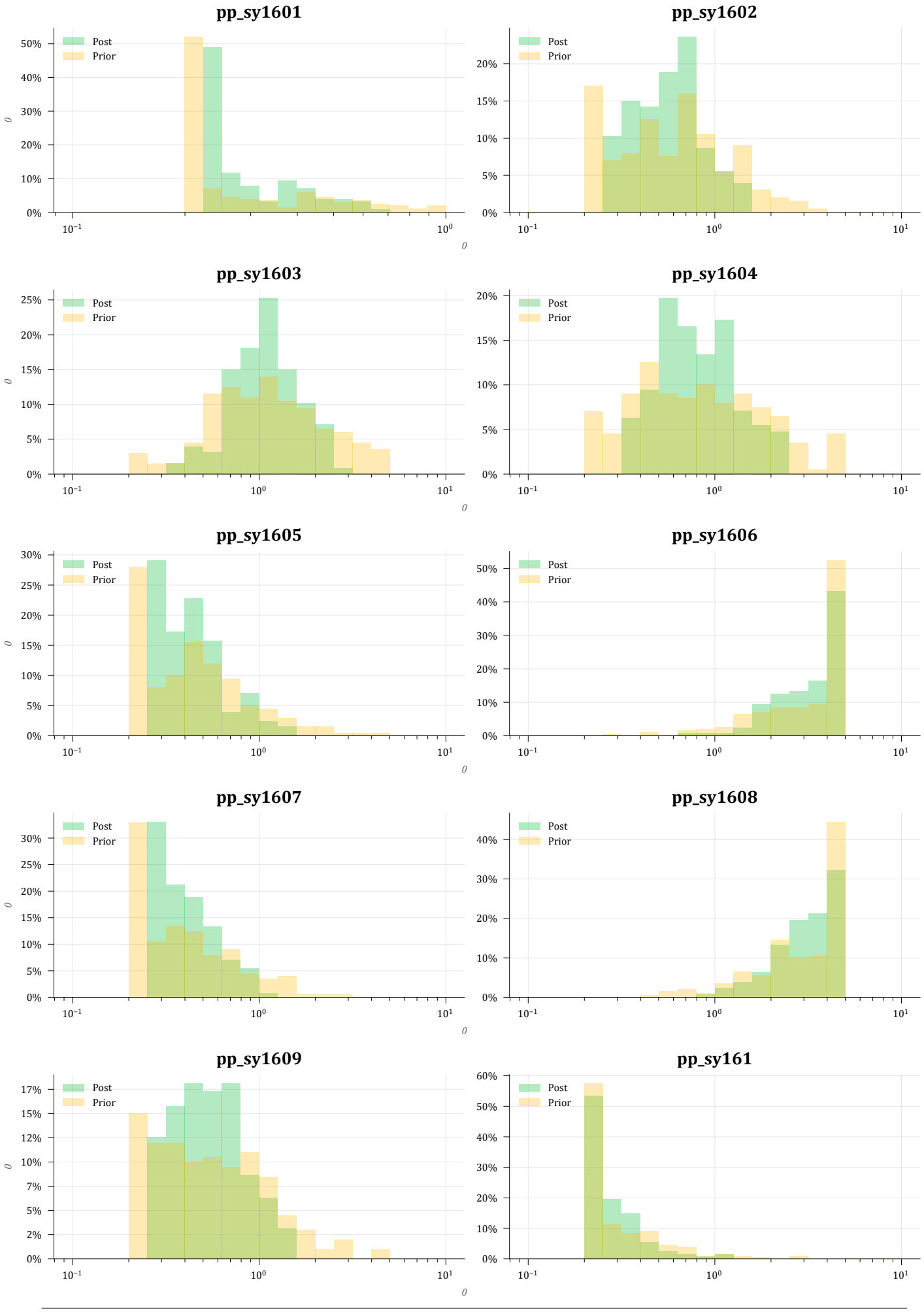

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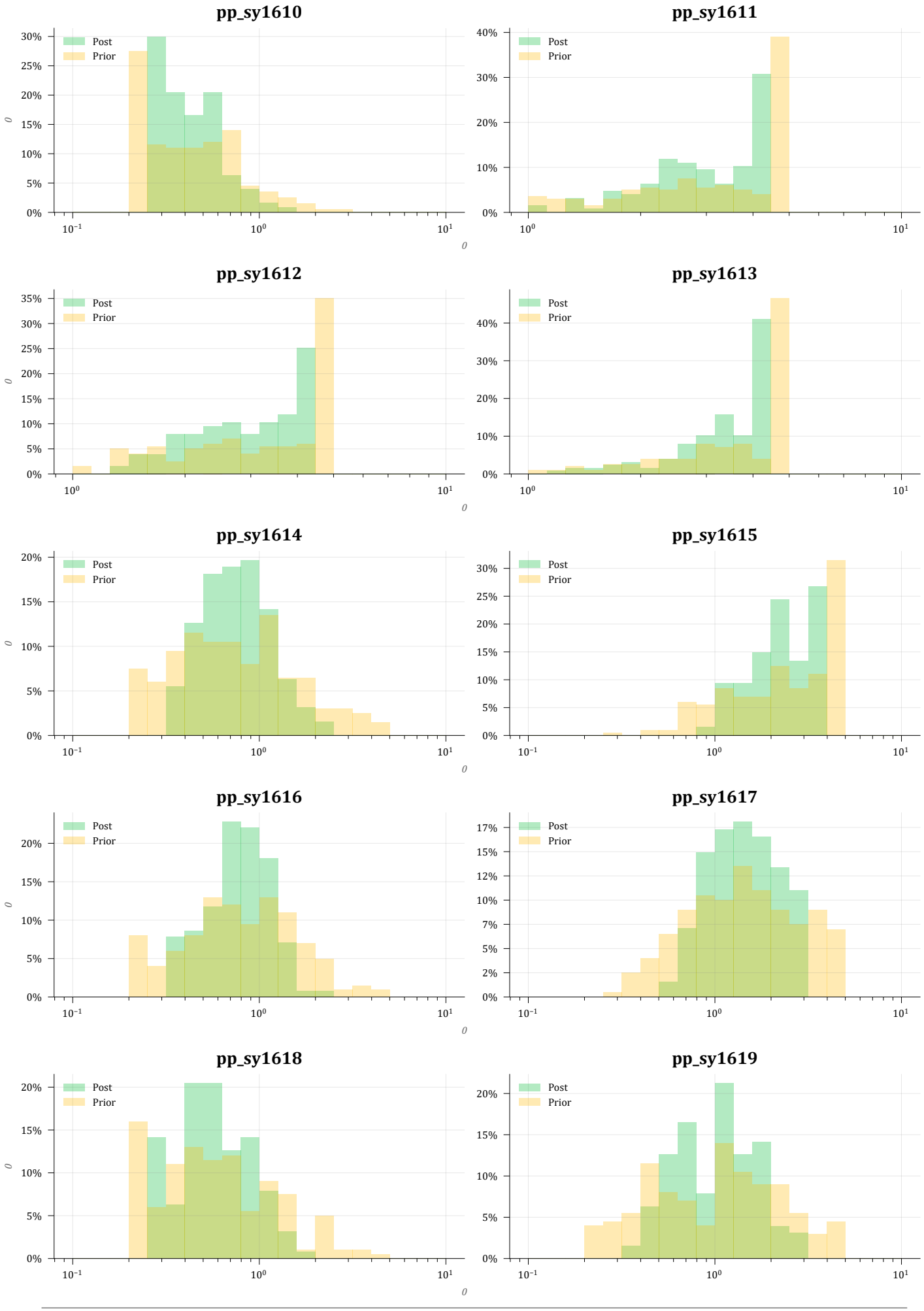

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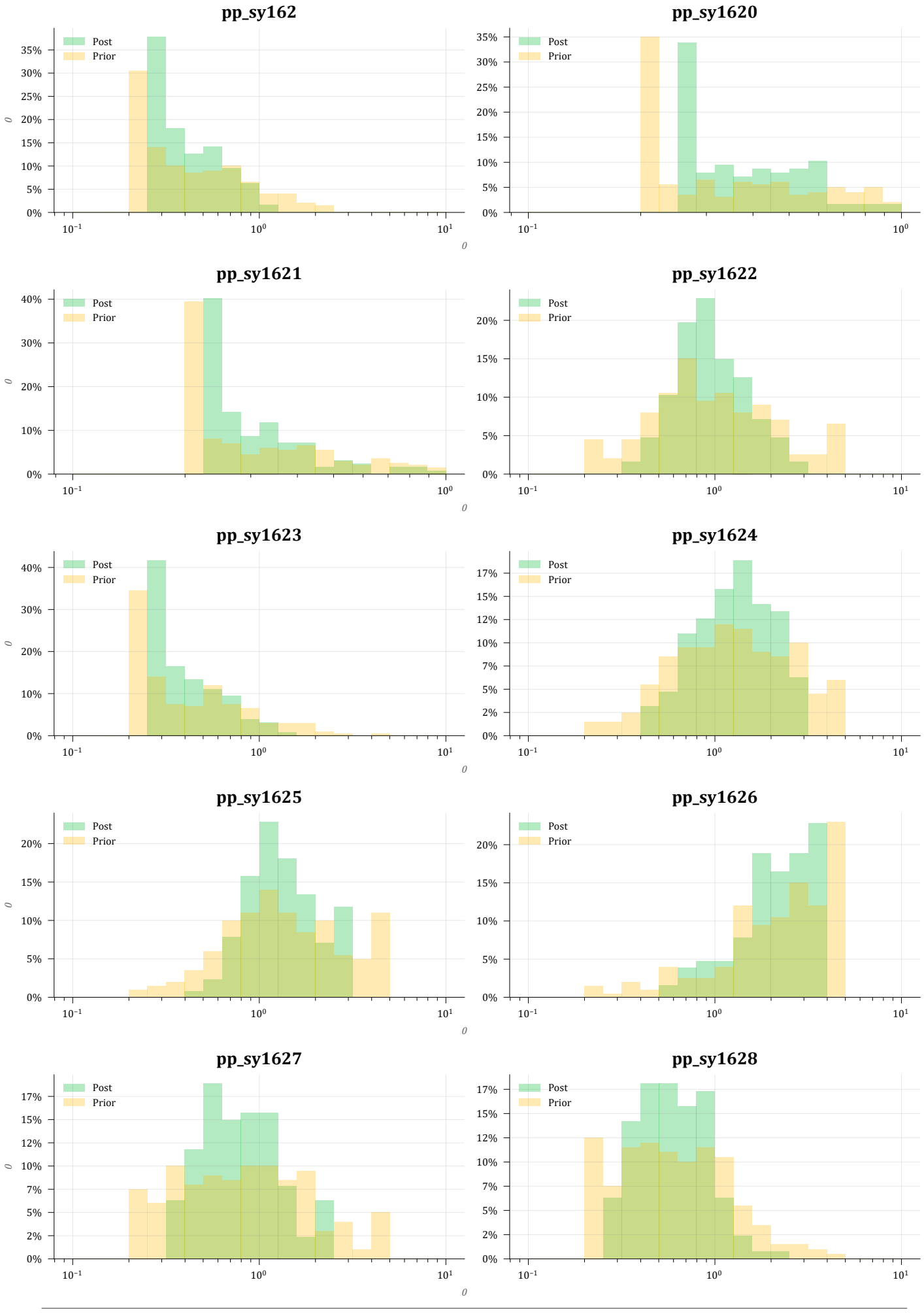

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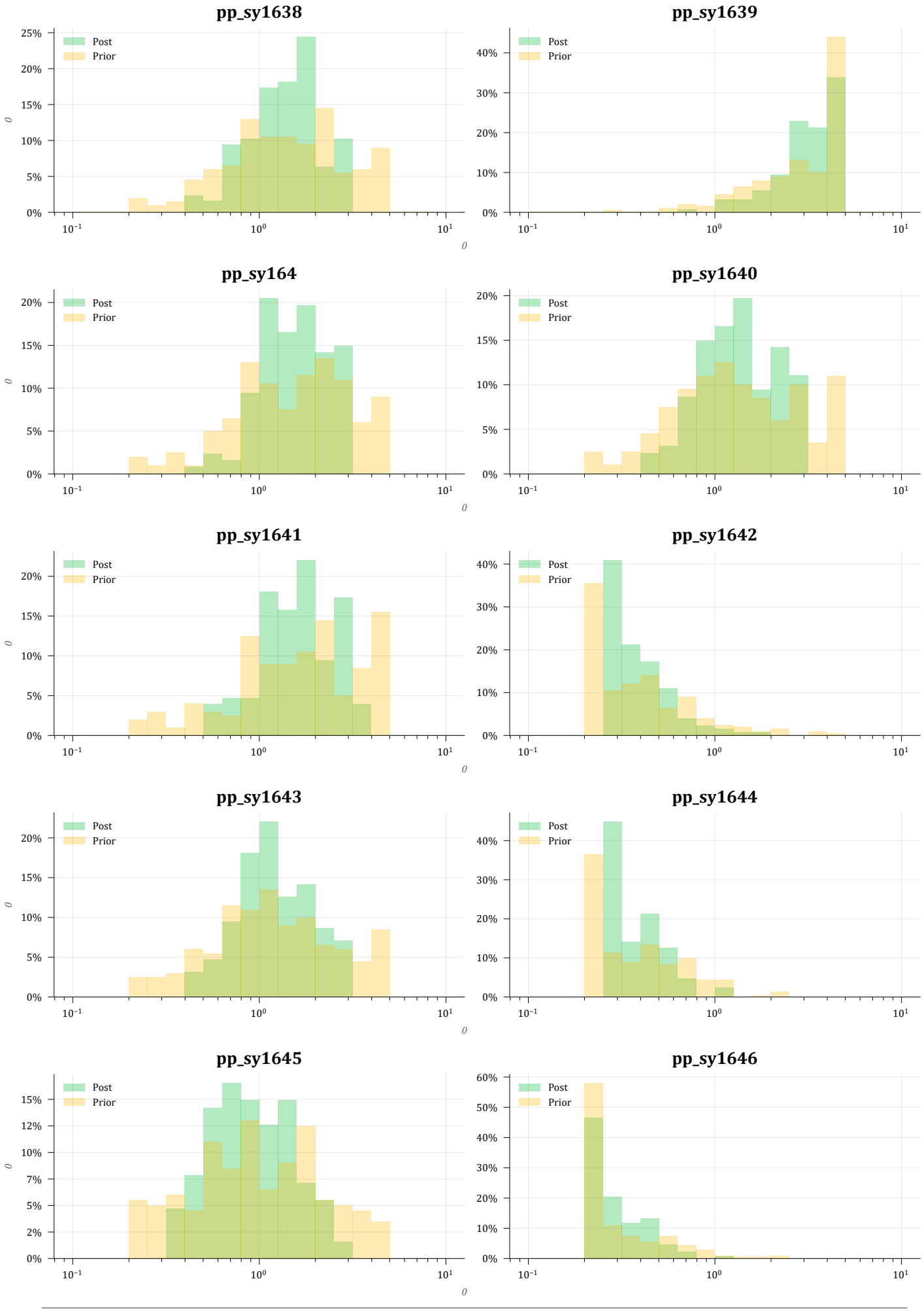

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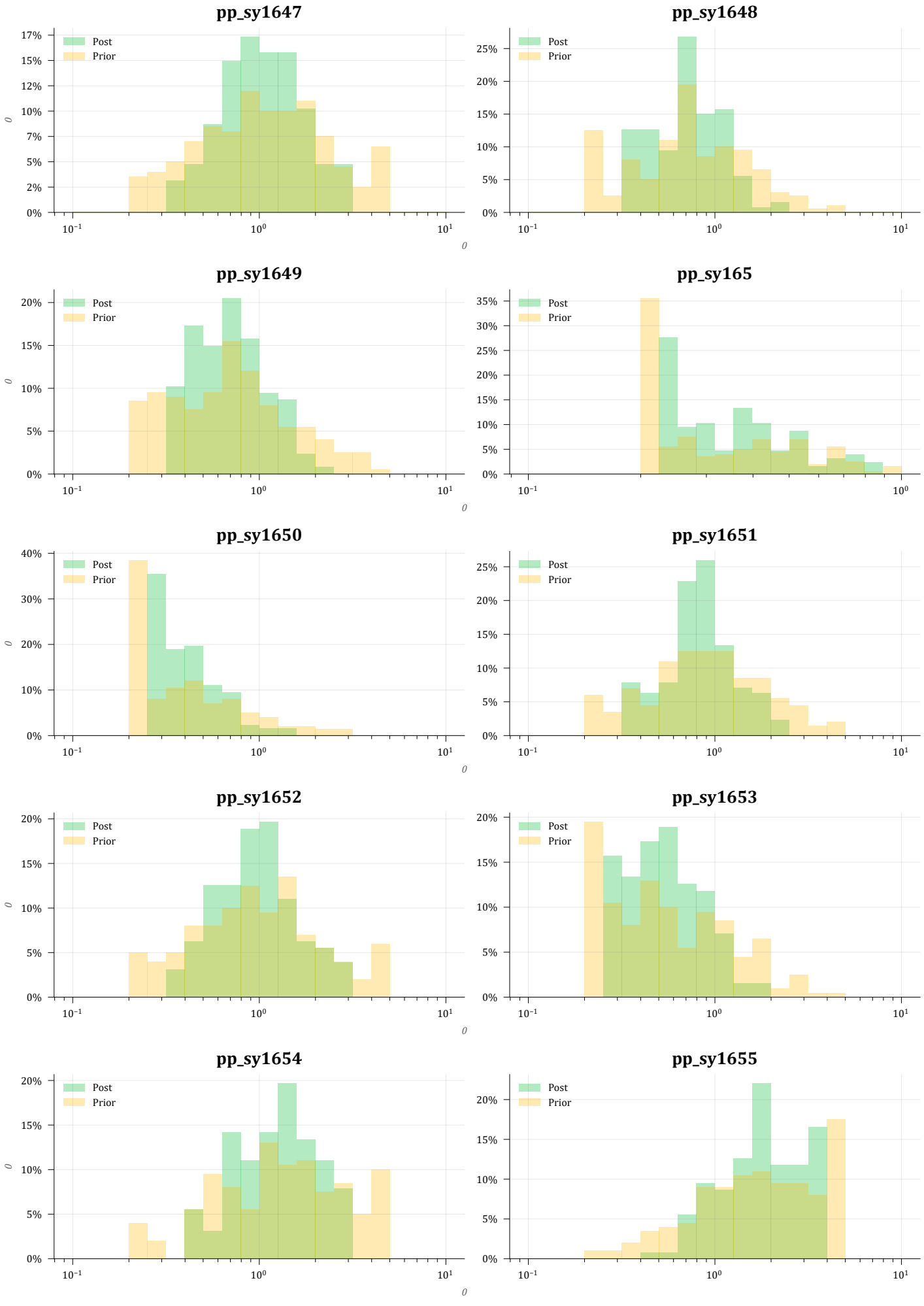

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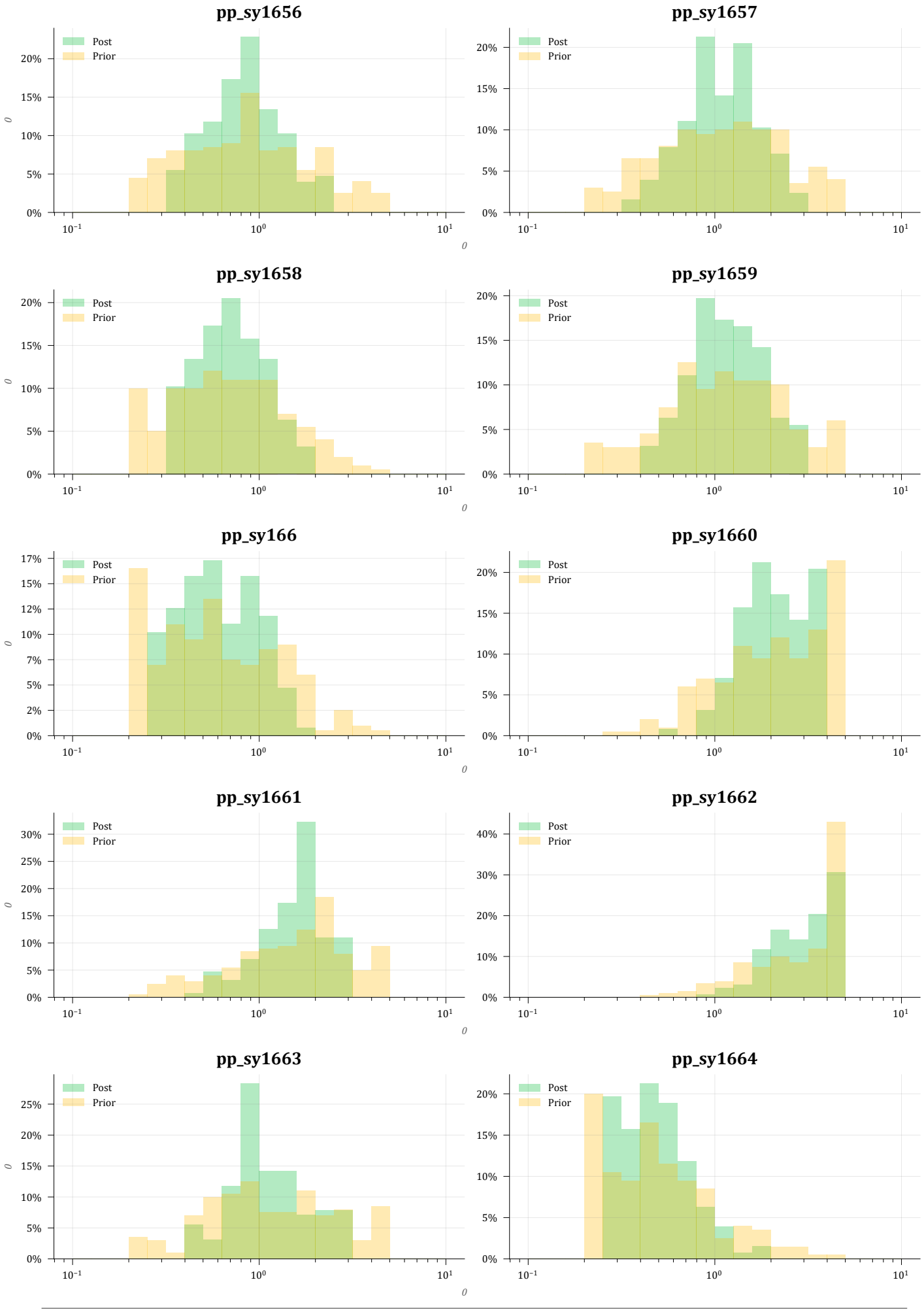

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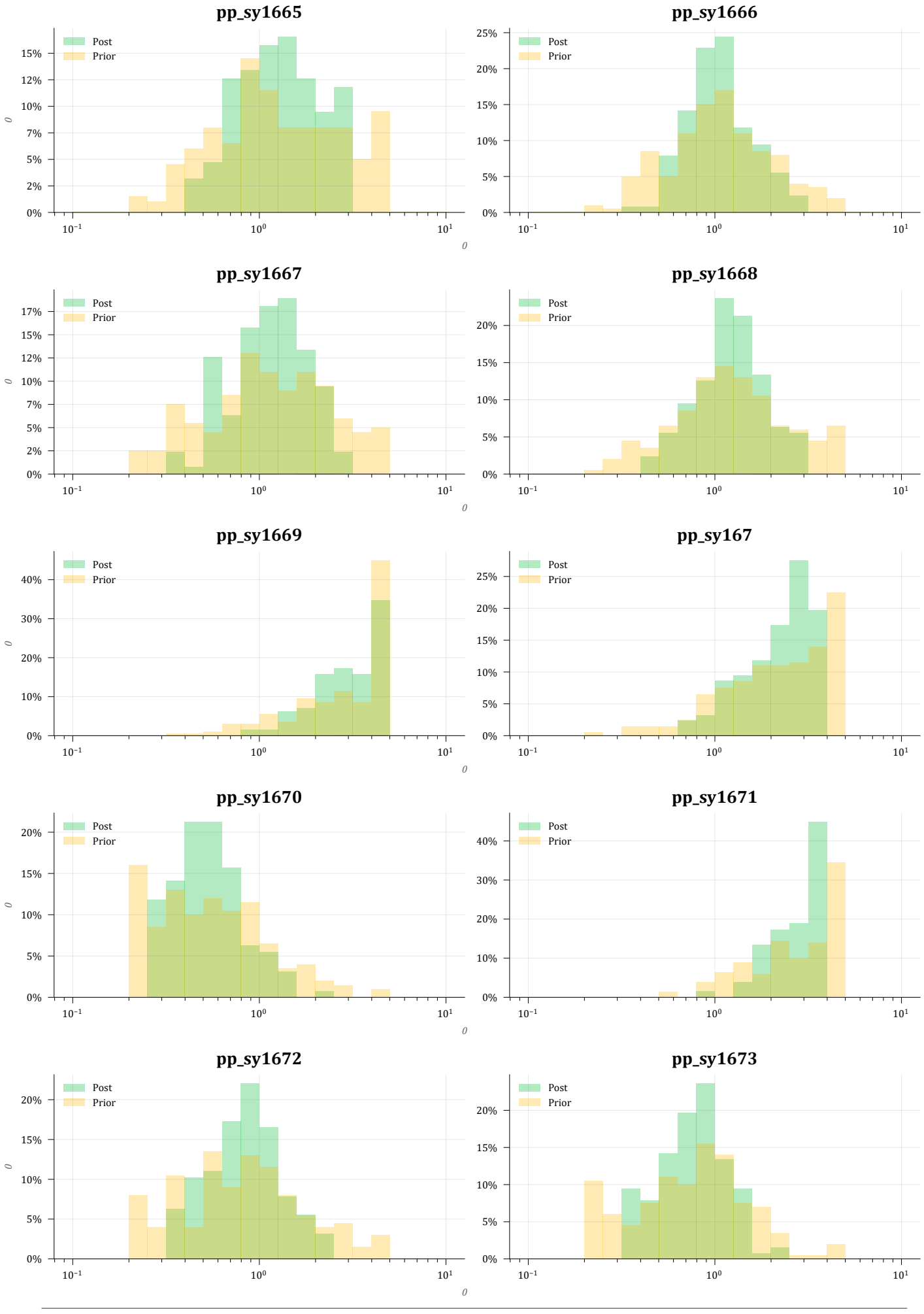

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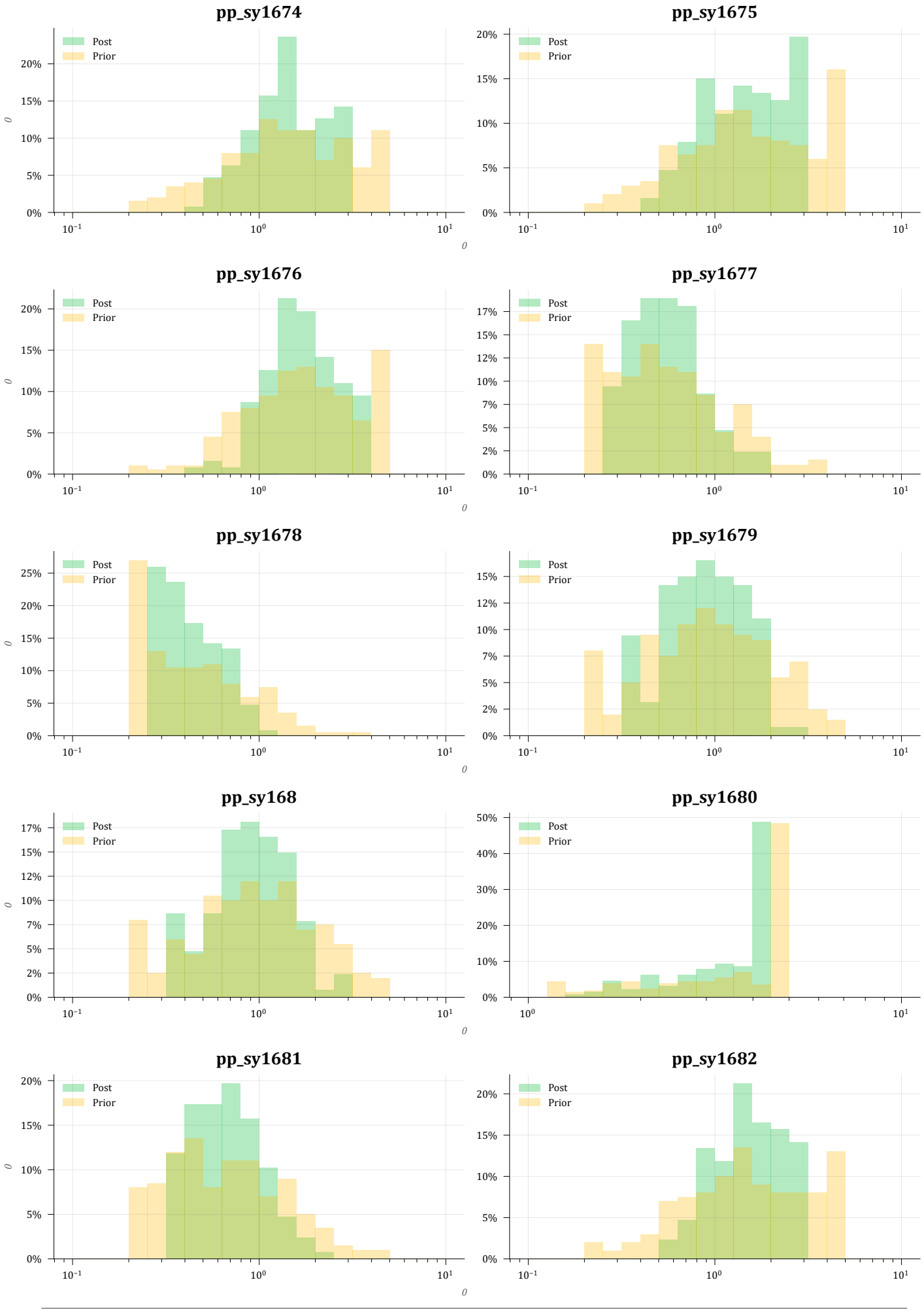

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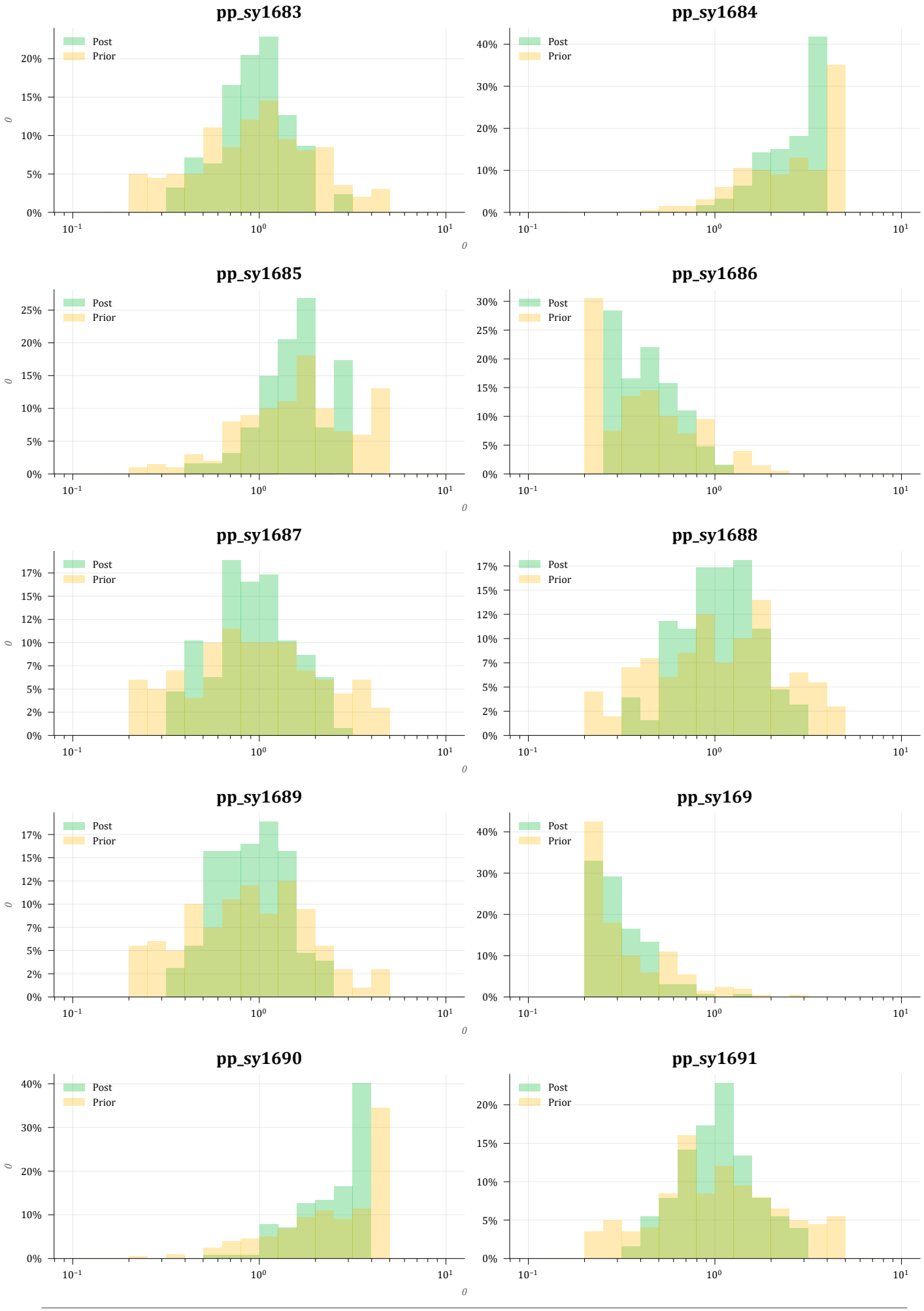

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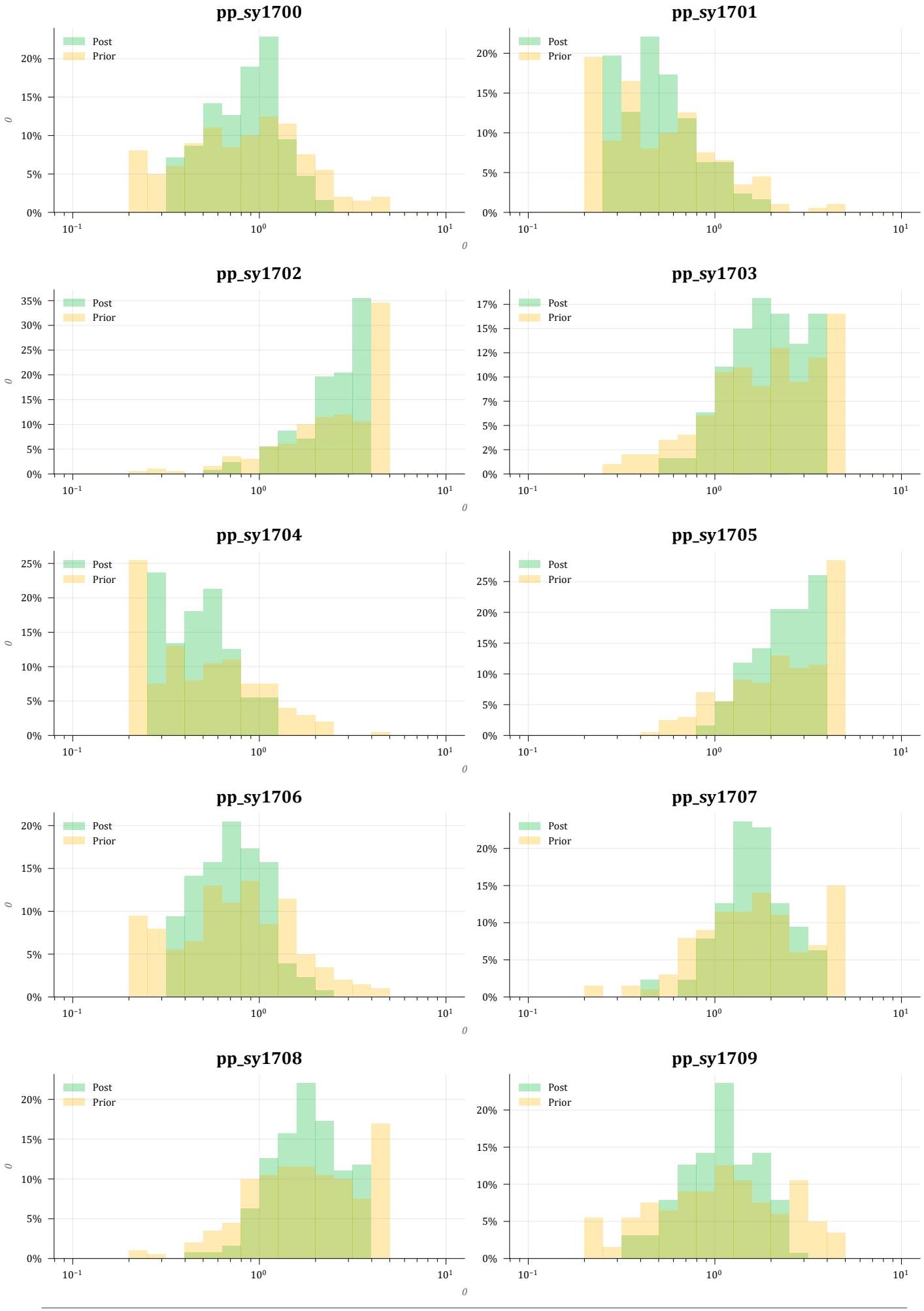

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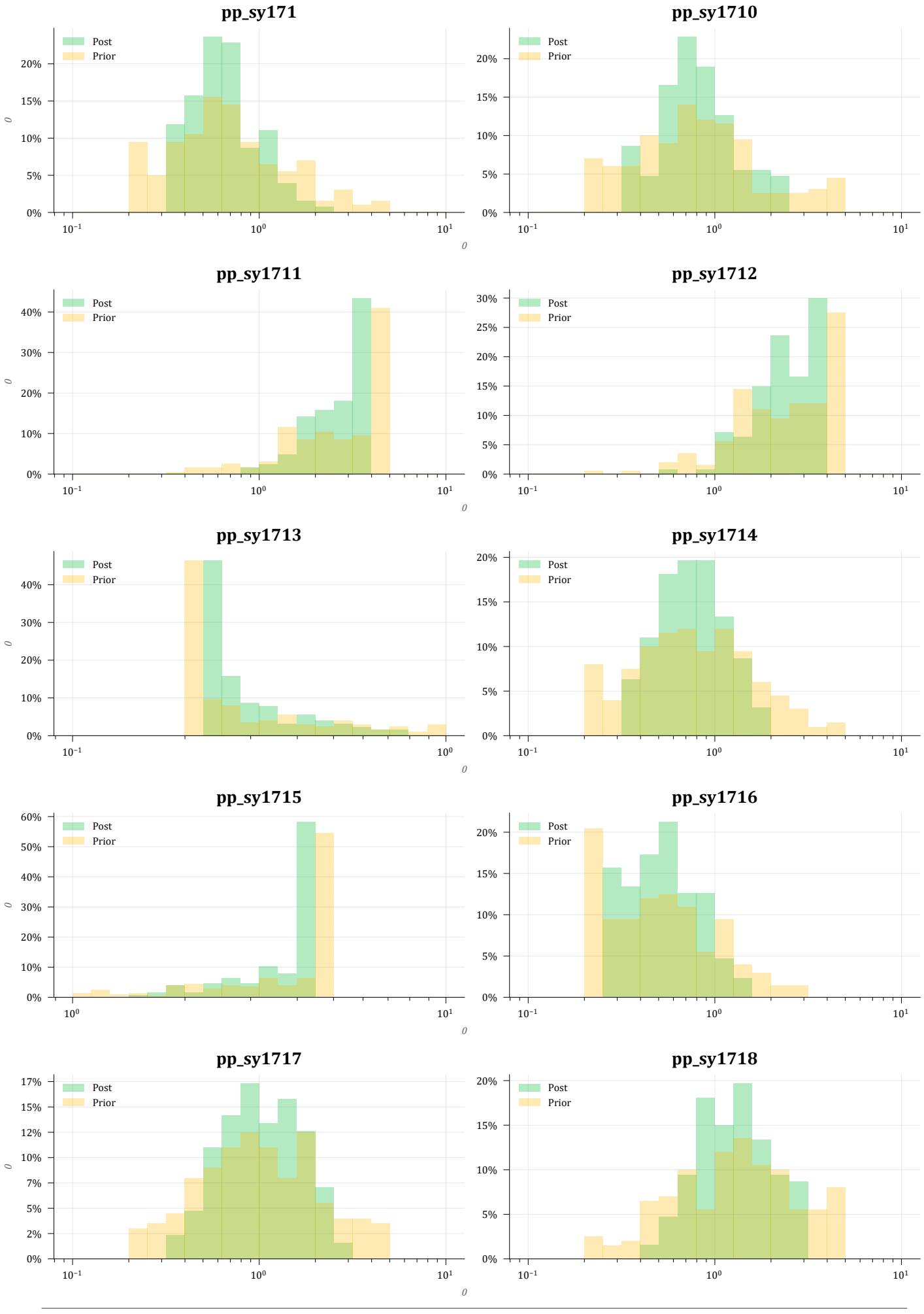

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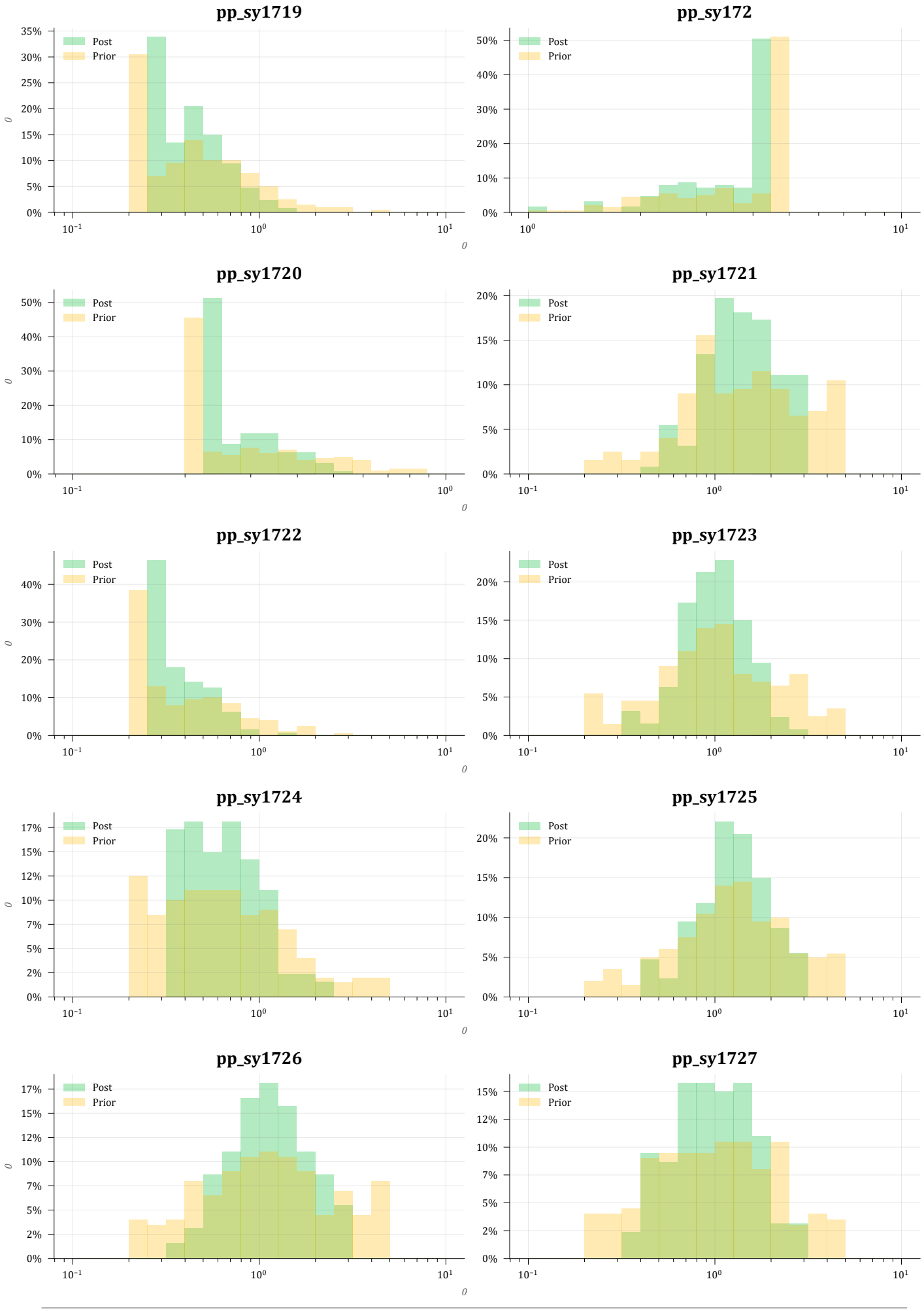

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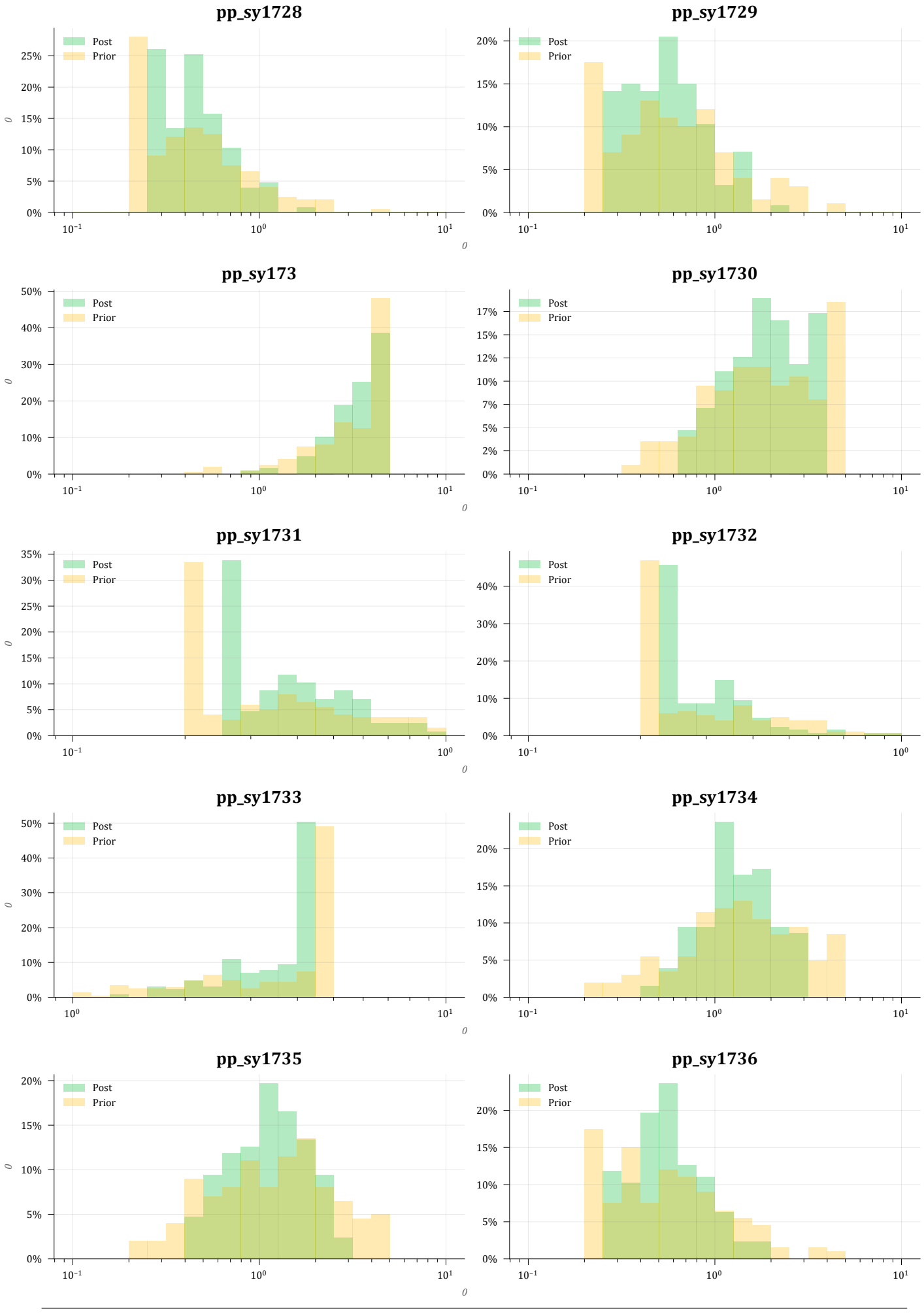

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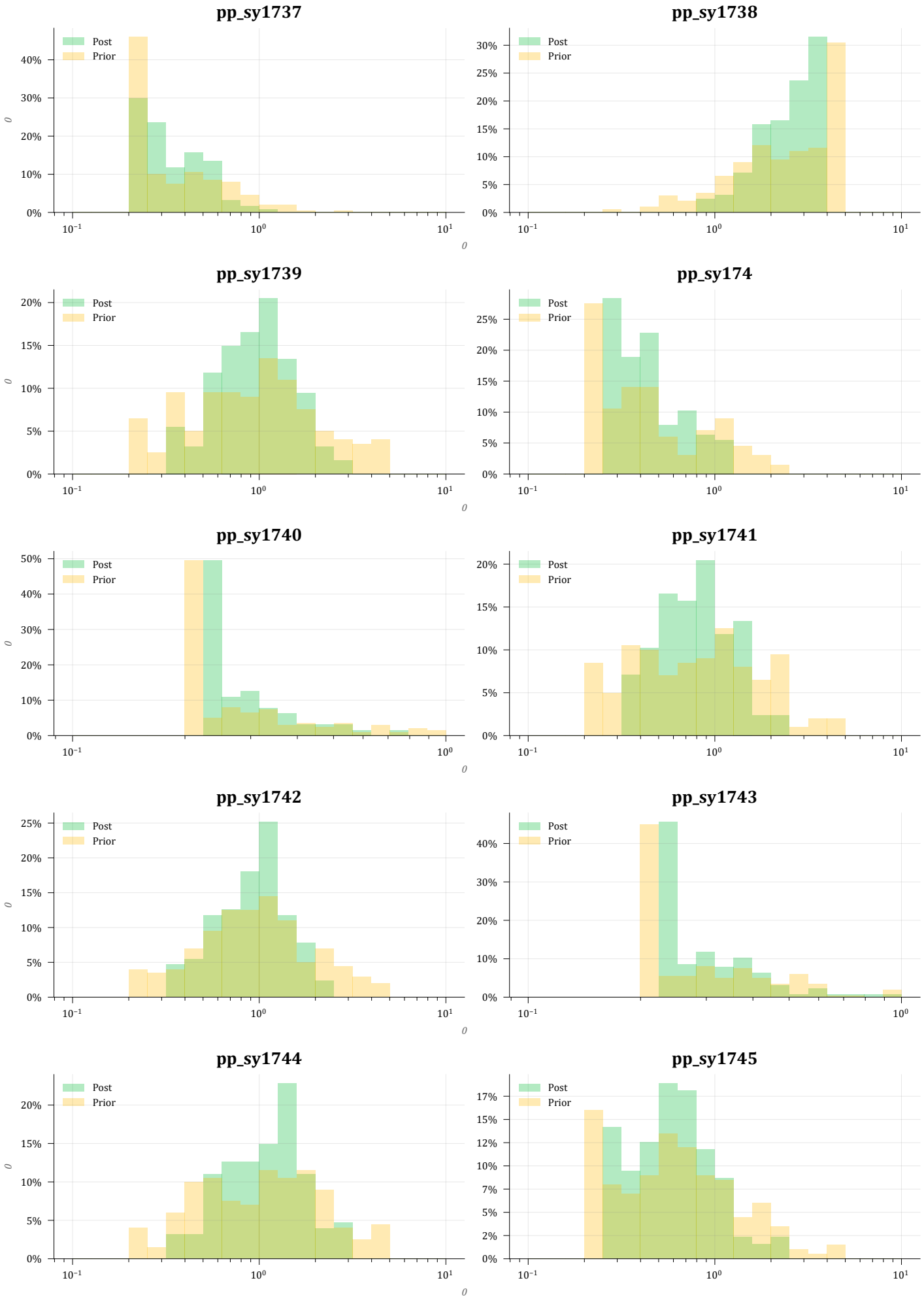

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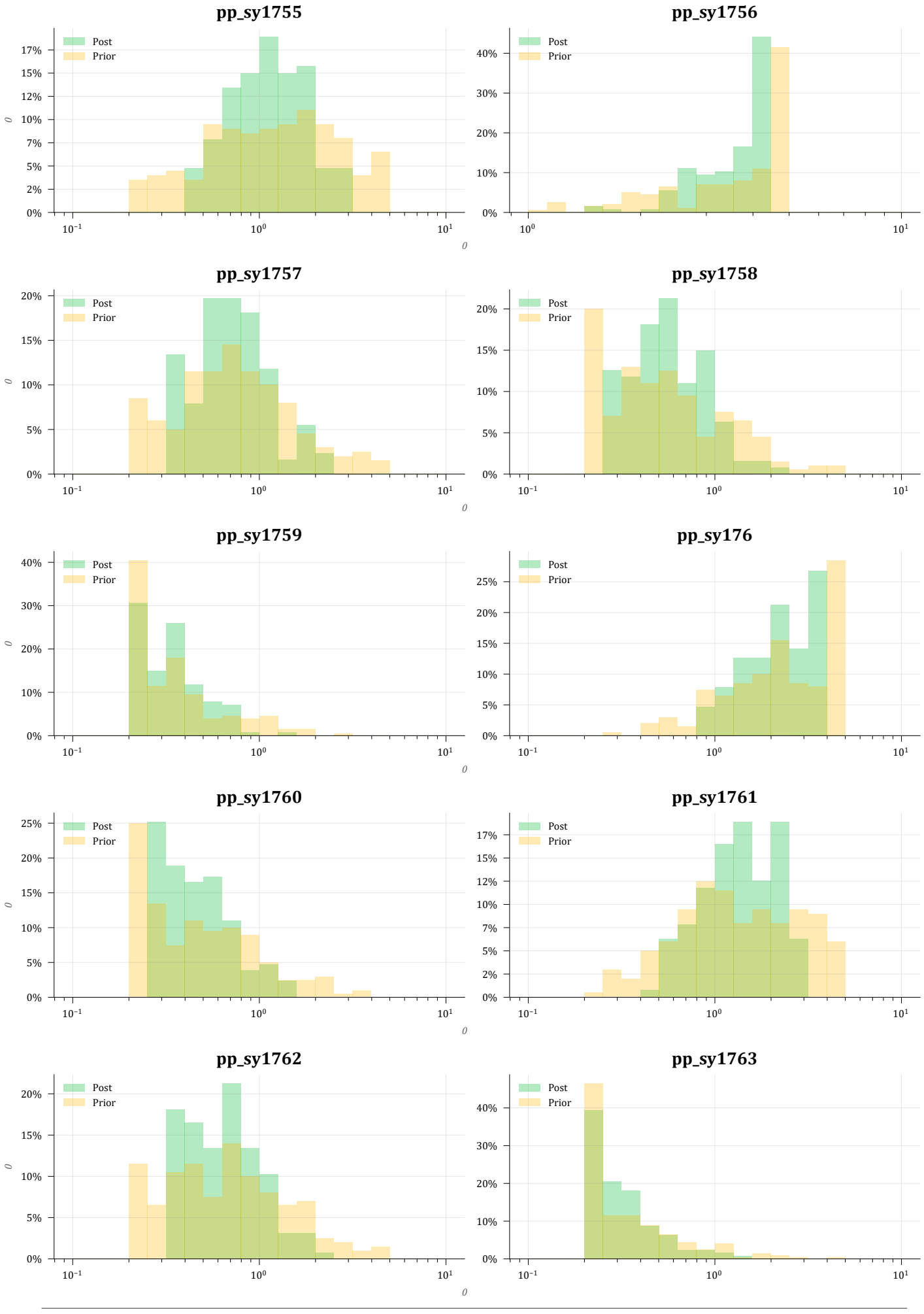

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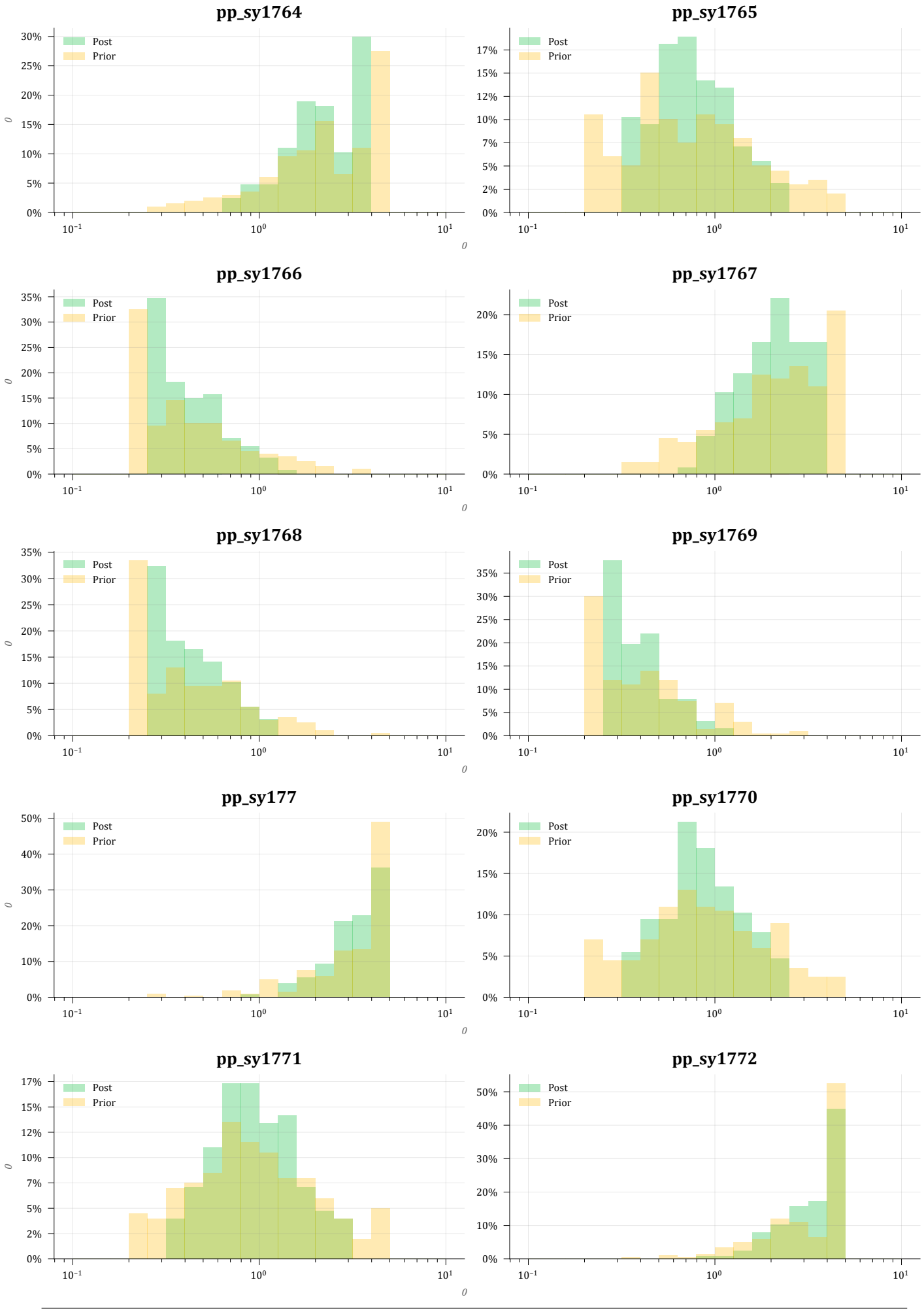

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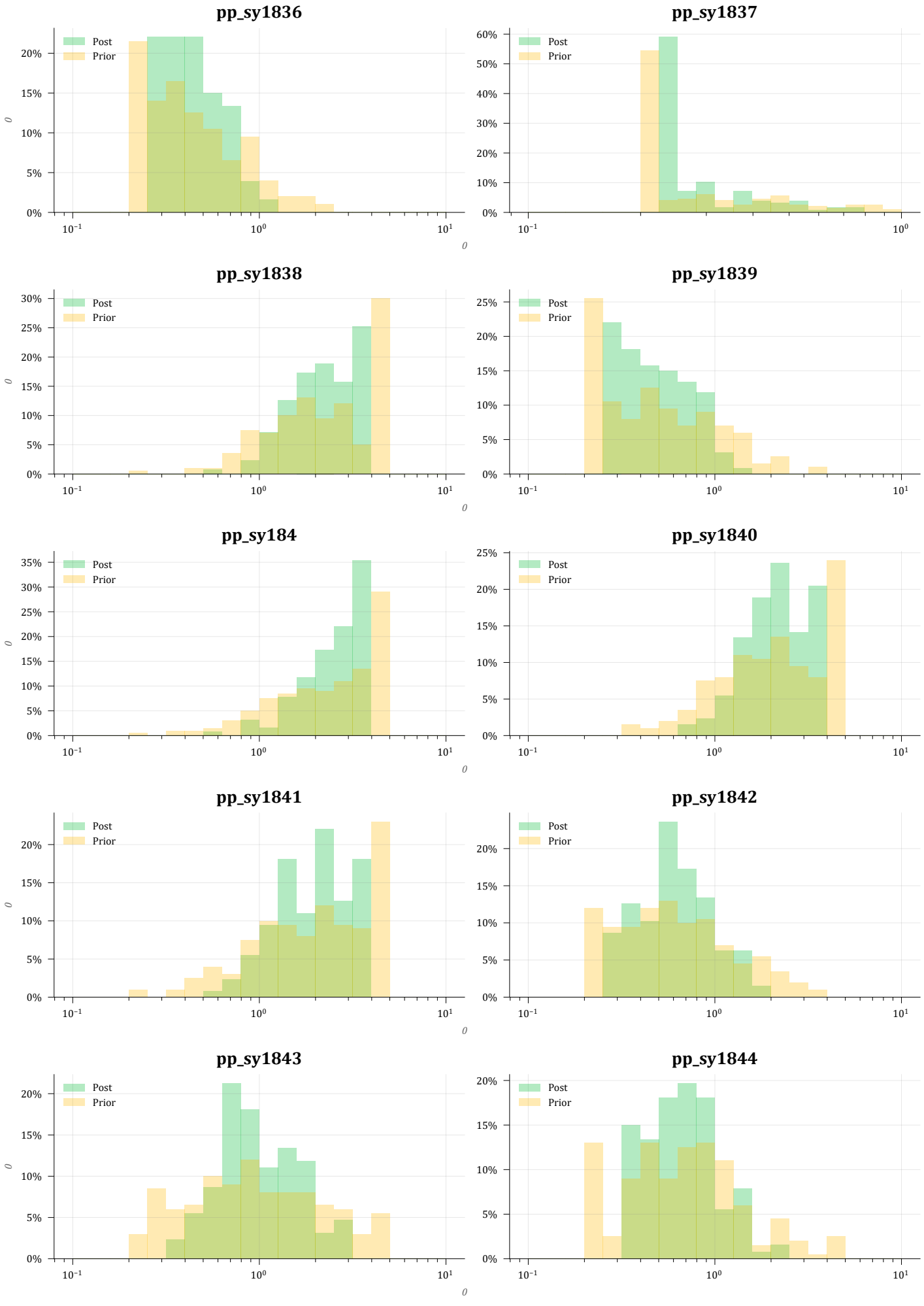

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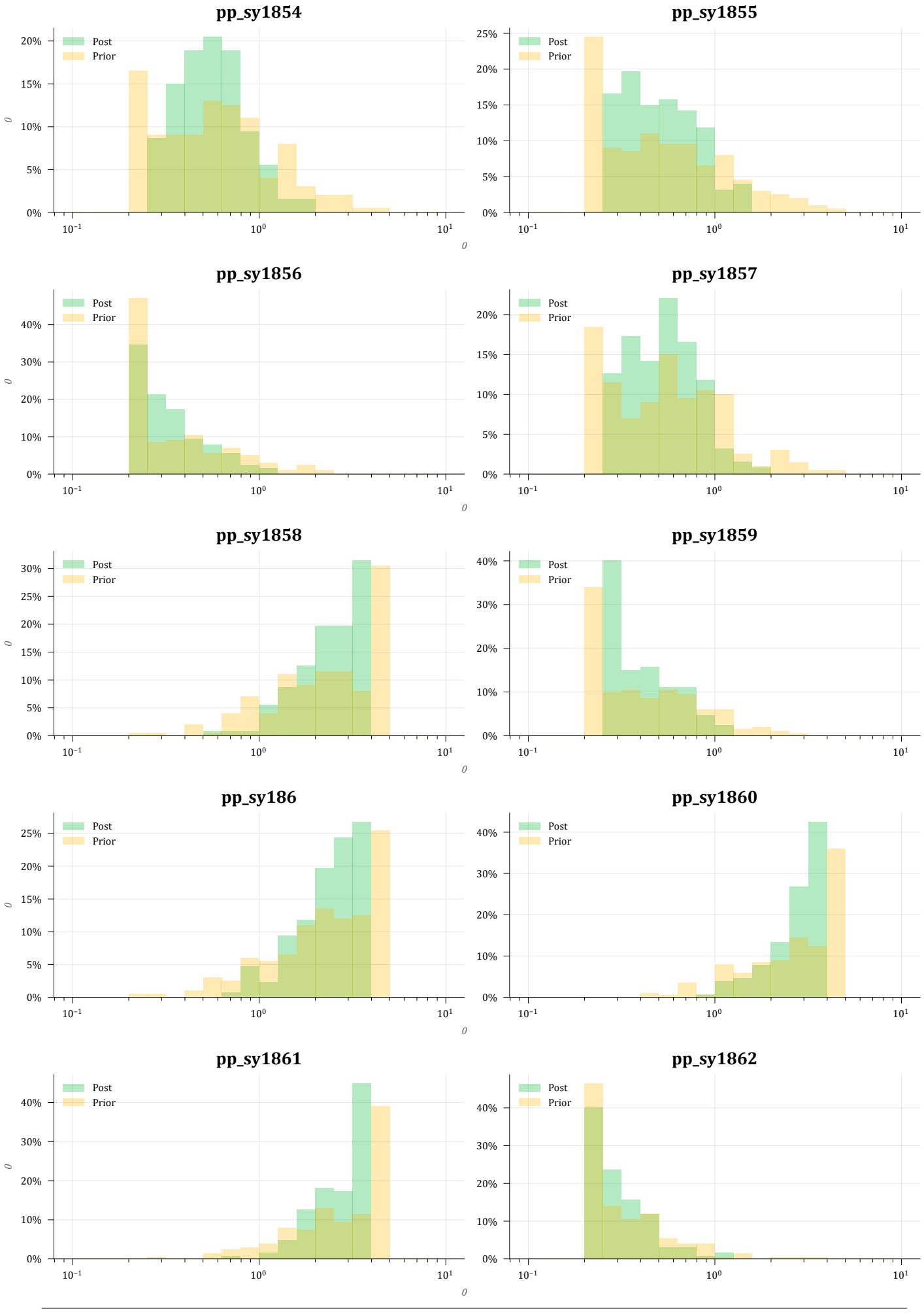

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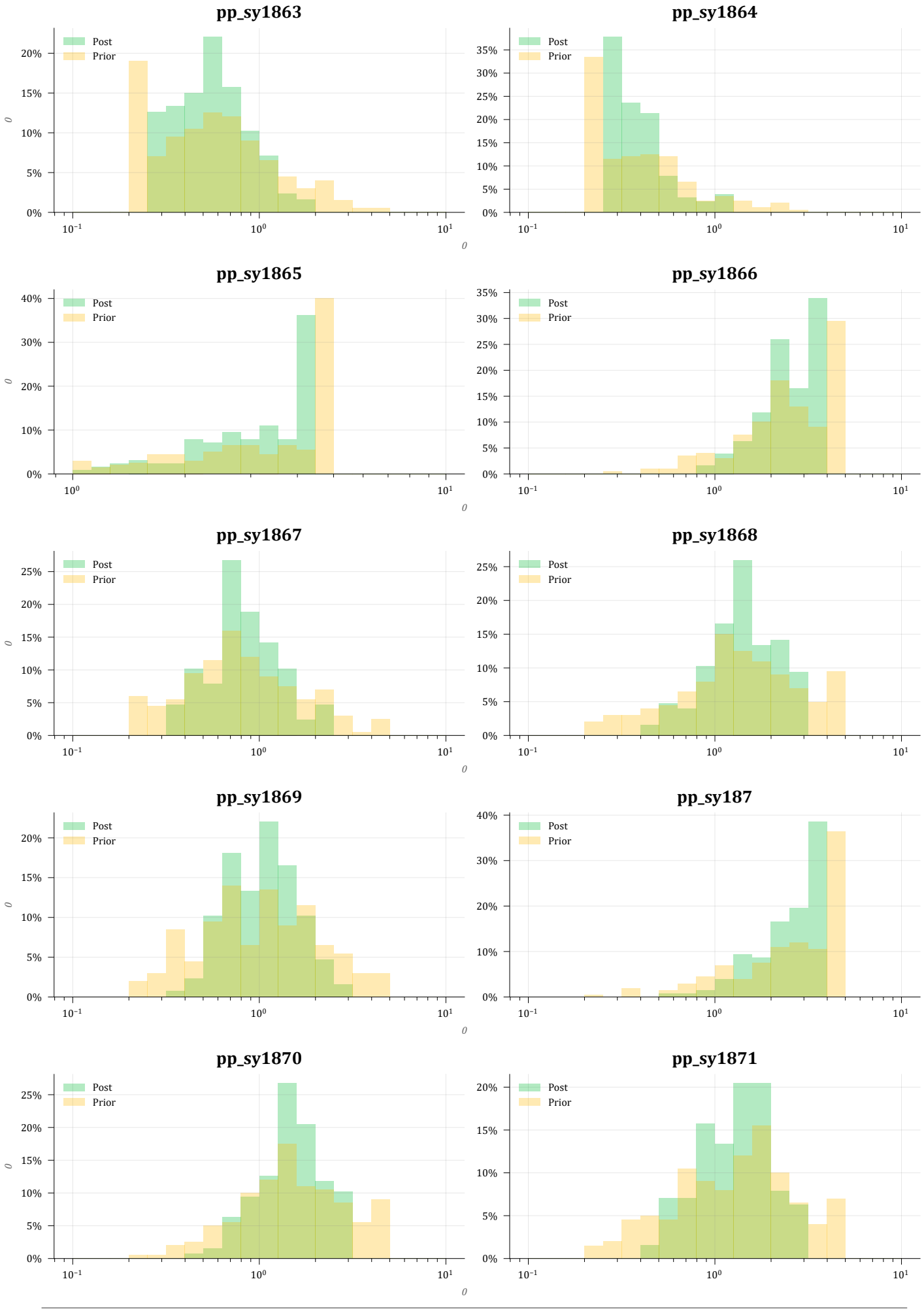

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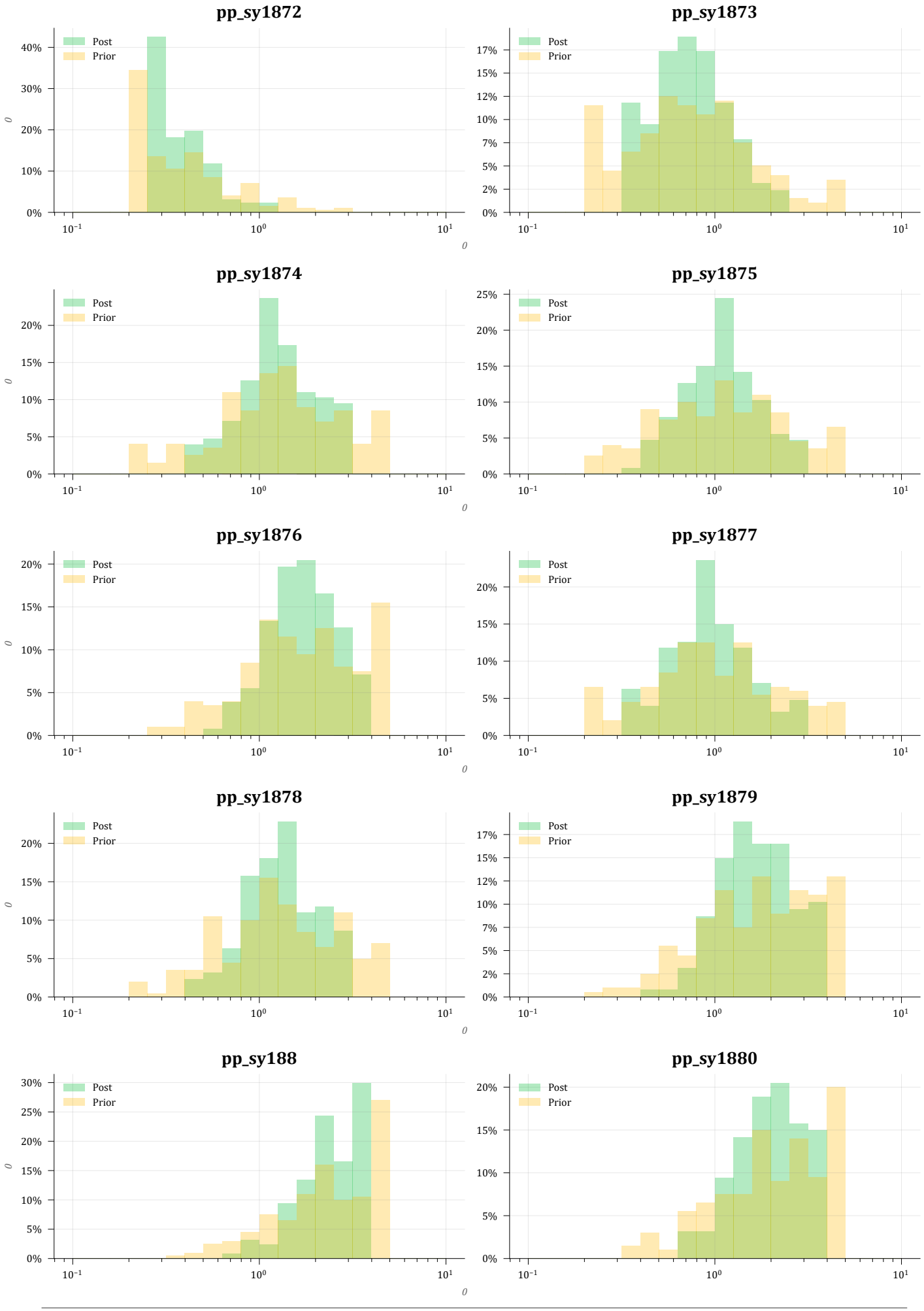

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Prior
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Parameters


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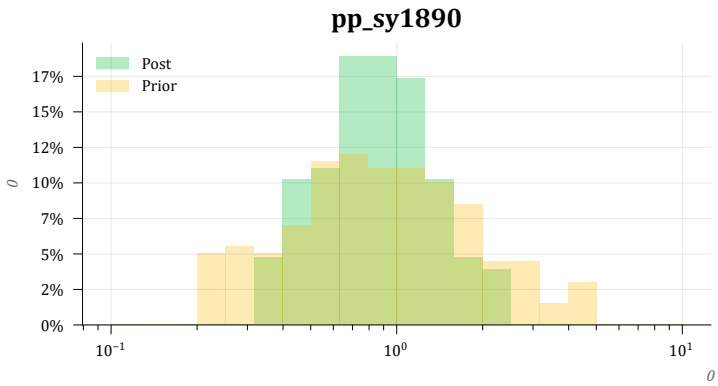

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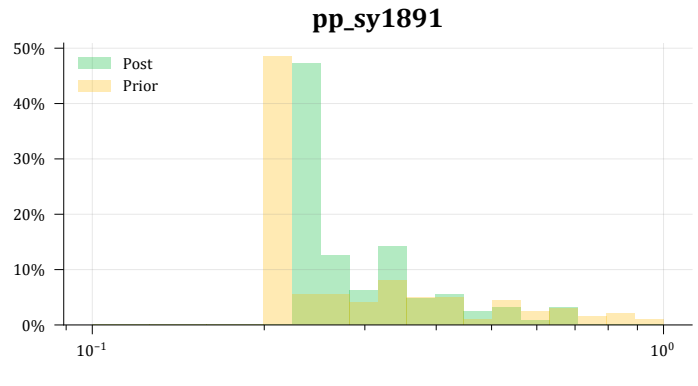

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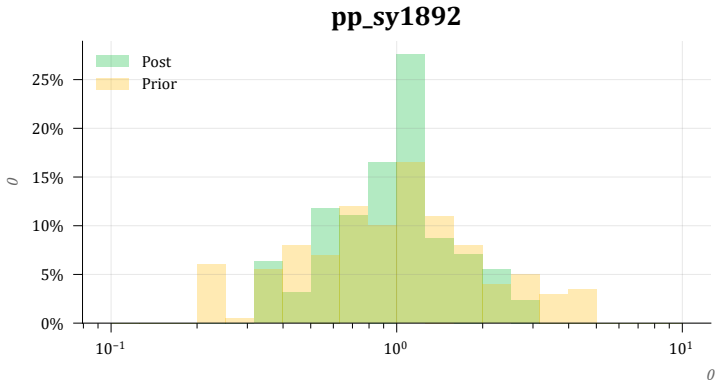

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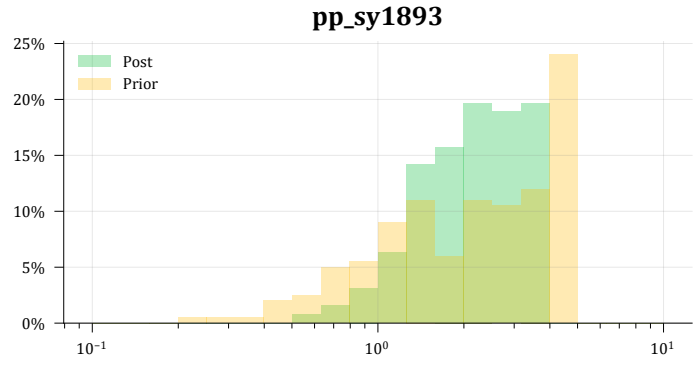

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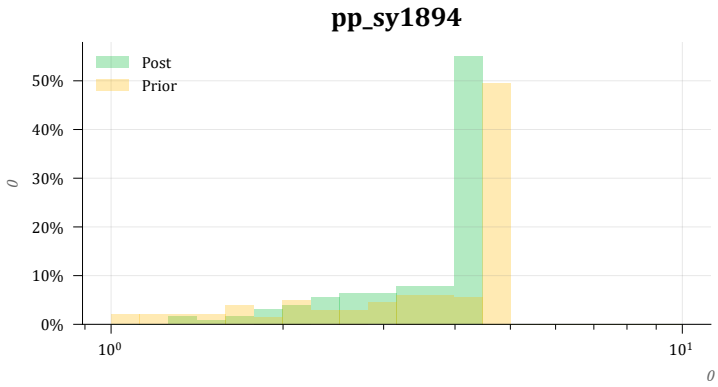

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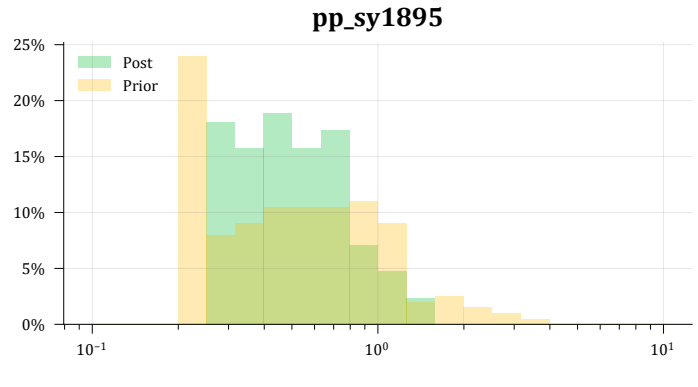

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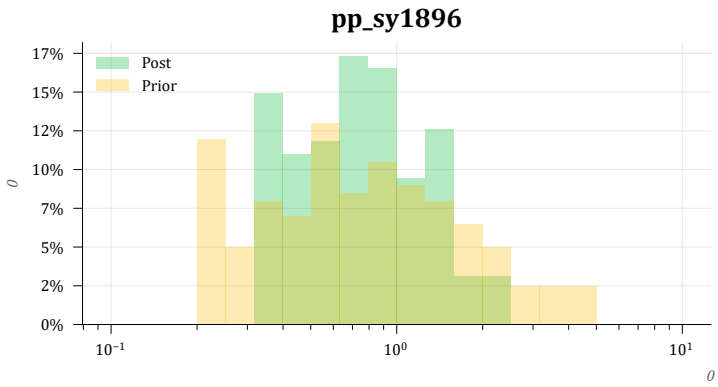

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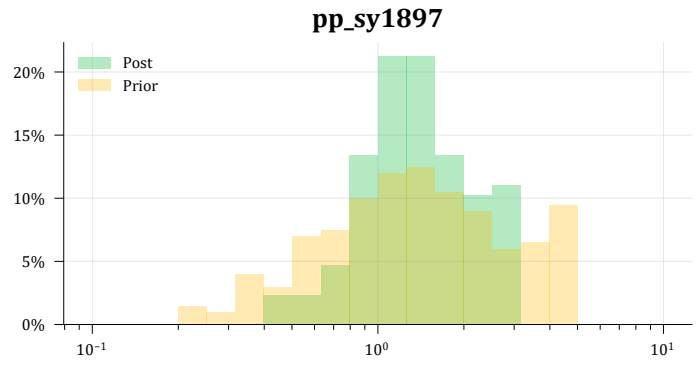

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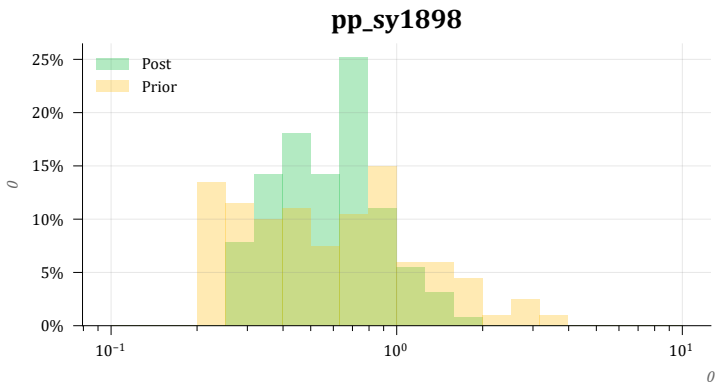

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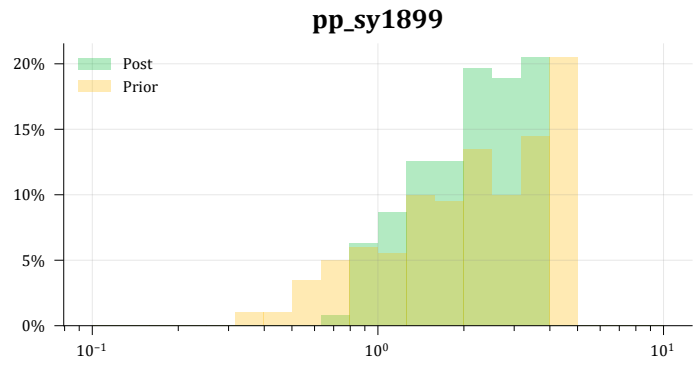

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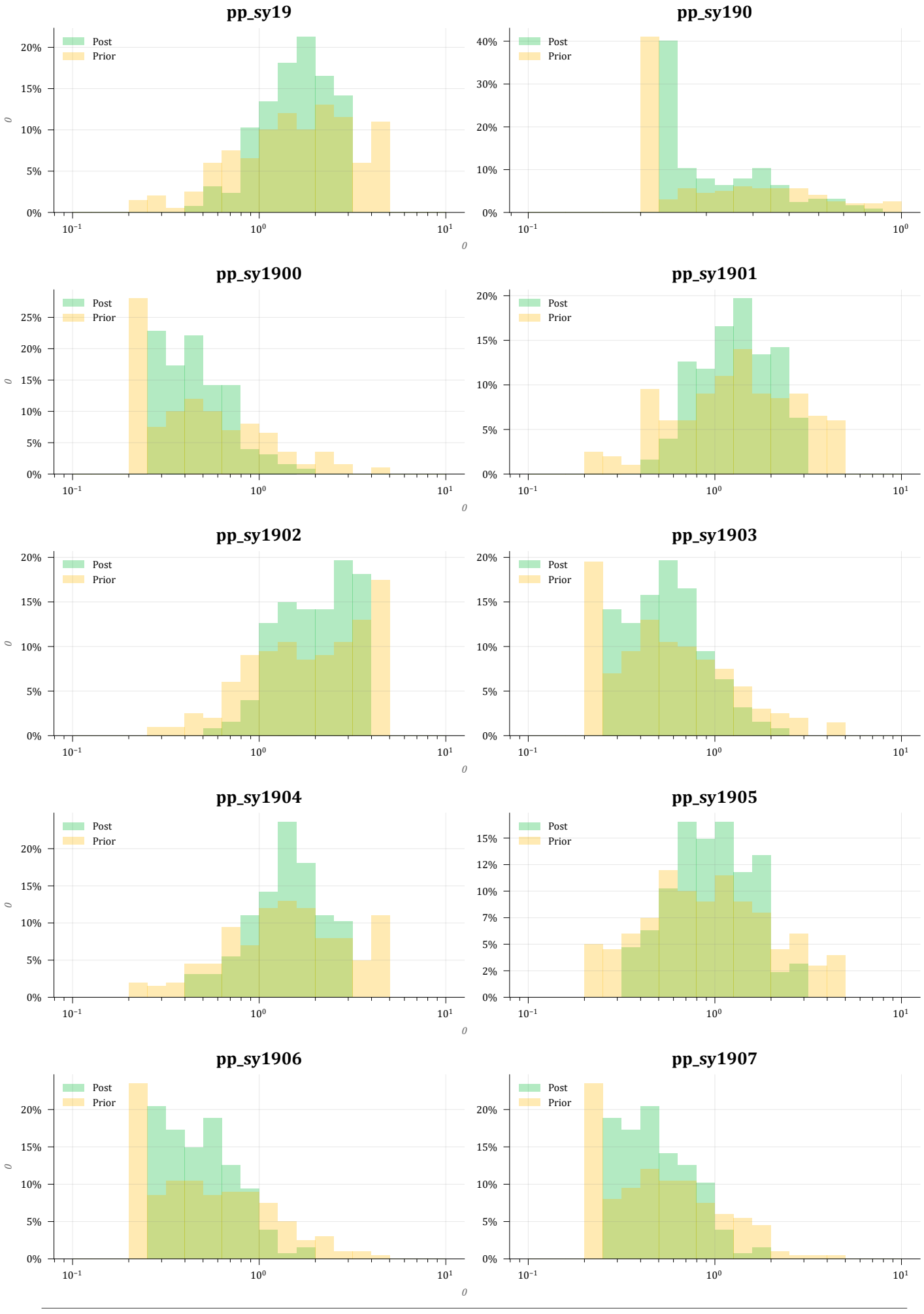

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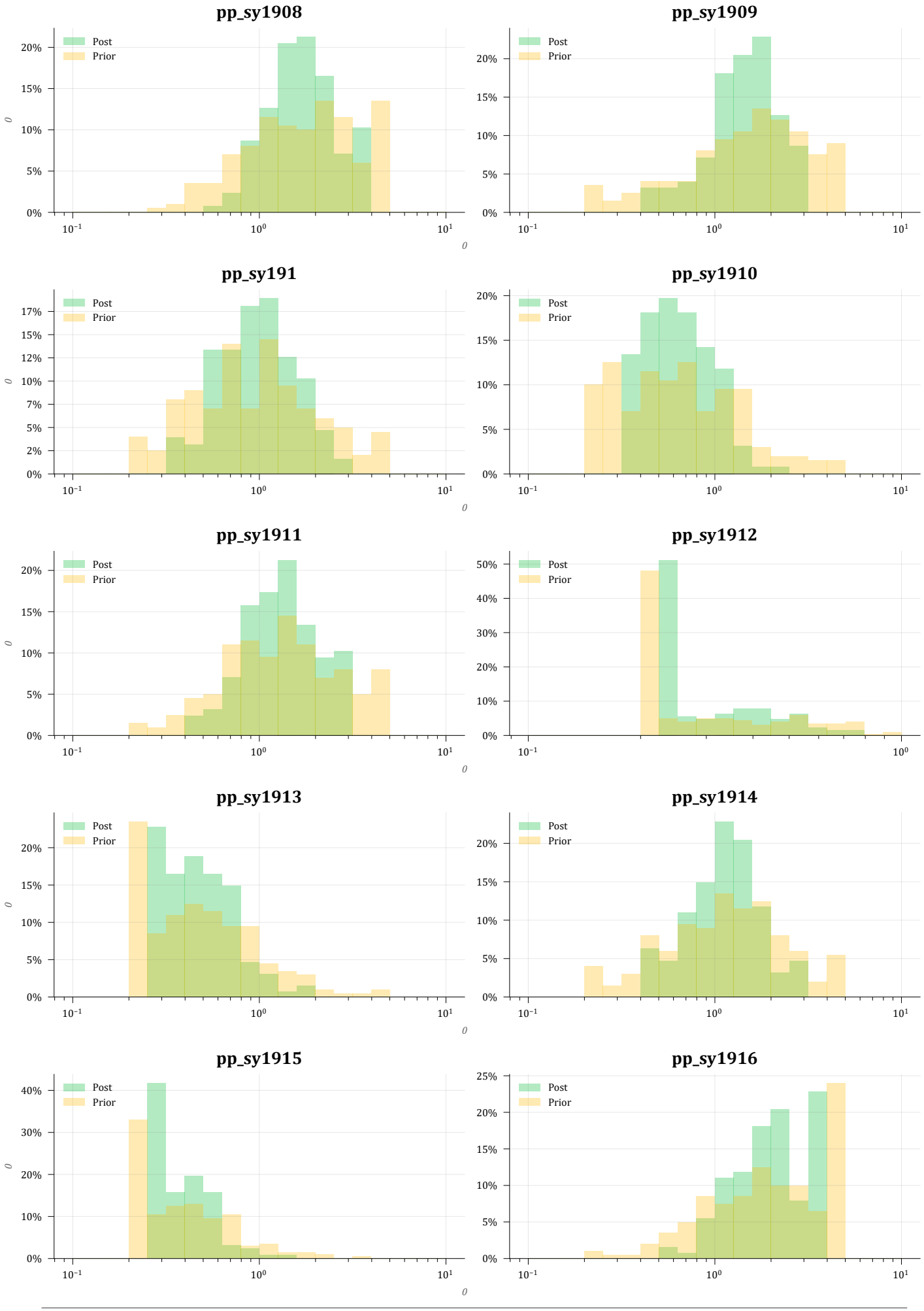

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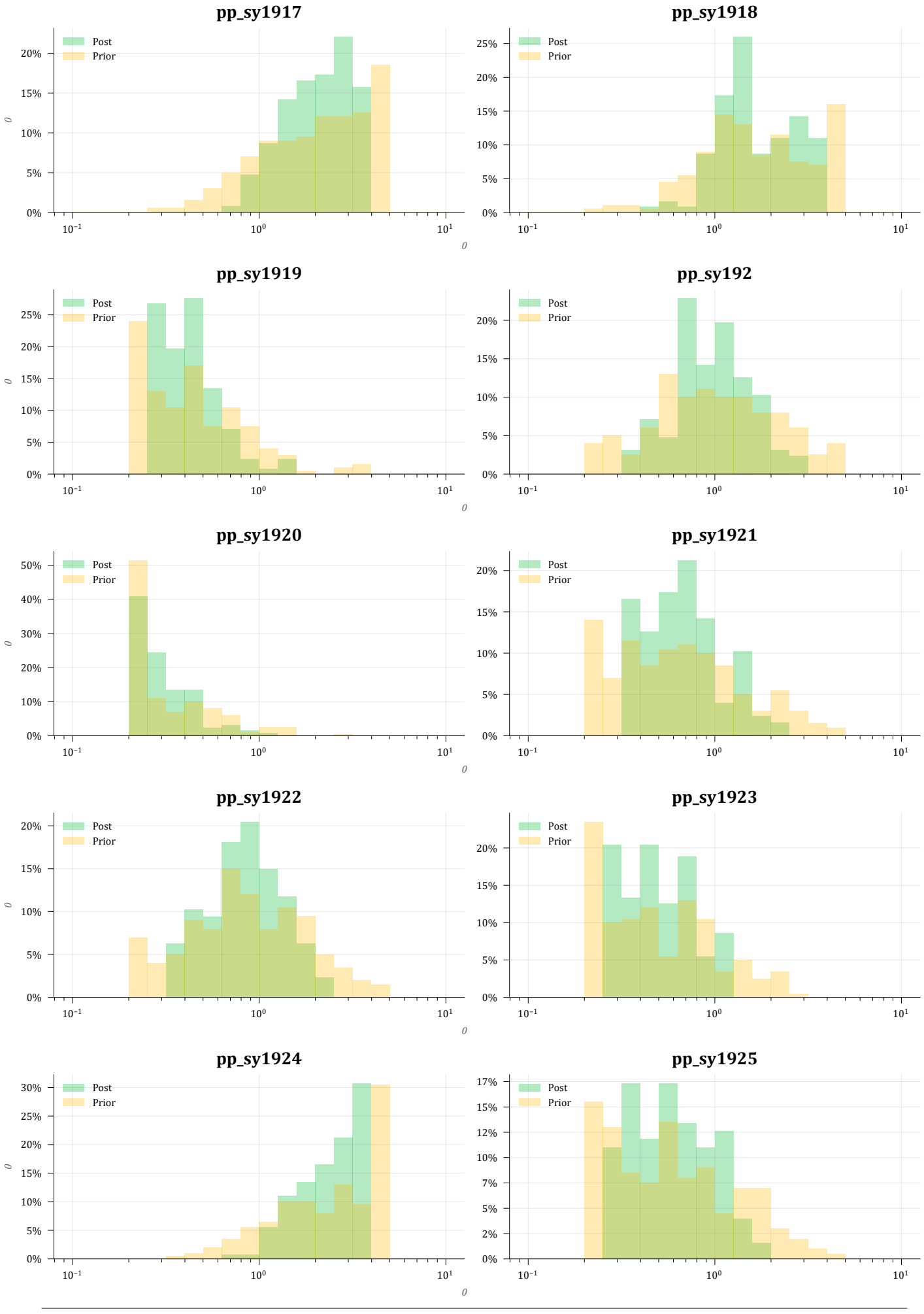

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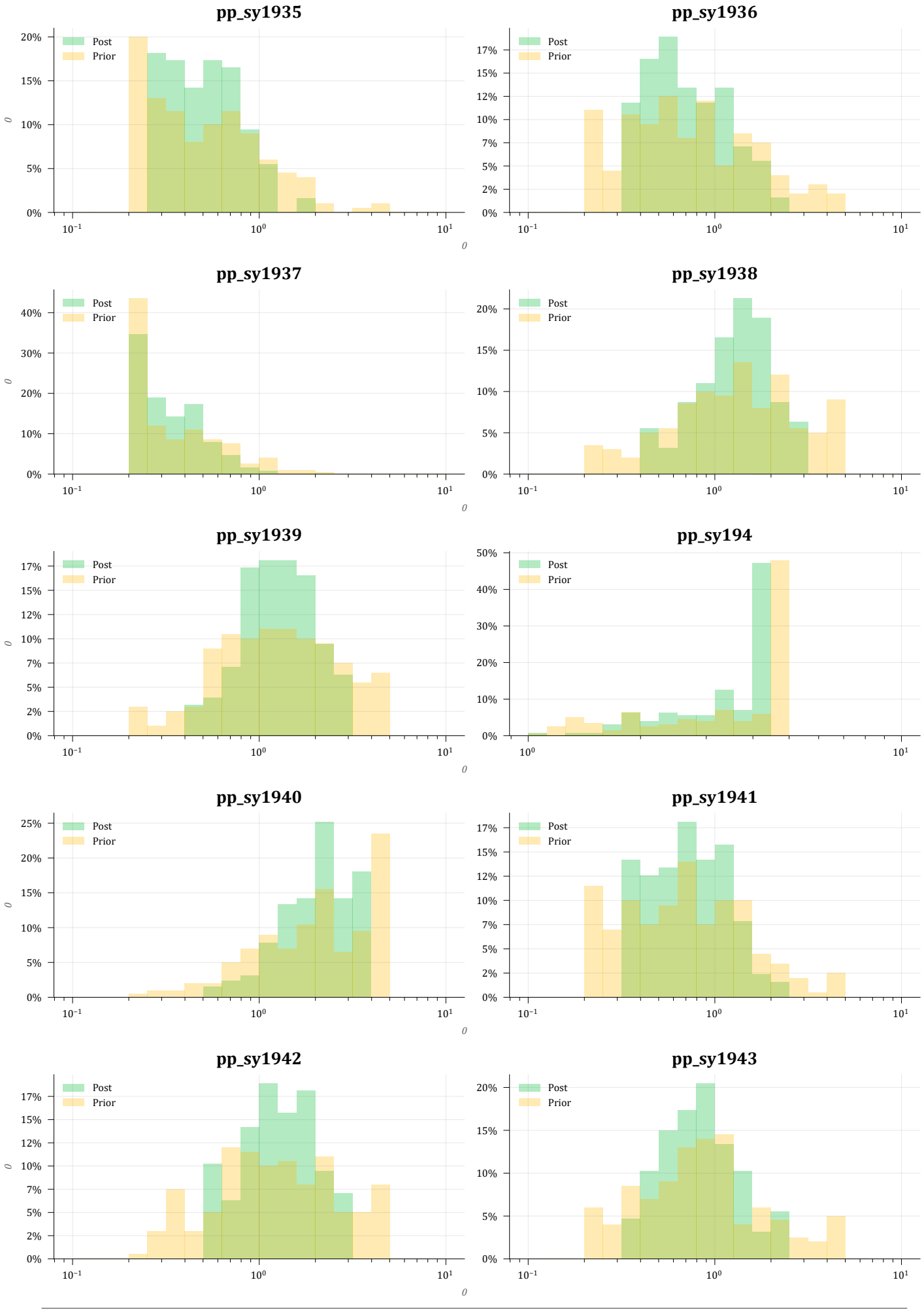

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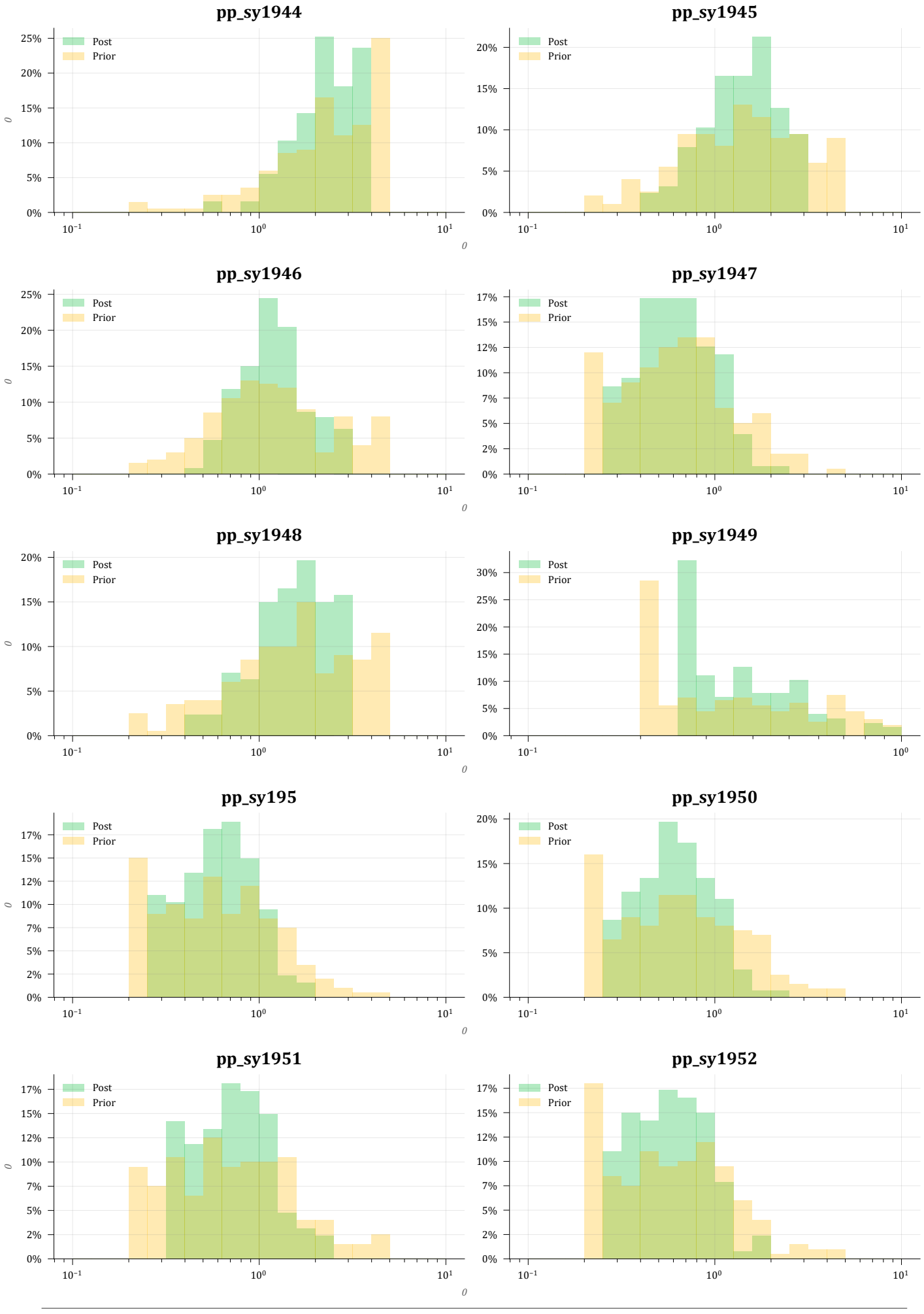

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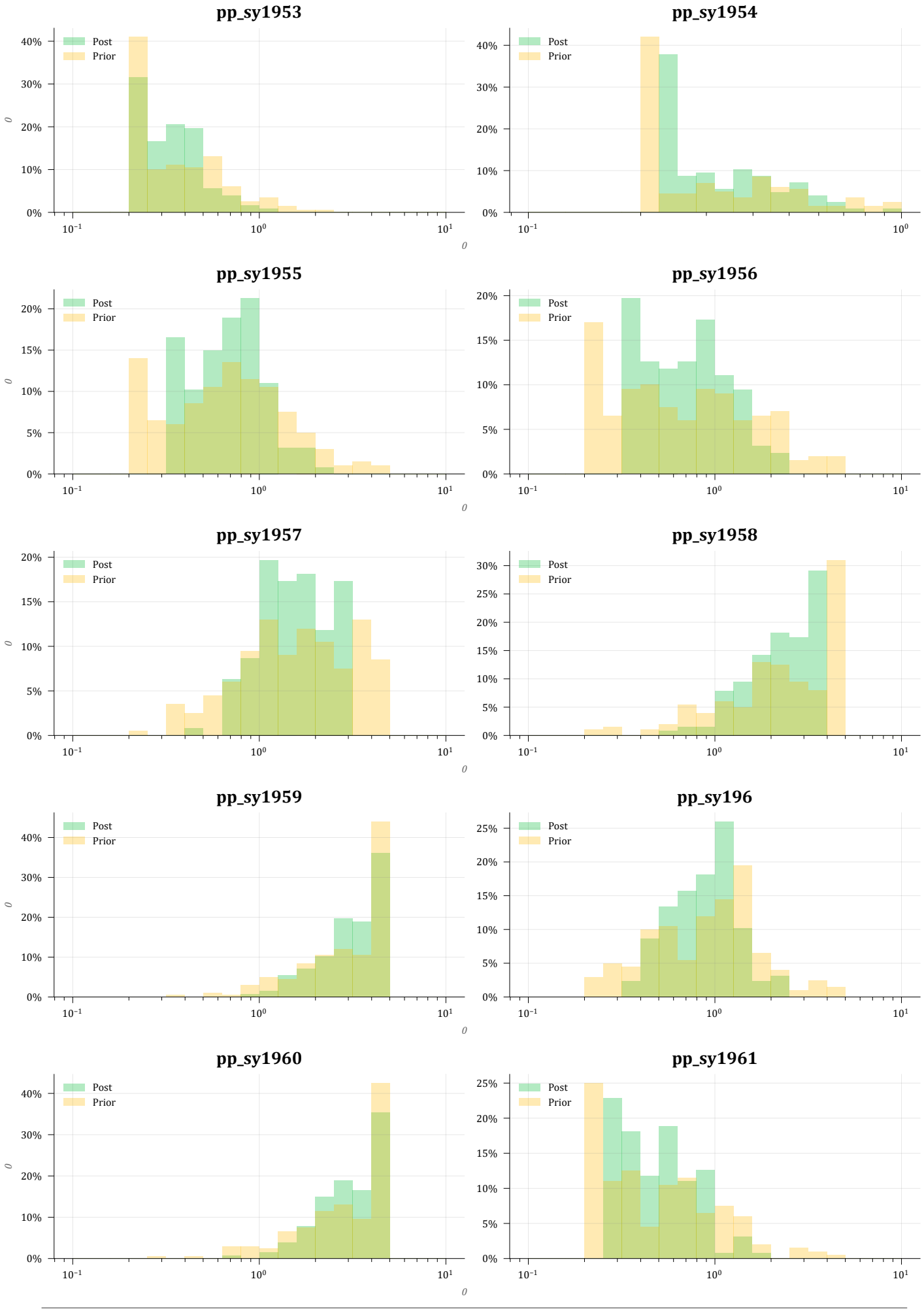

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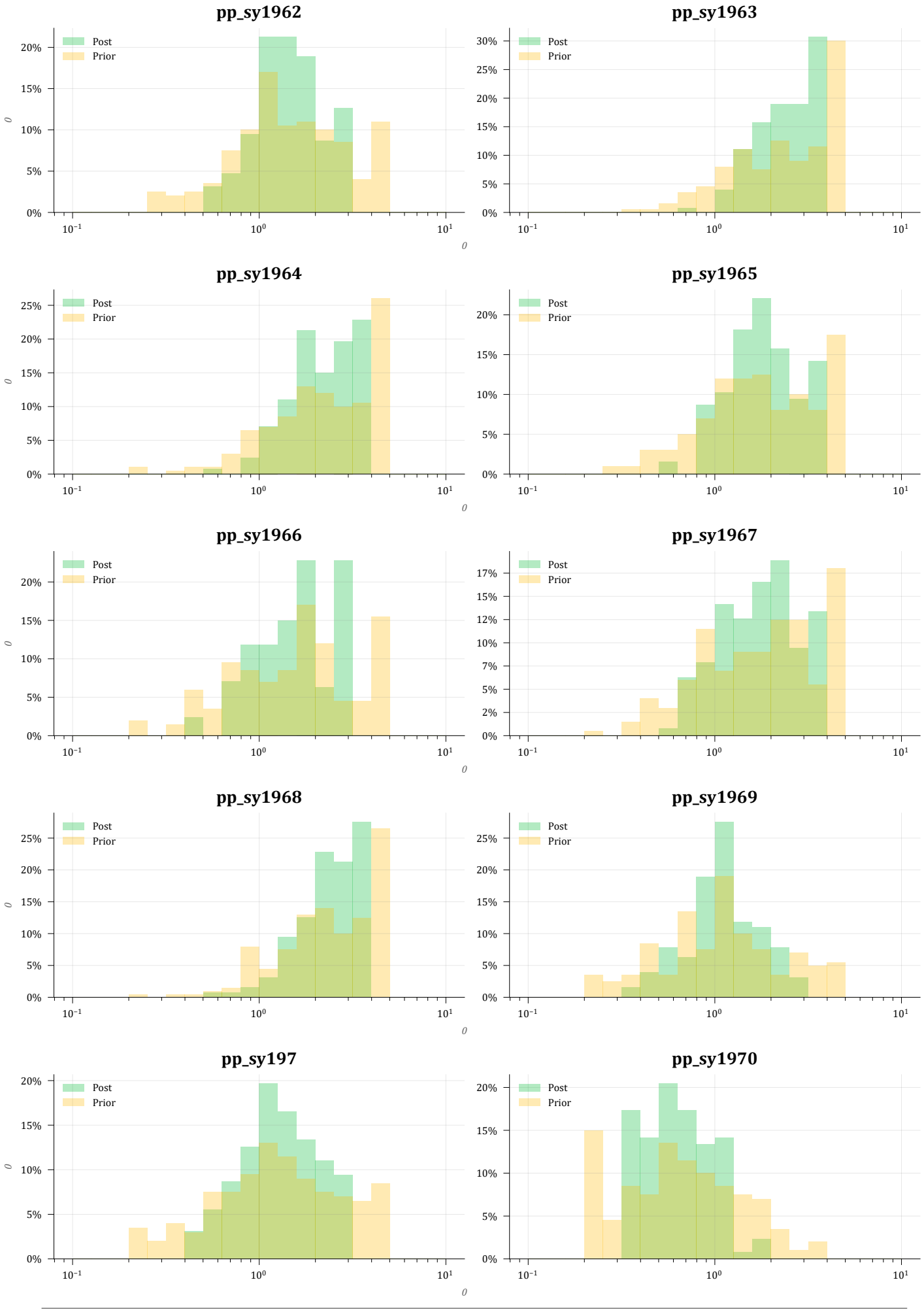

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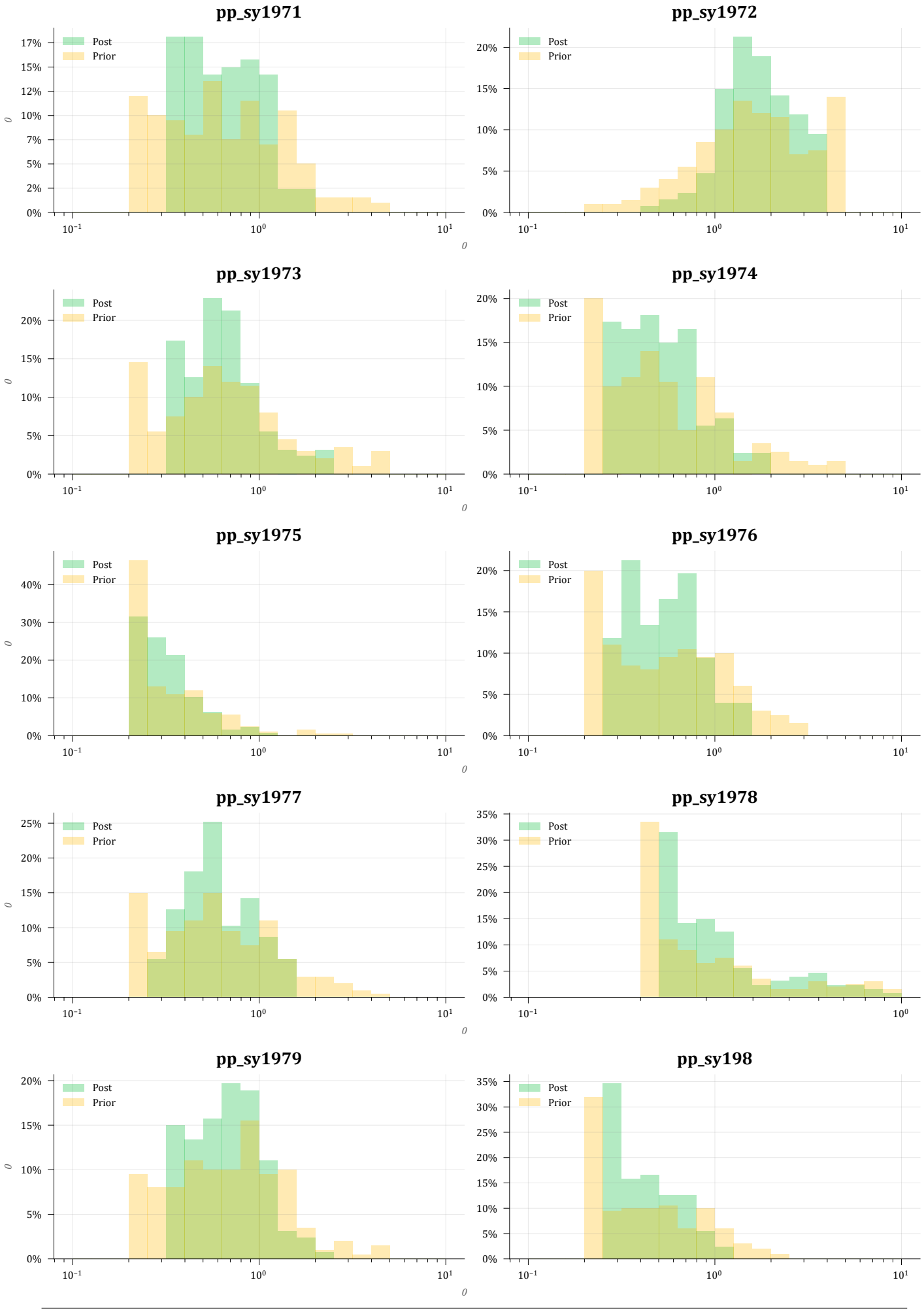

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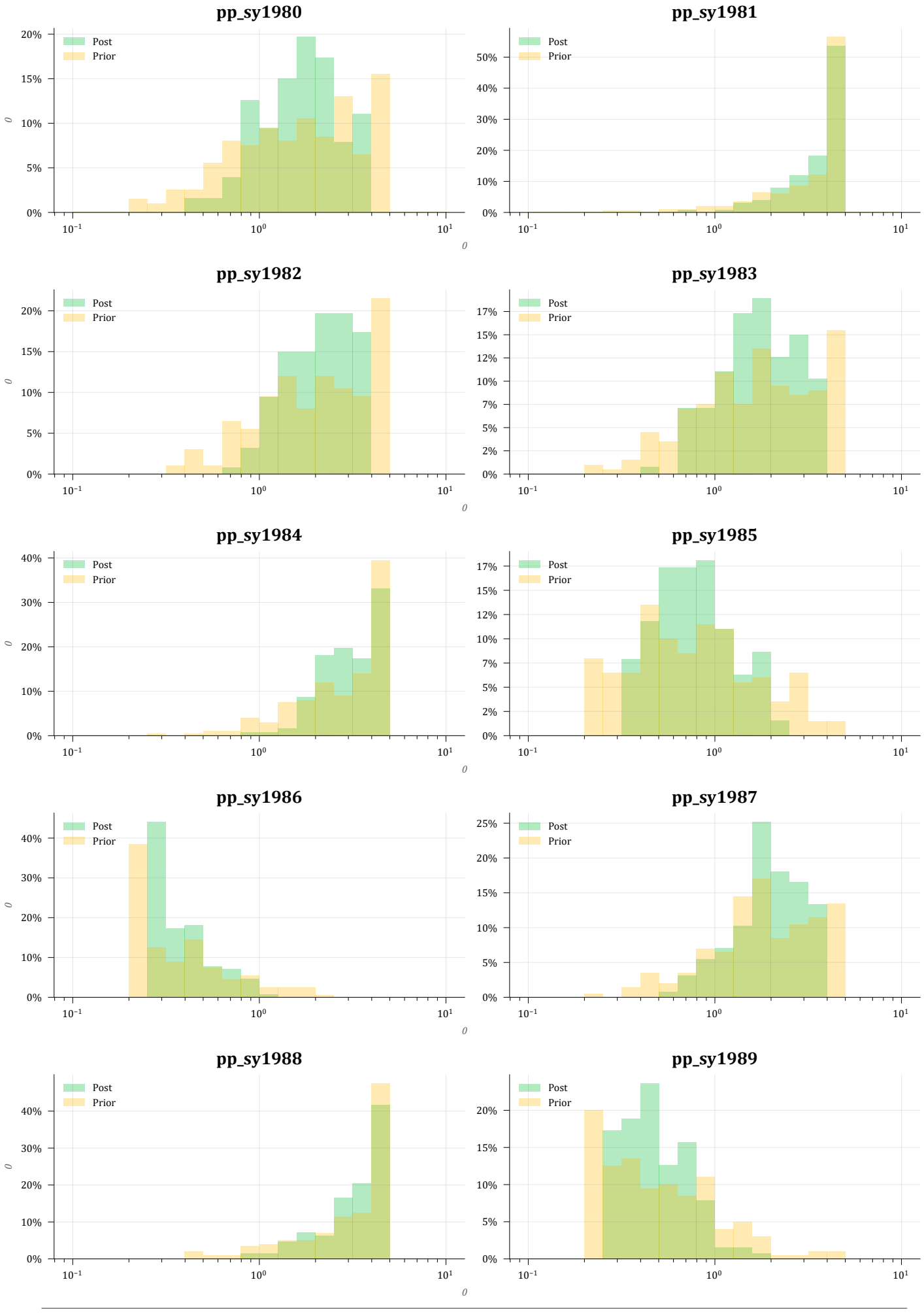

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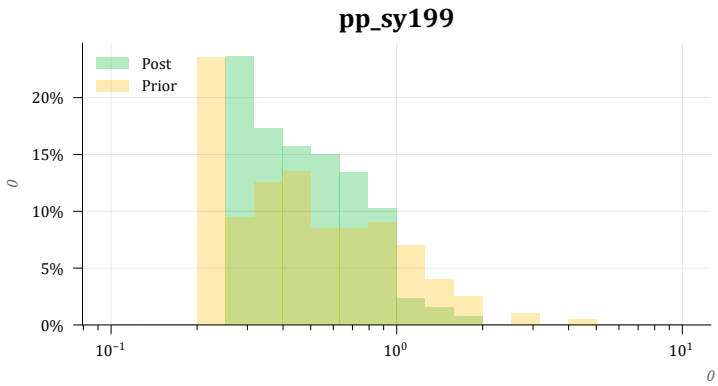

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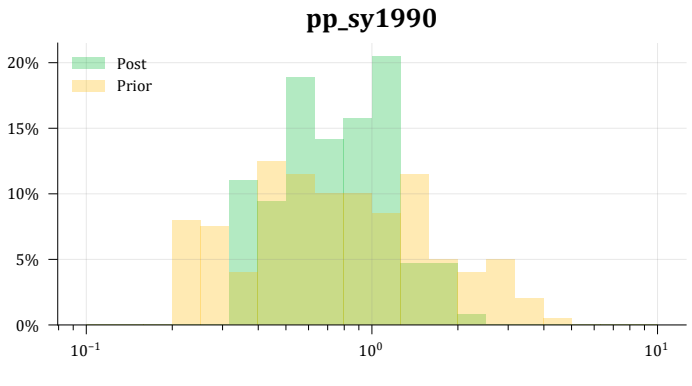

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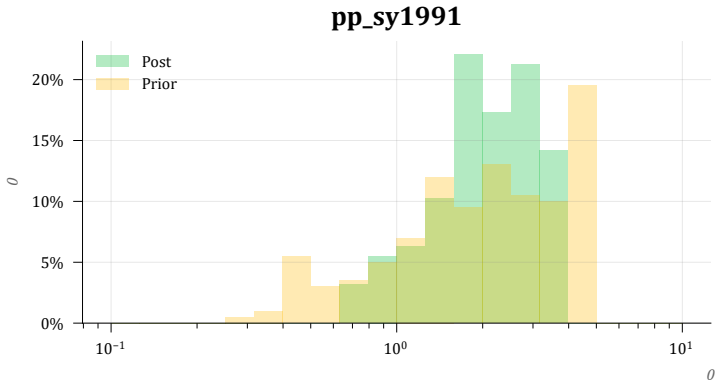

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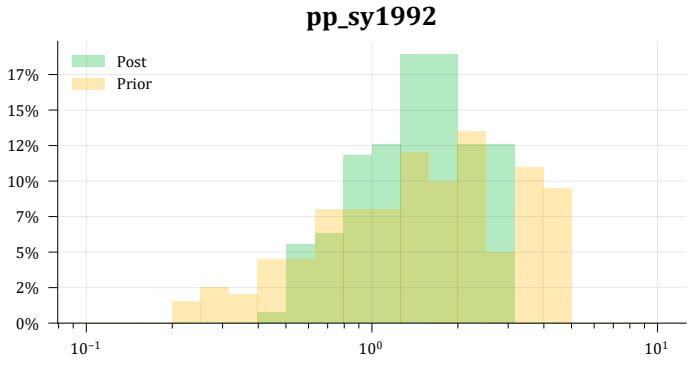

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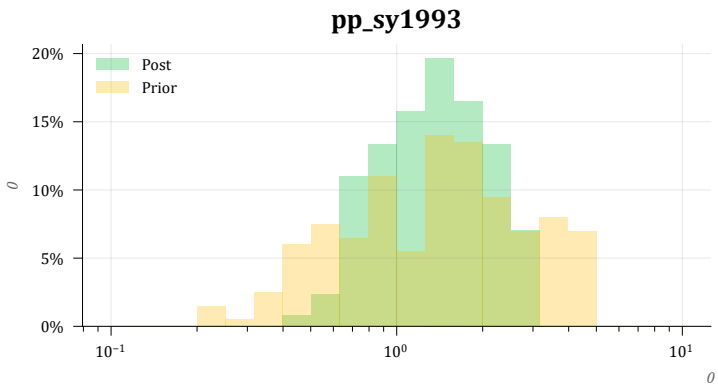

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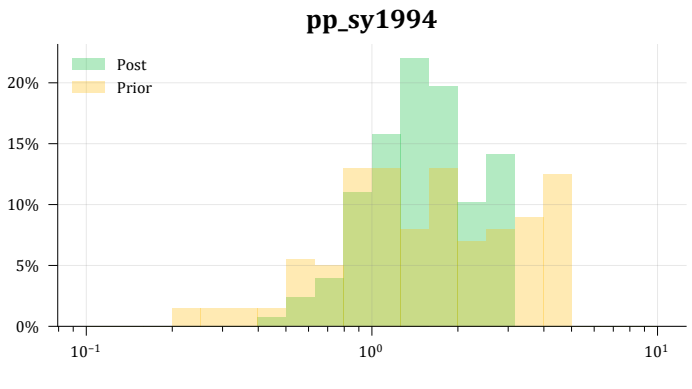

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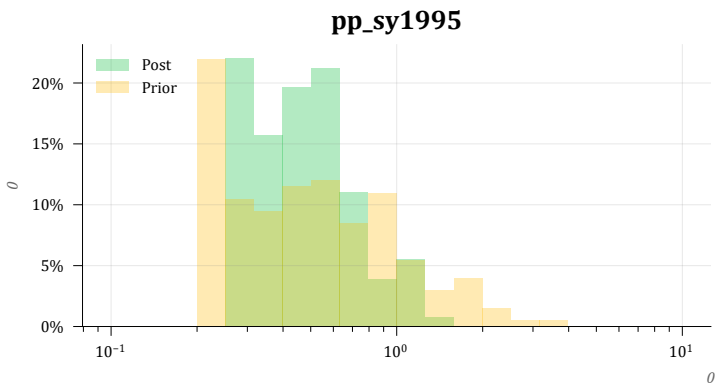

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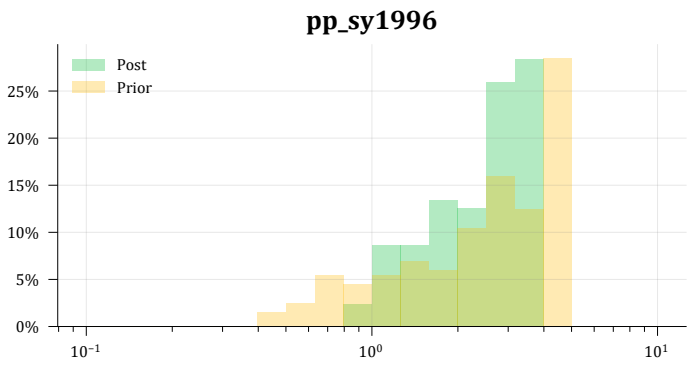

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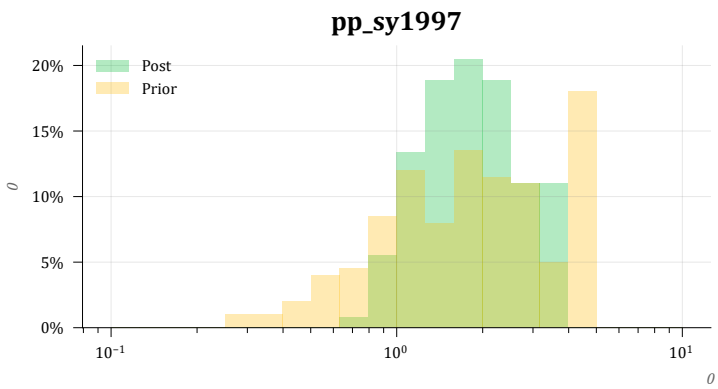

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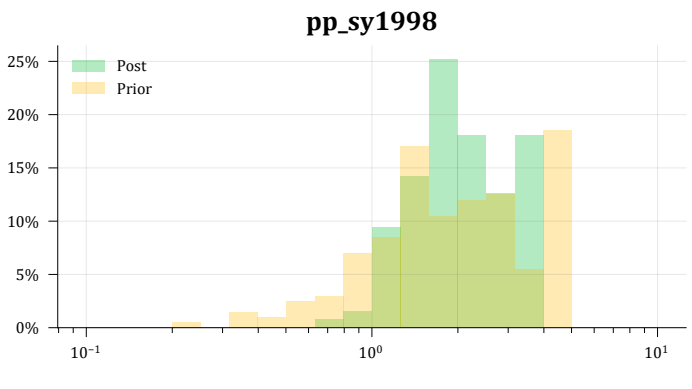

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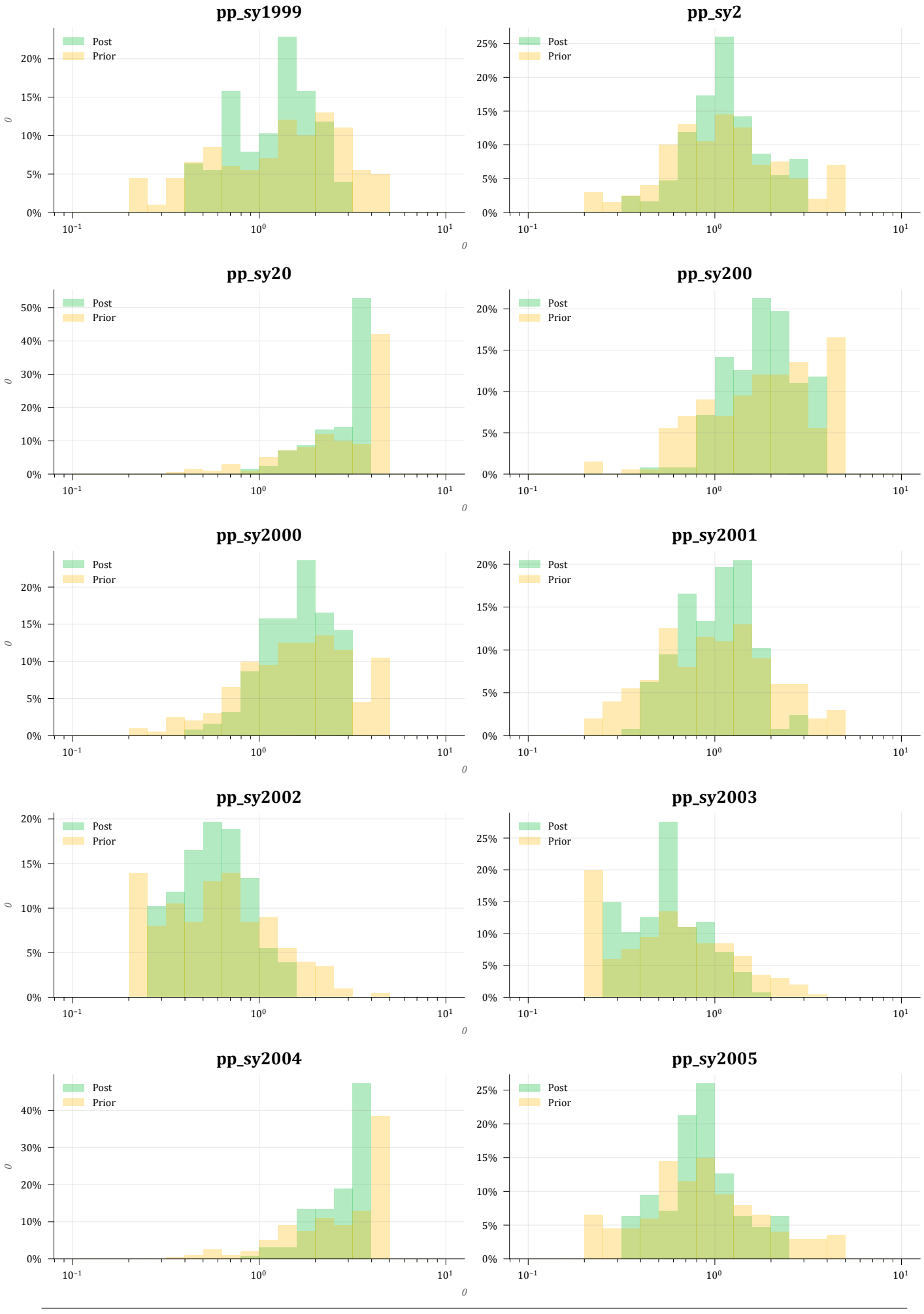

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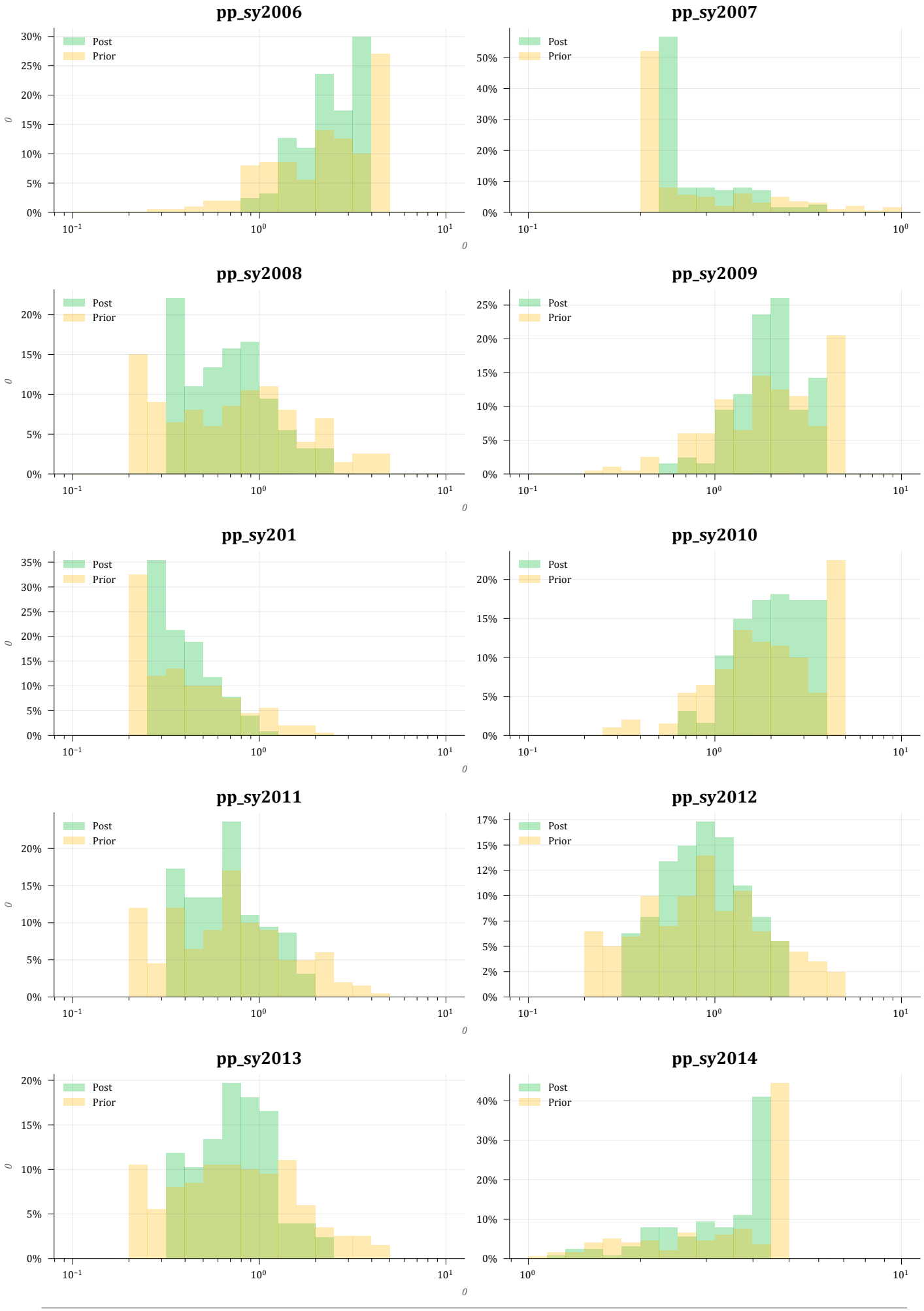

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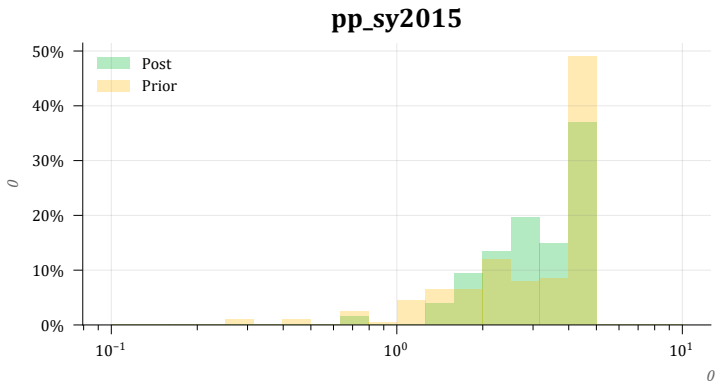

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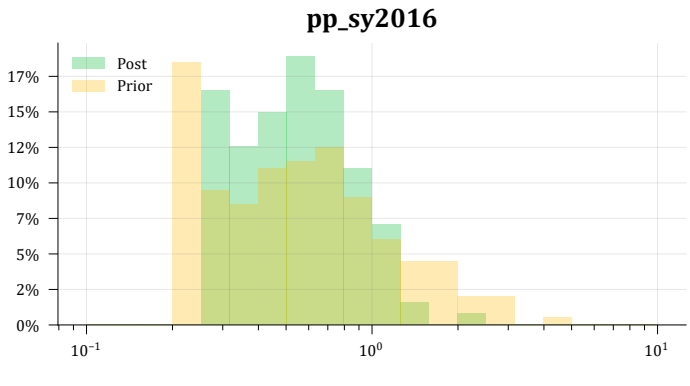

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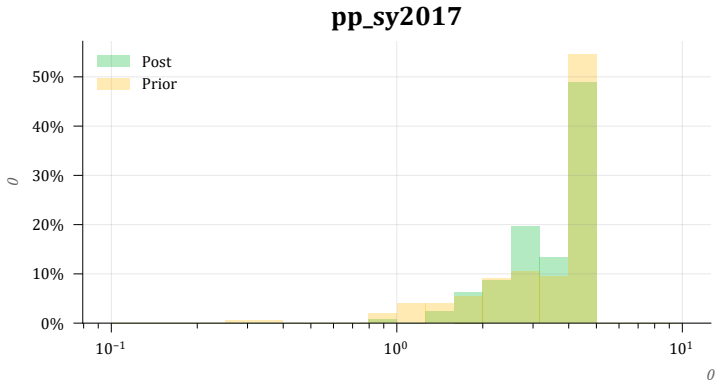

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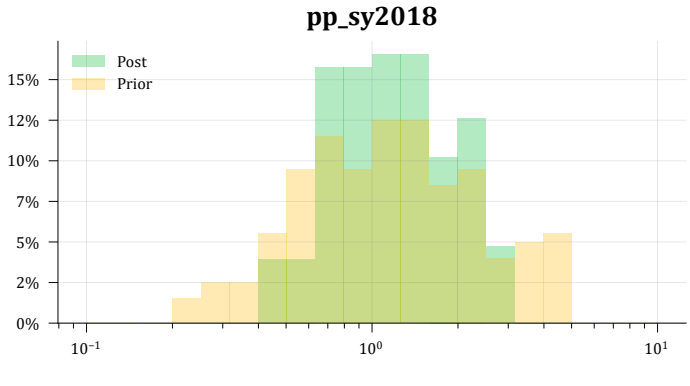

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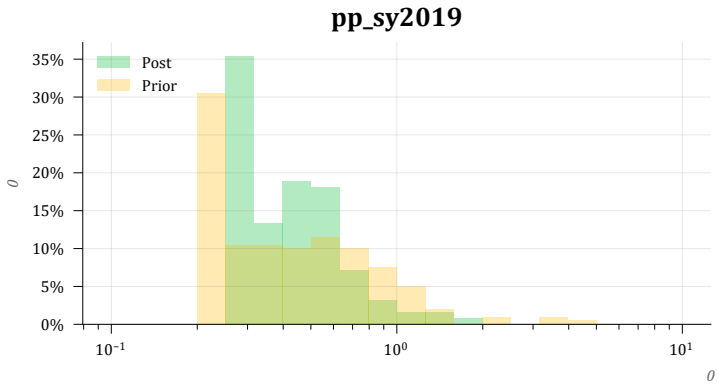

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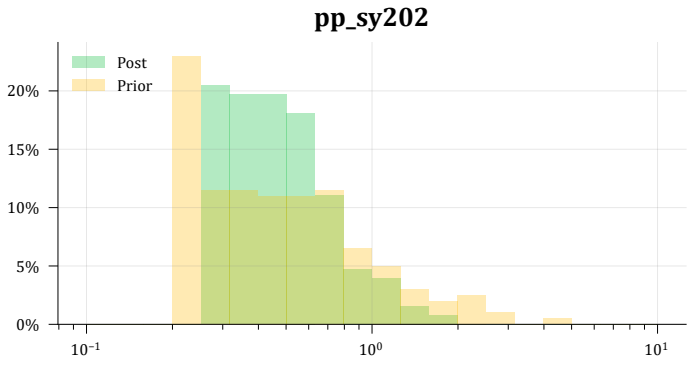

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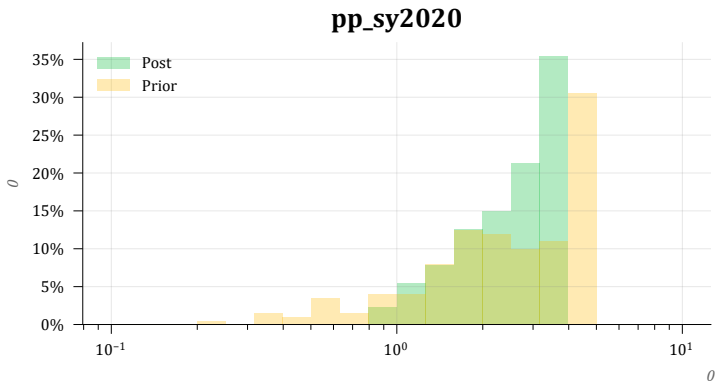

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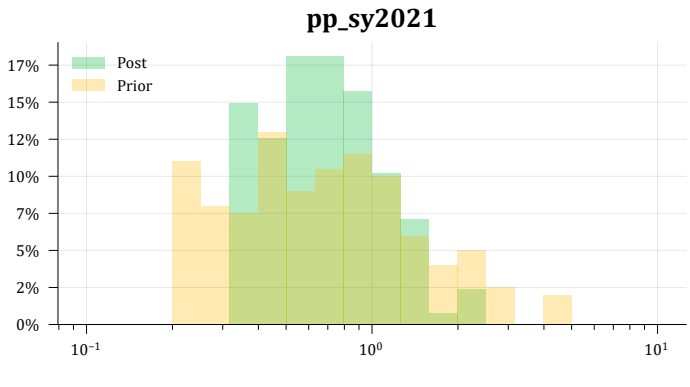

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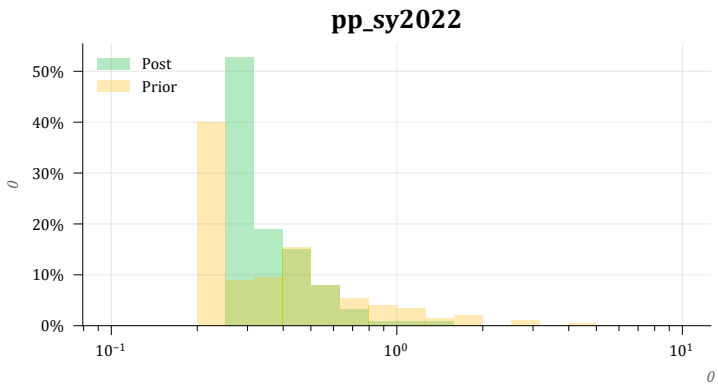

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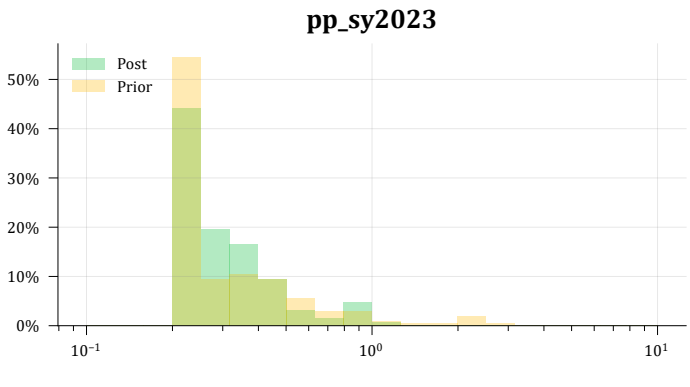

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pp_sy202
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pp_sy2020
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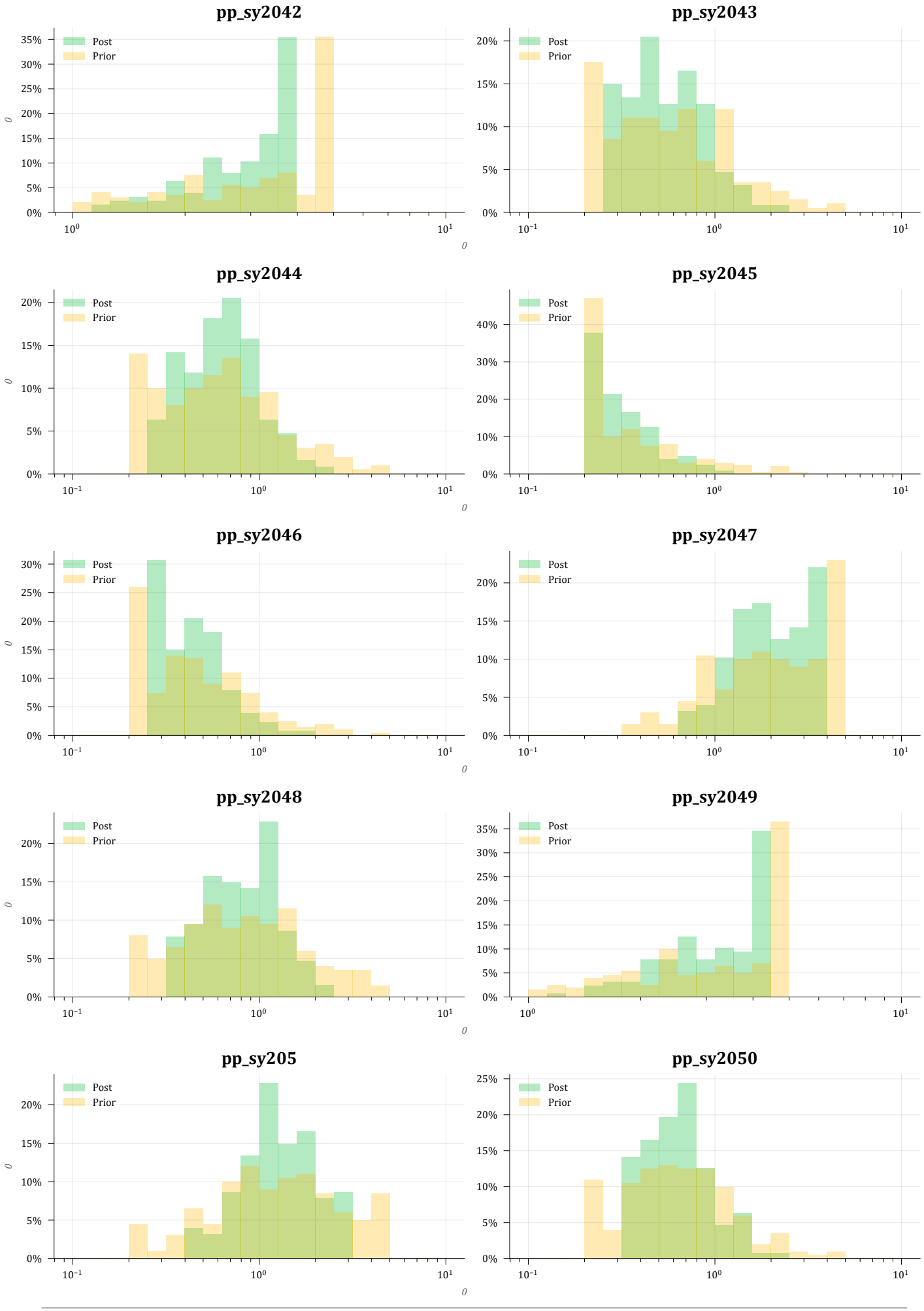

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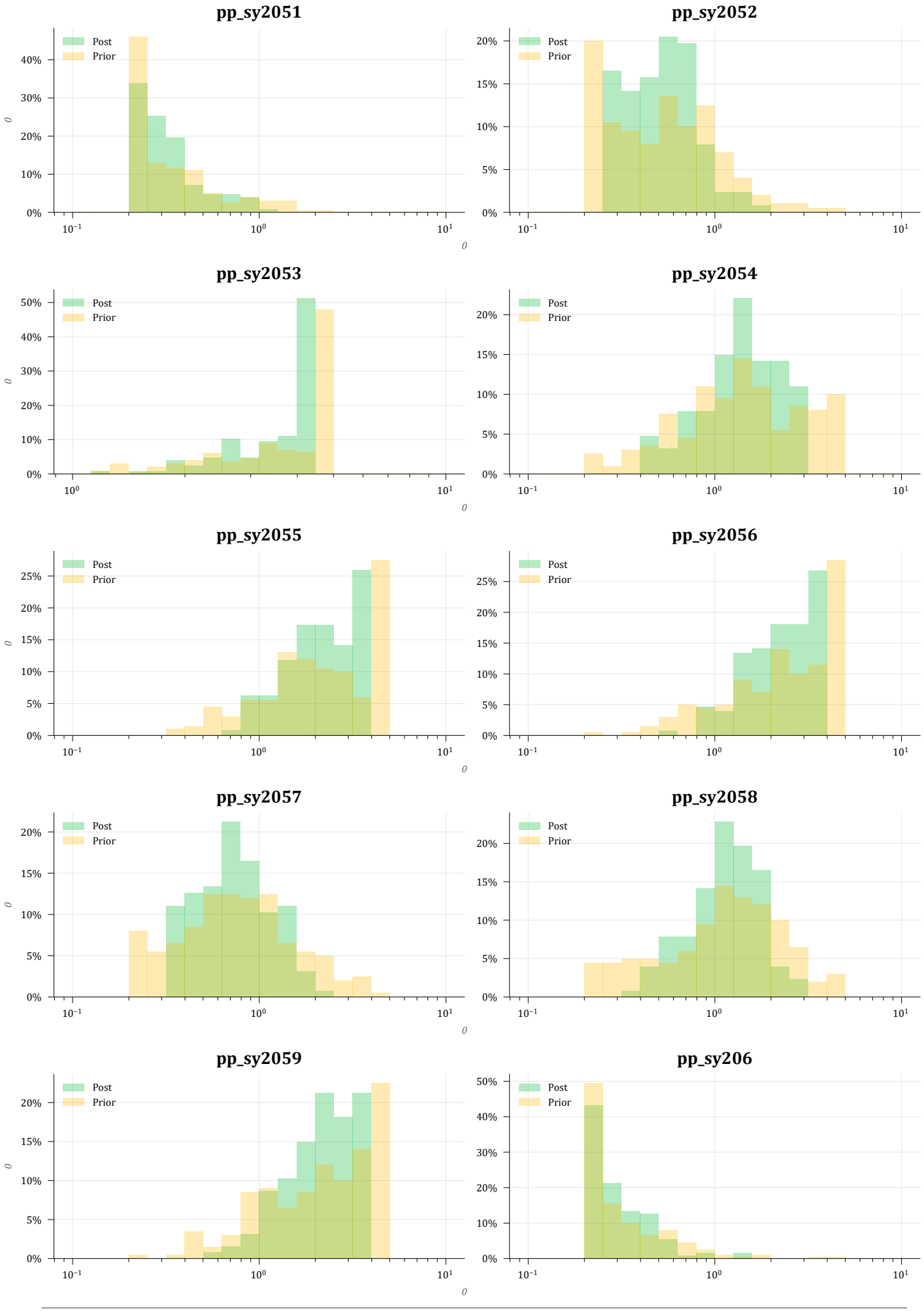

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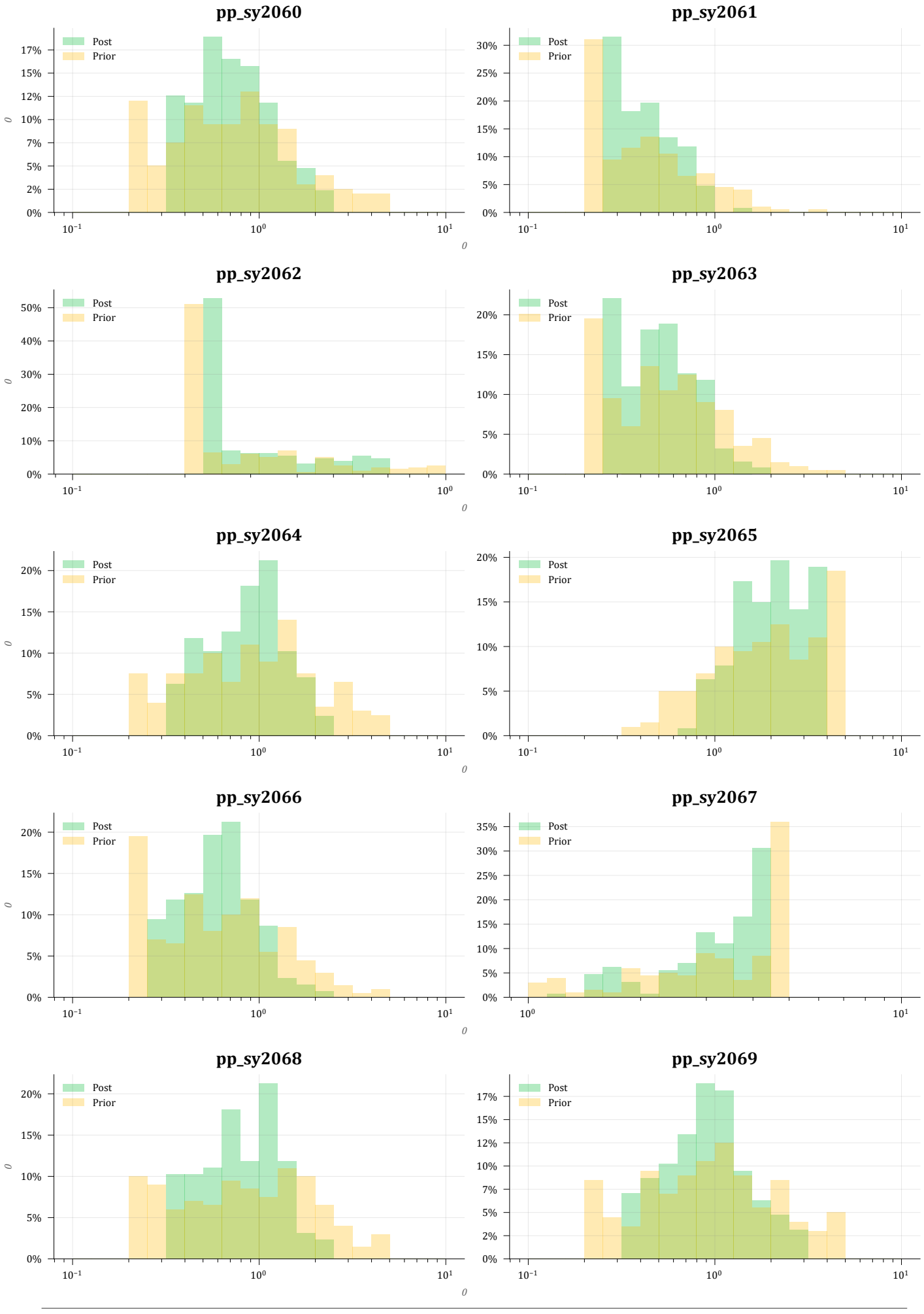

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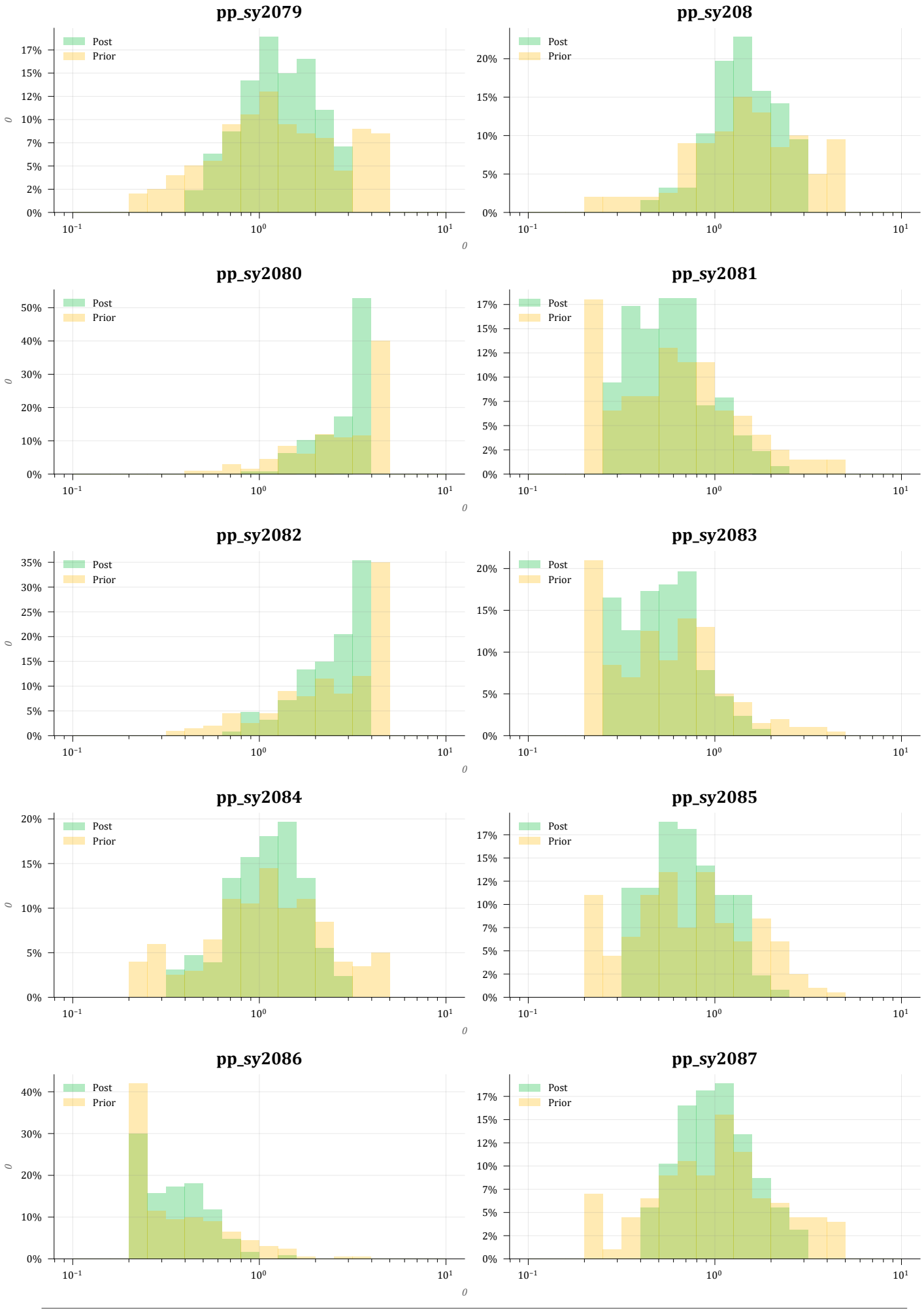

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Post
Prior
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pp_sy2042
pp_sy2043
pp_sy2044
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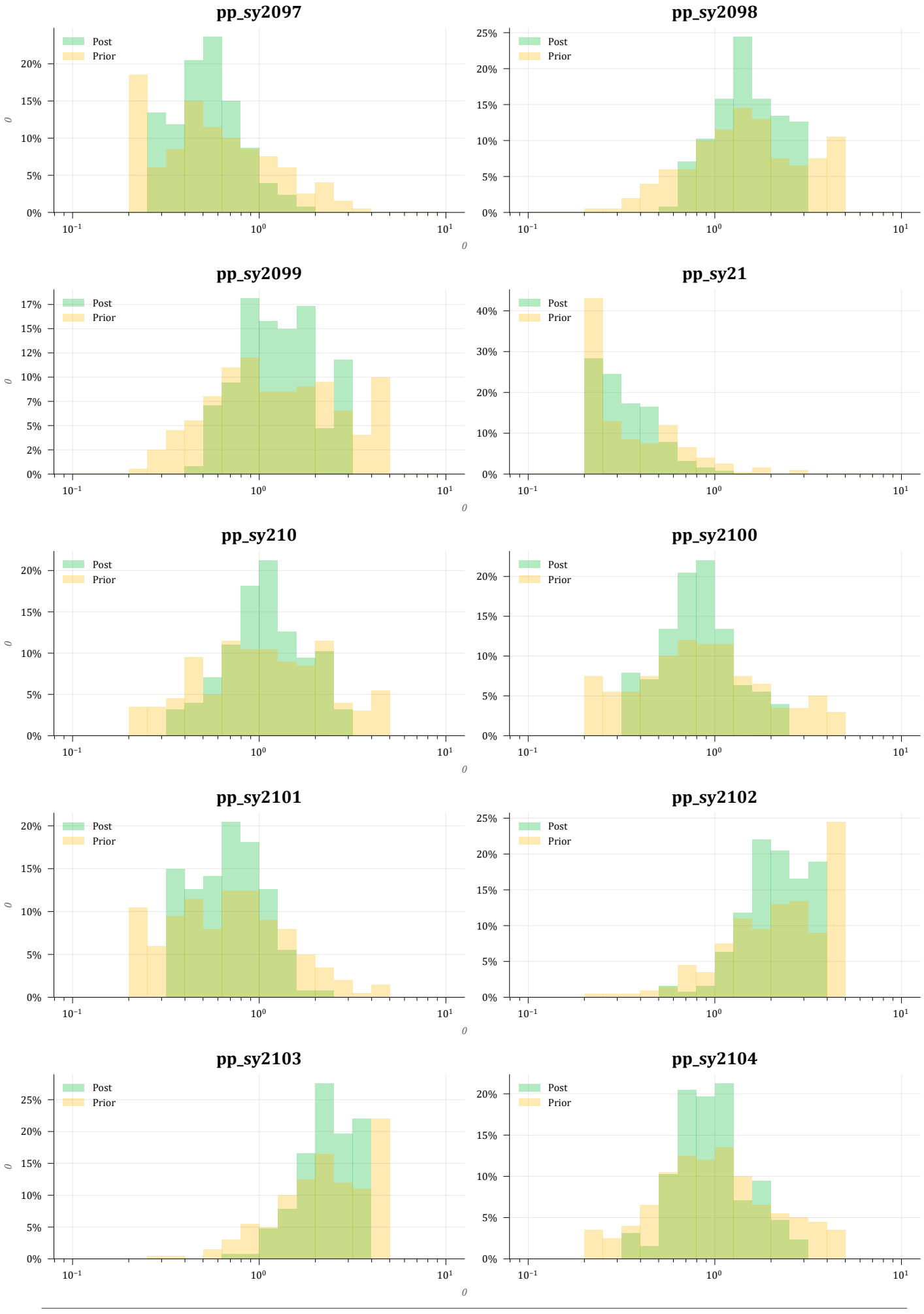

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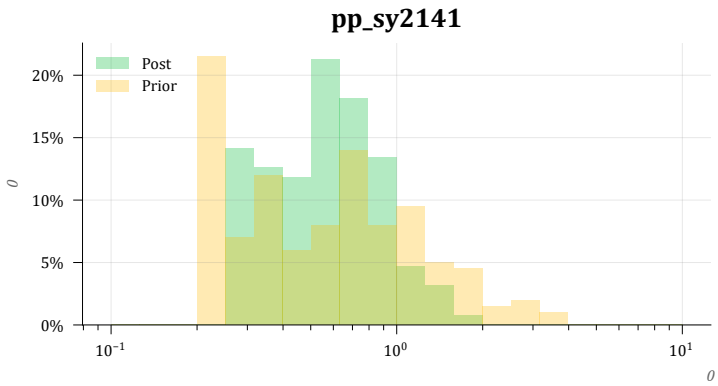

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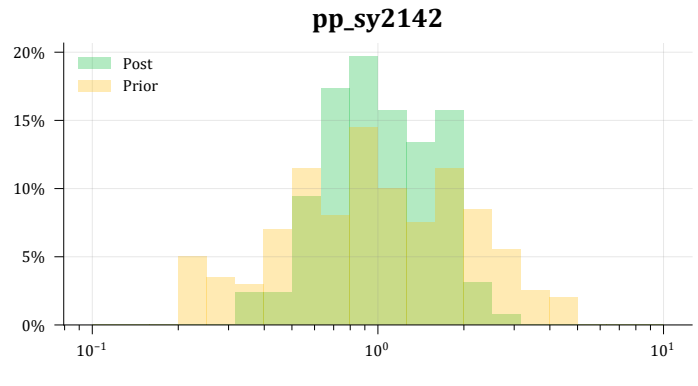

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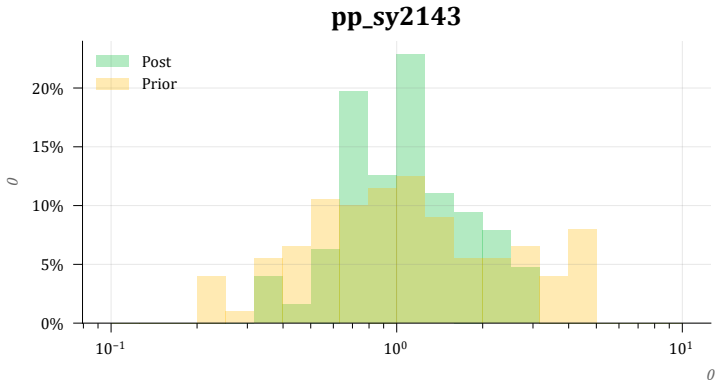

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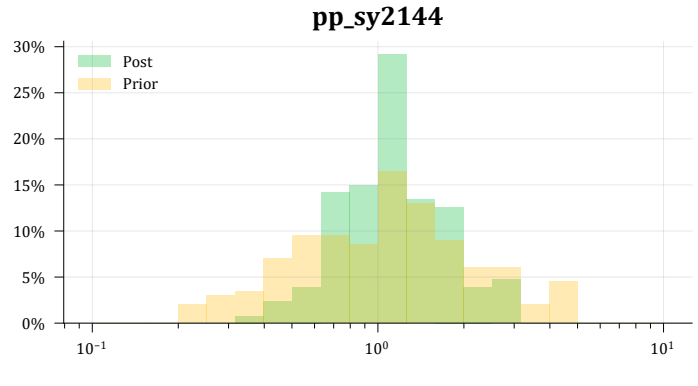

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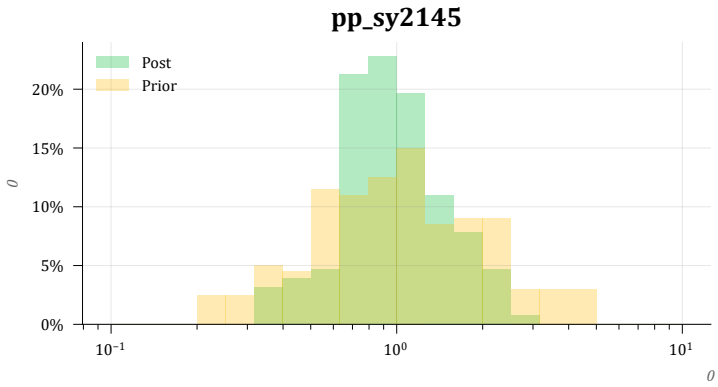

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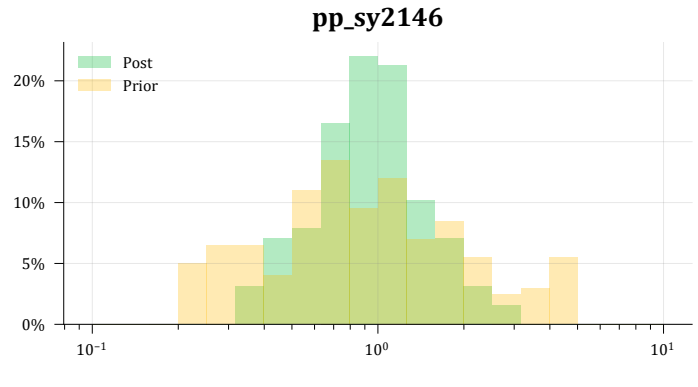

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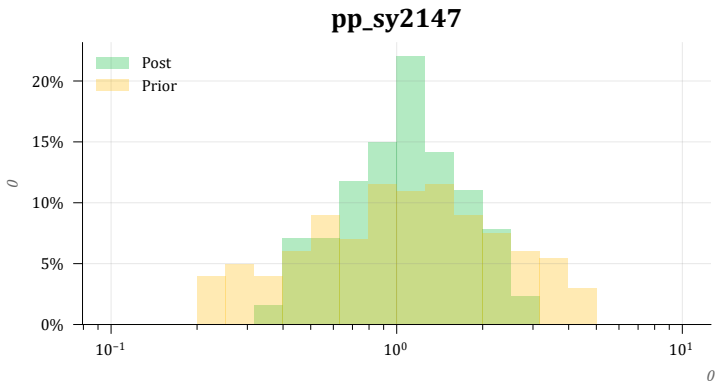

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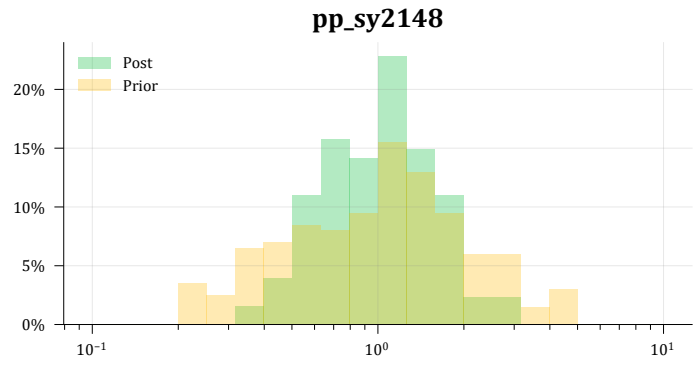

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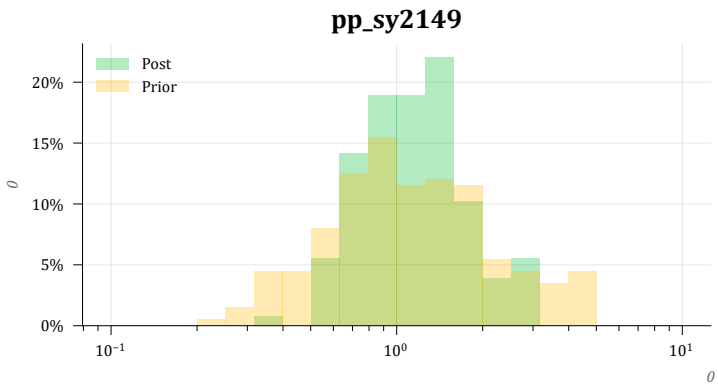

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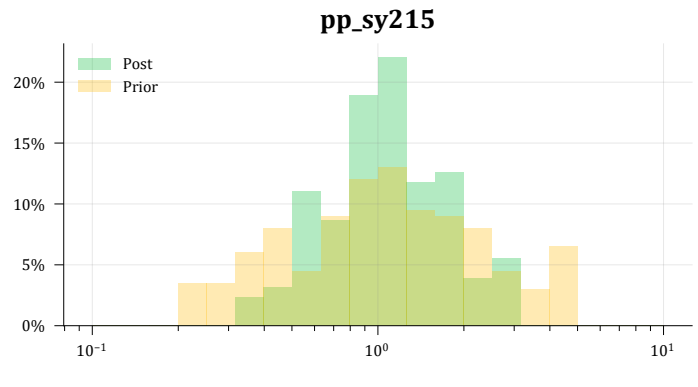

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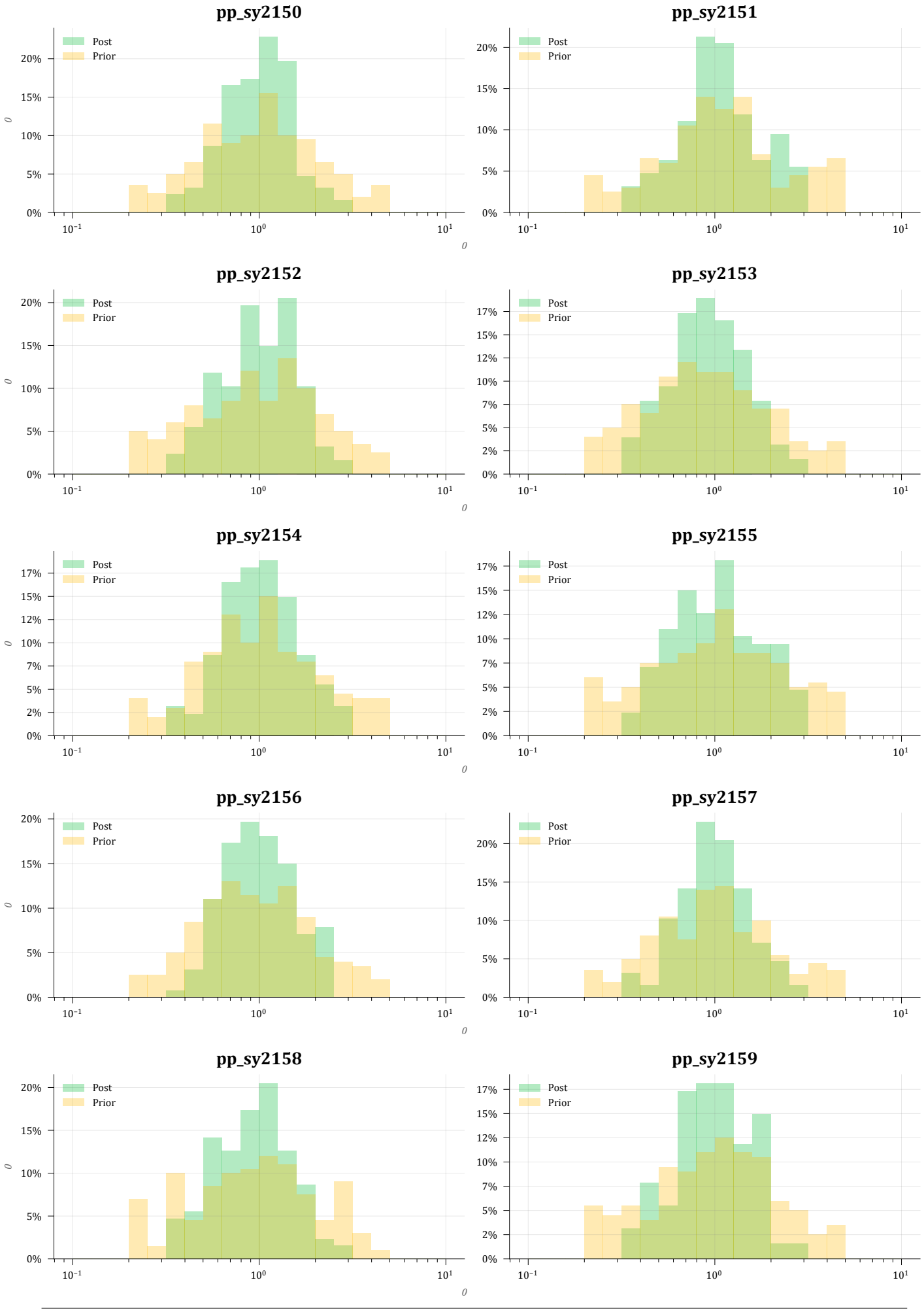

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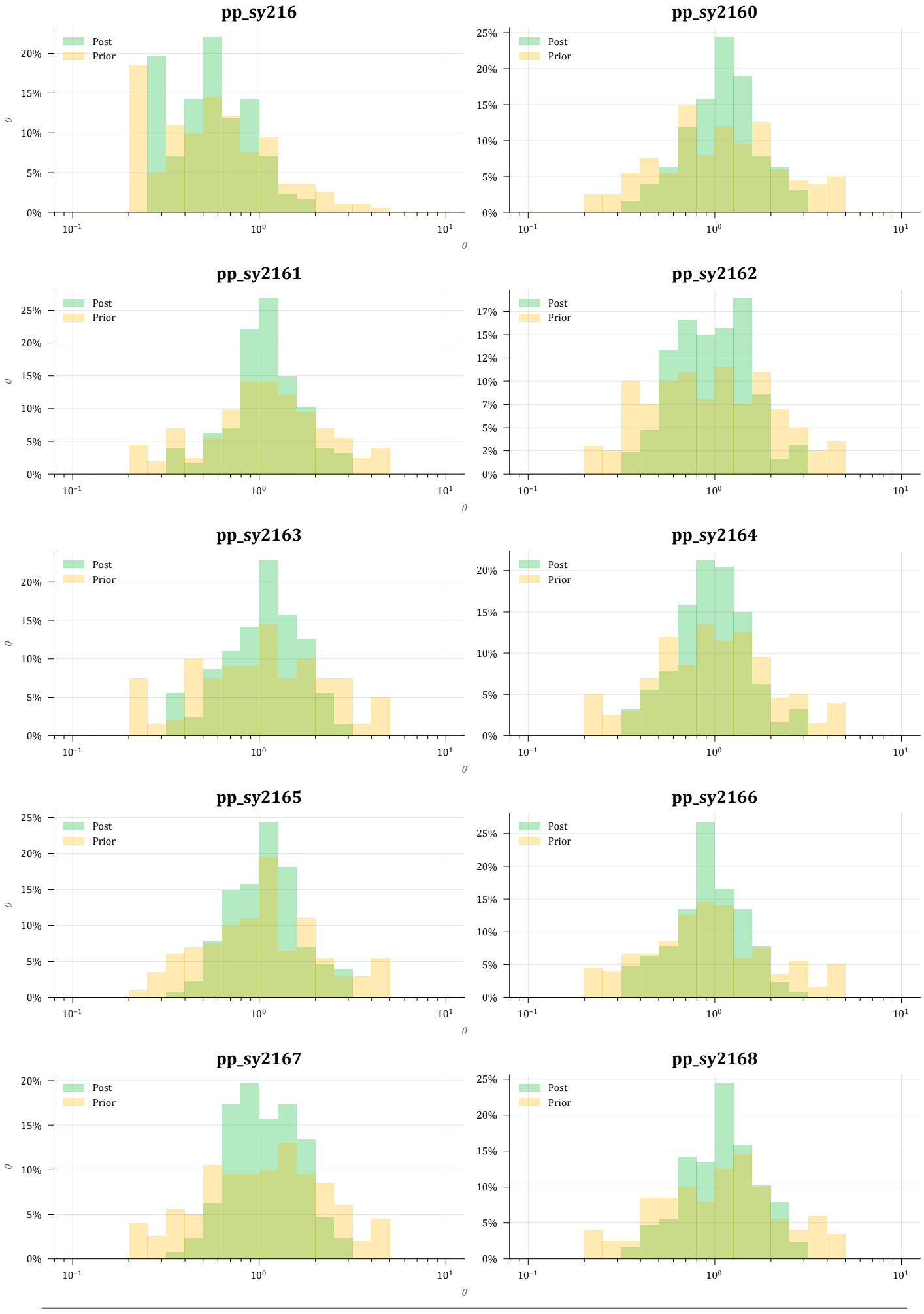

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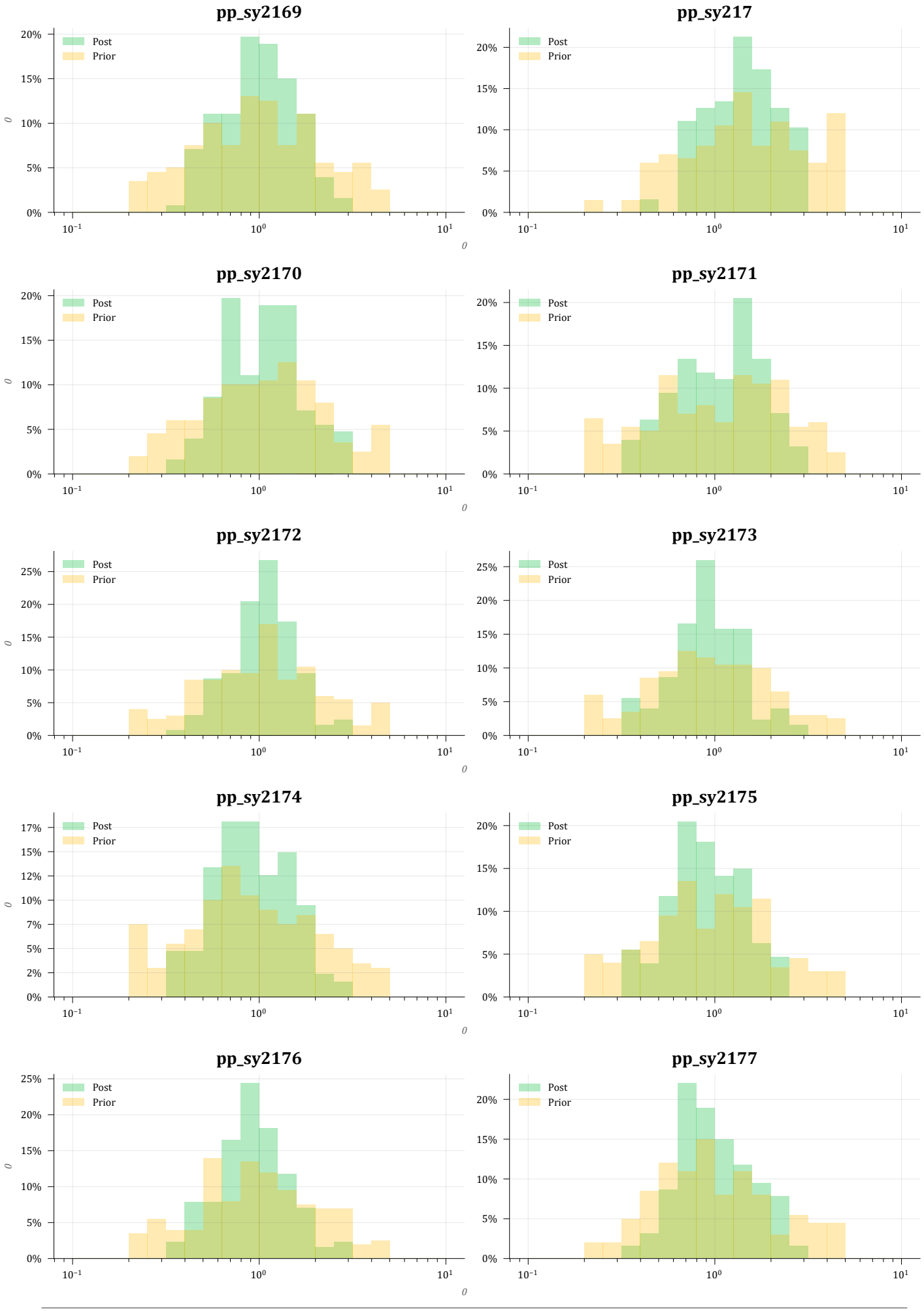

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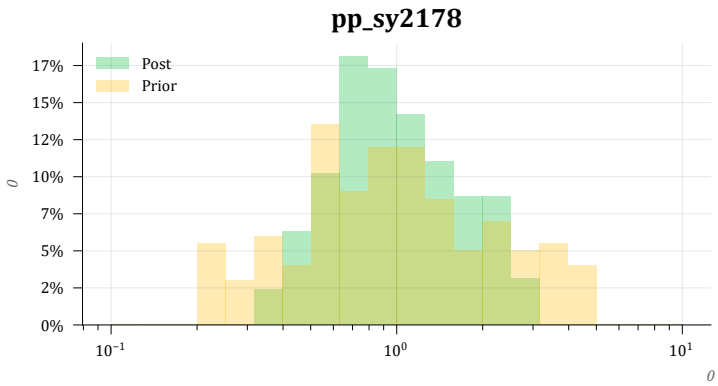

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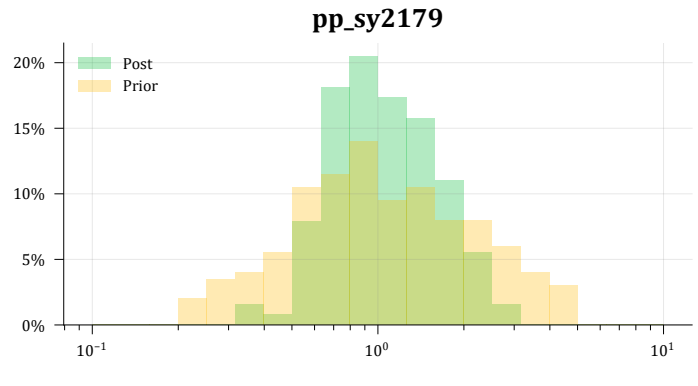

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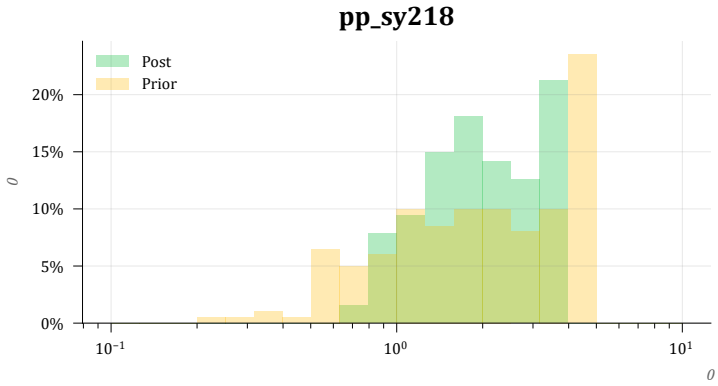

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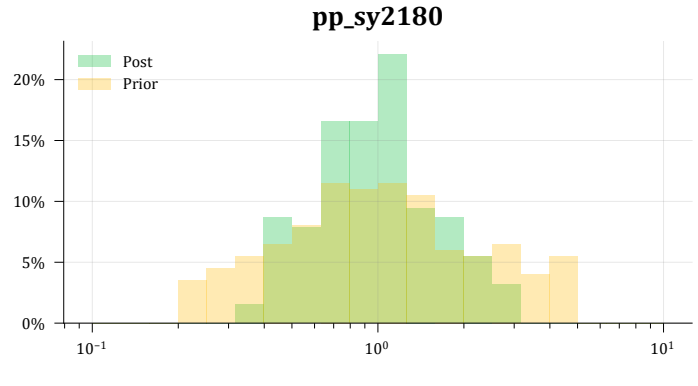

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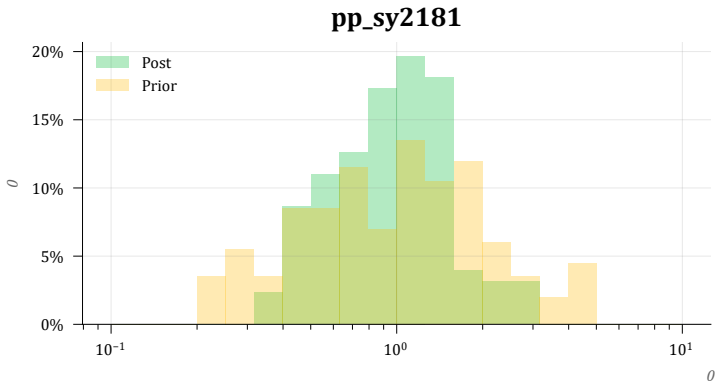

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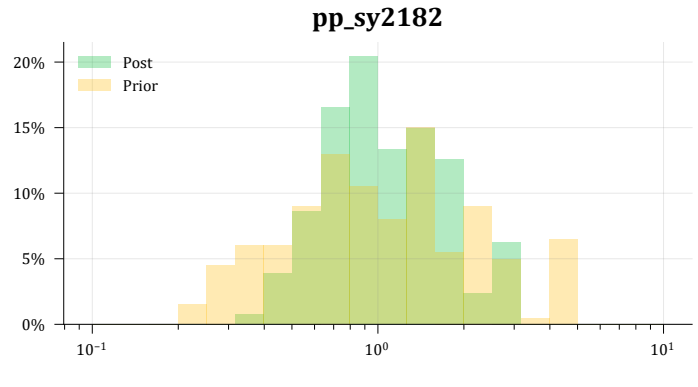

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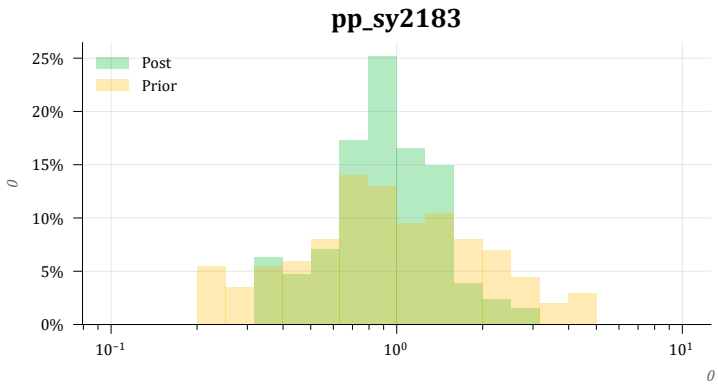

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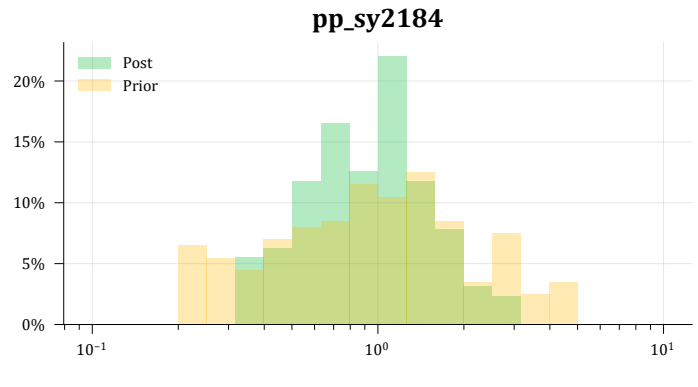

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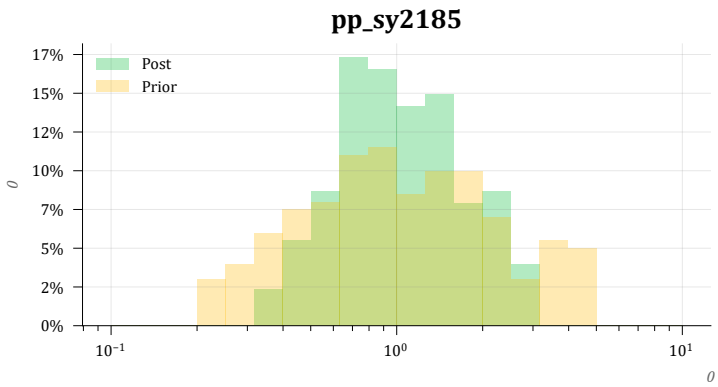

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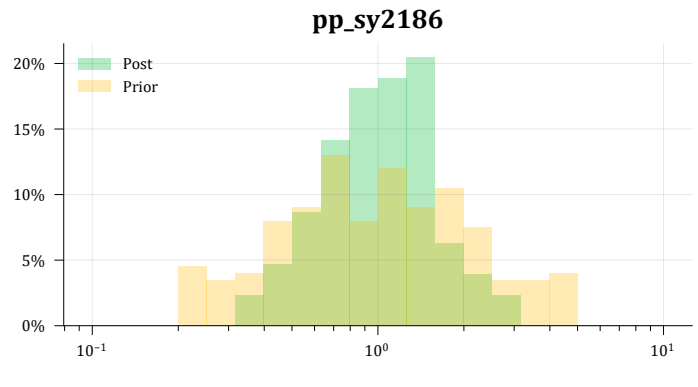

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pp_sy2182
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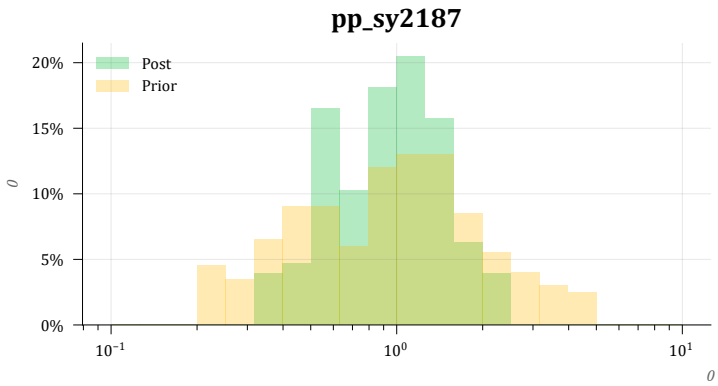

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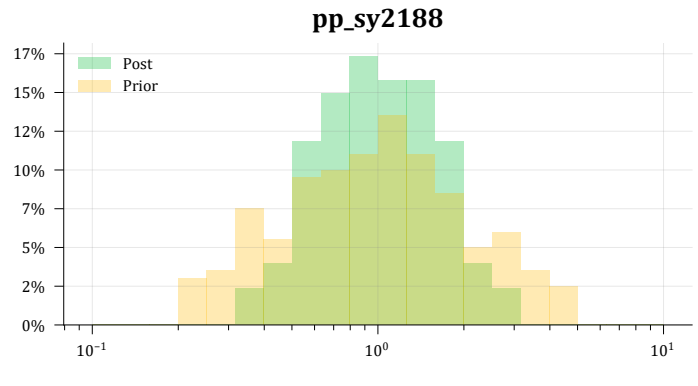

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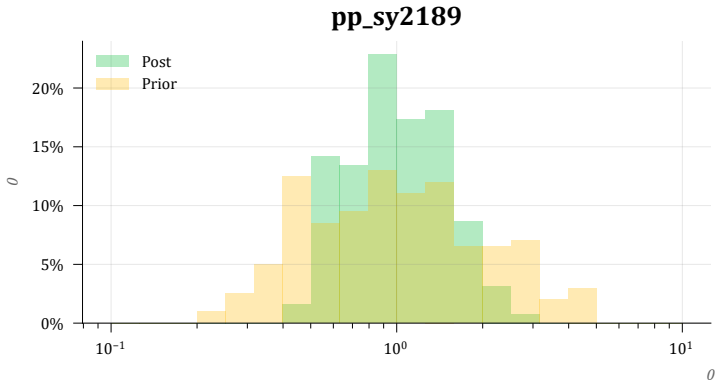

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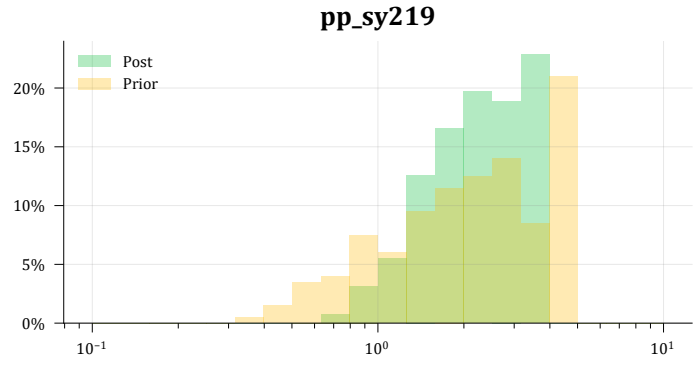

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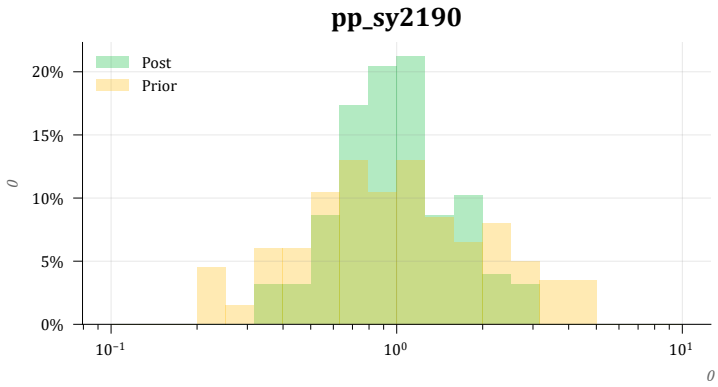
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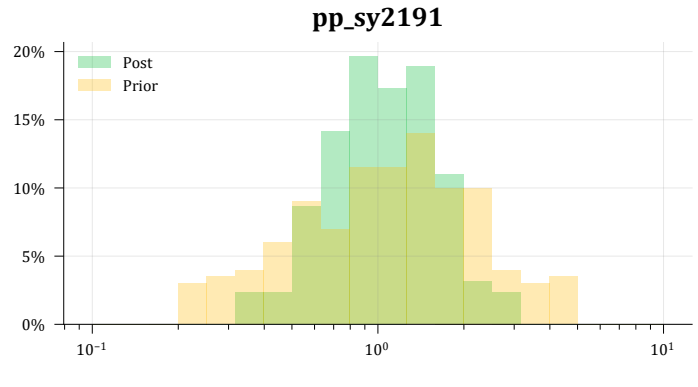

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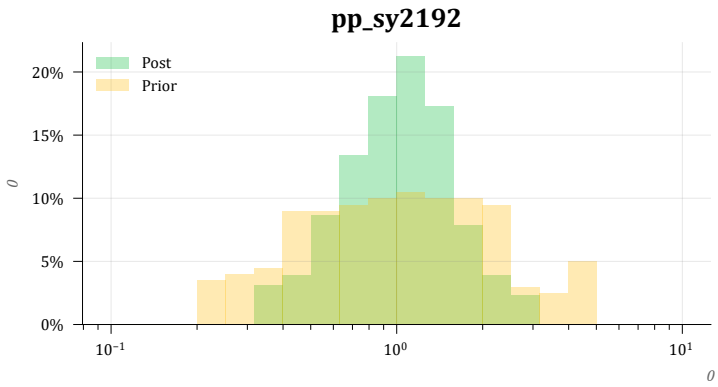

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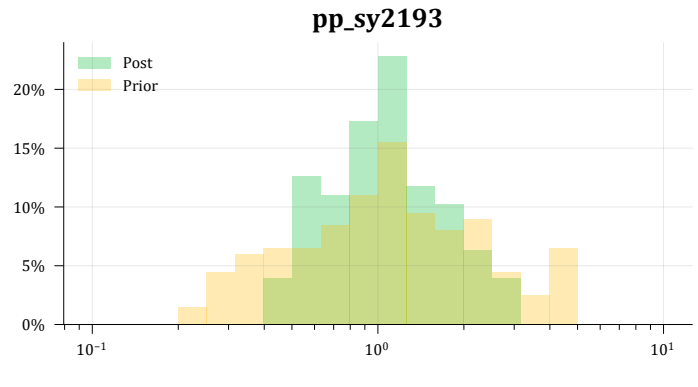

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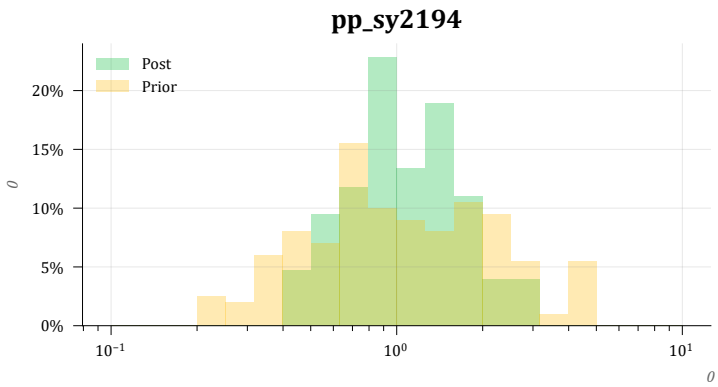

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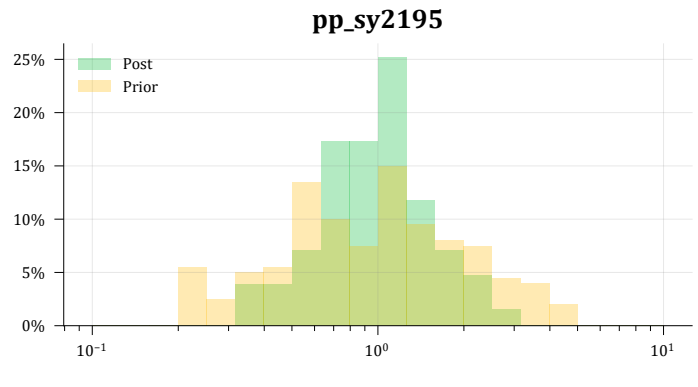

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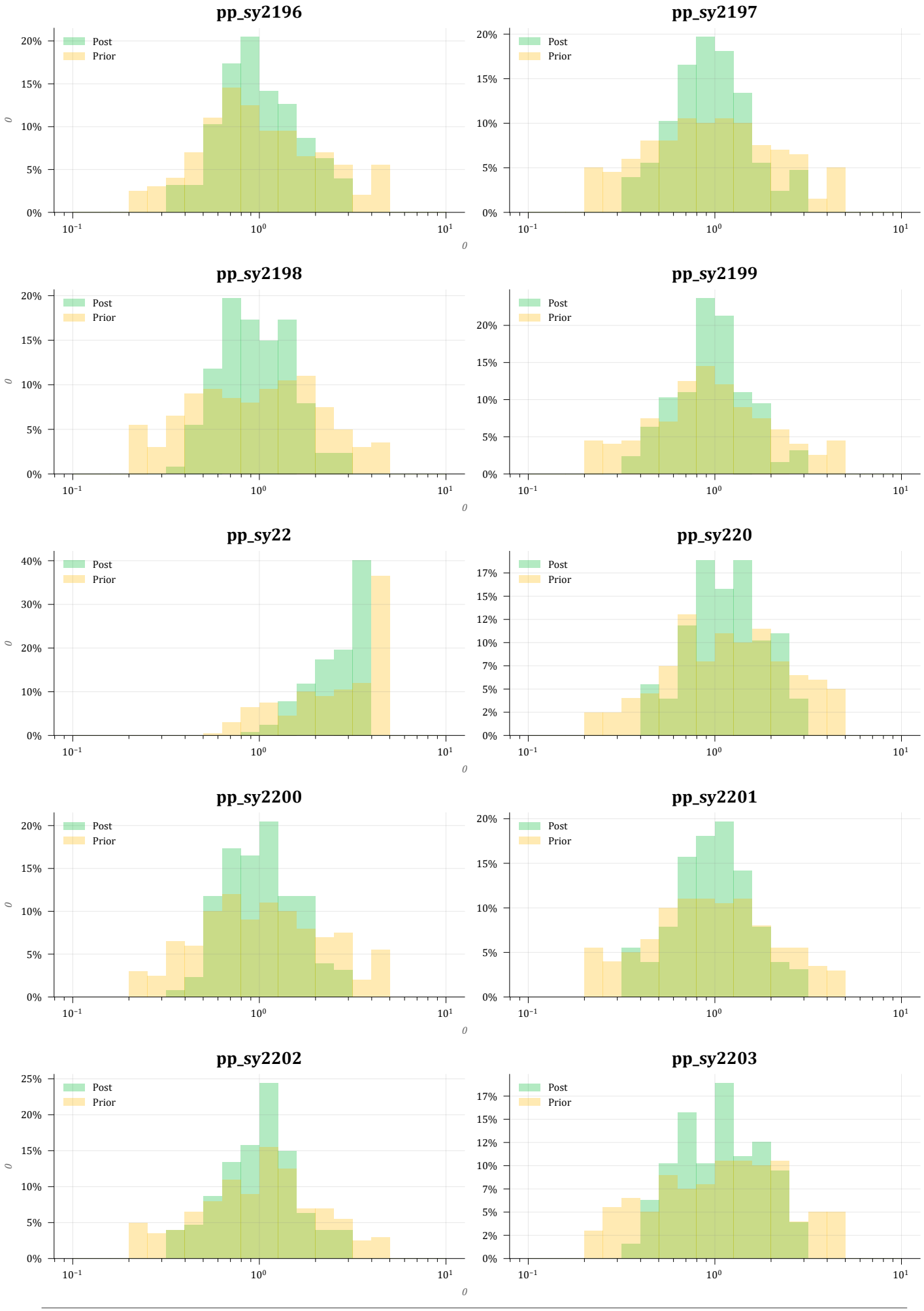

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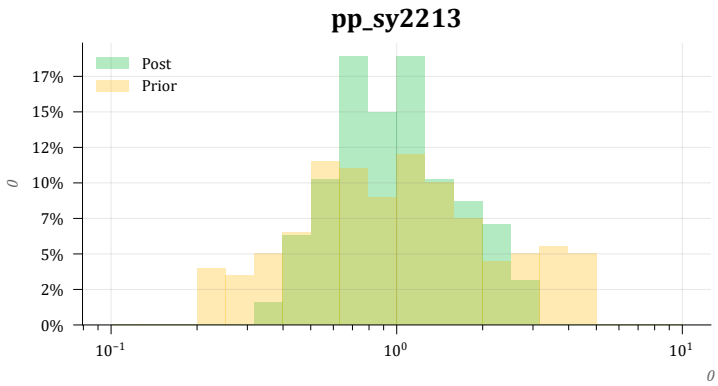

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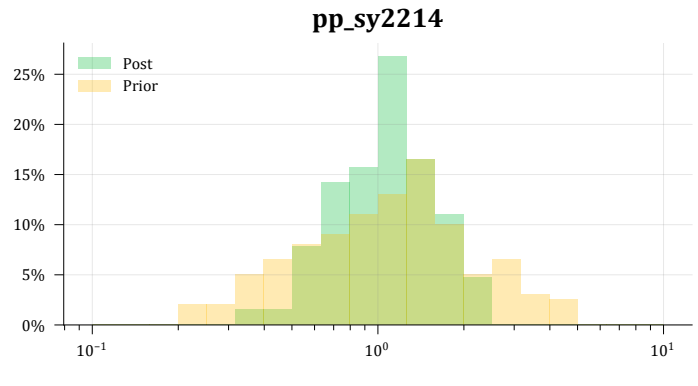

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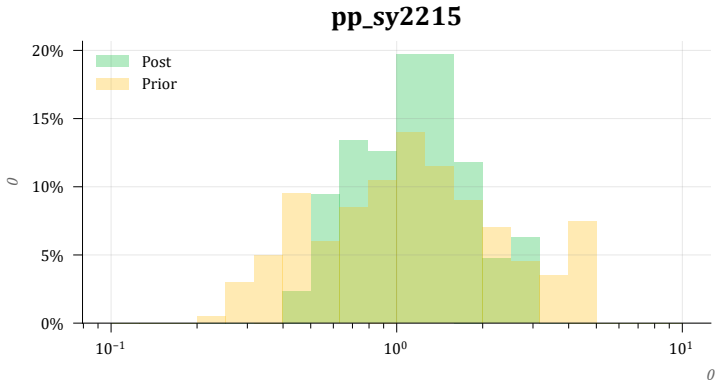

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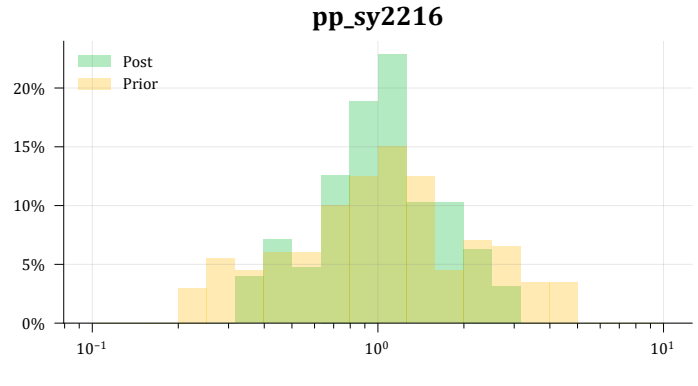

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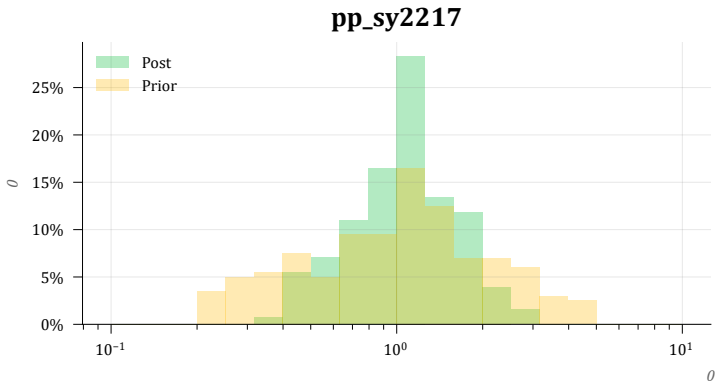

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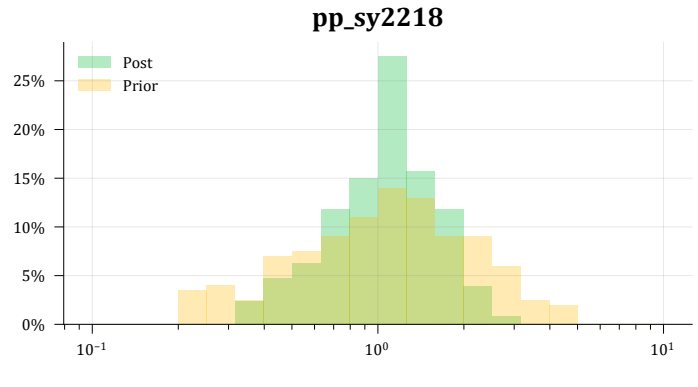

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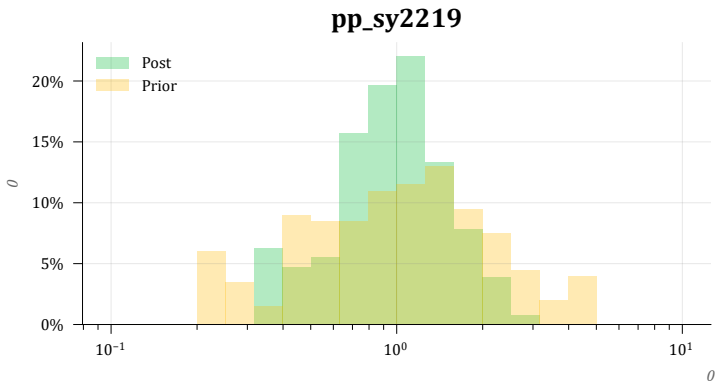

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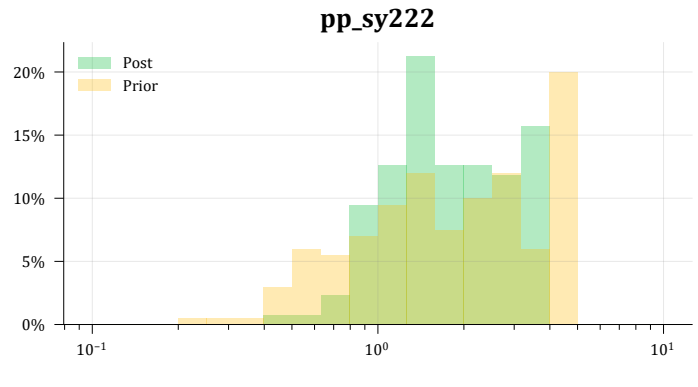

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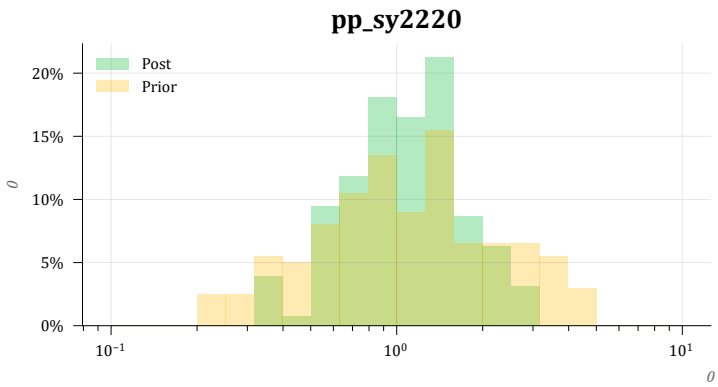

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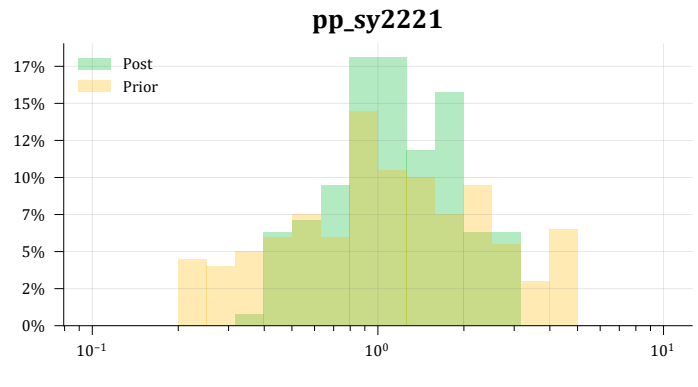

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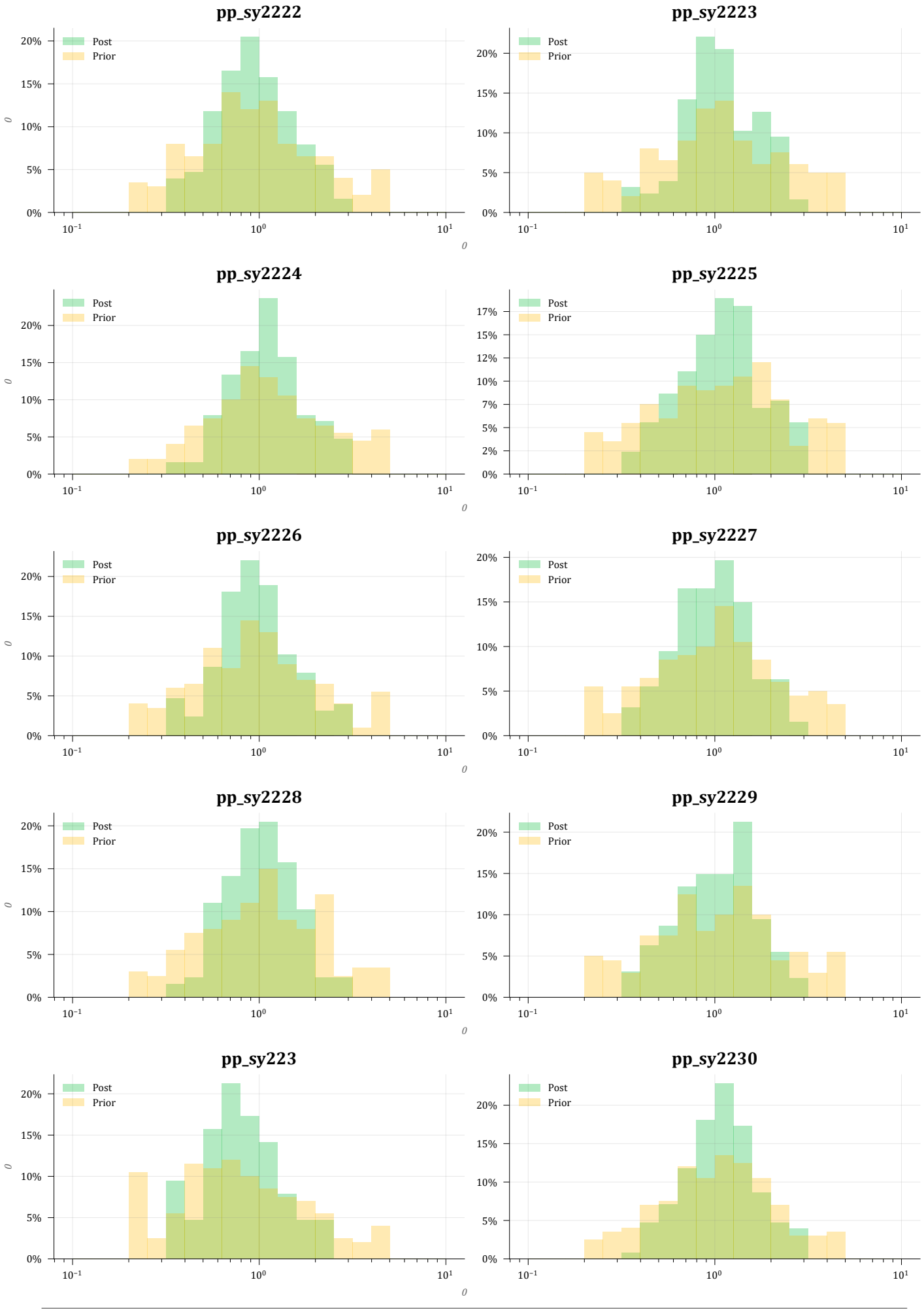

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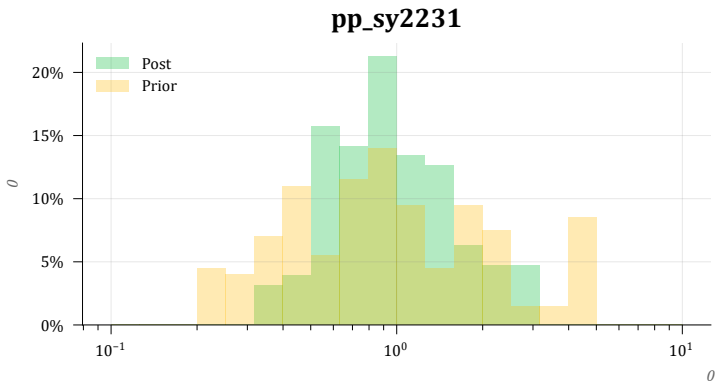

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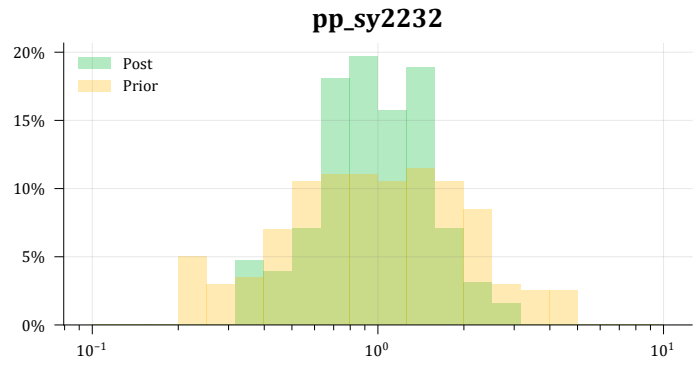

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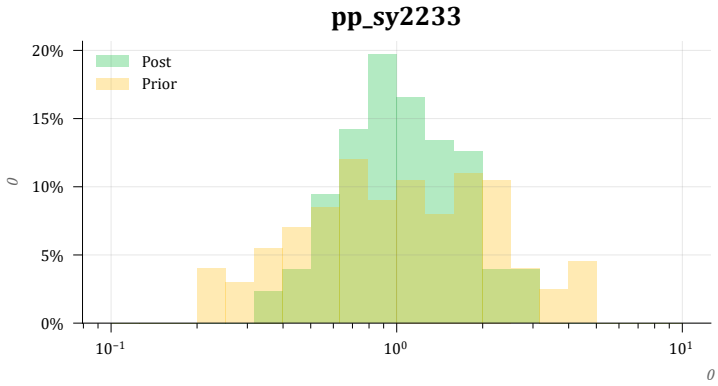

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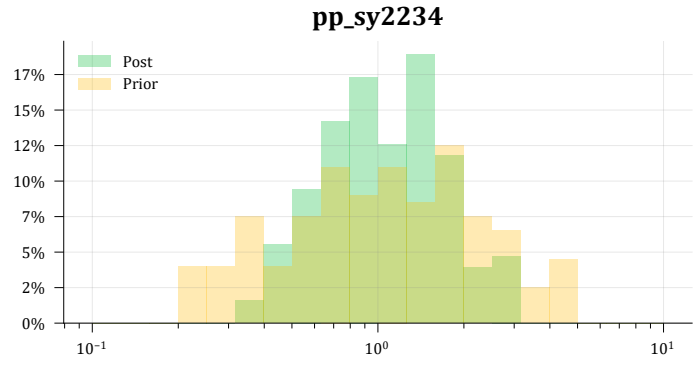

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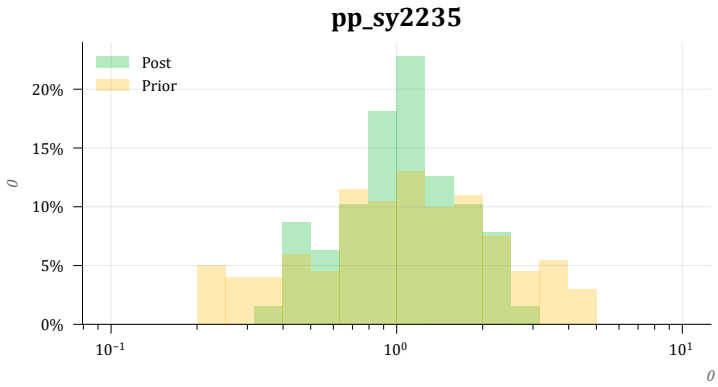

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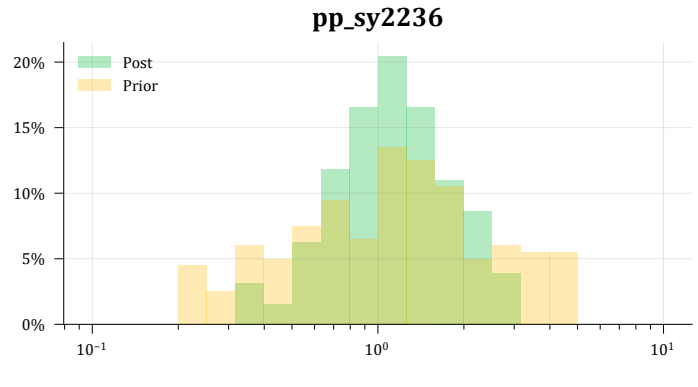

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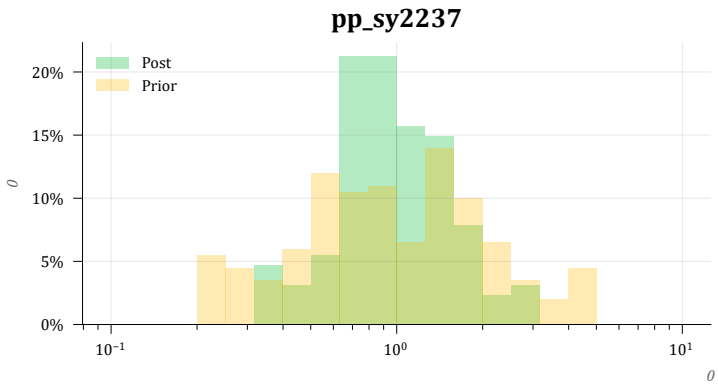

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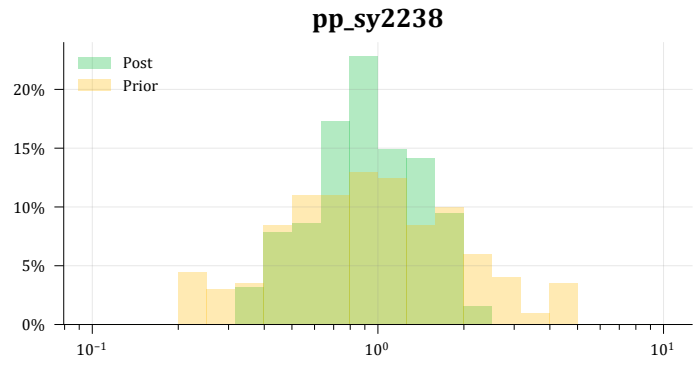

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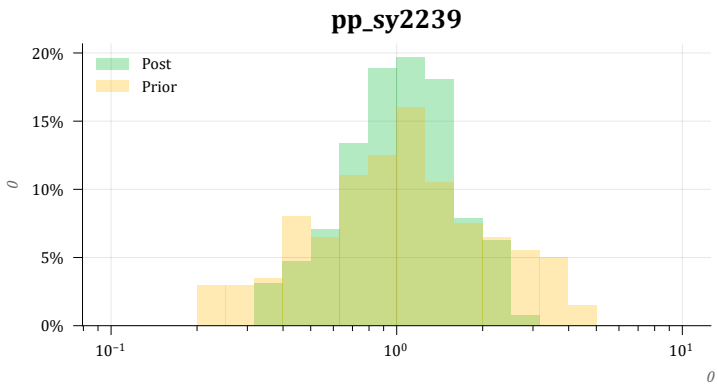

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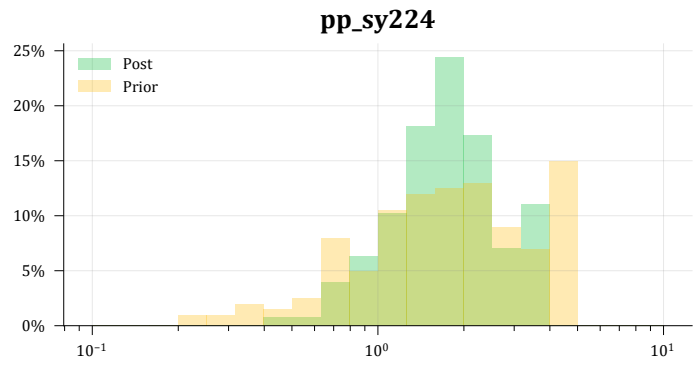

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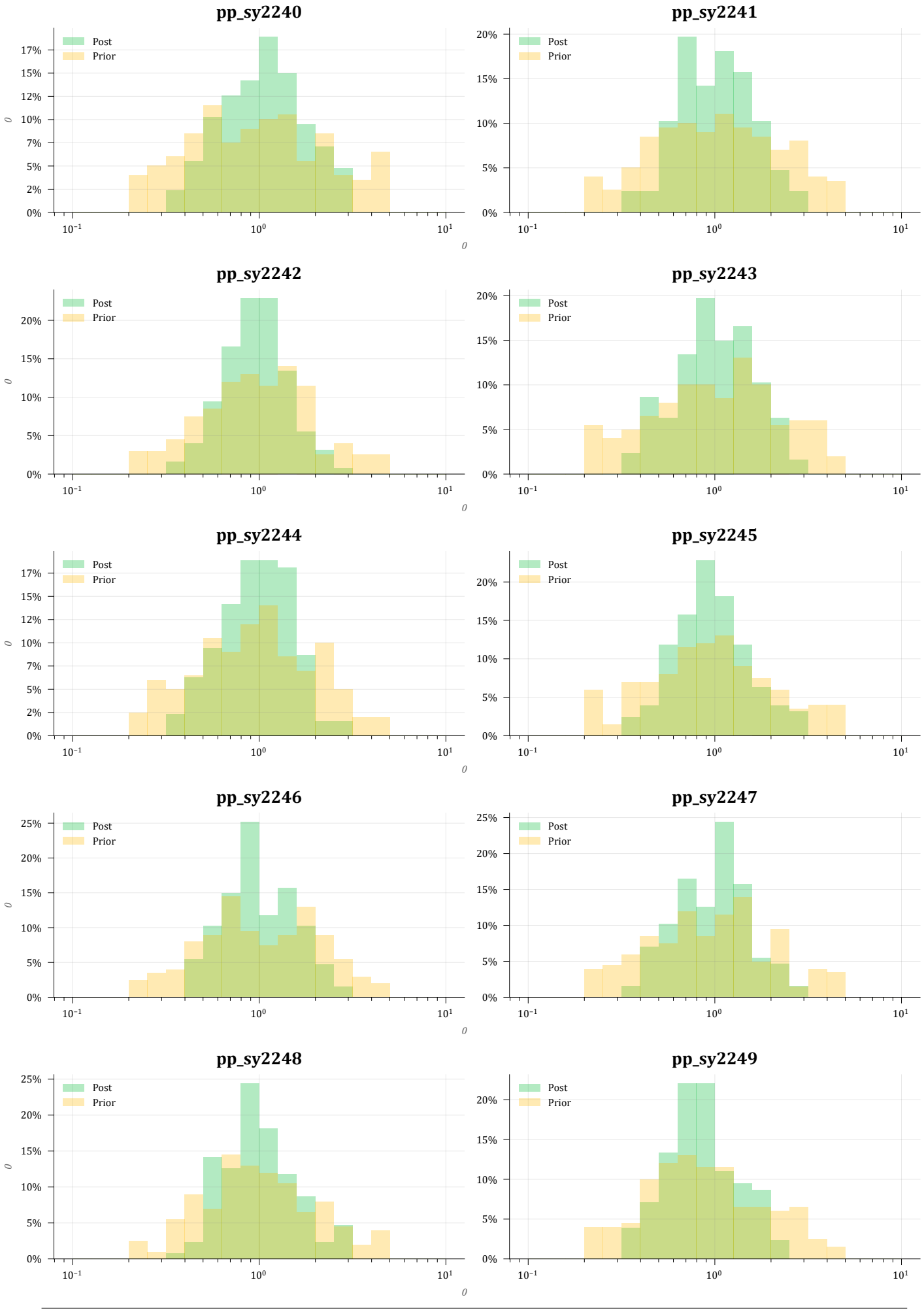

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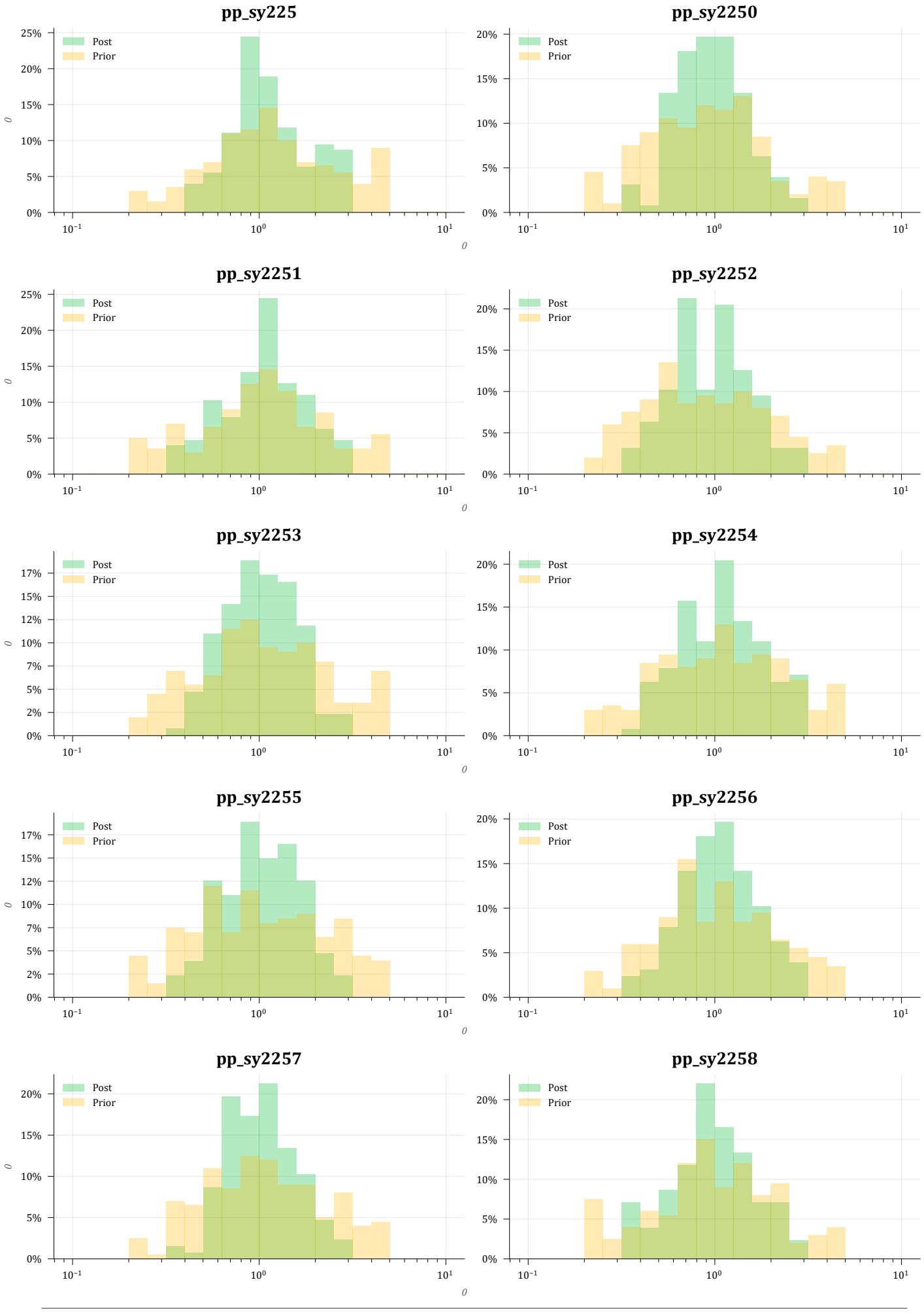

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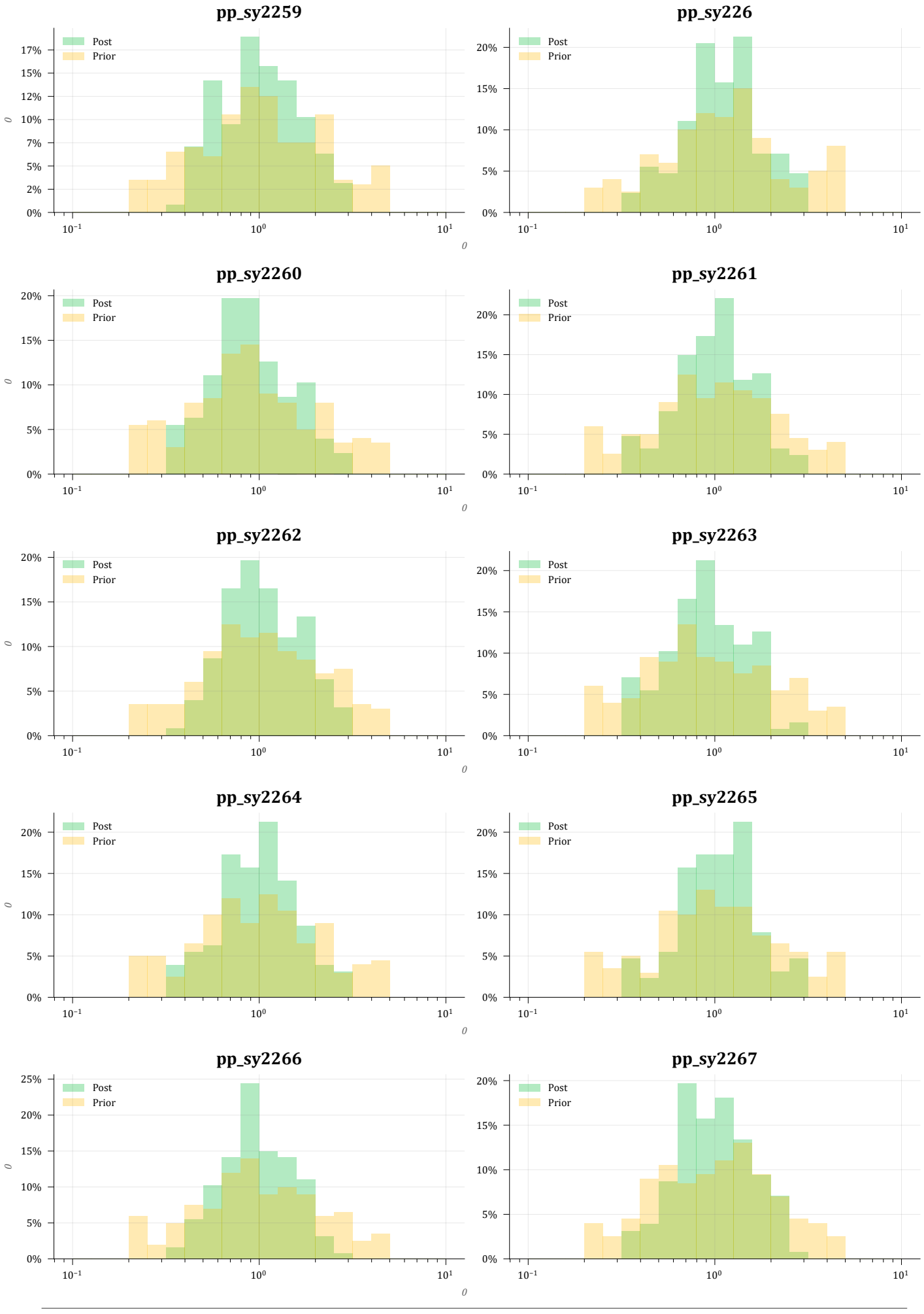

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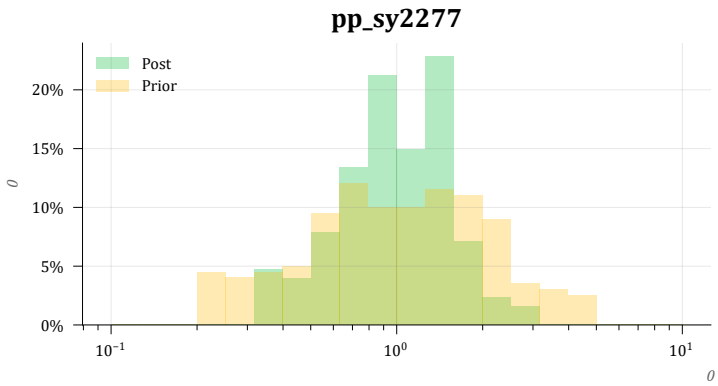

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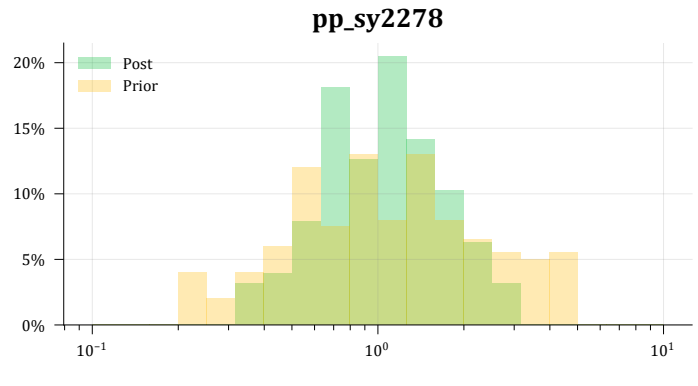

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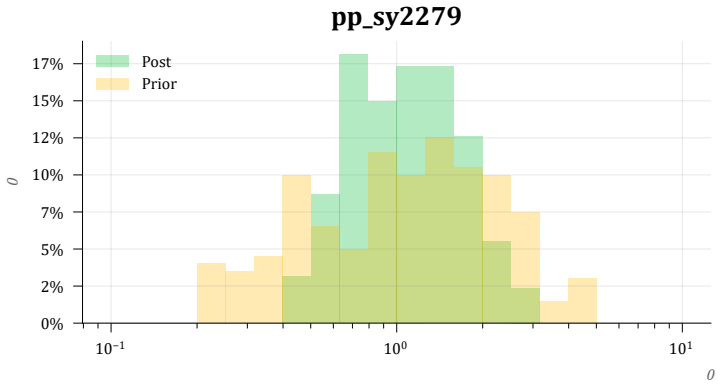

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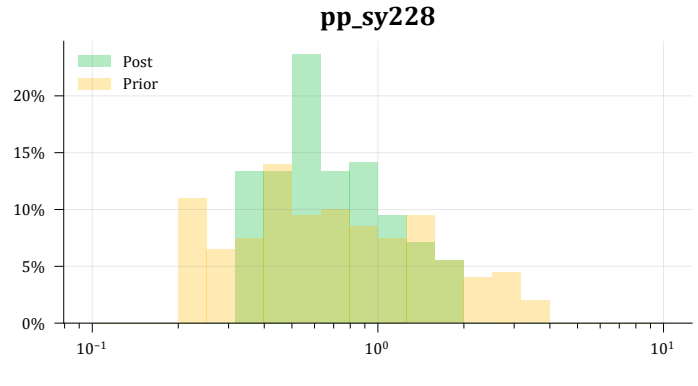

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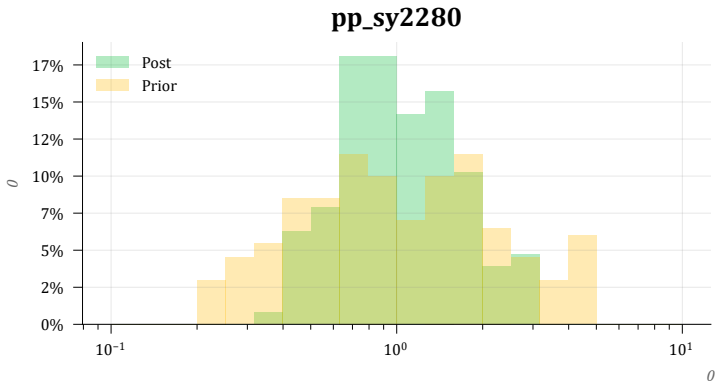

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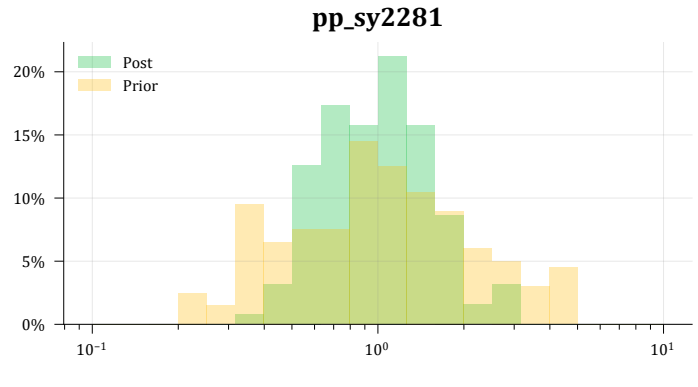

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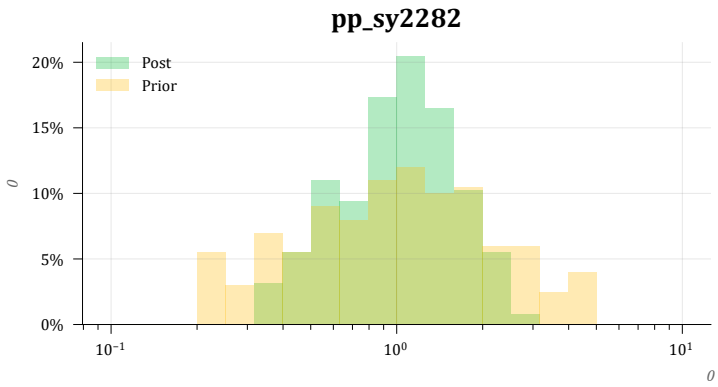

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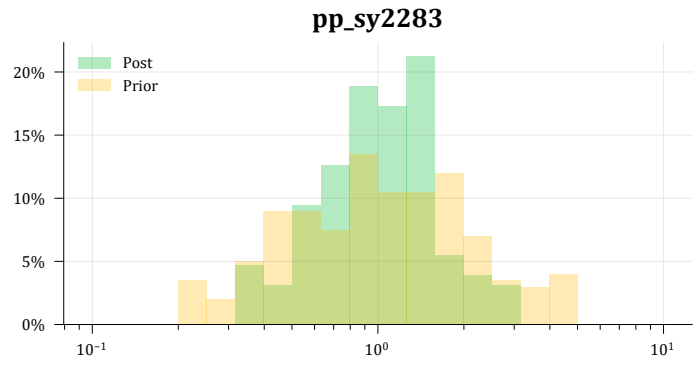

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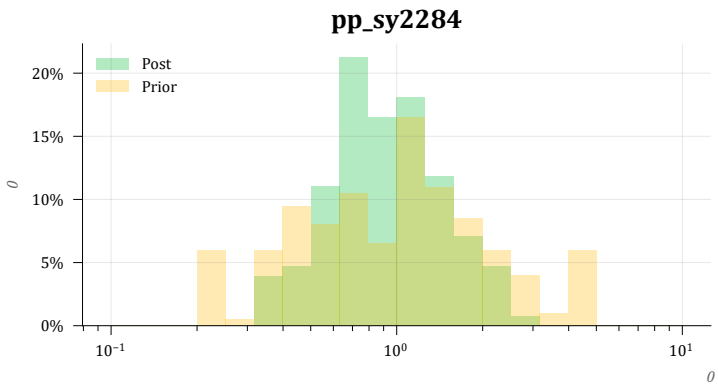

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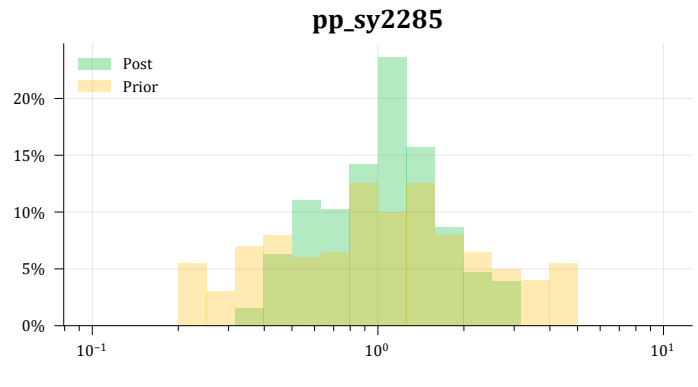

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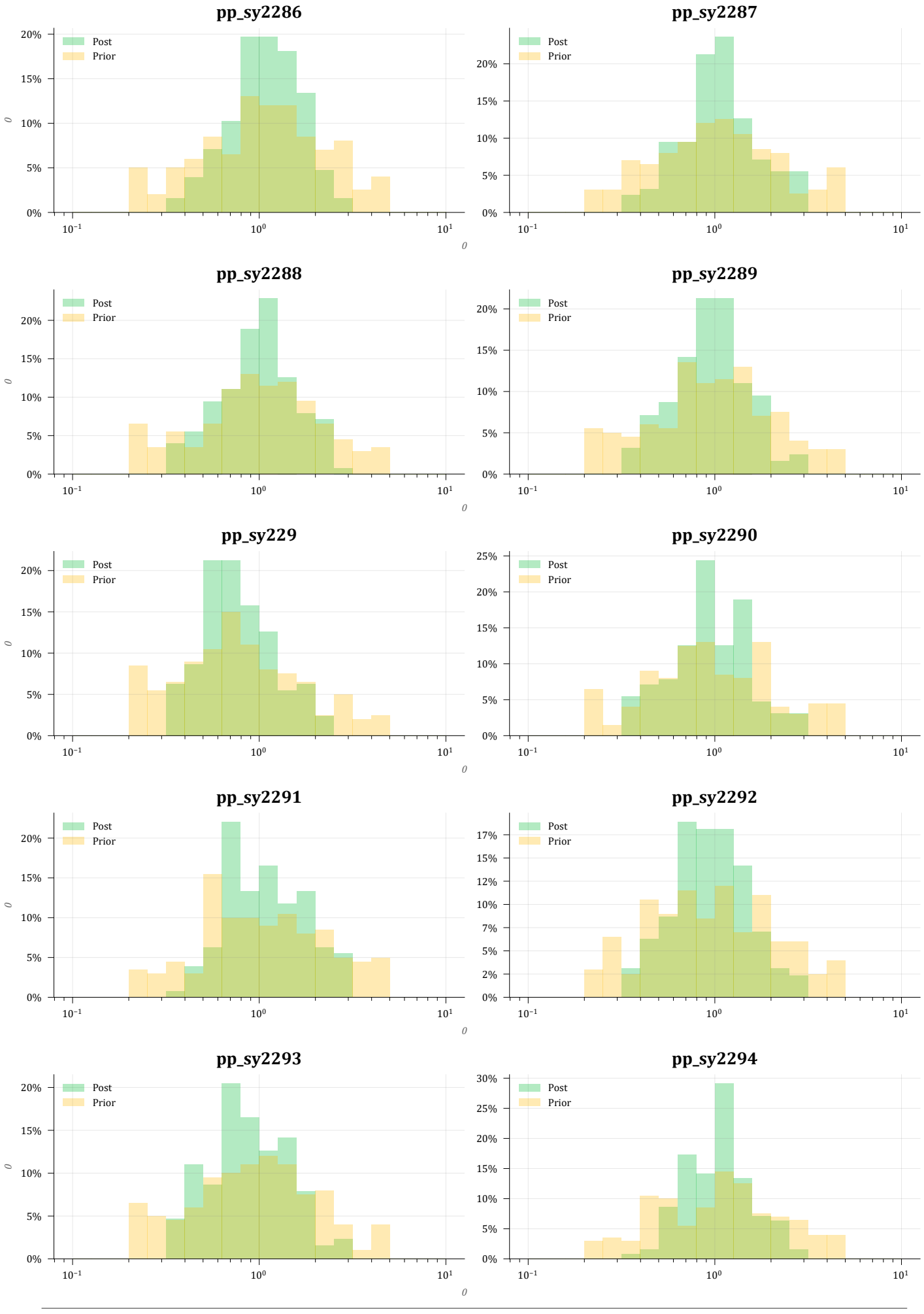

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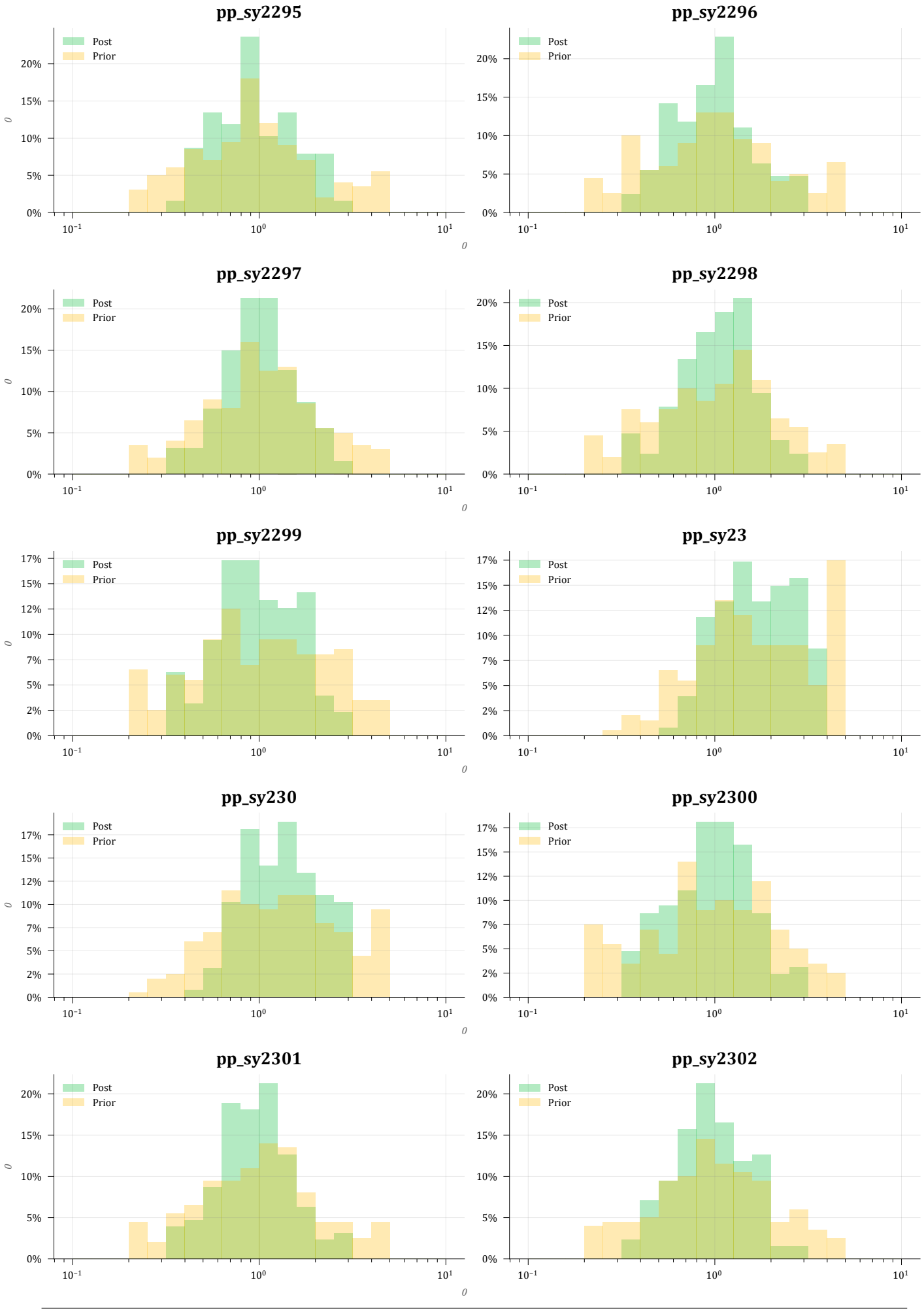

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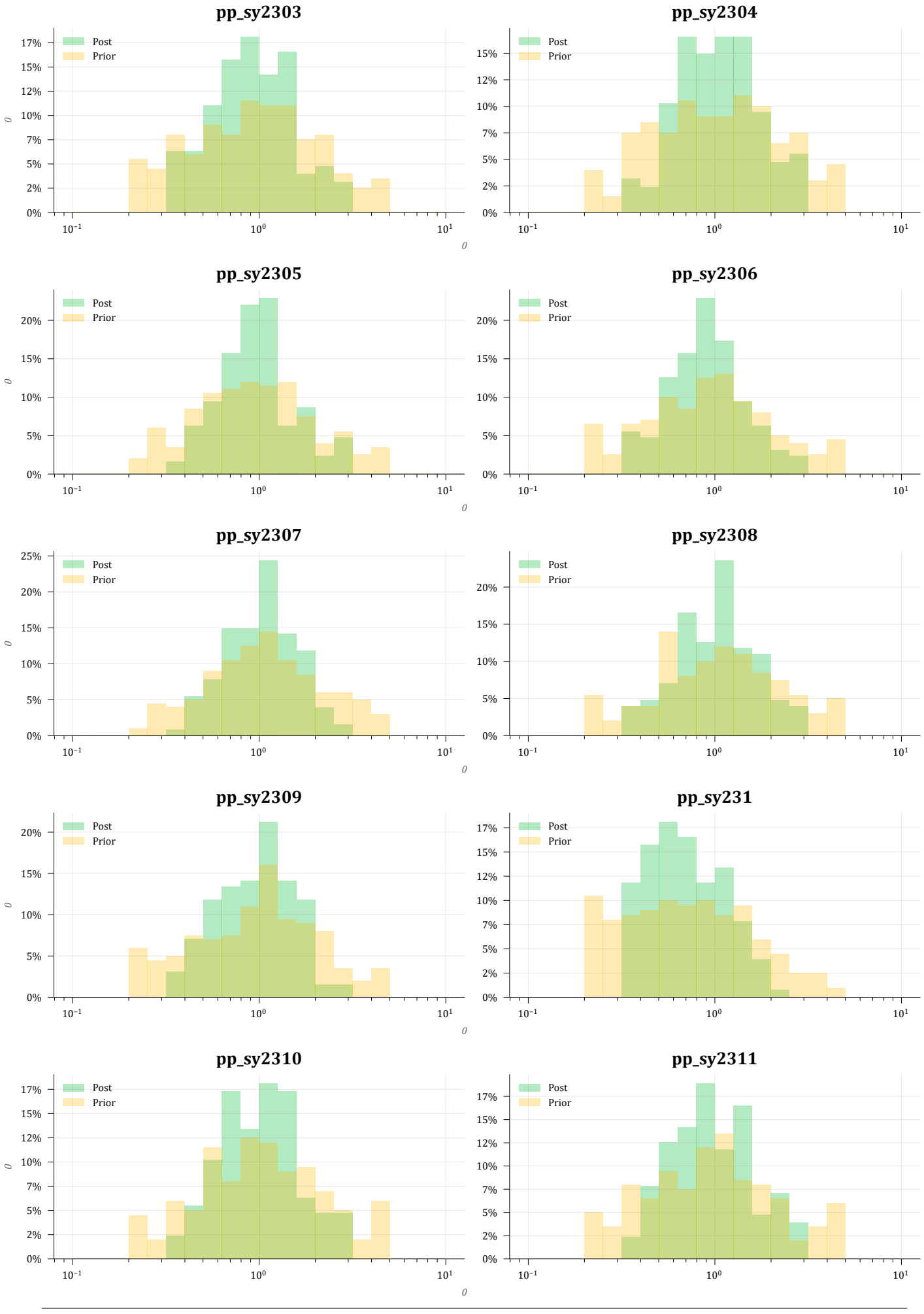

pp_sy2283
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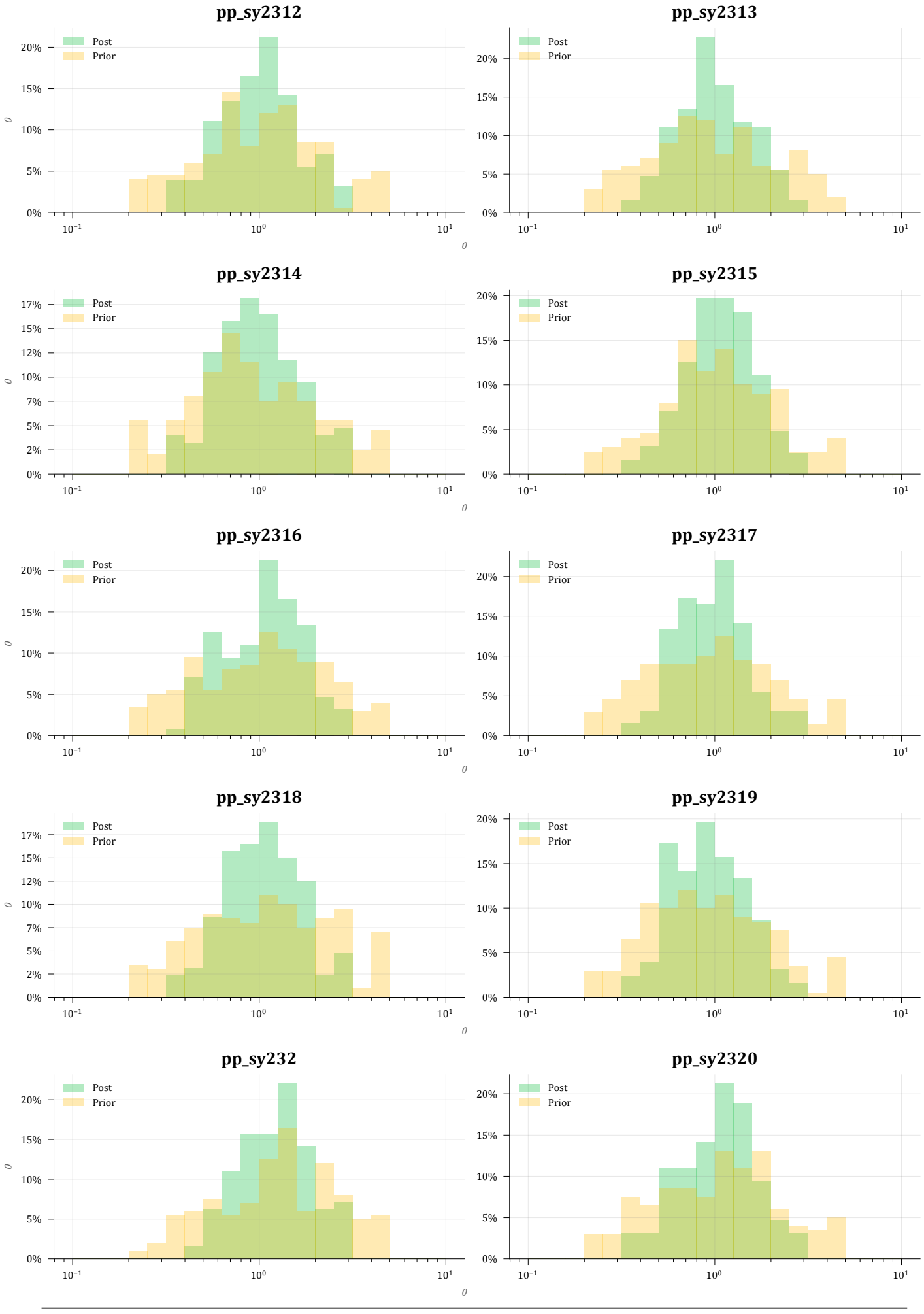

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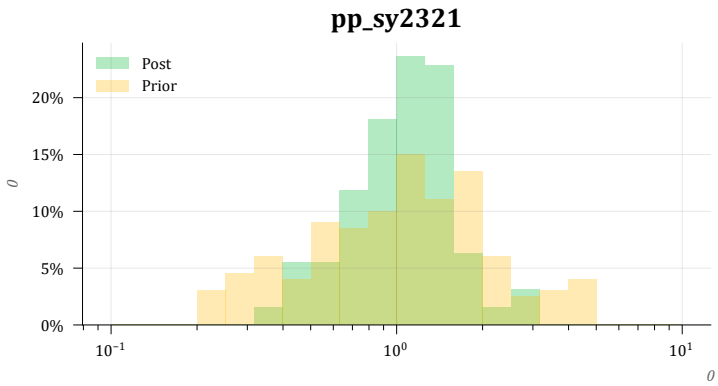

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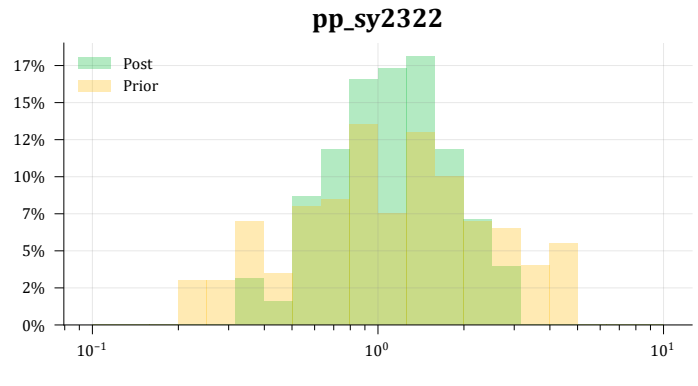

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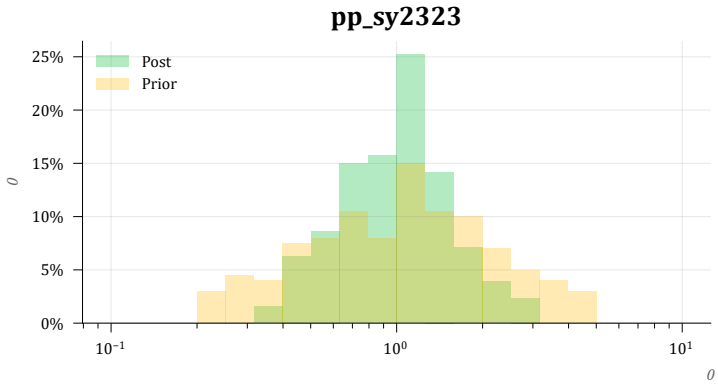

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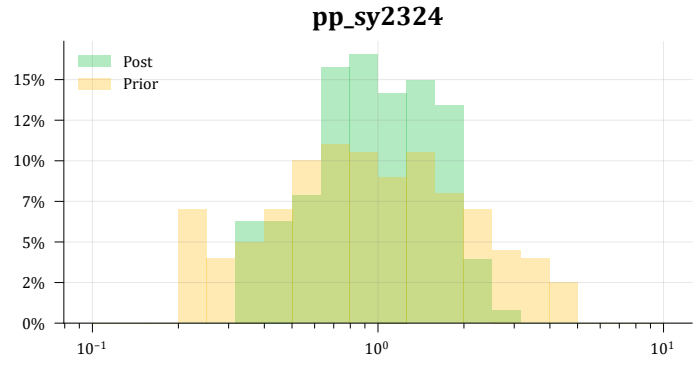

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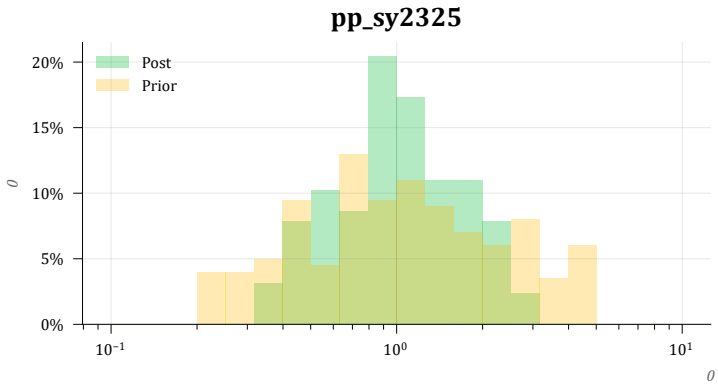

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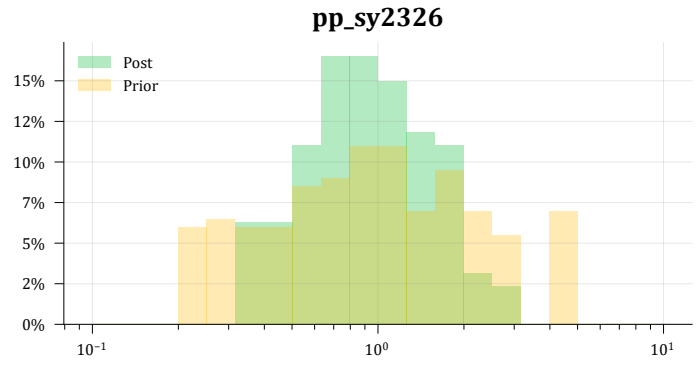

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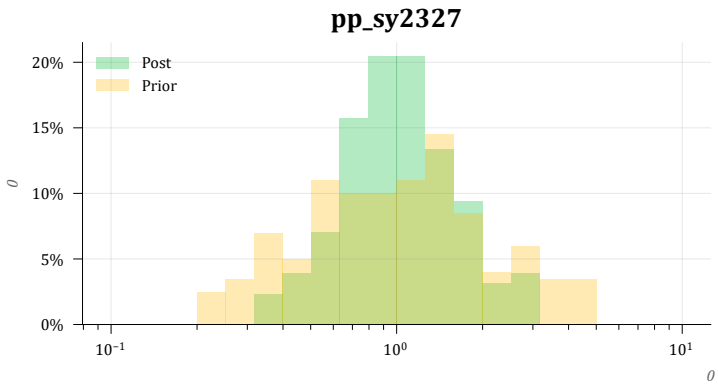

pp_sy2322
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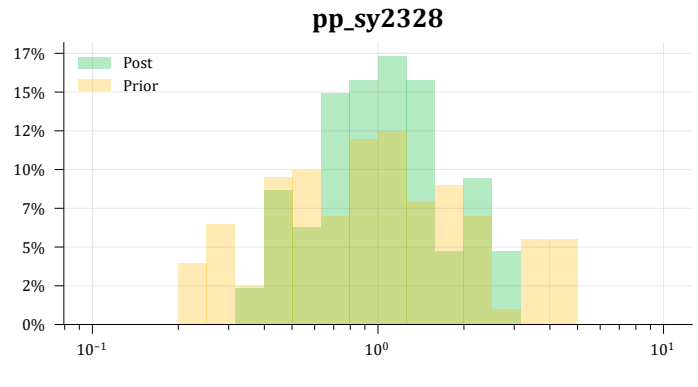

pp_sy2323
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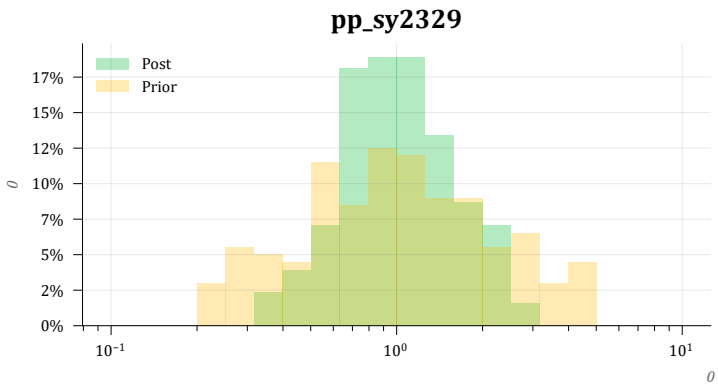

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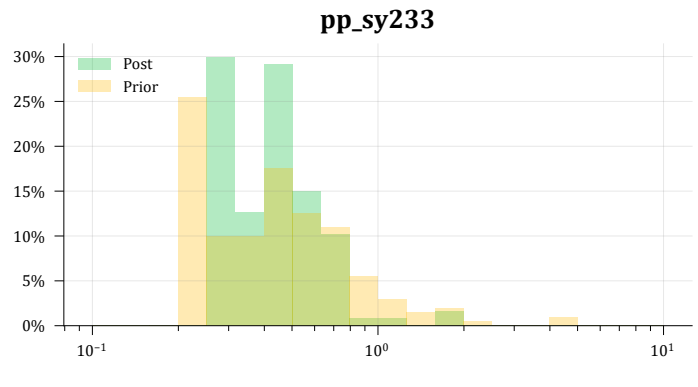

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pp_sy2326
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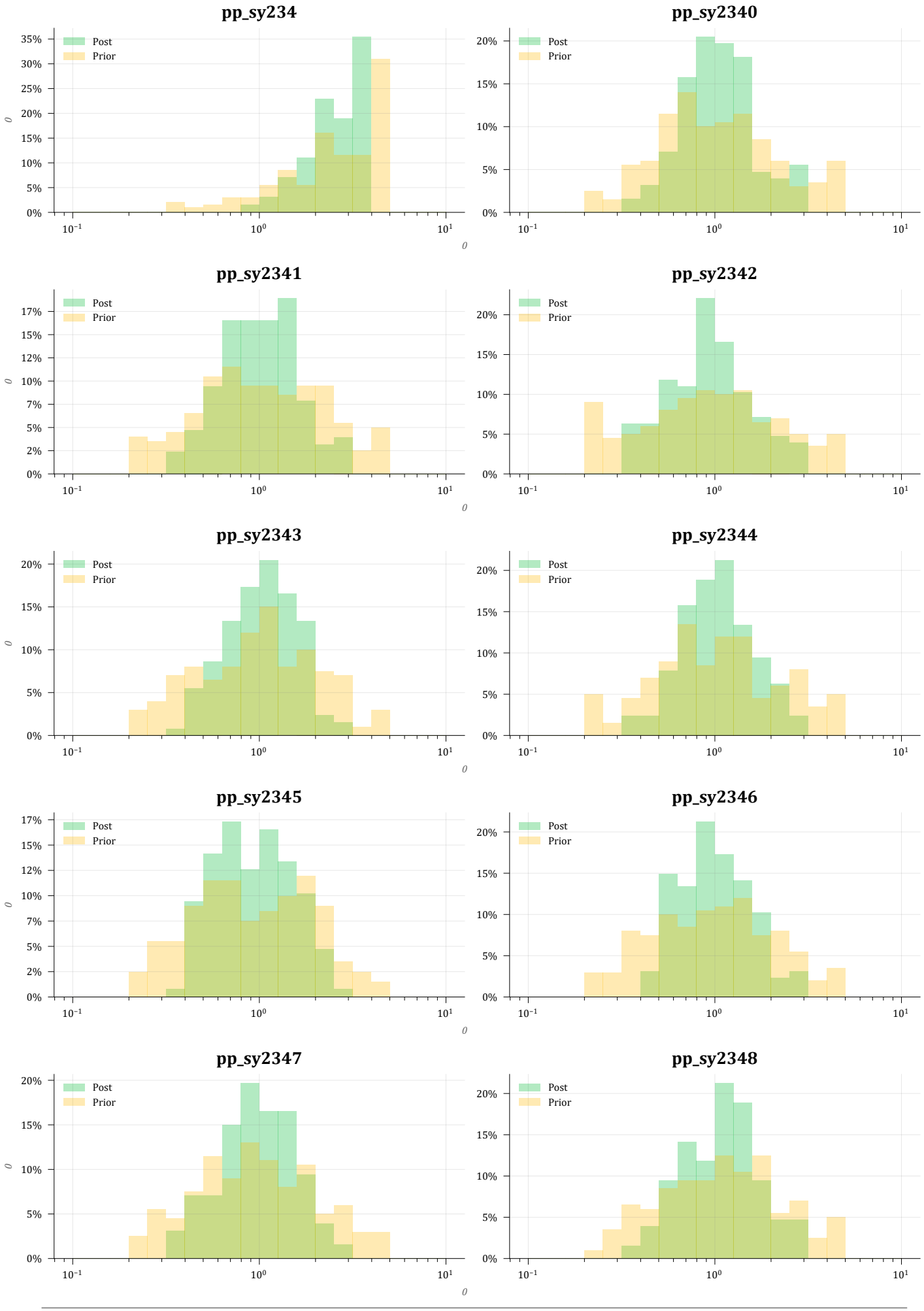

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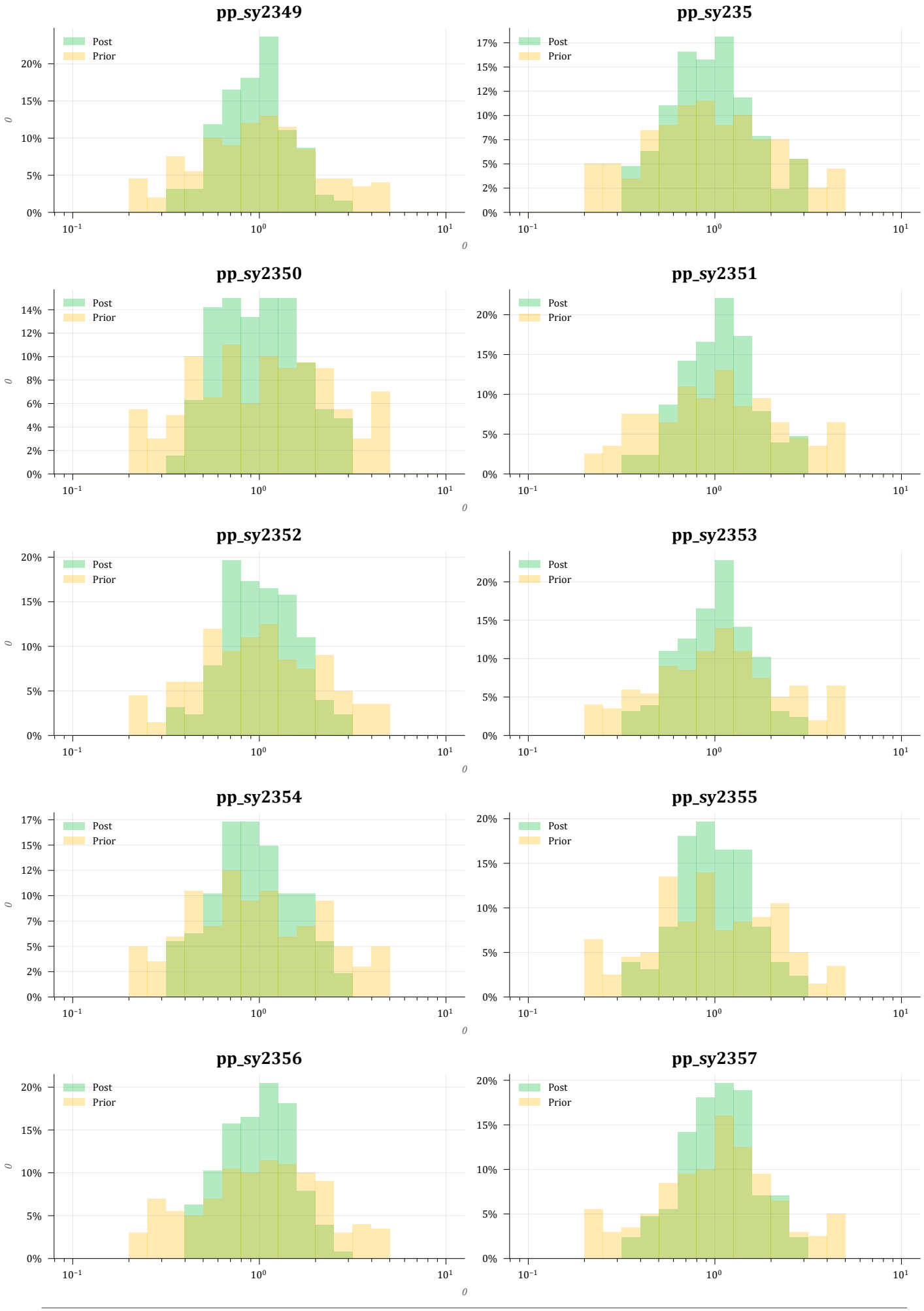

pp_sy2328
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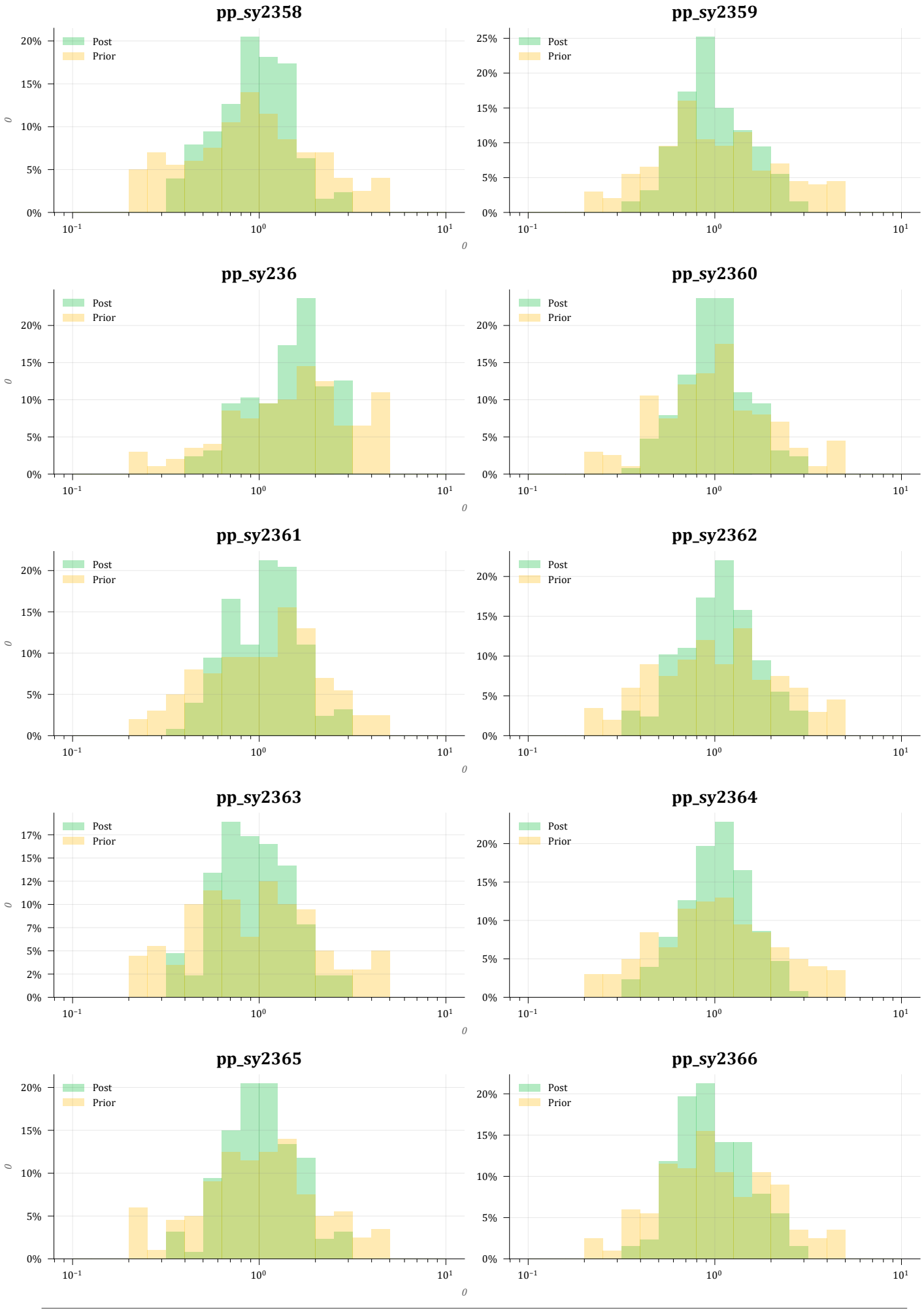

pp_sy2329
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pp_sy233
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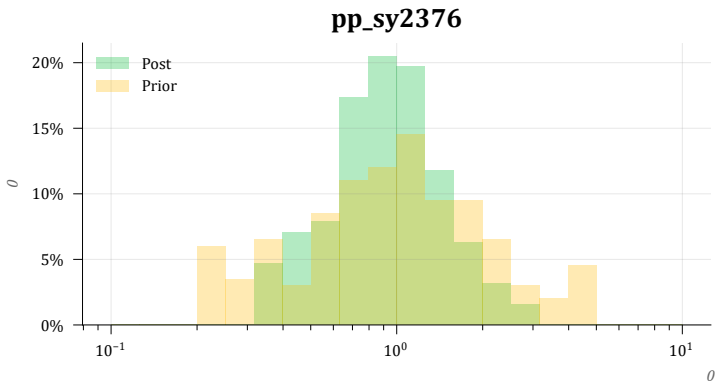

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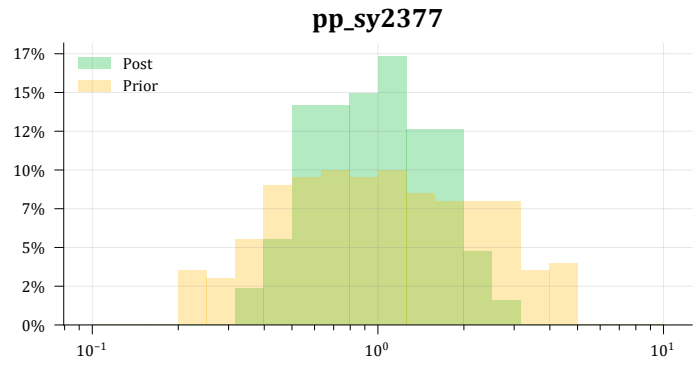

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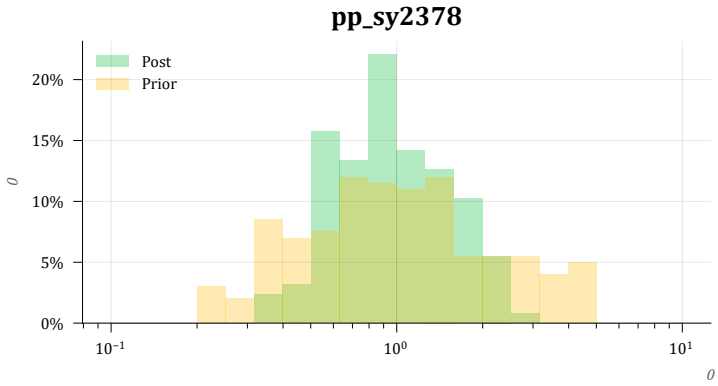

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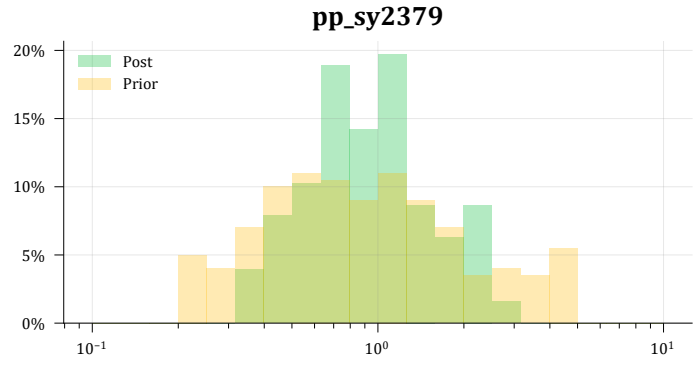

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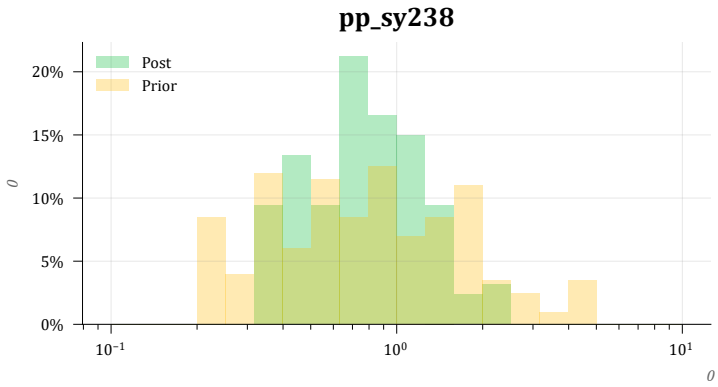

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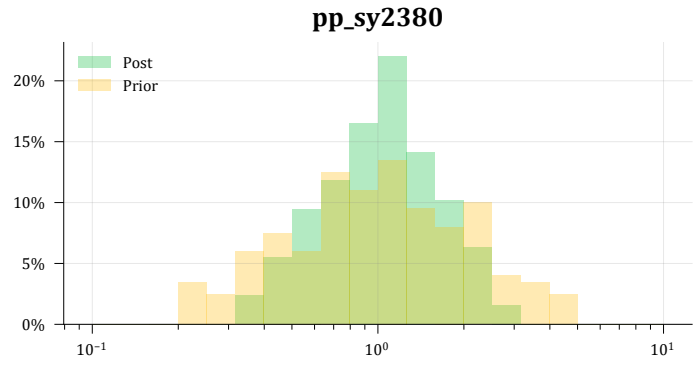

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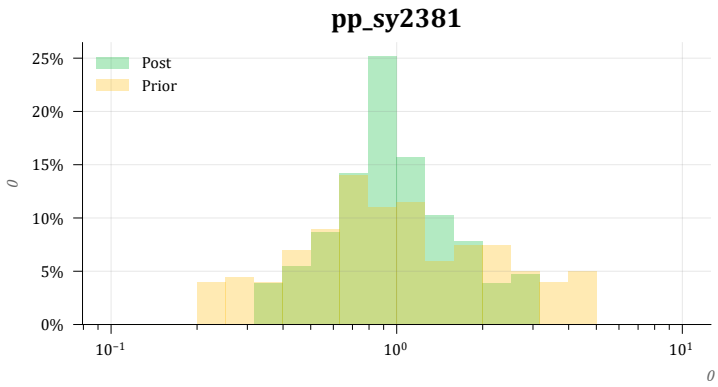

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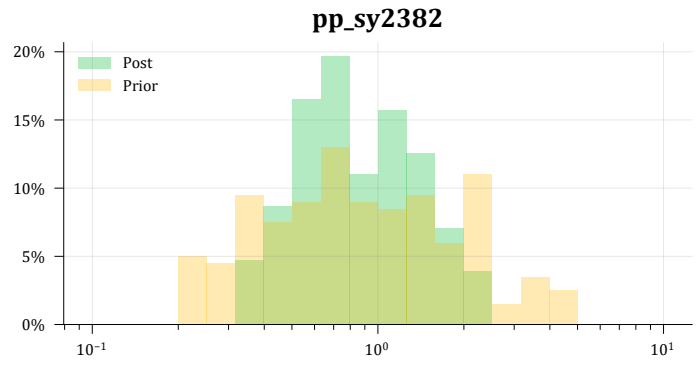

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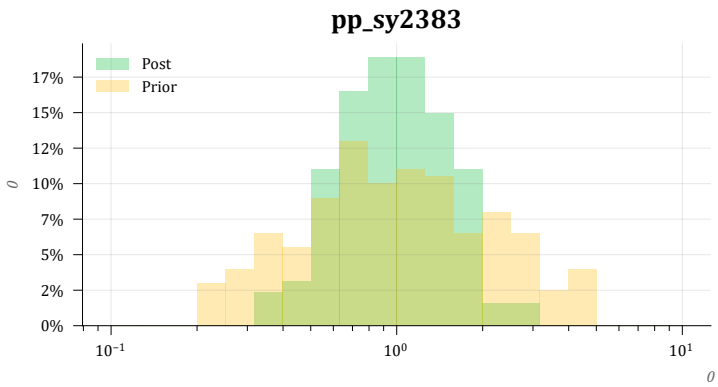

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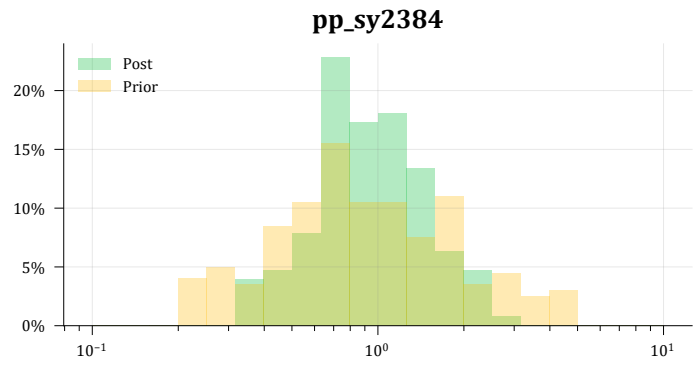

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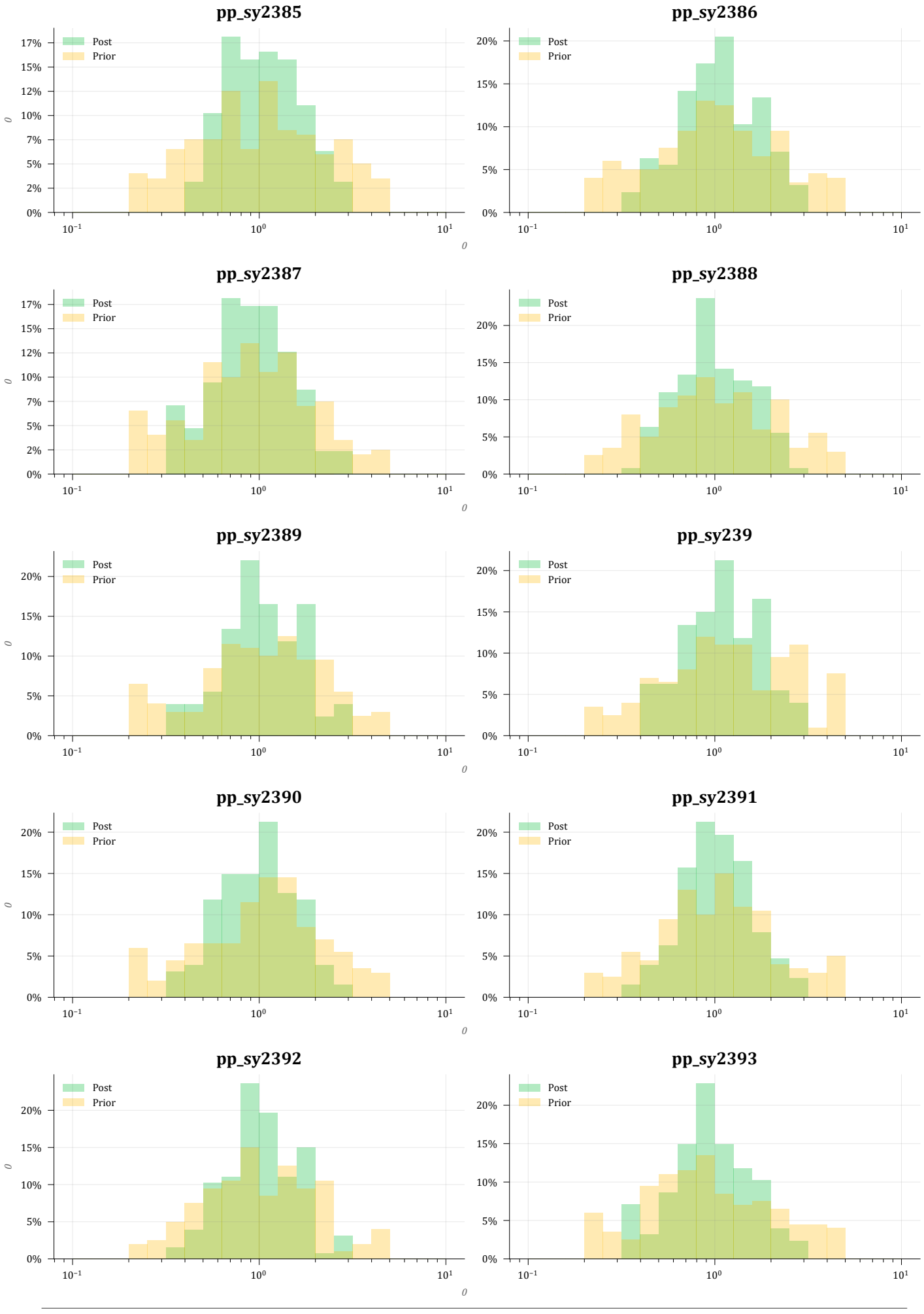

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pp_sy2381
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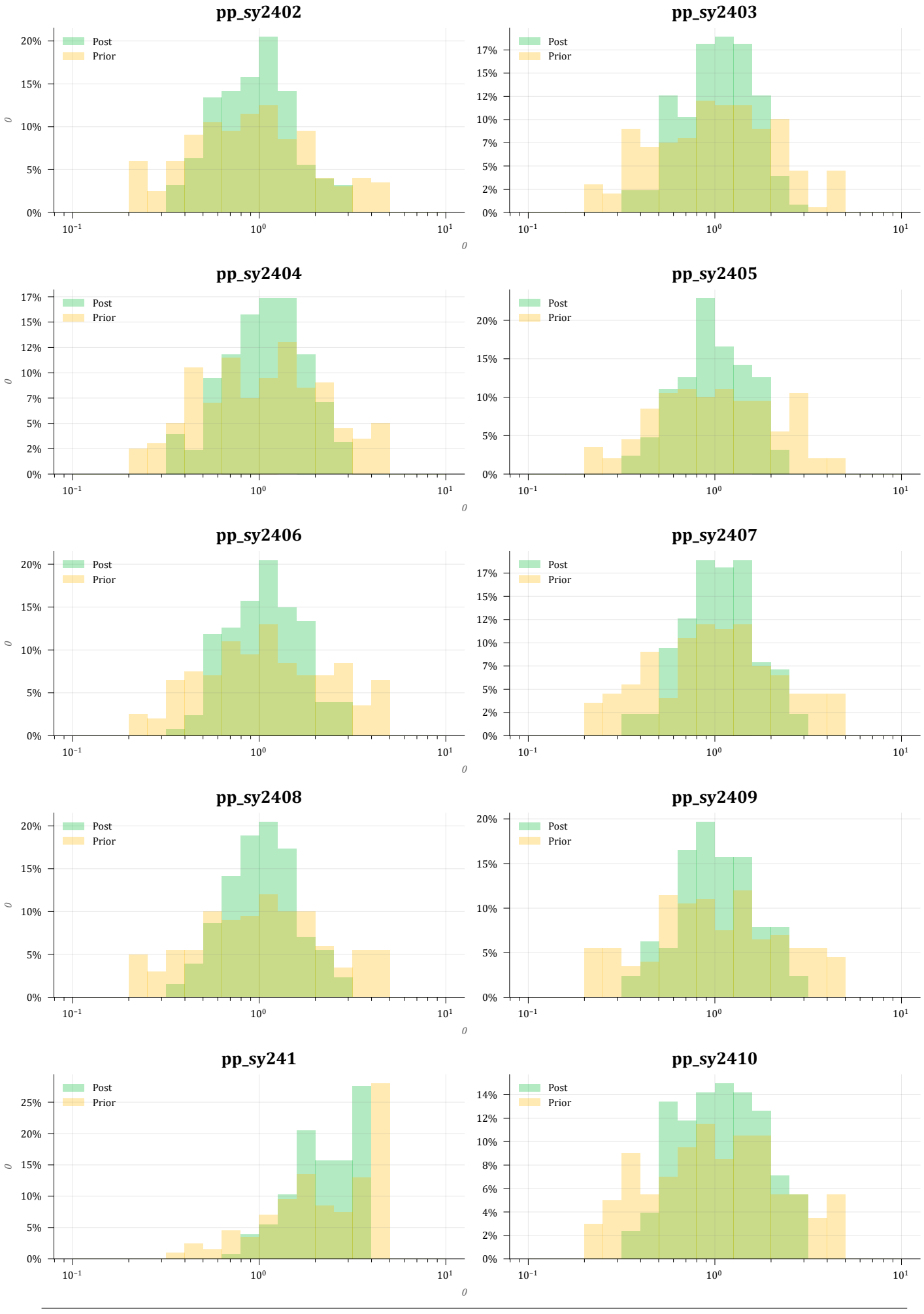

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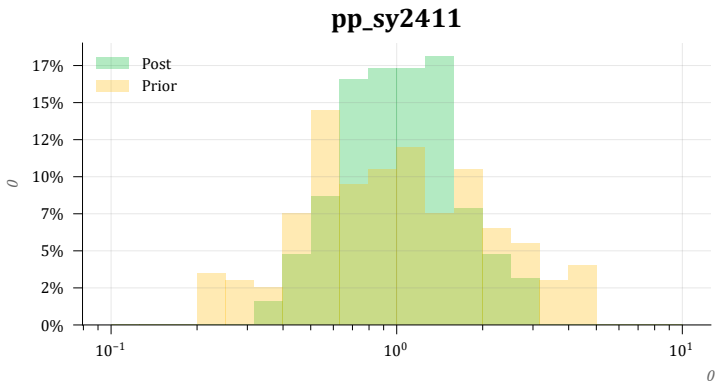

pp_sy2383
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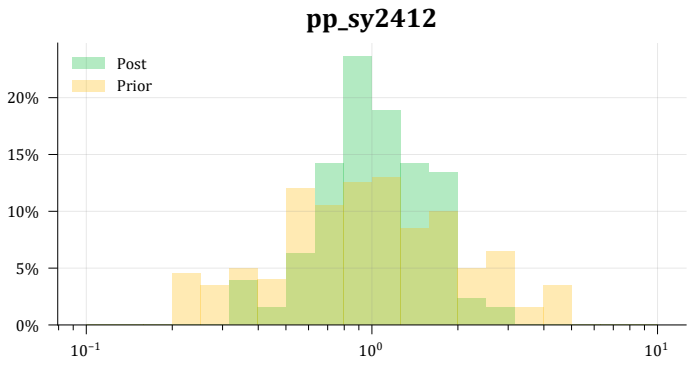

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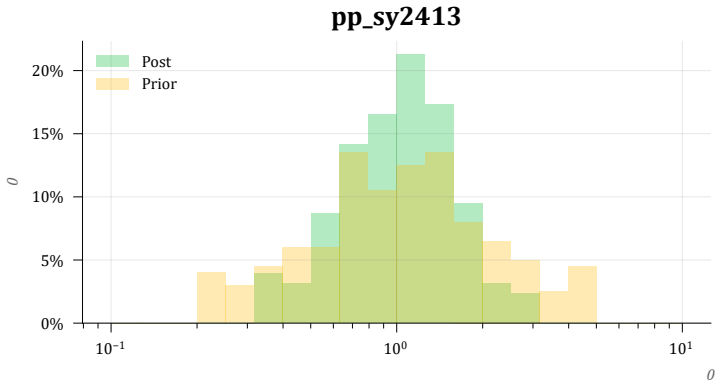

pp_sy2385
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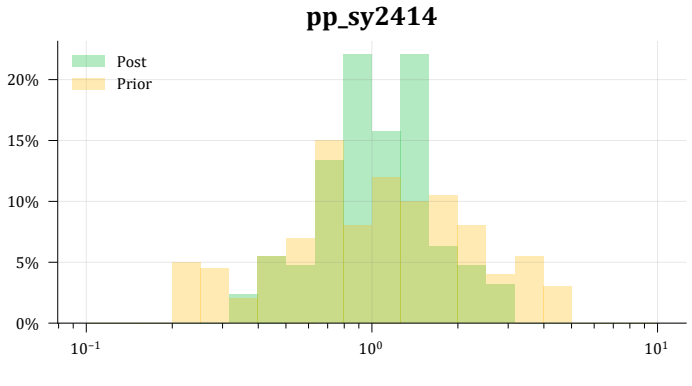

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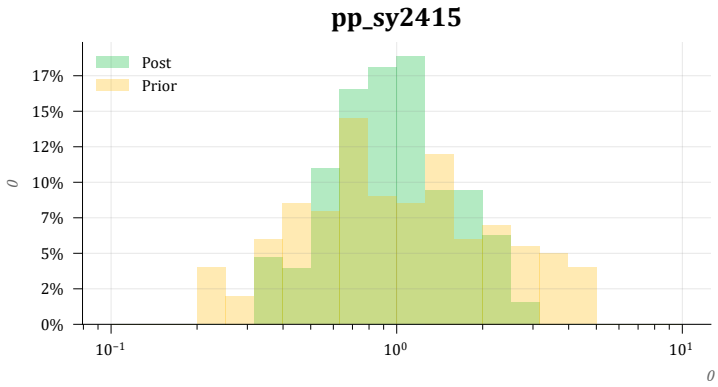

pp_sy2402
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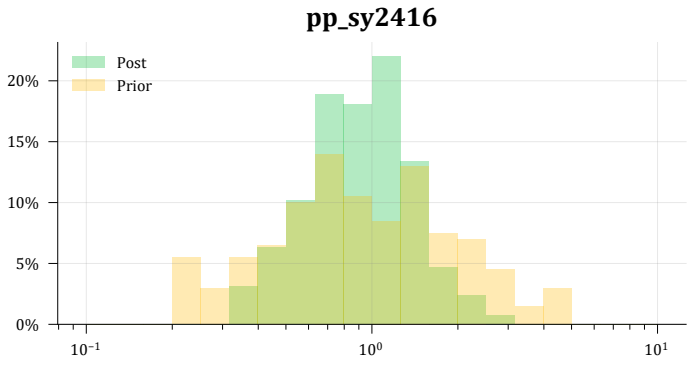

pp_sy2411
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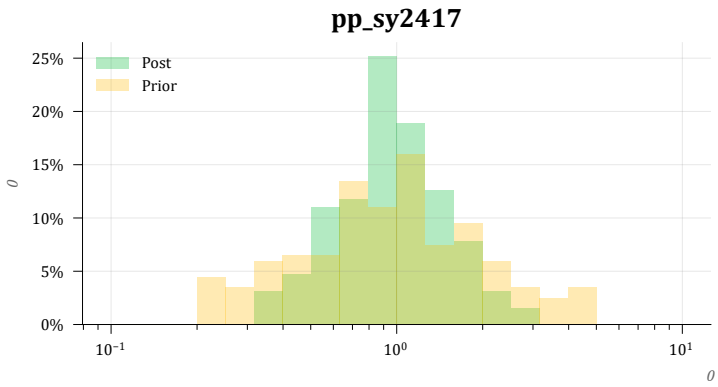

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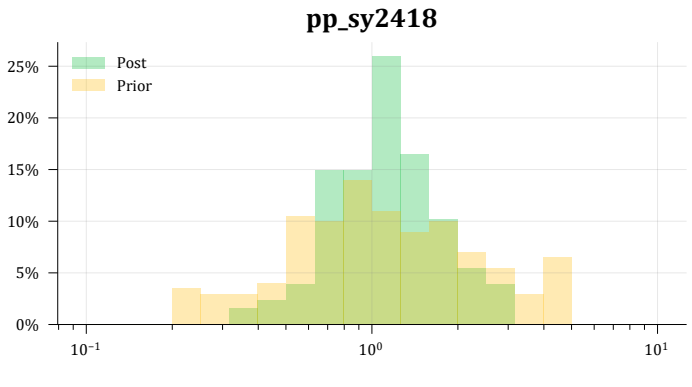

pp_sy2413
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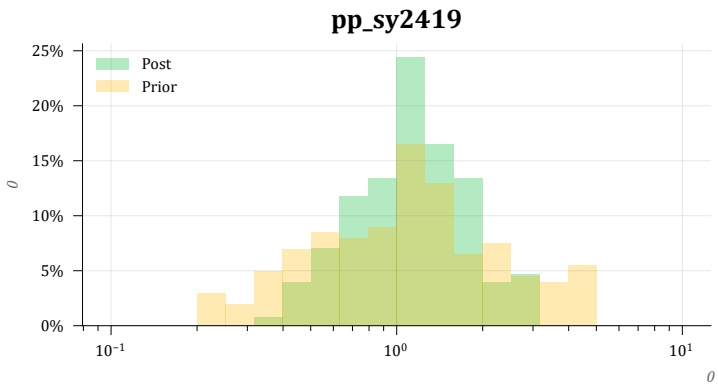

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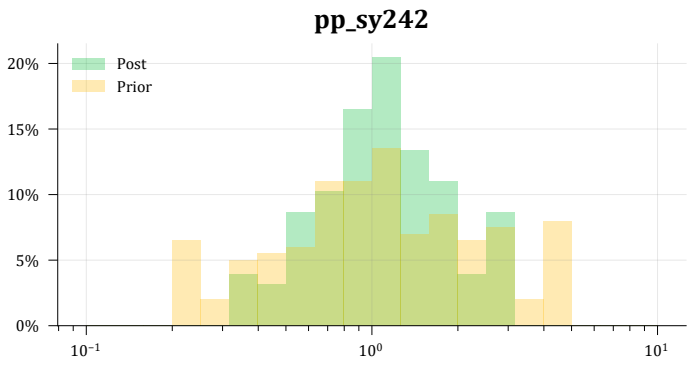

pp_sy2415
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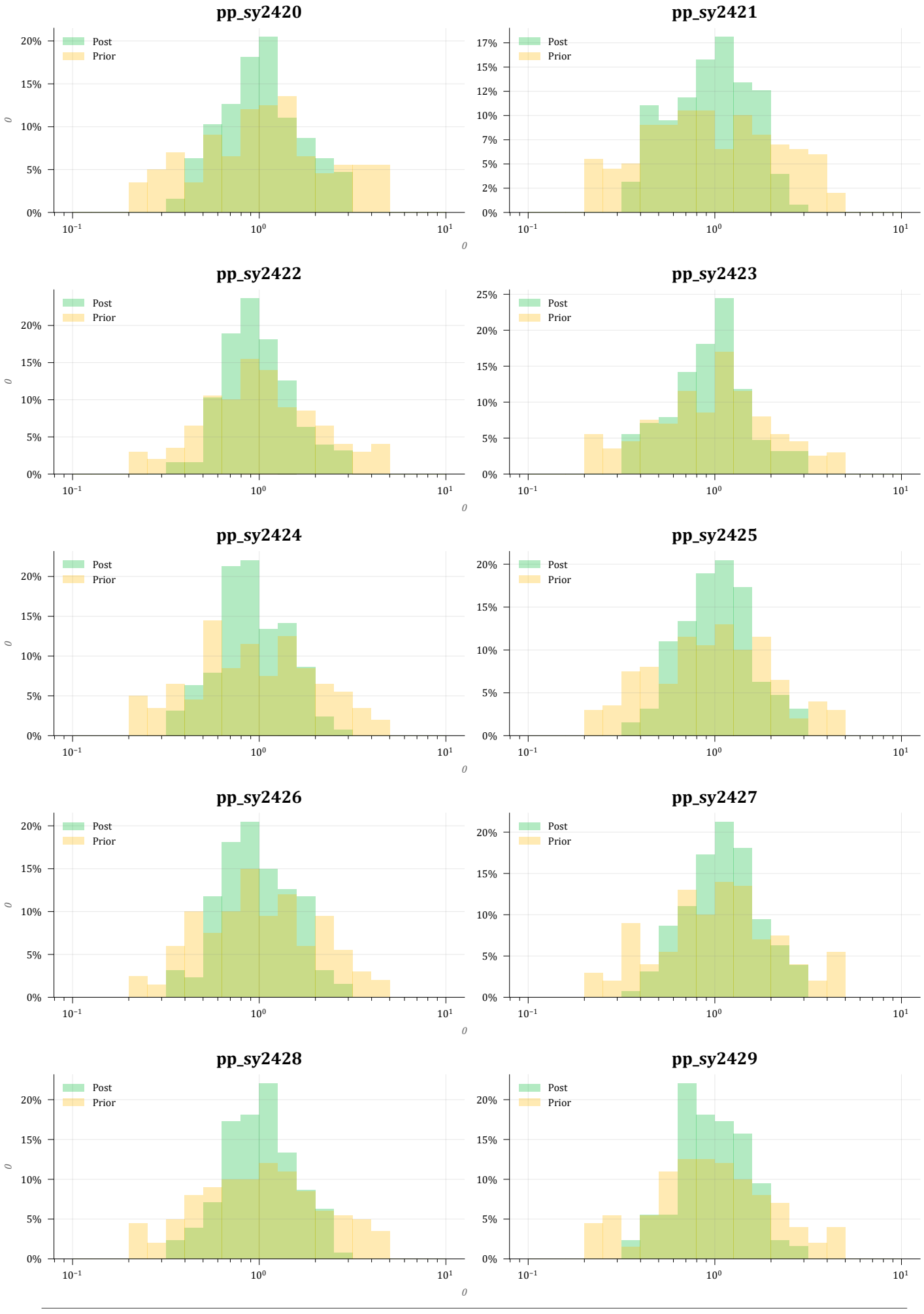

pp_sy2416
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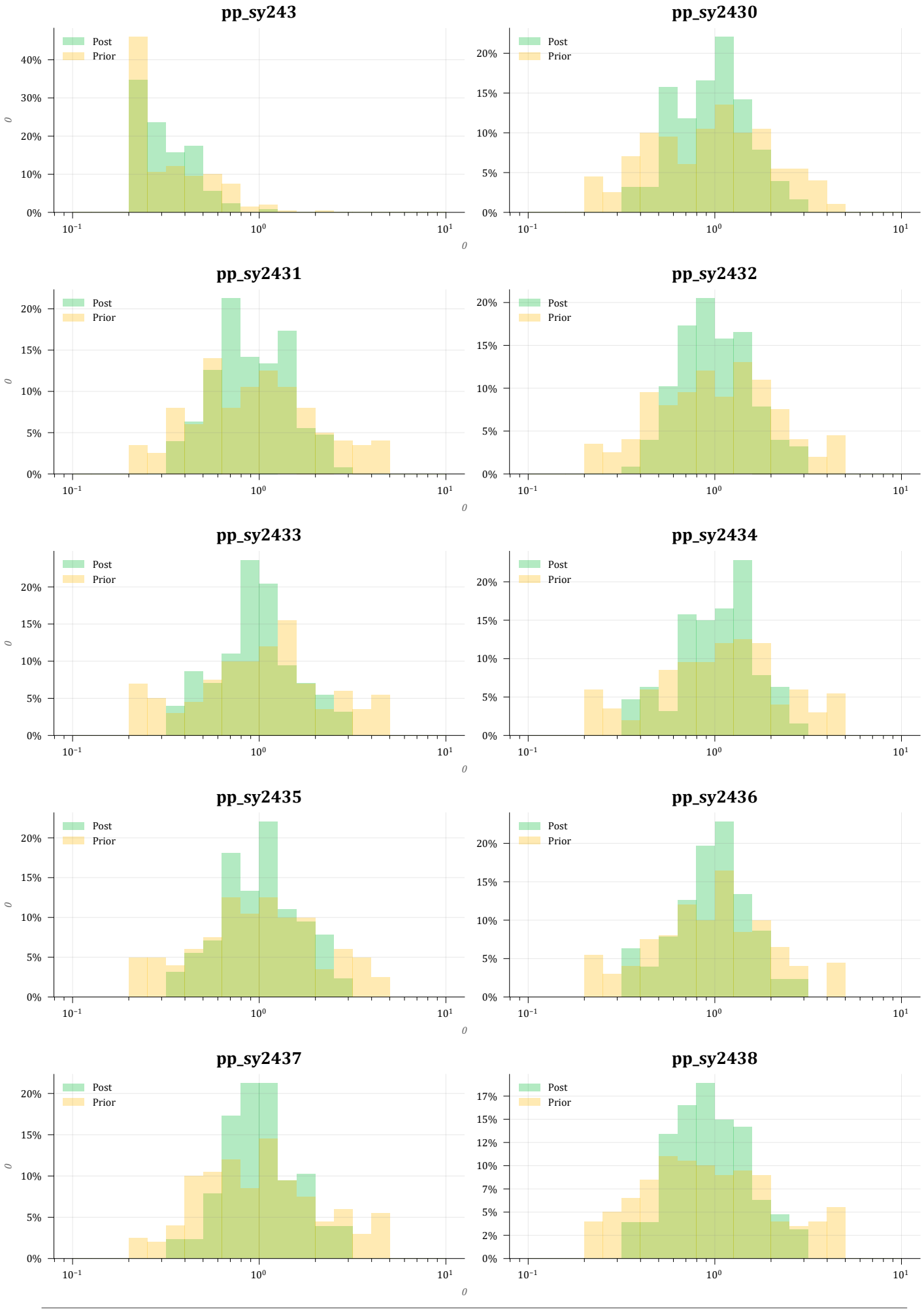

pp_sy2417
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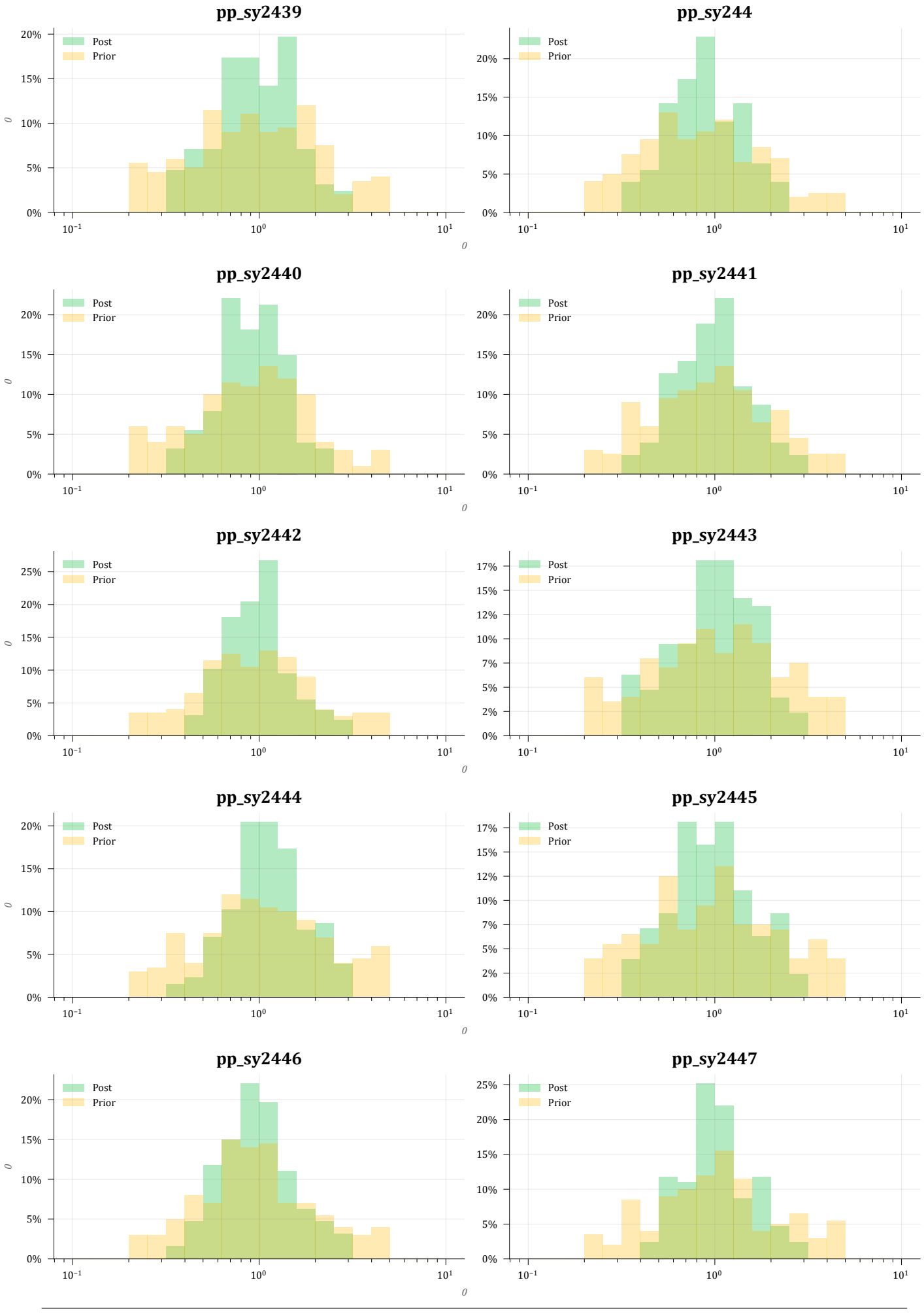

pp_sy2418
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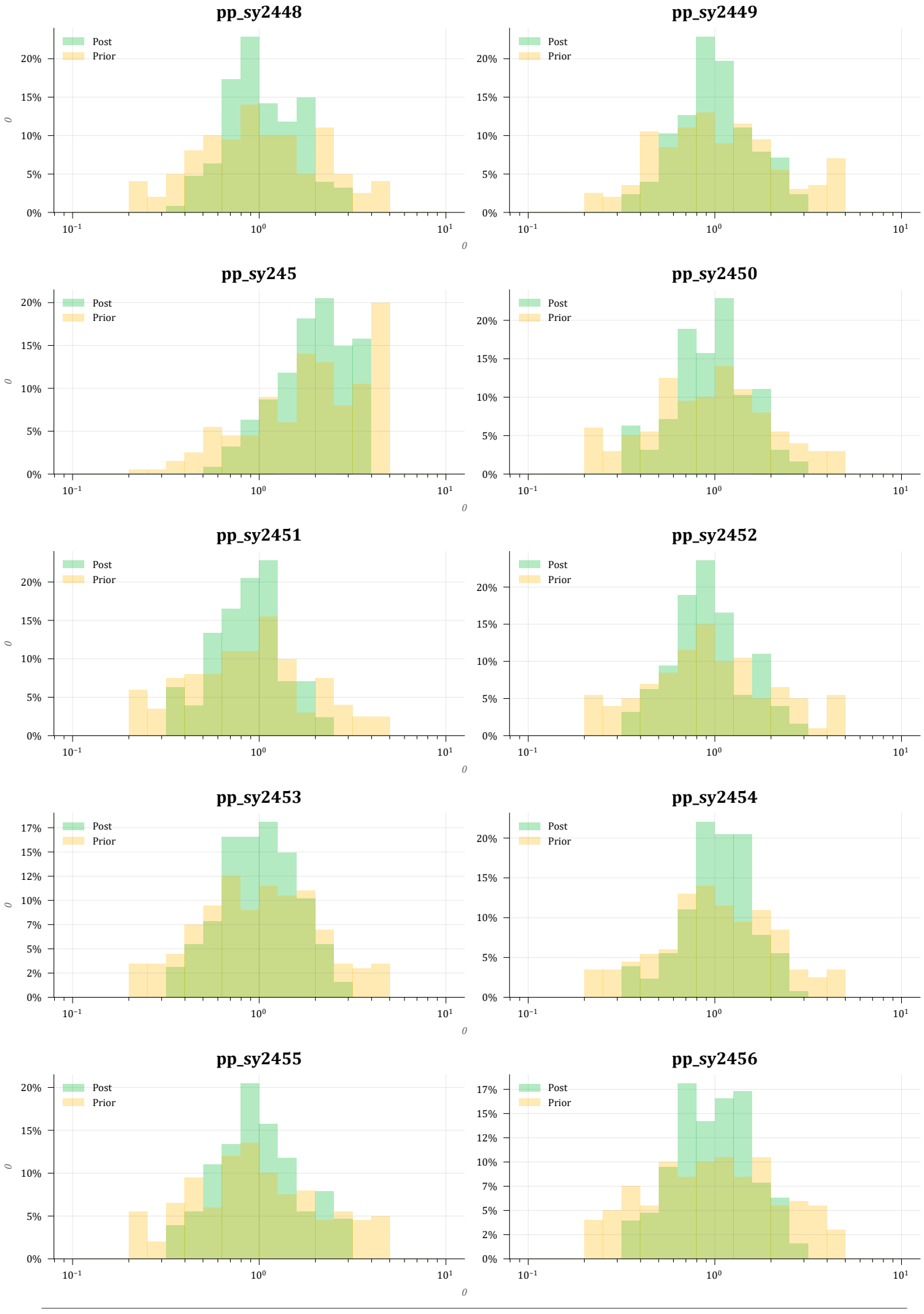

pp_sy2419
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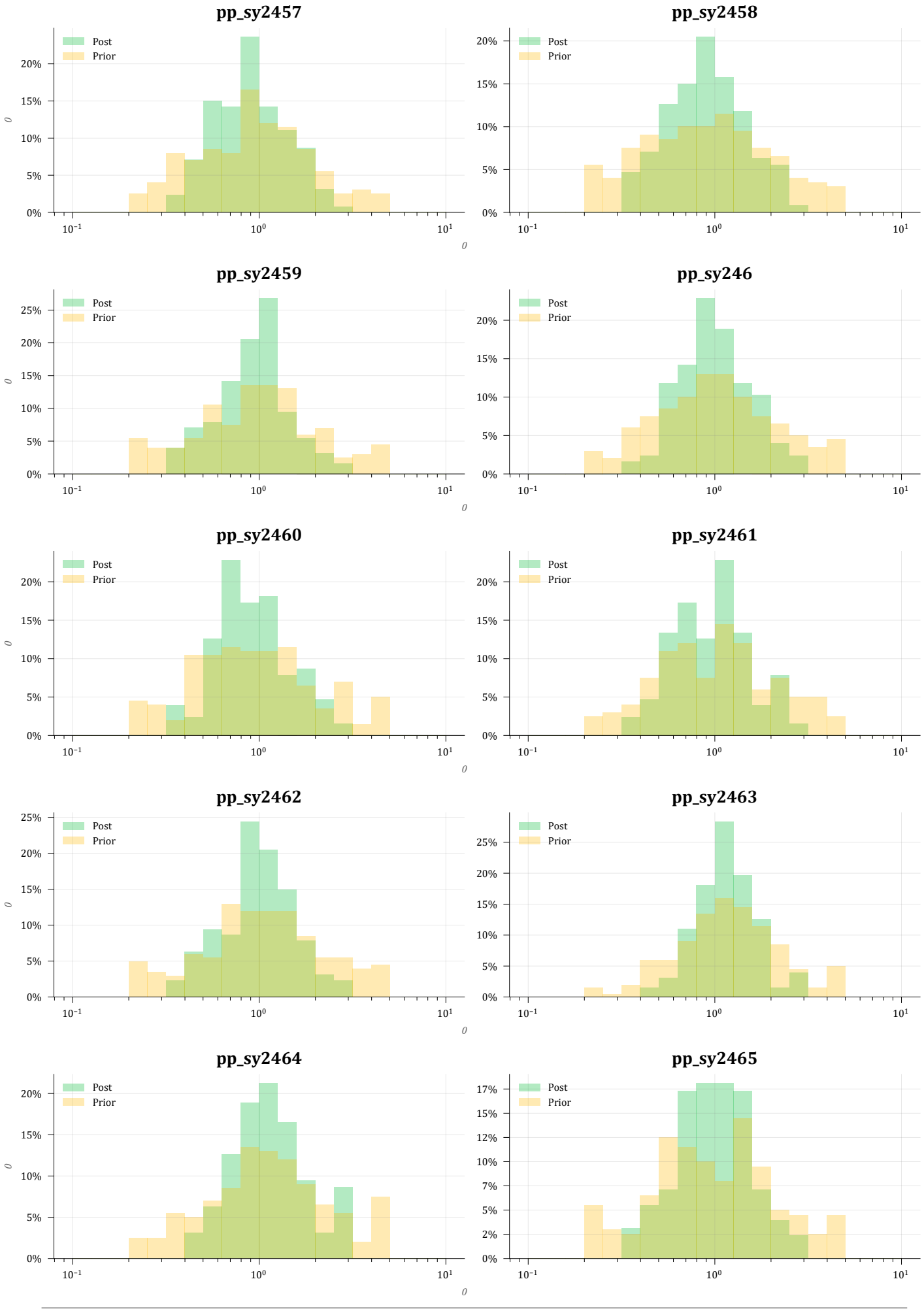

pp_sy242
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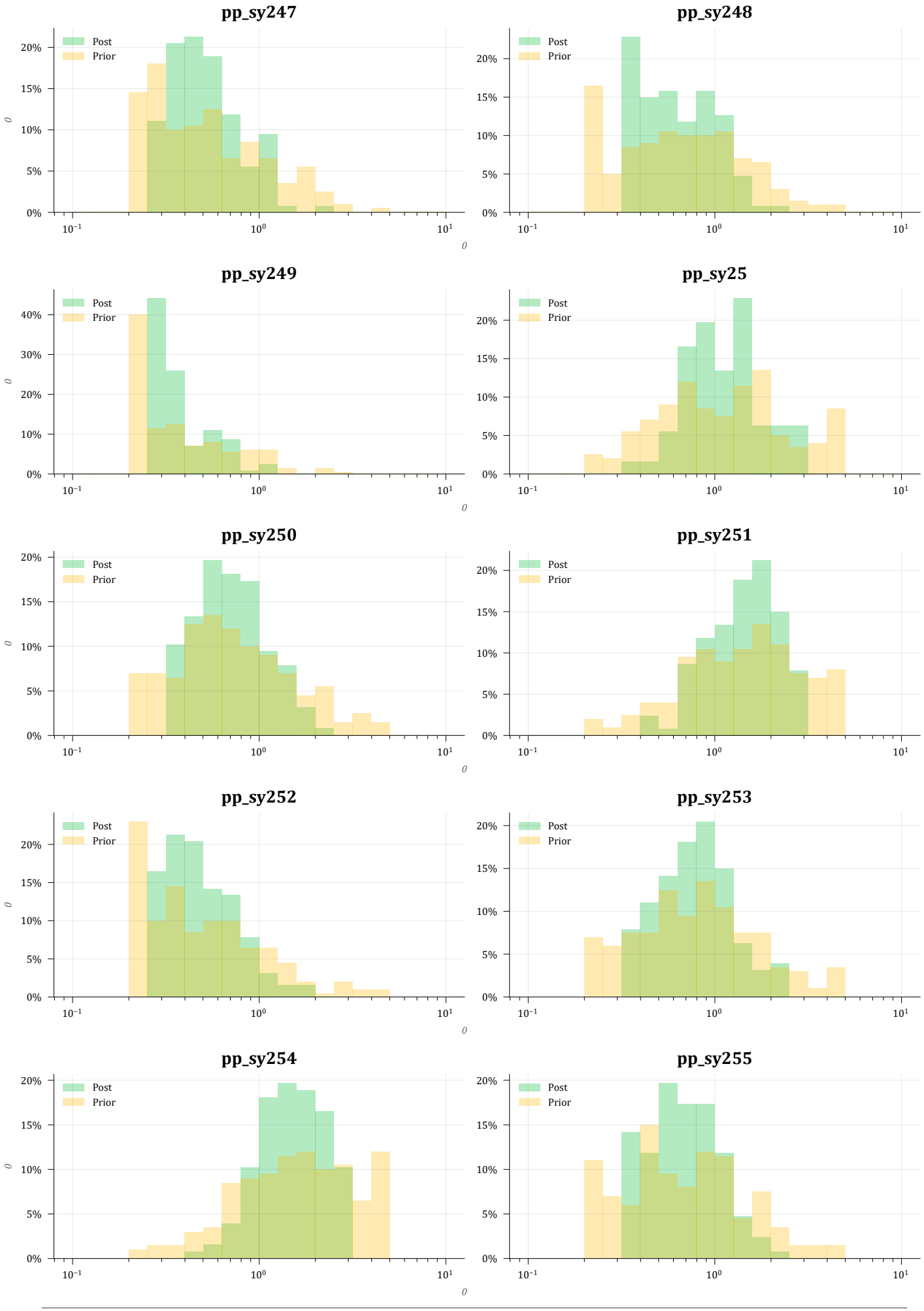

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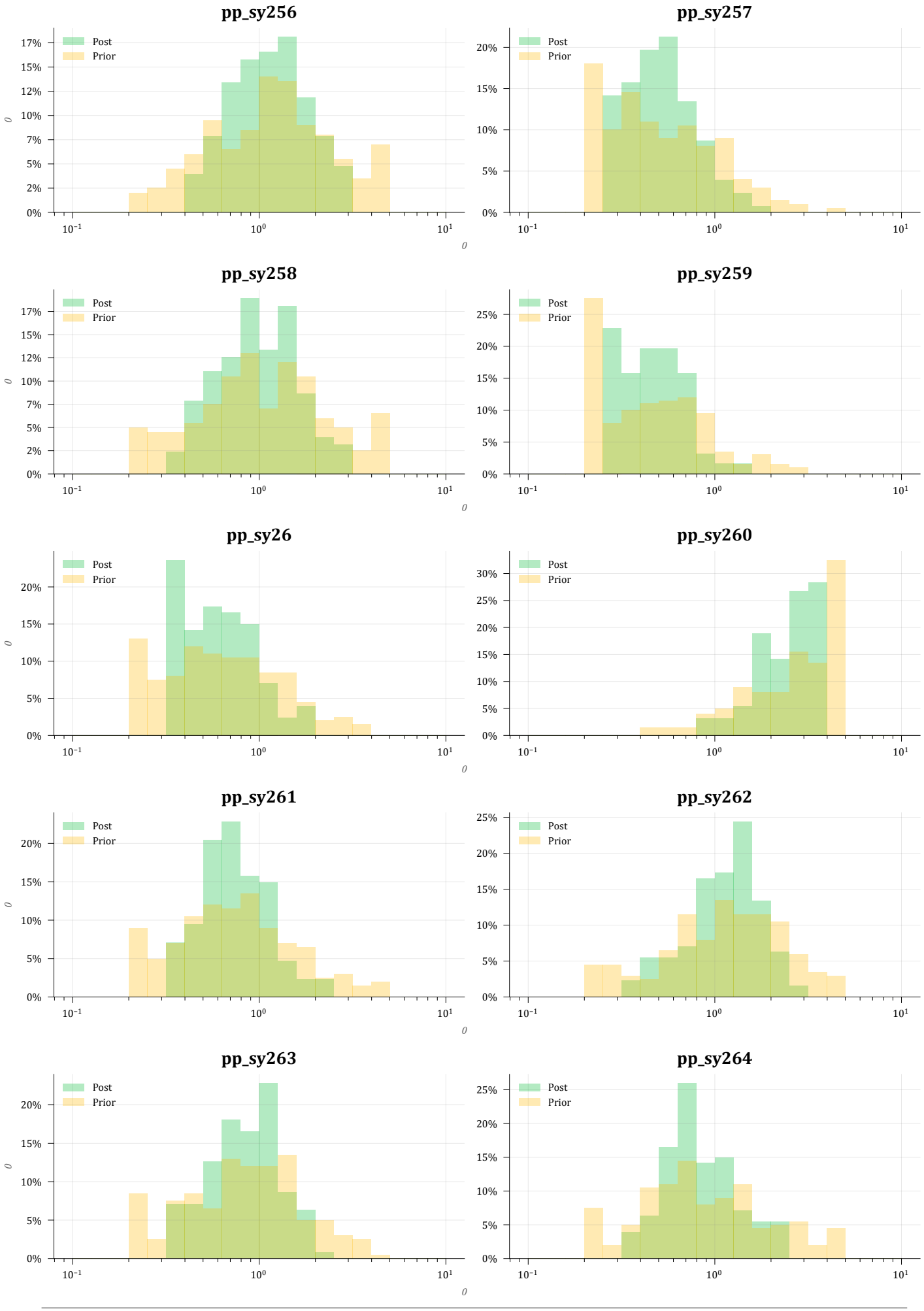

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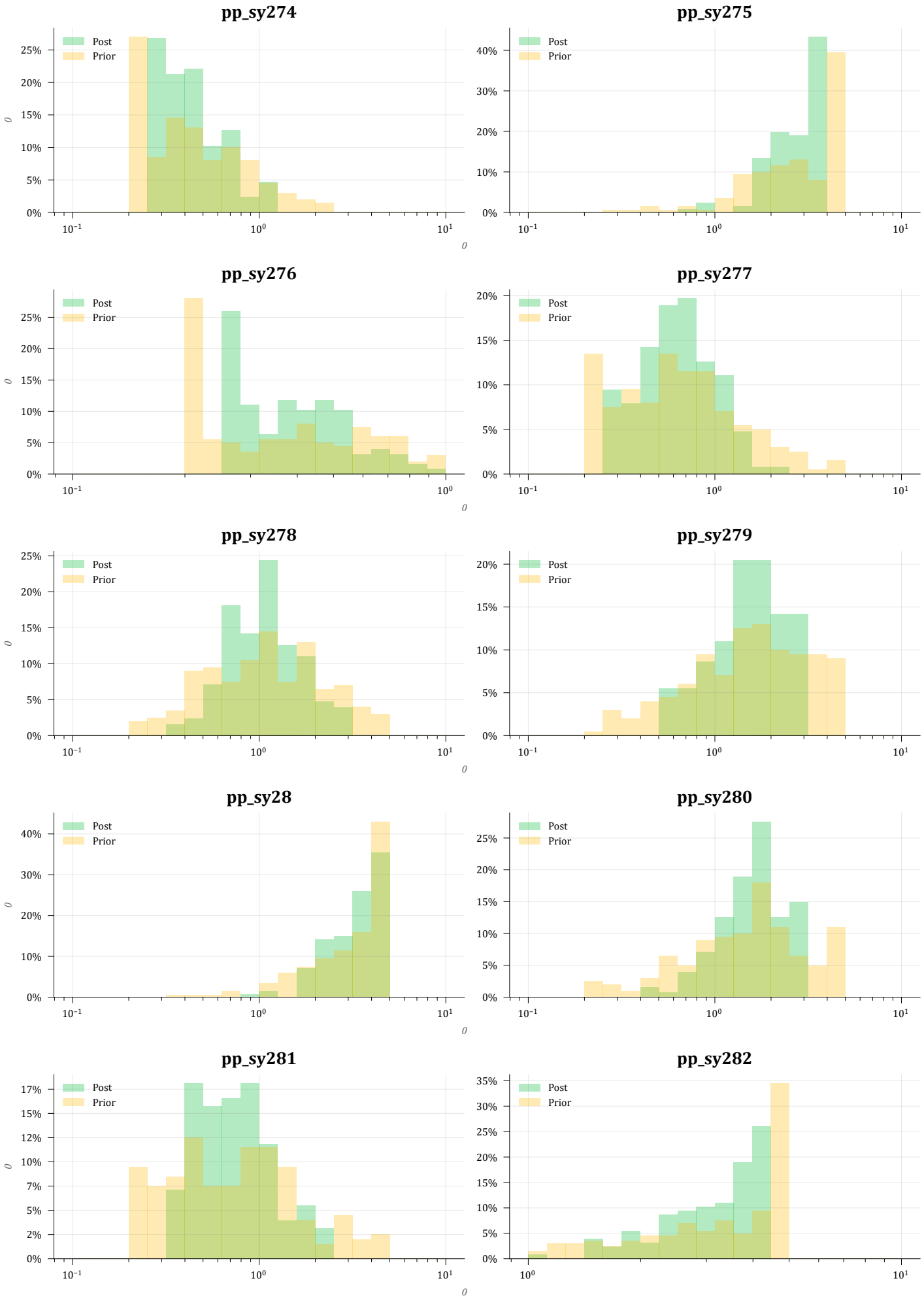

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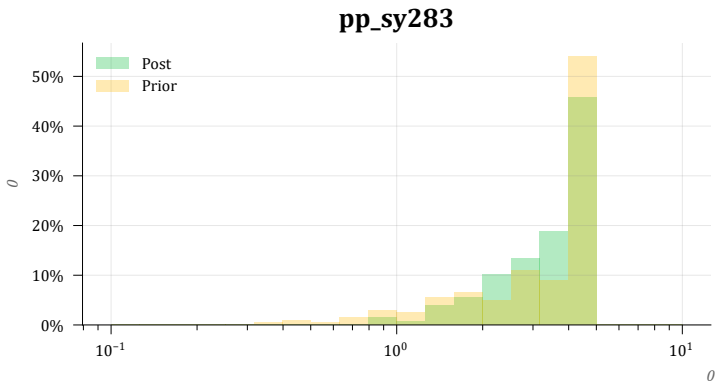

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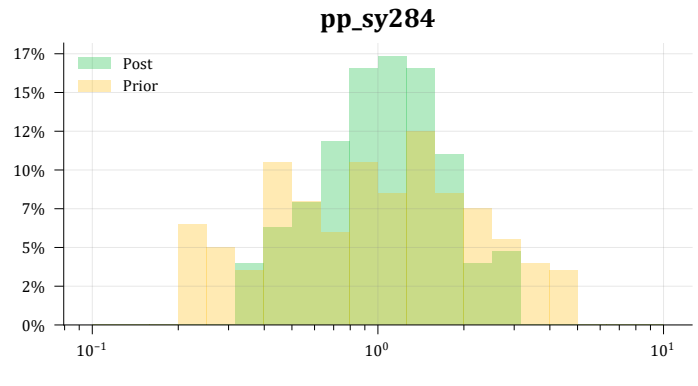

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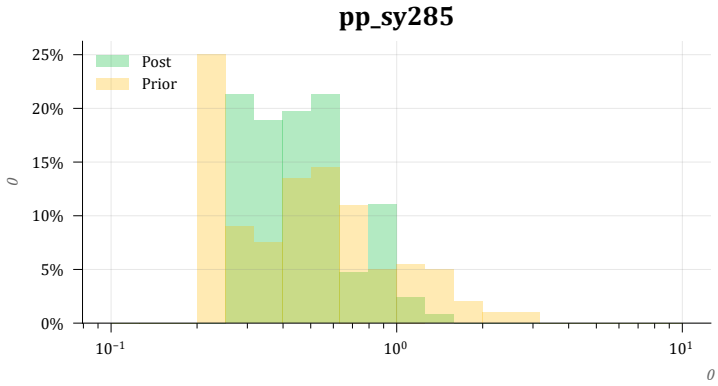

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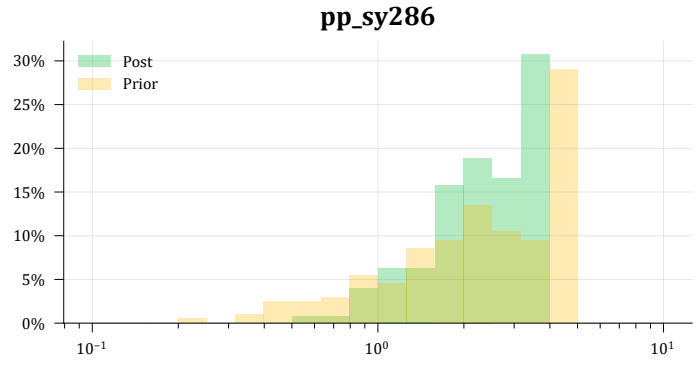

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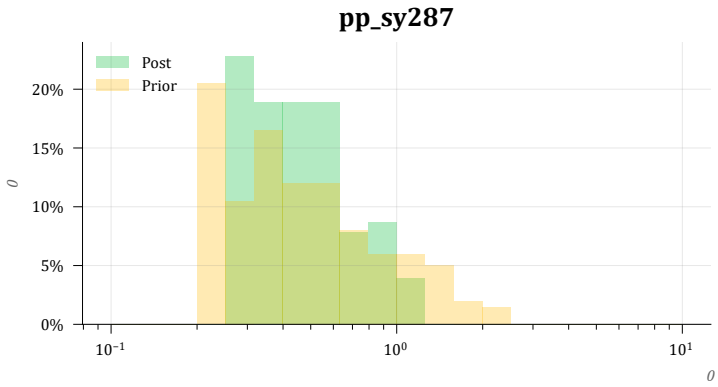

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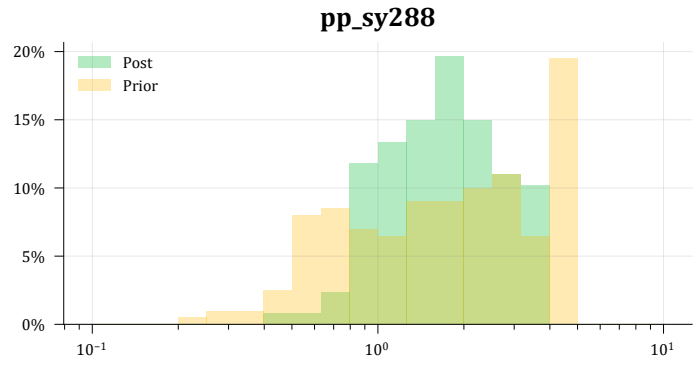

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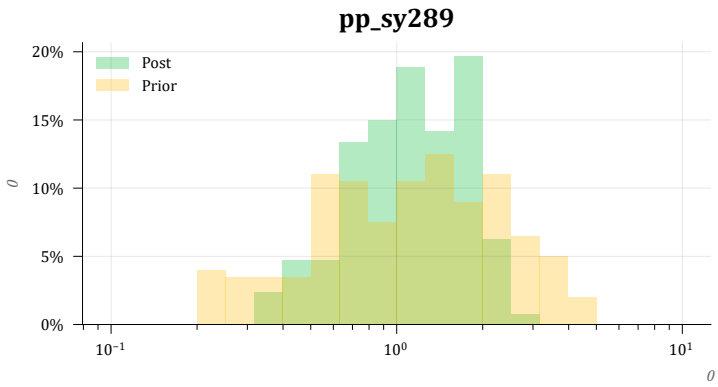

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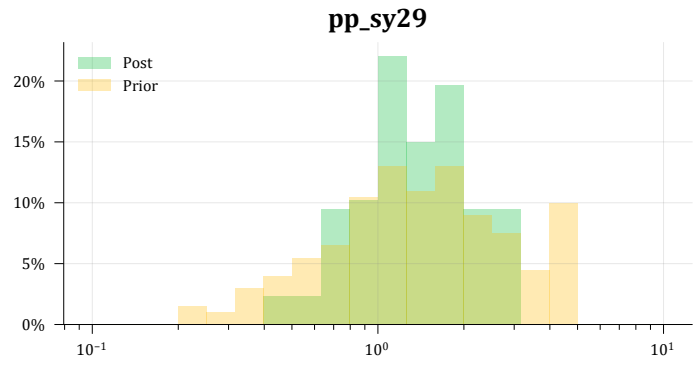

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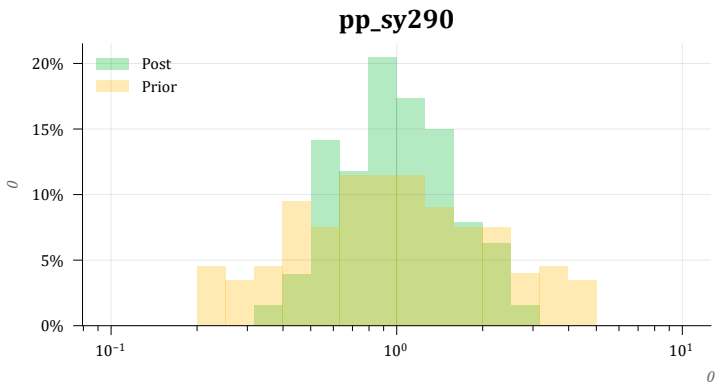

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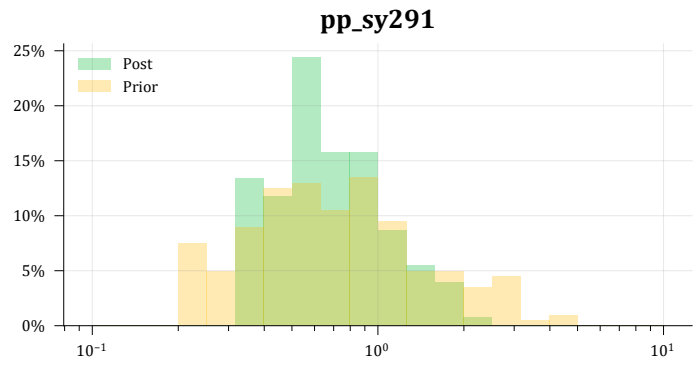

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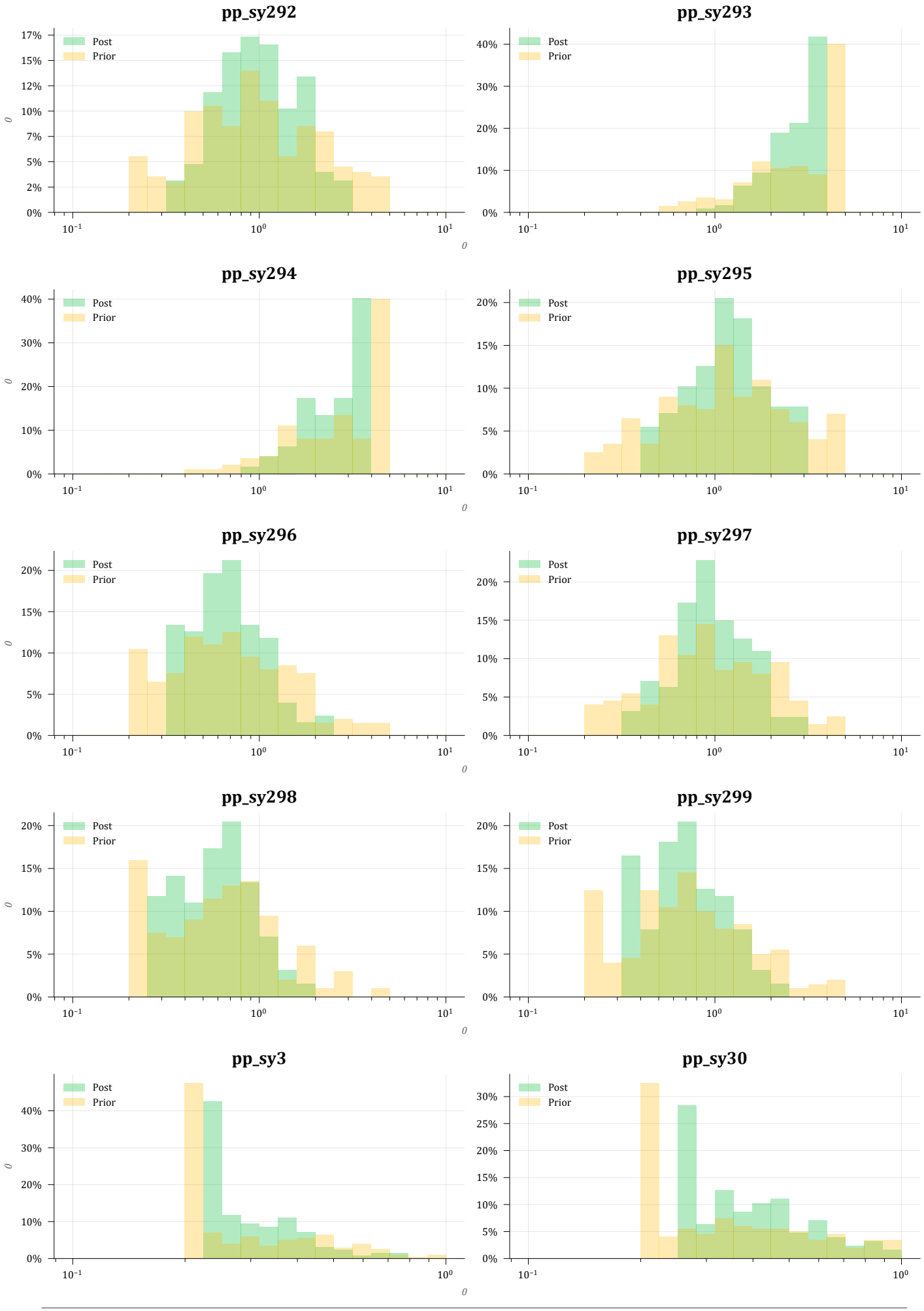

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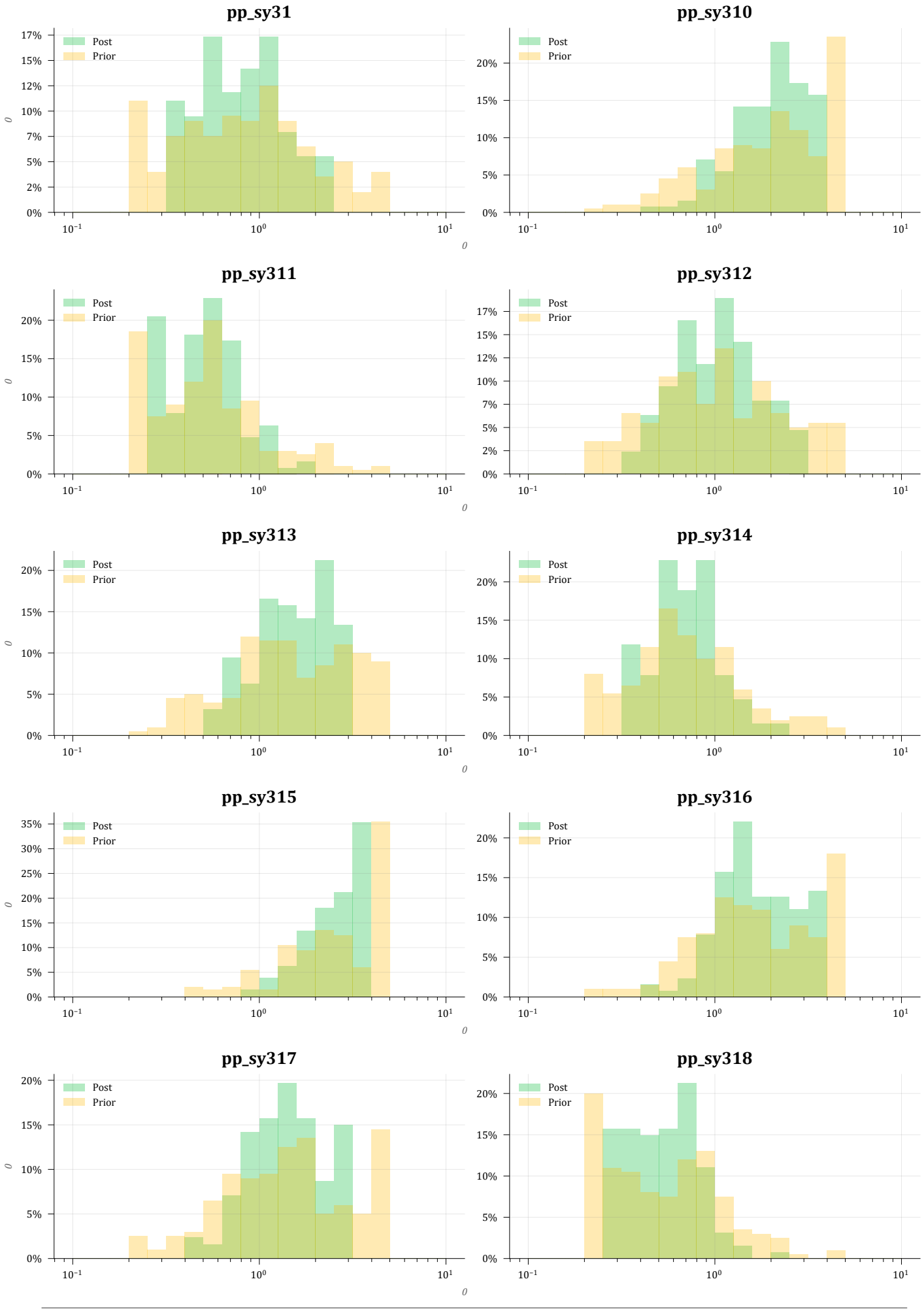

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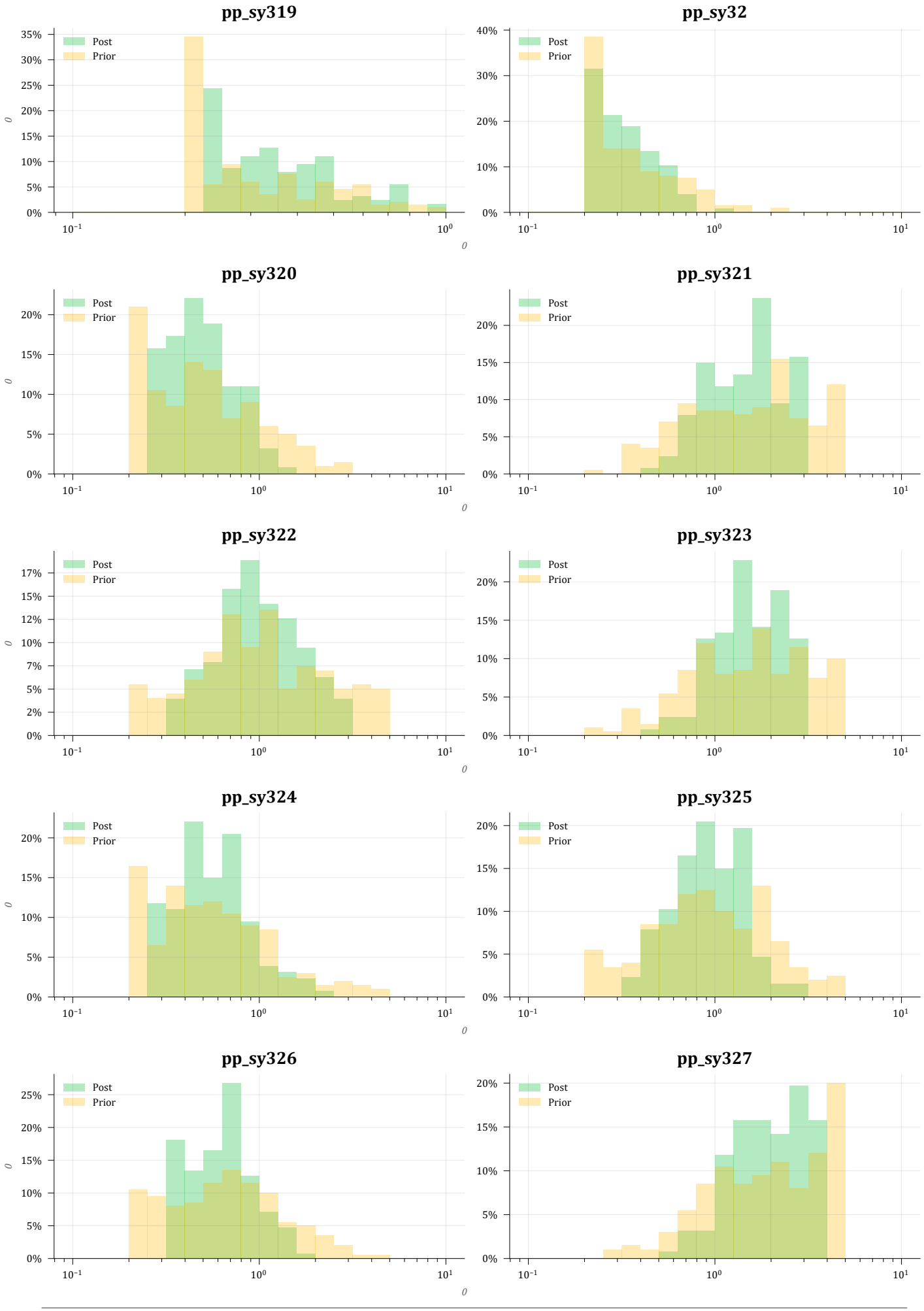

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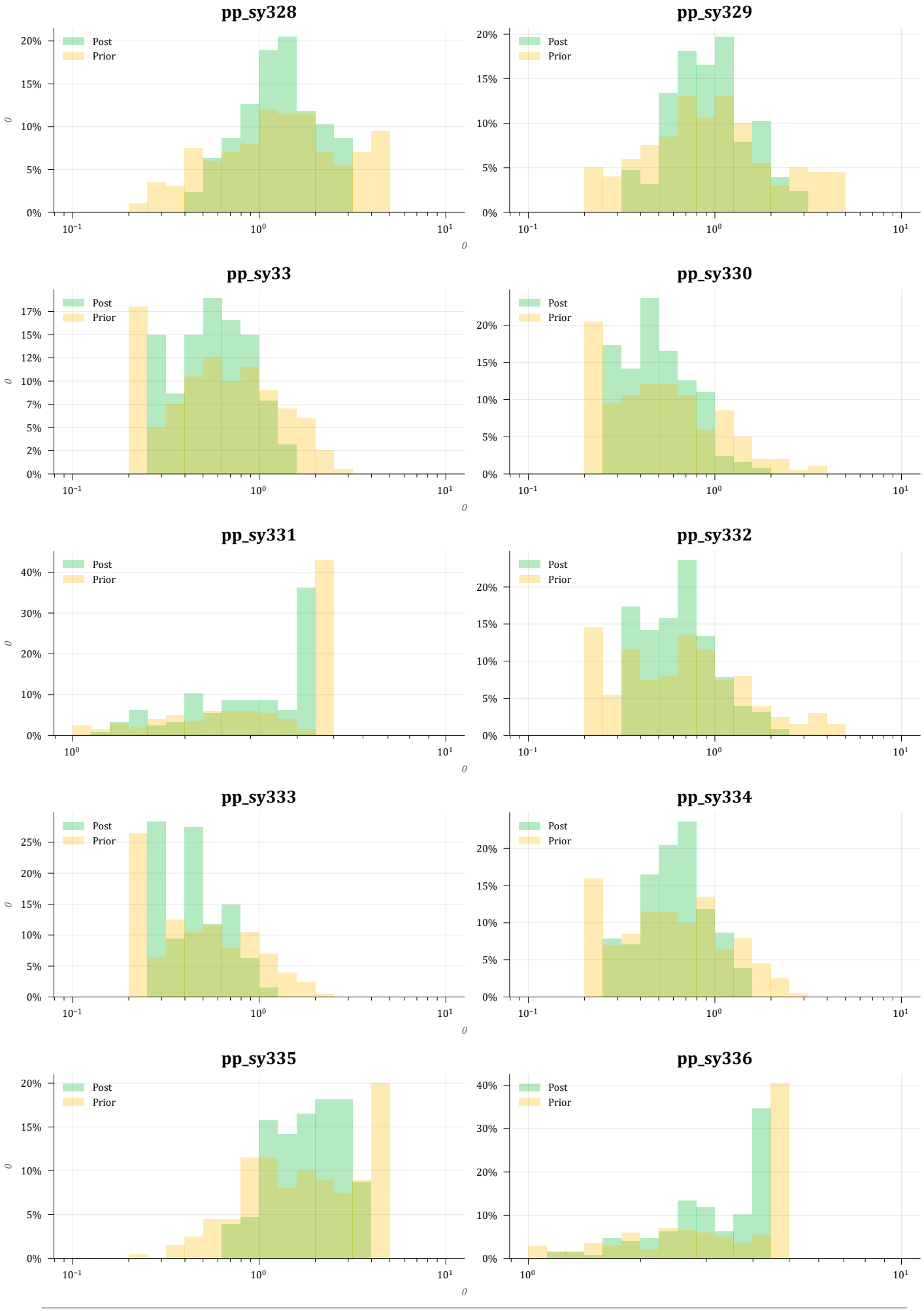

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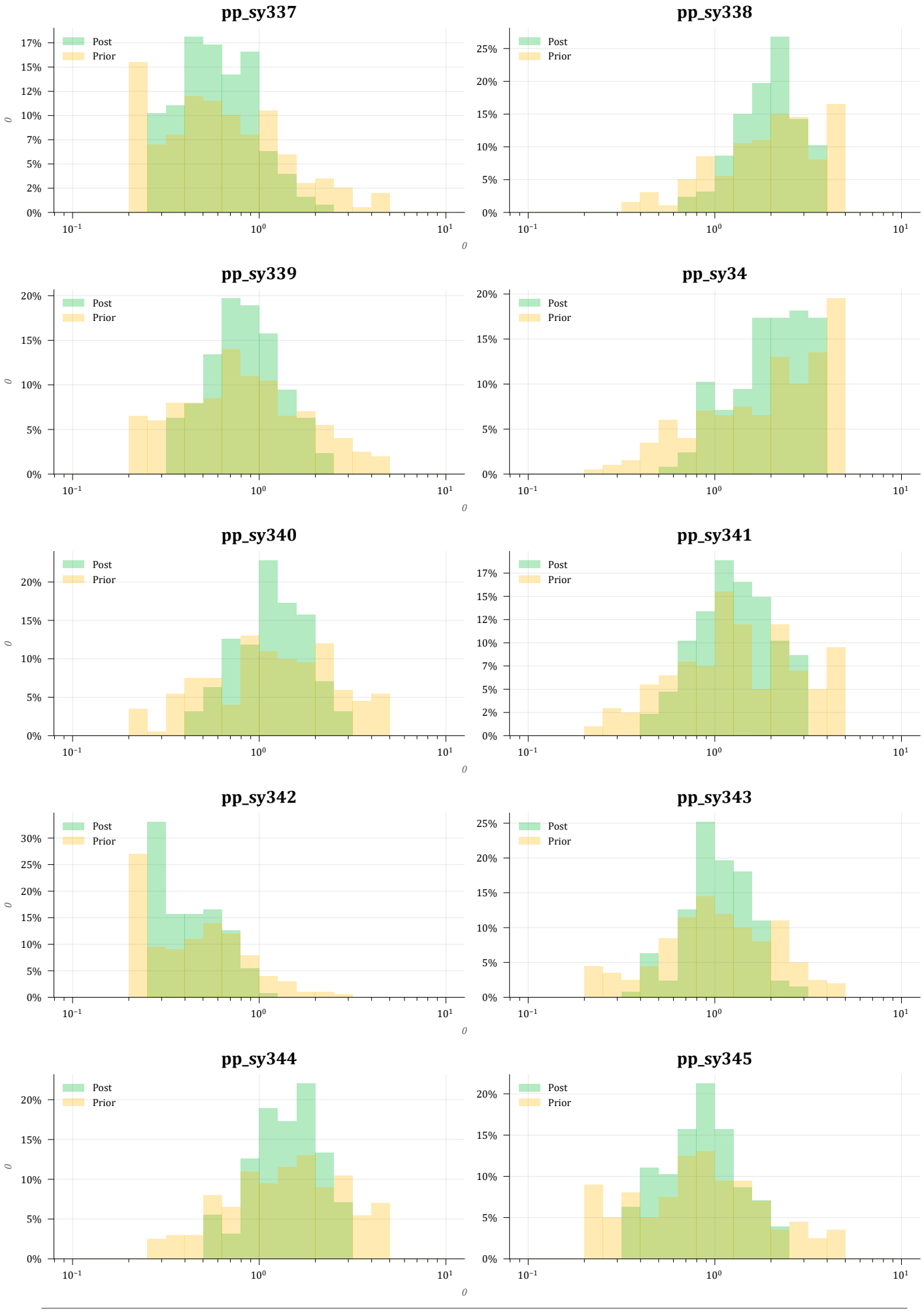

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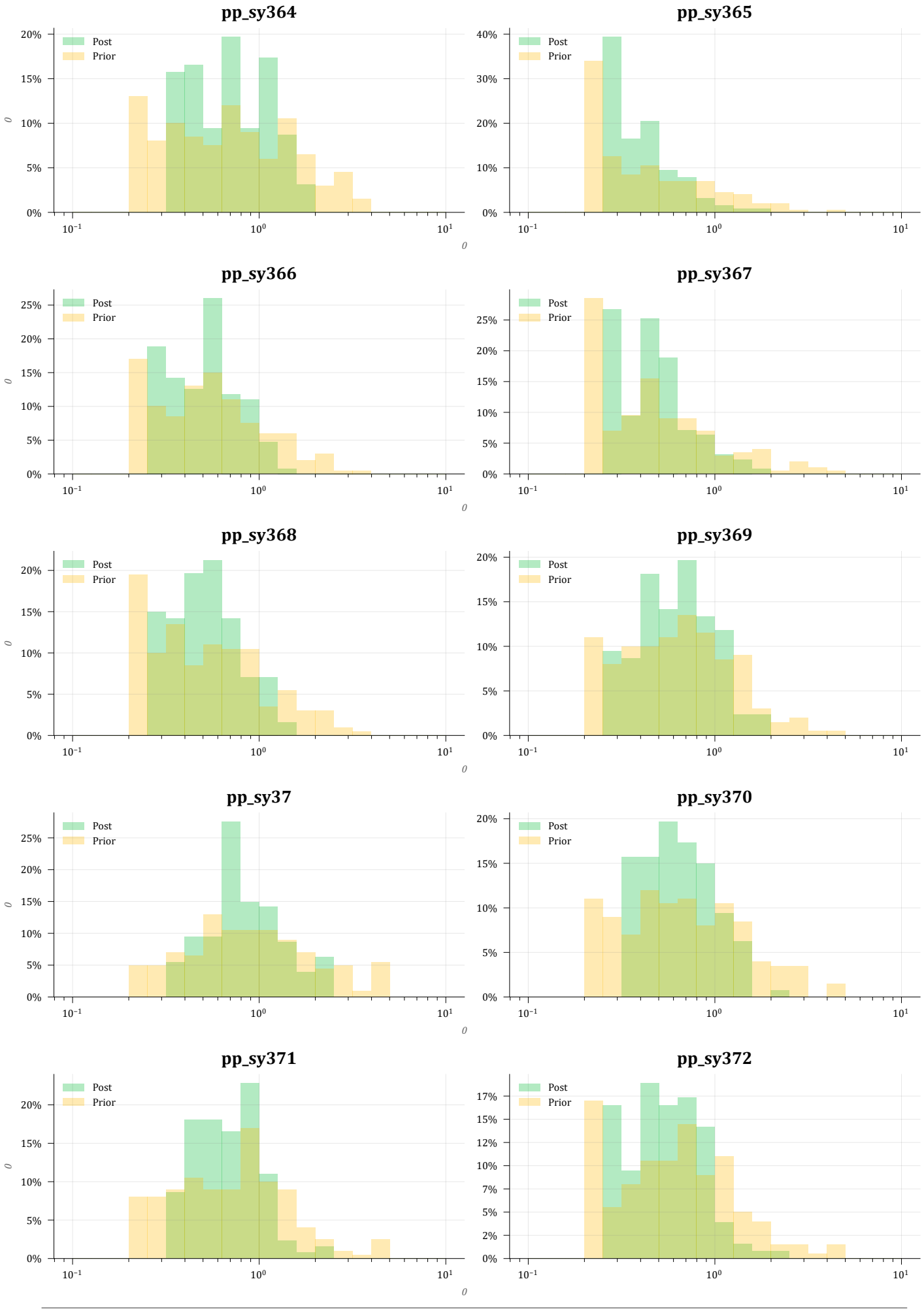

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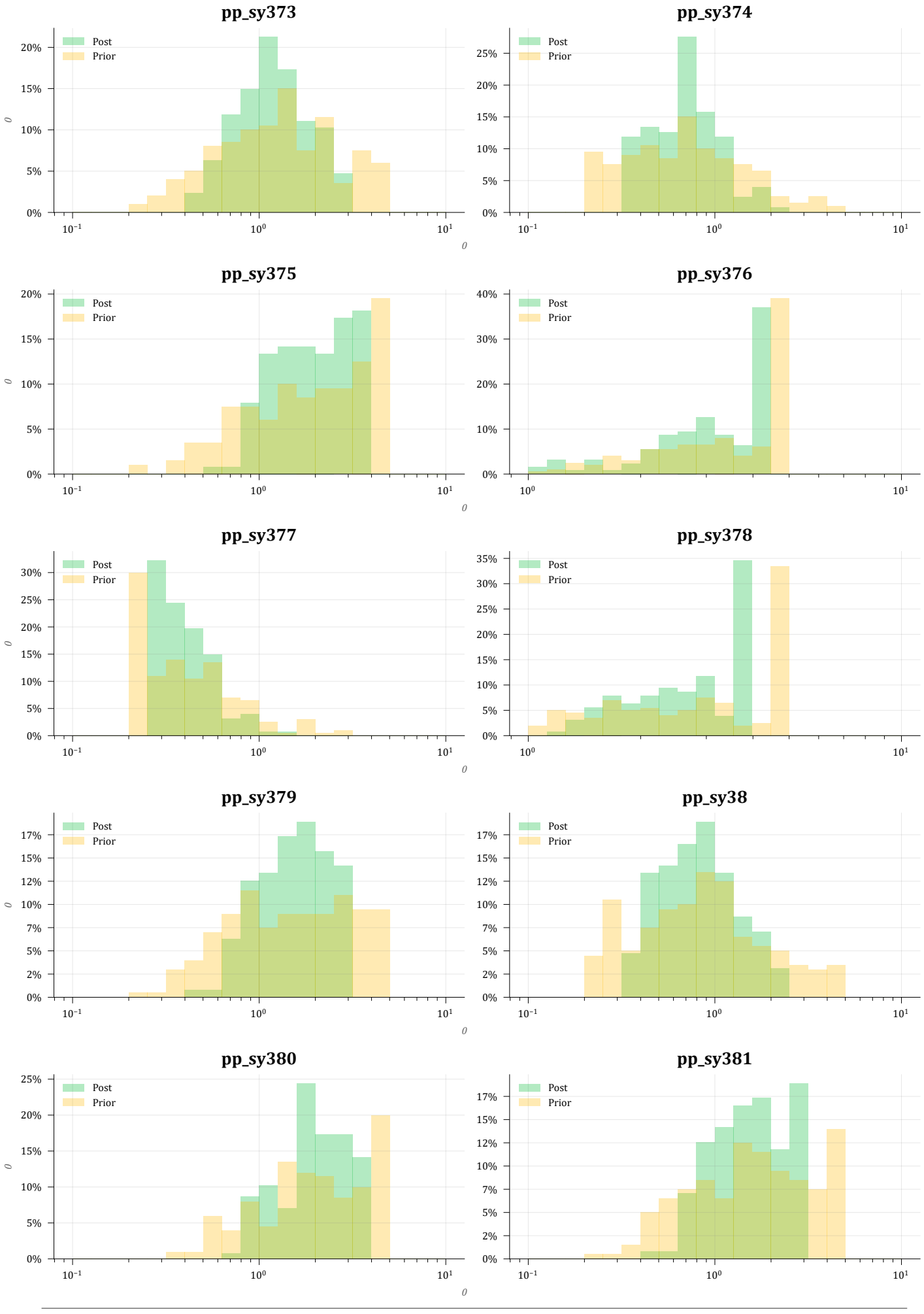

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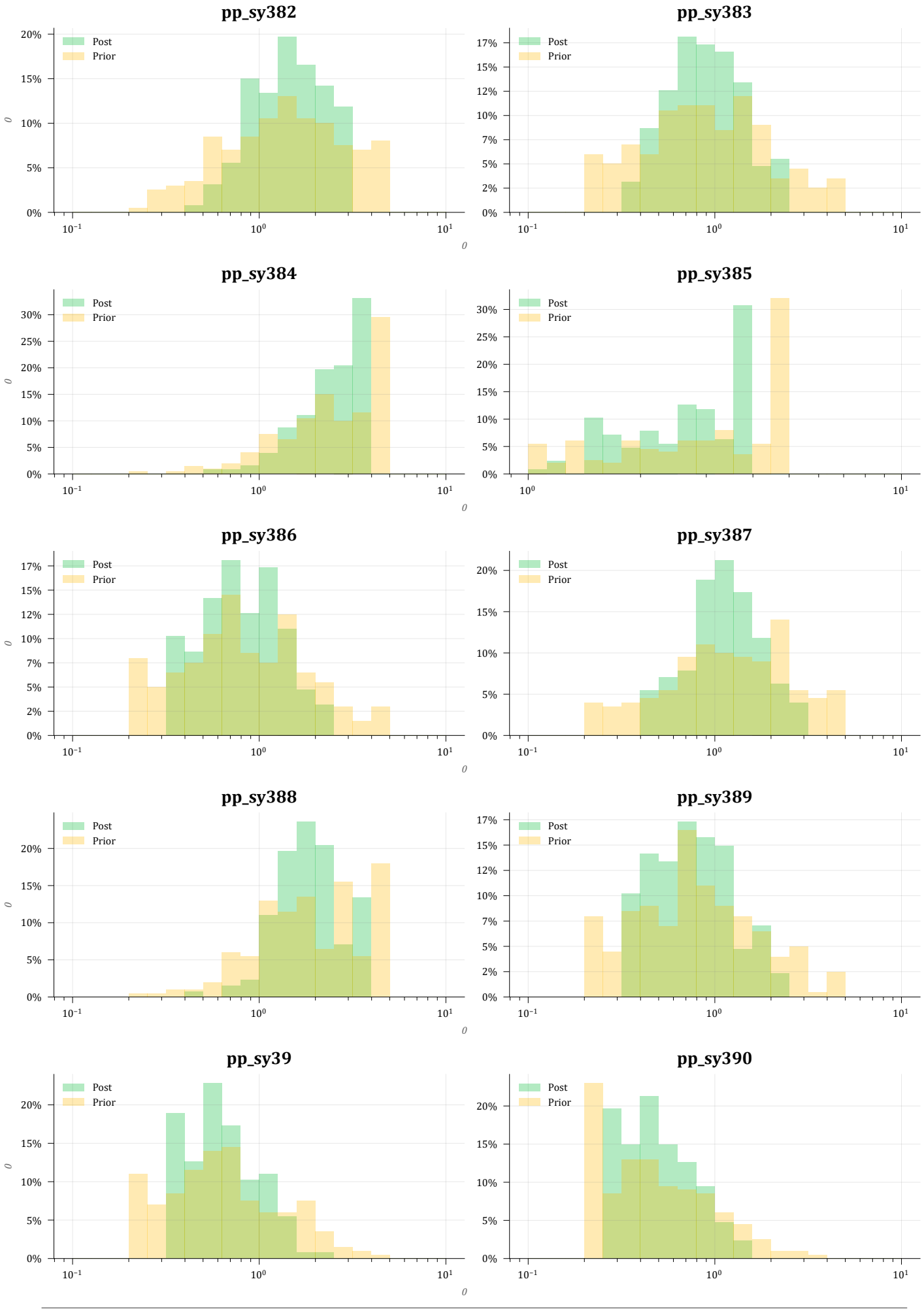

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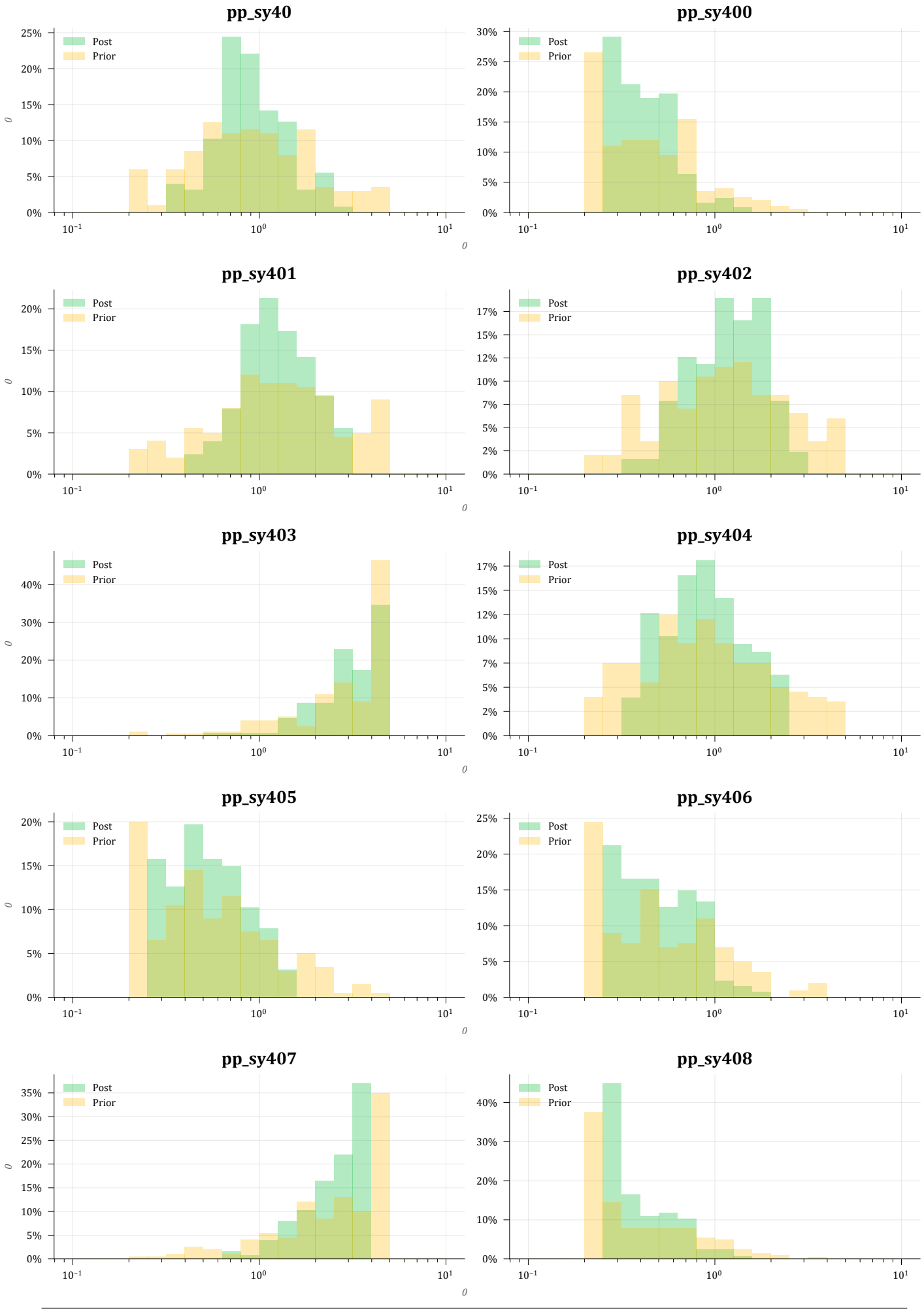

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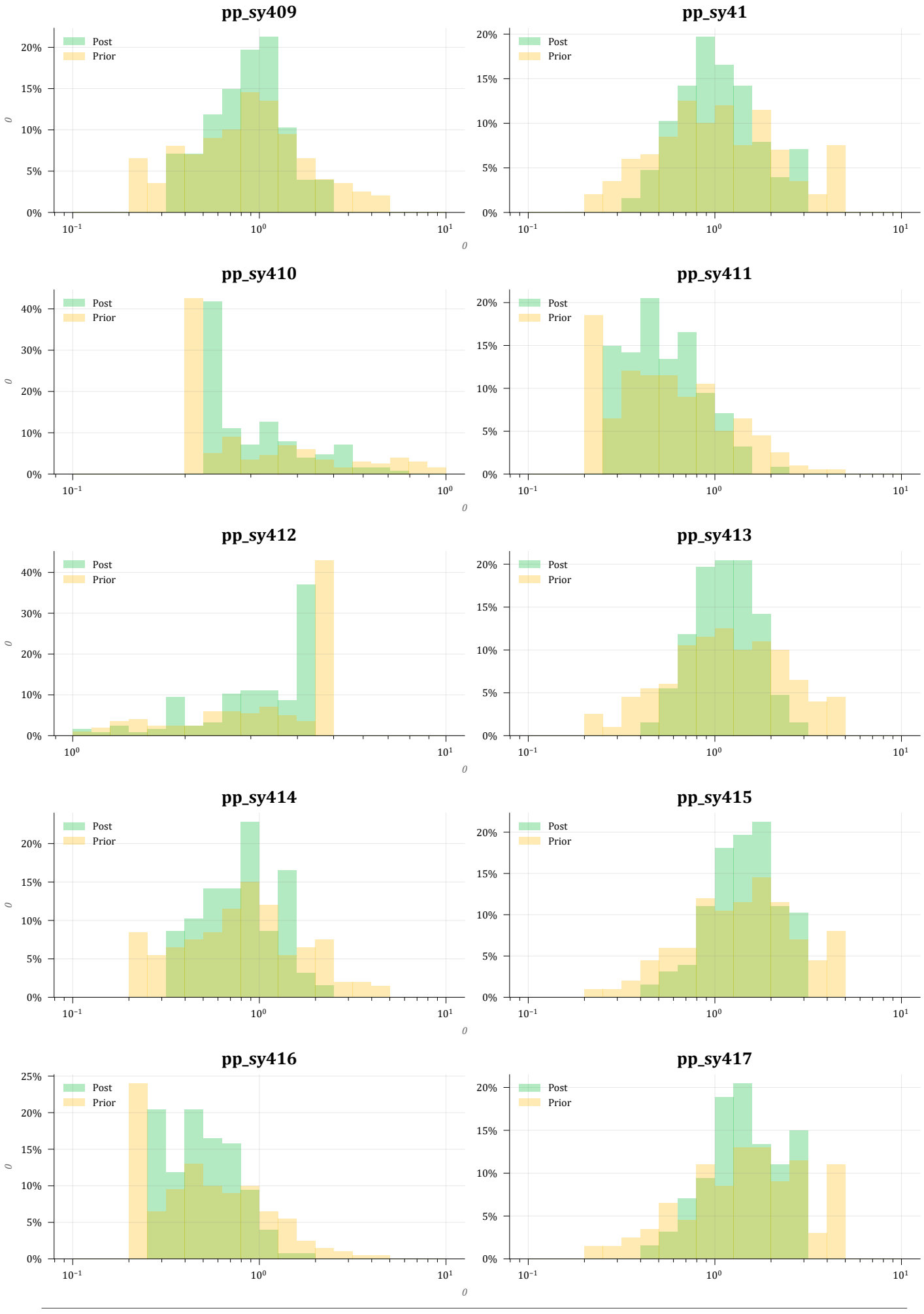

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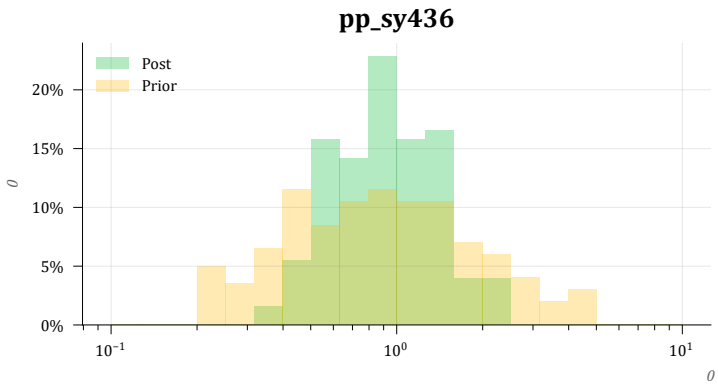

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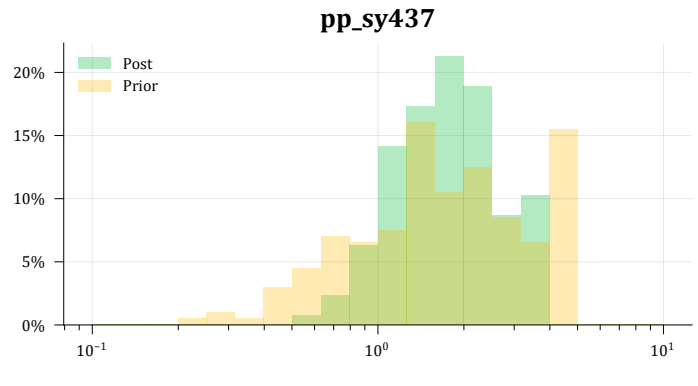

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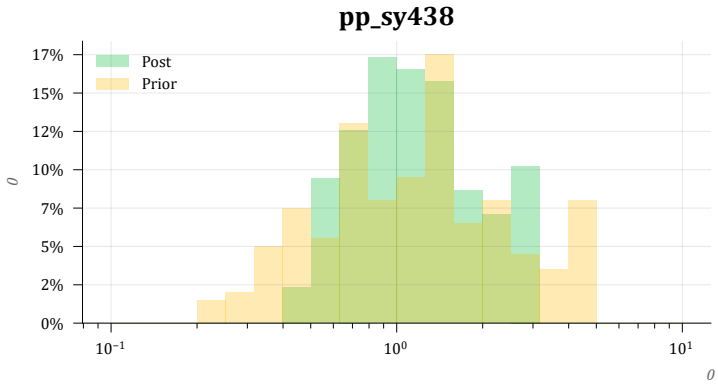

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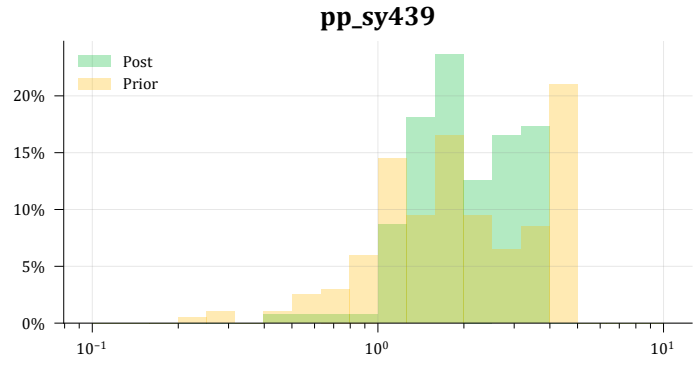

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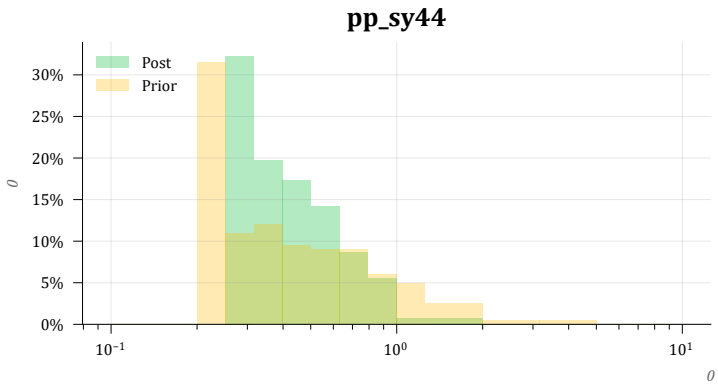

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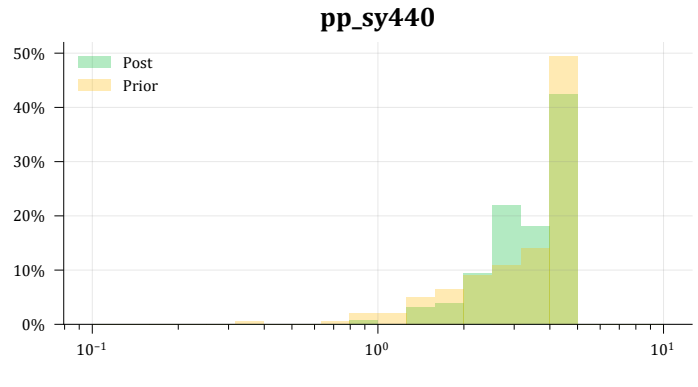

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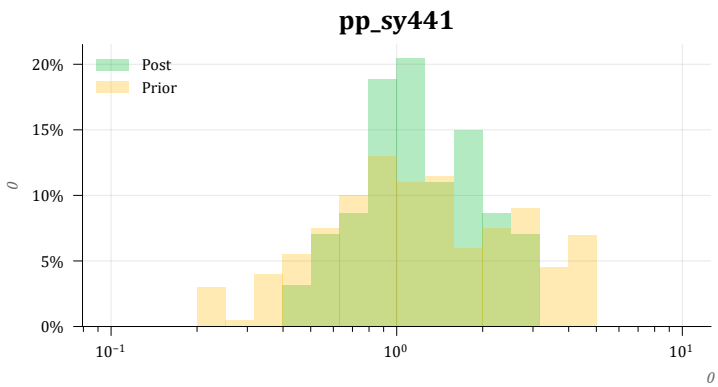

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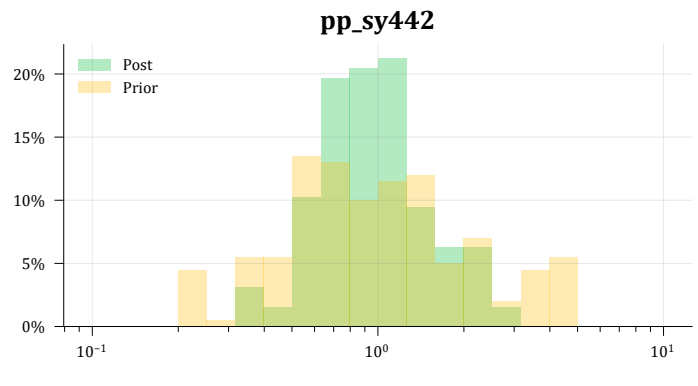

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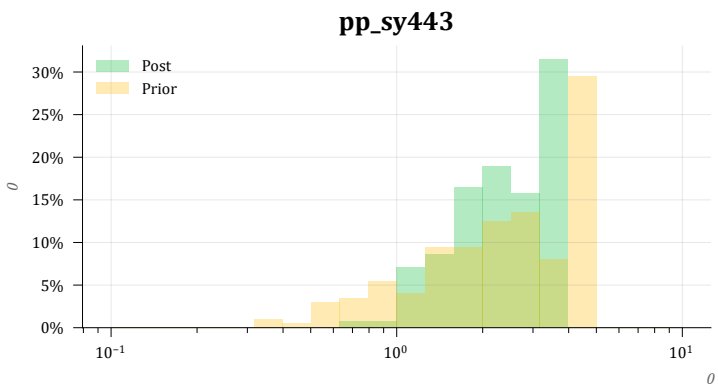

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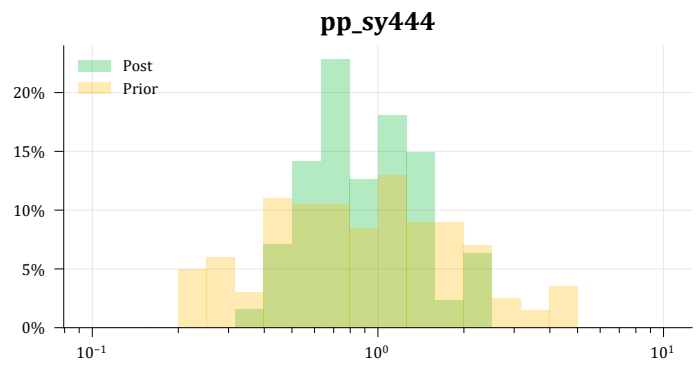

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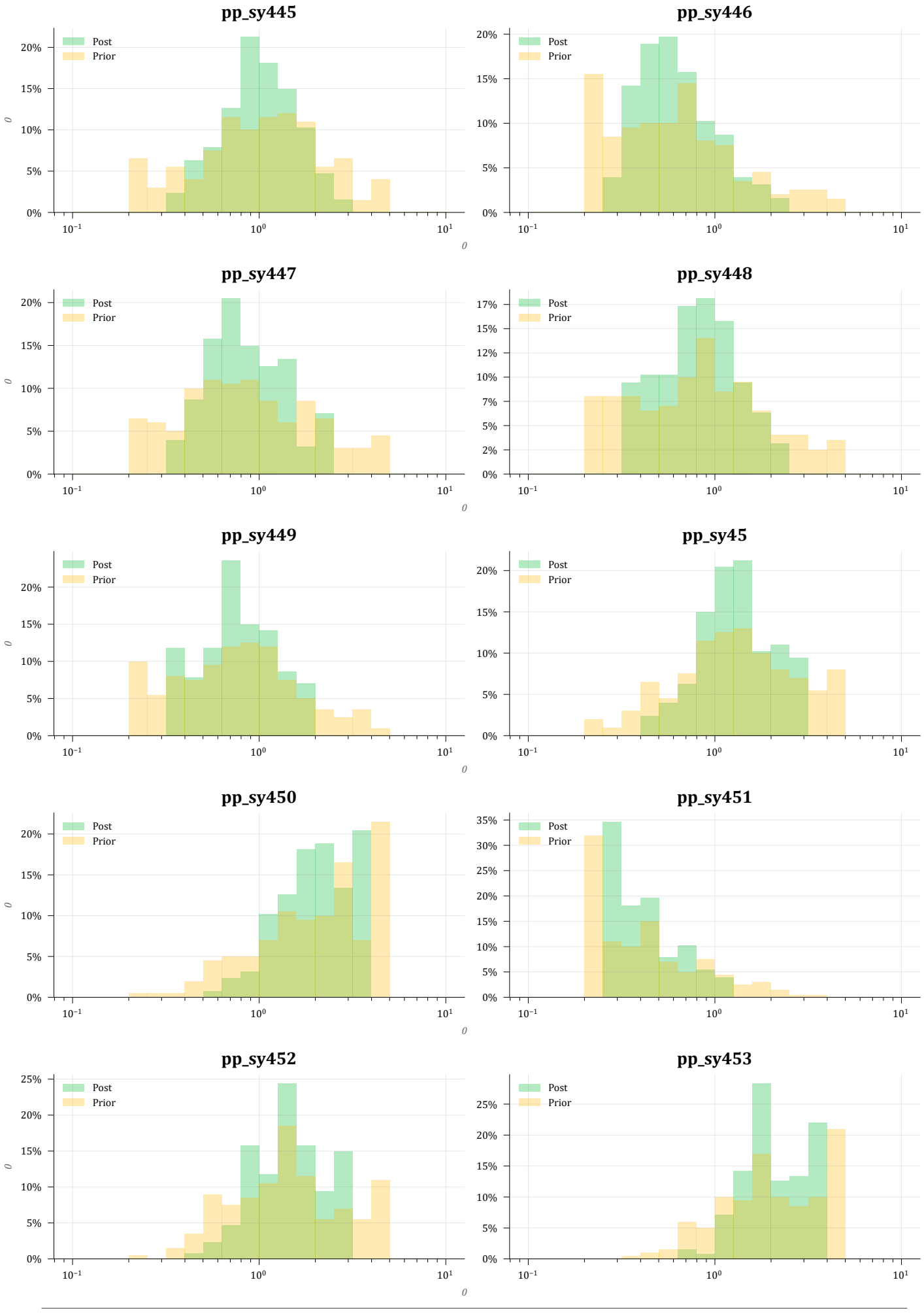

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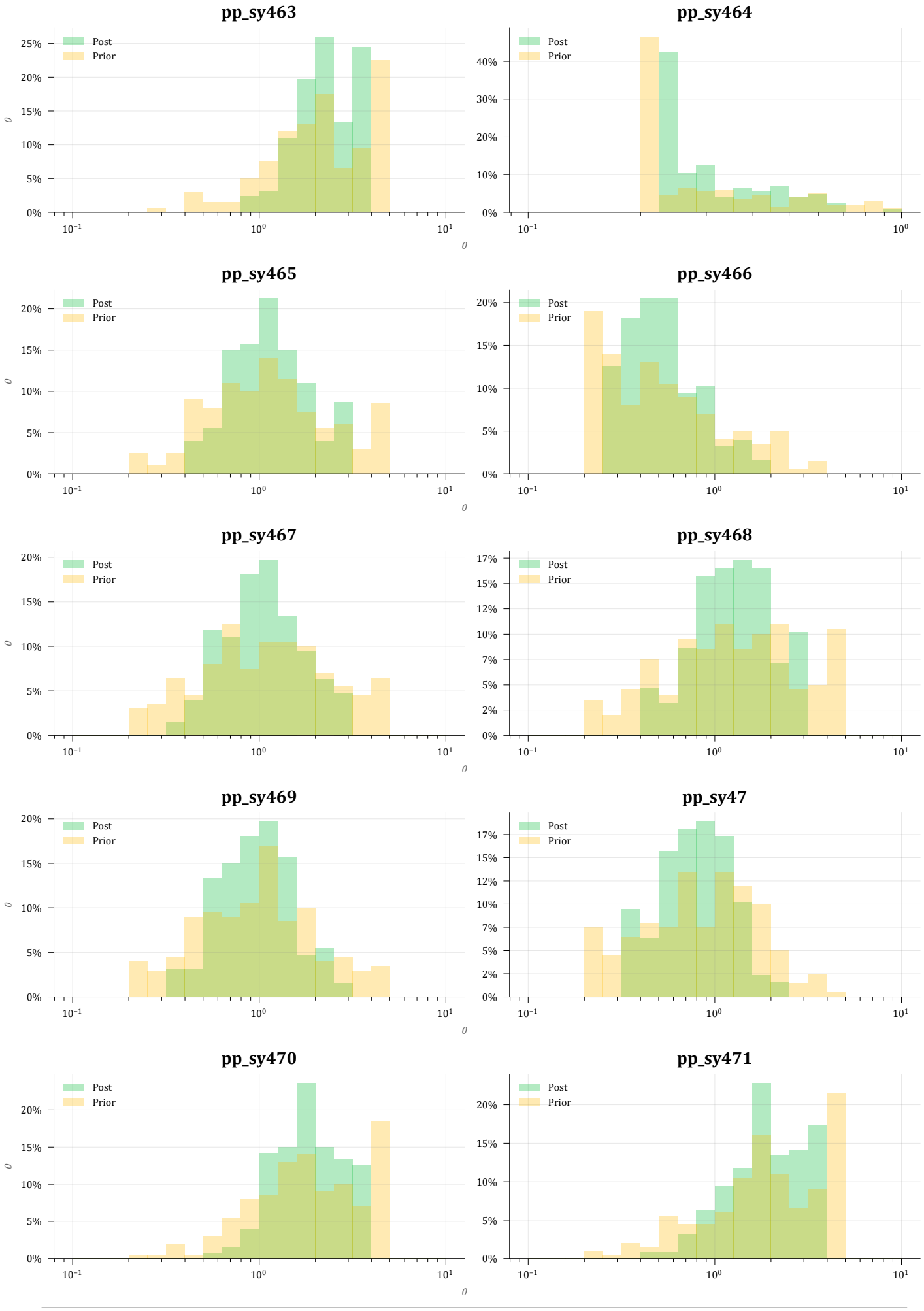

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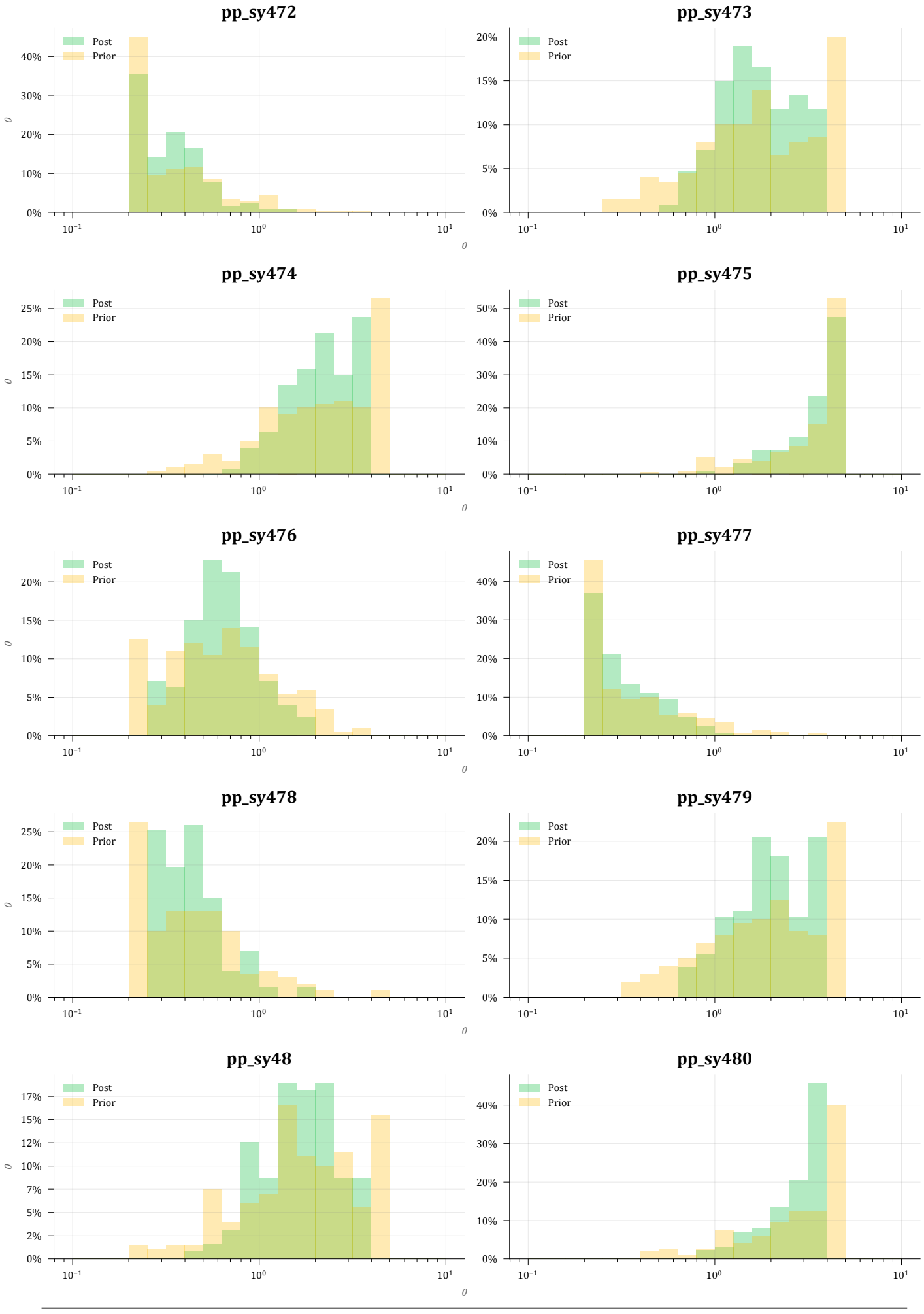

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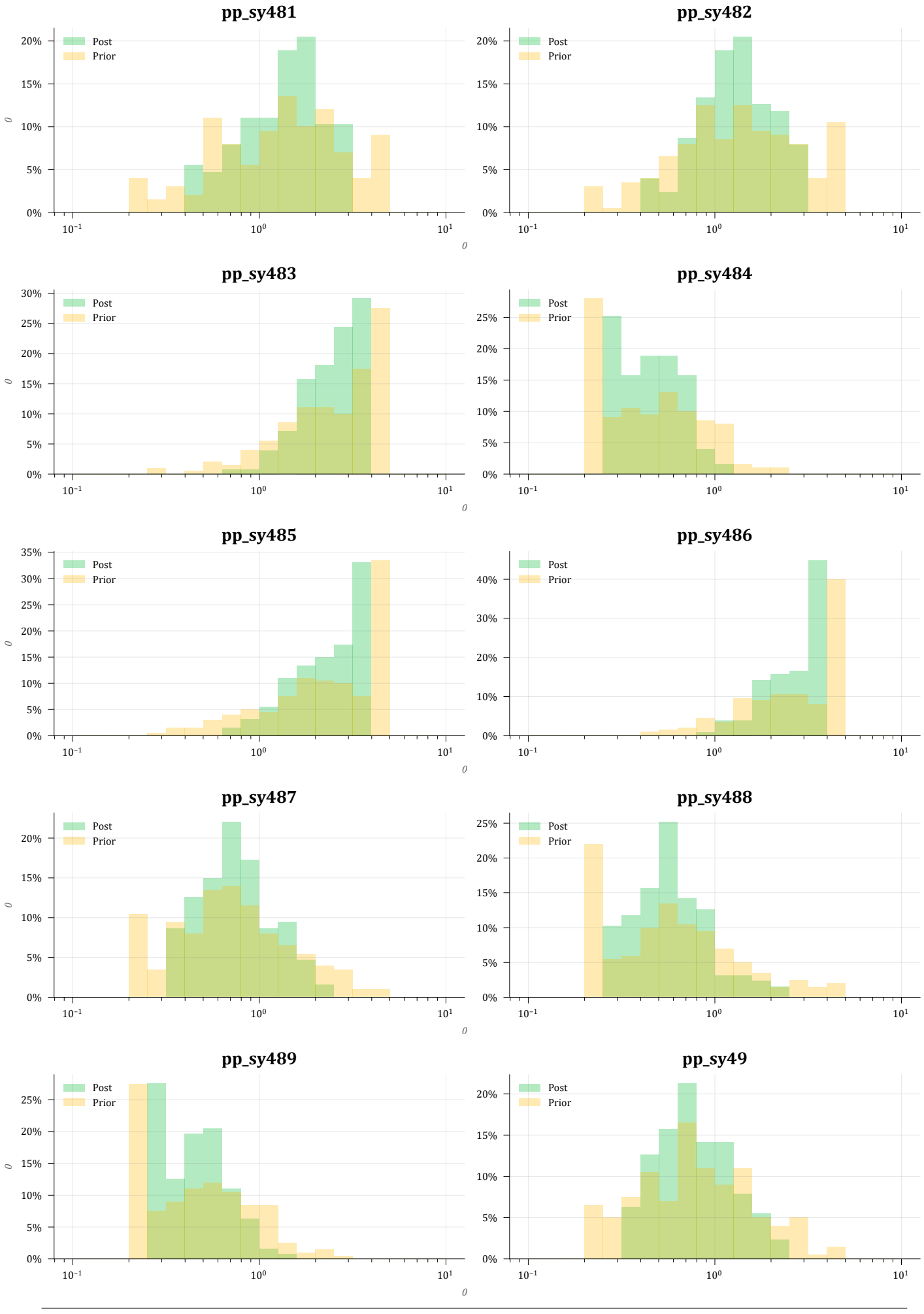

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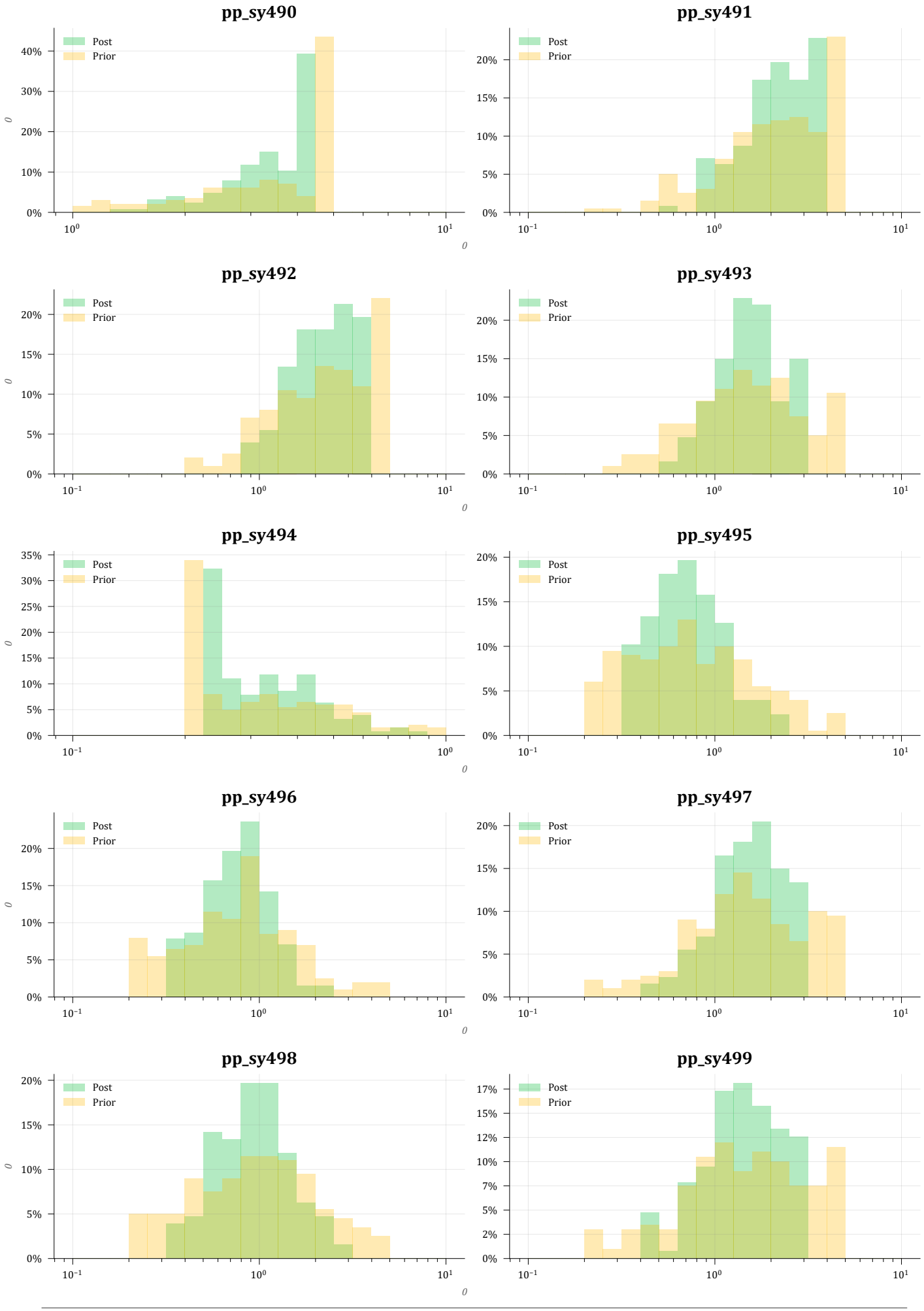

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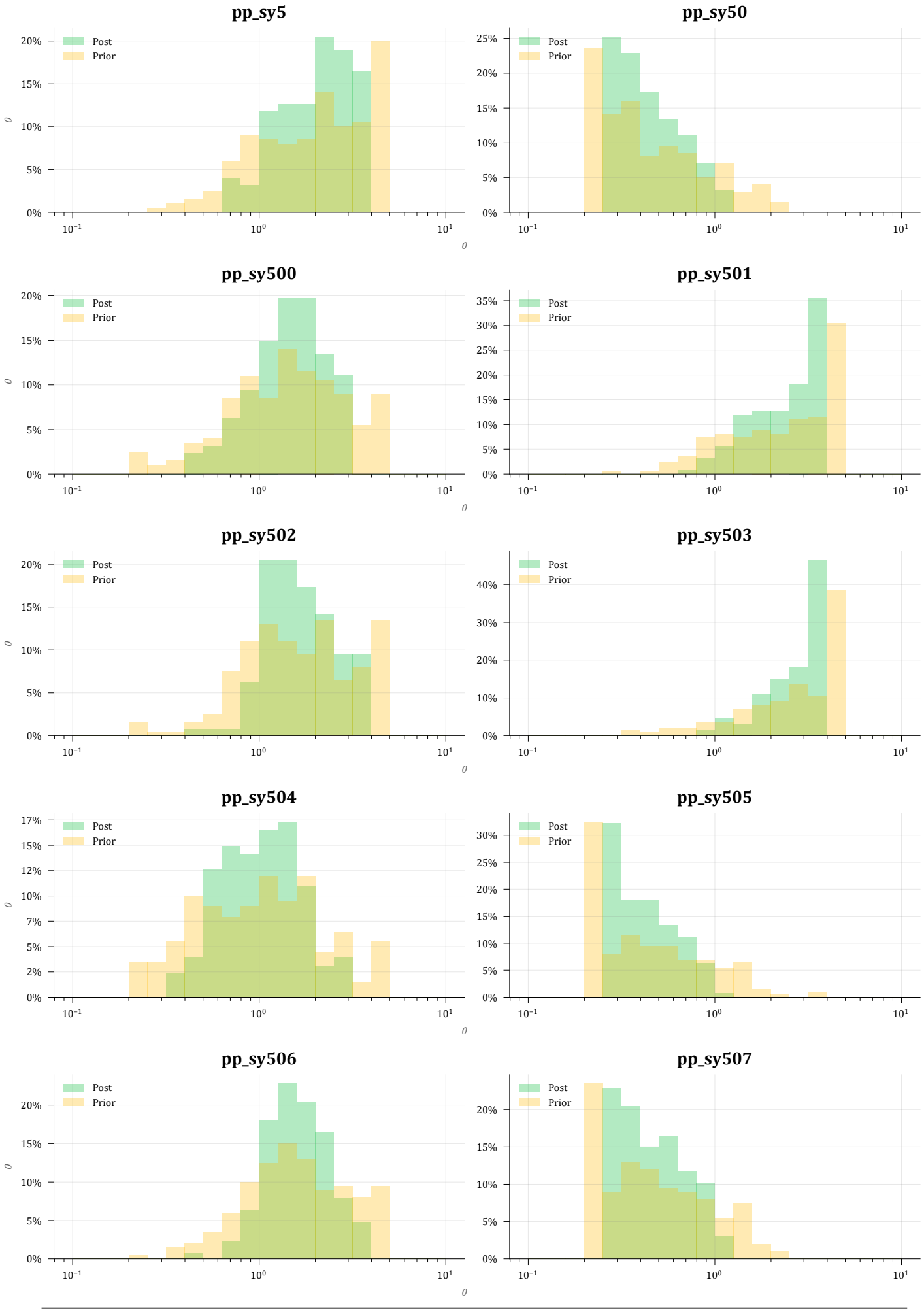

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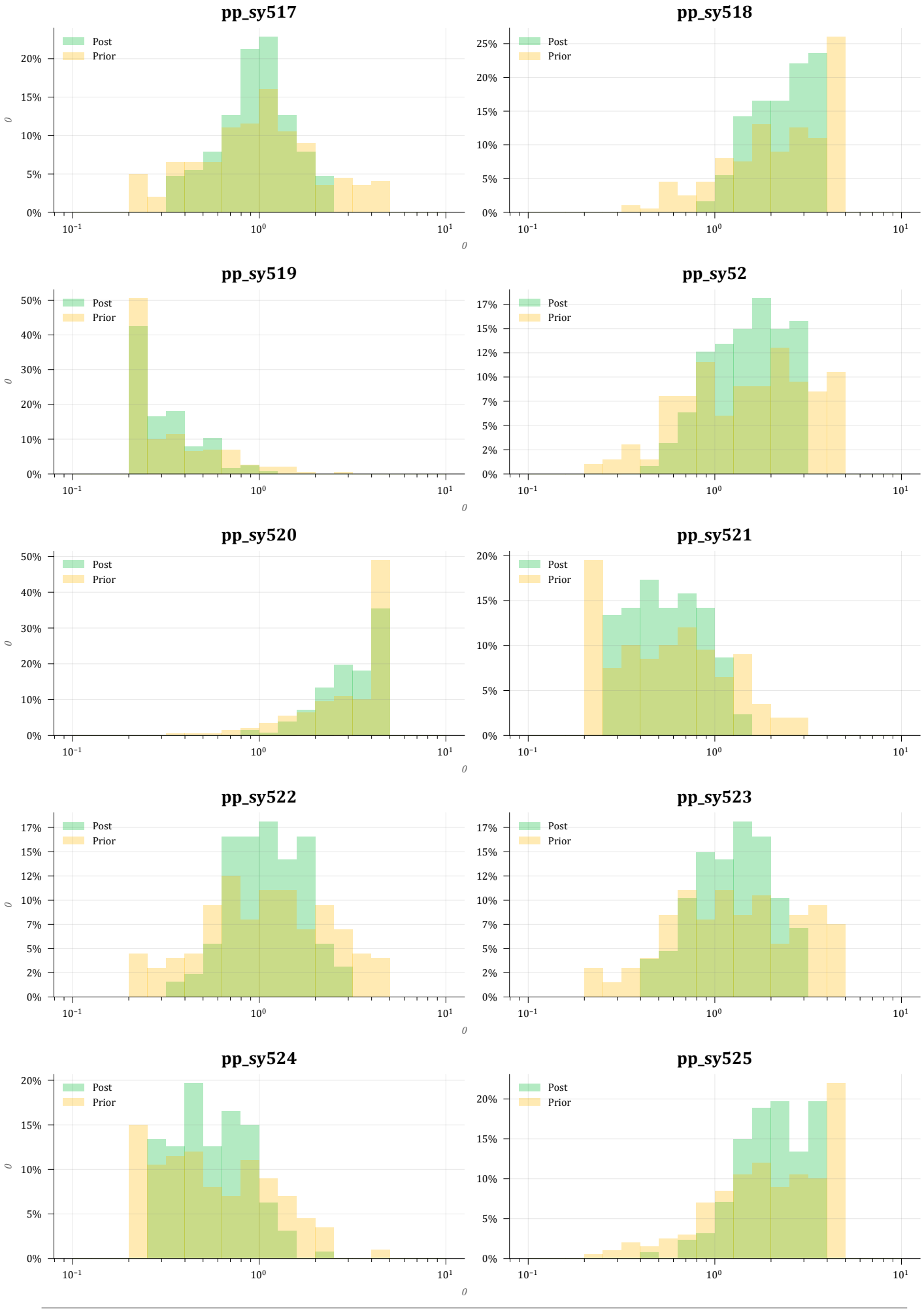

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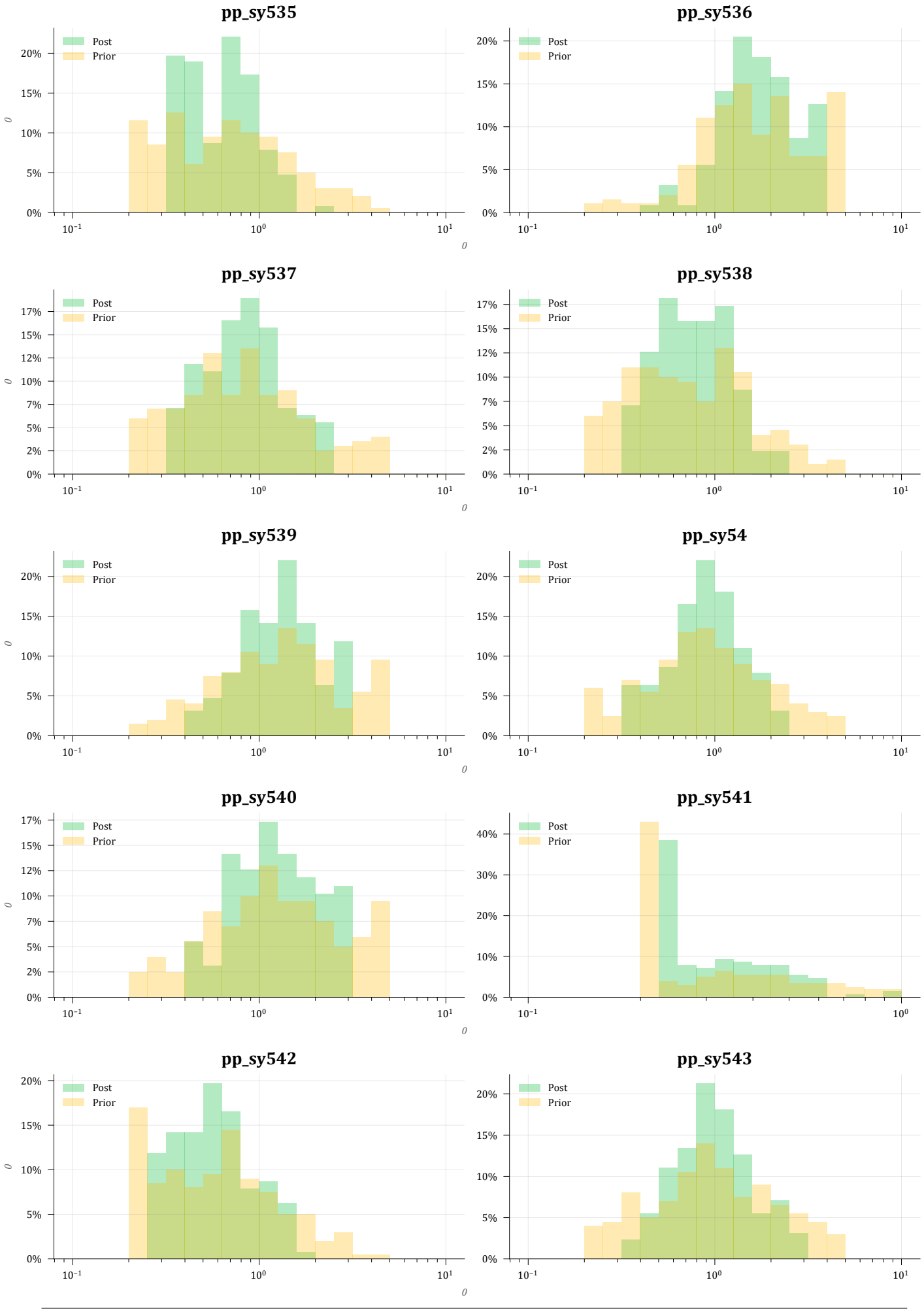

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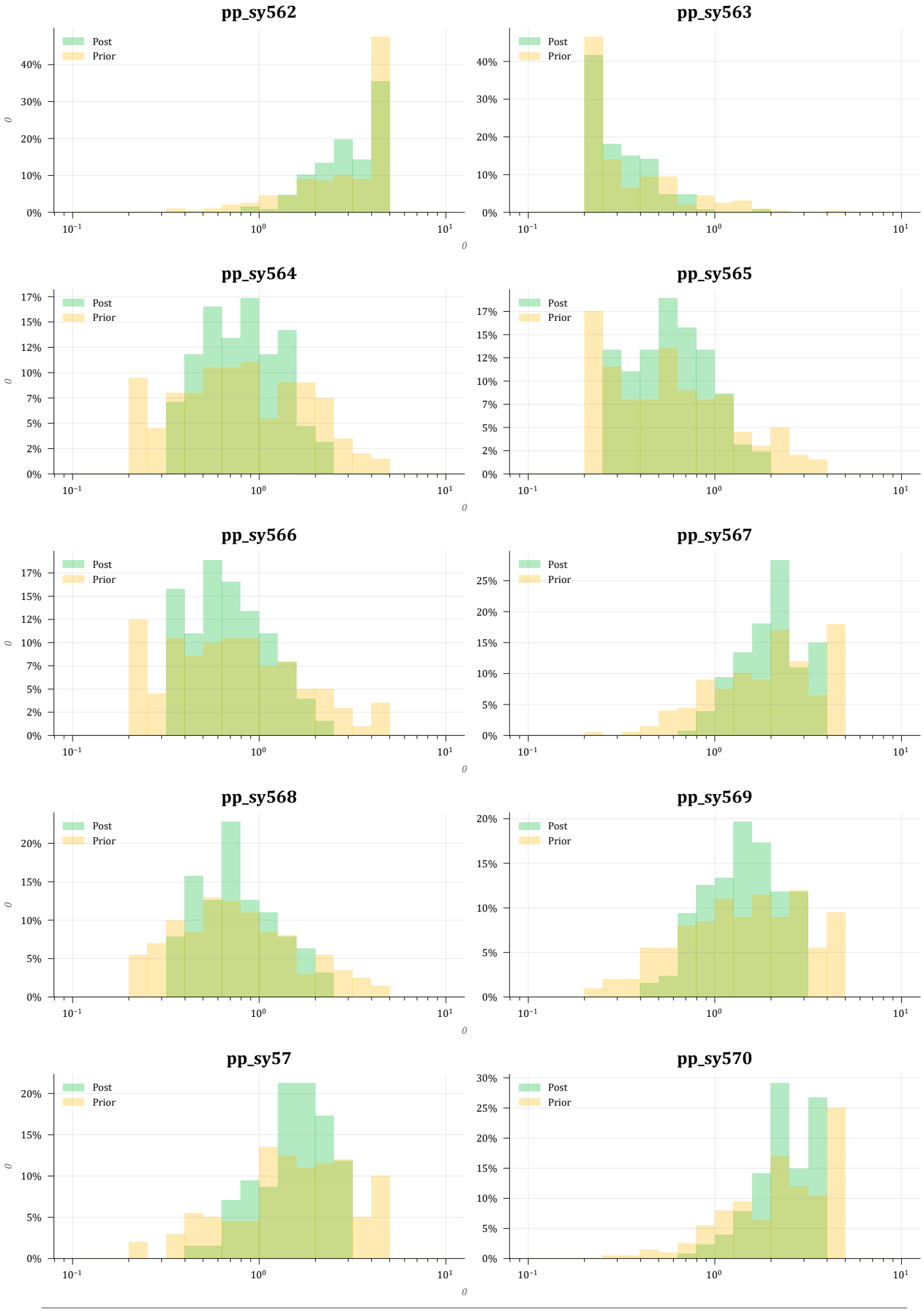

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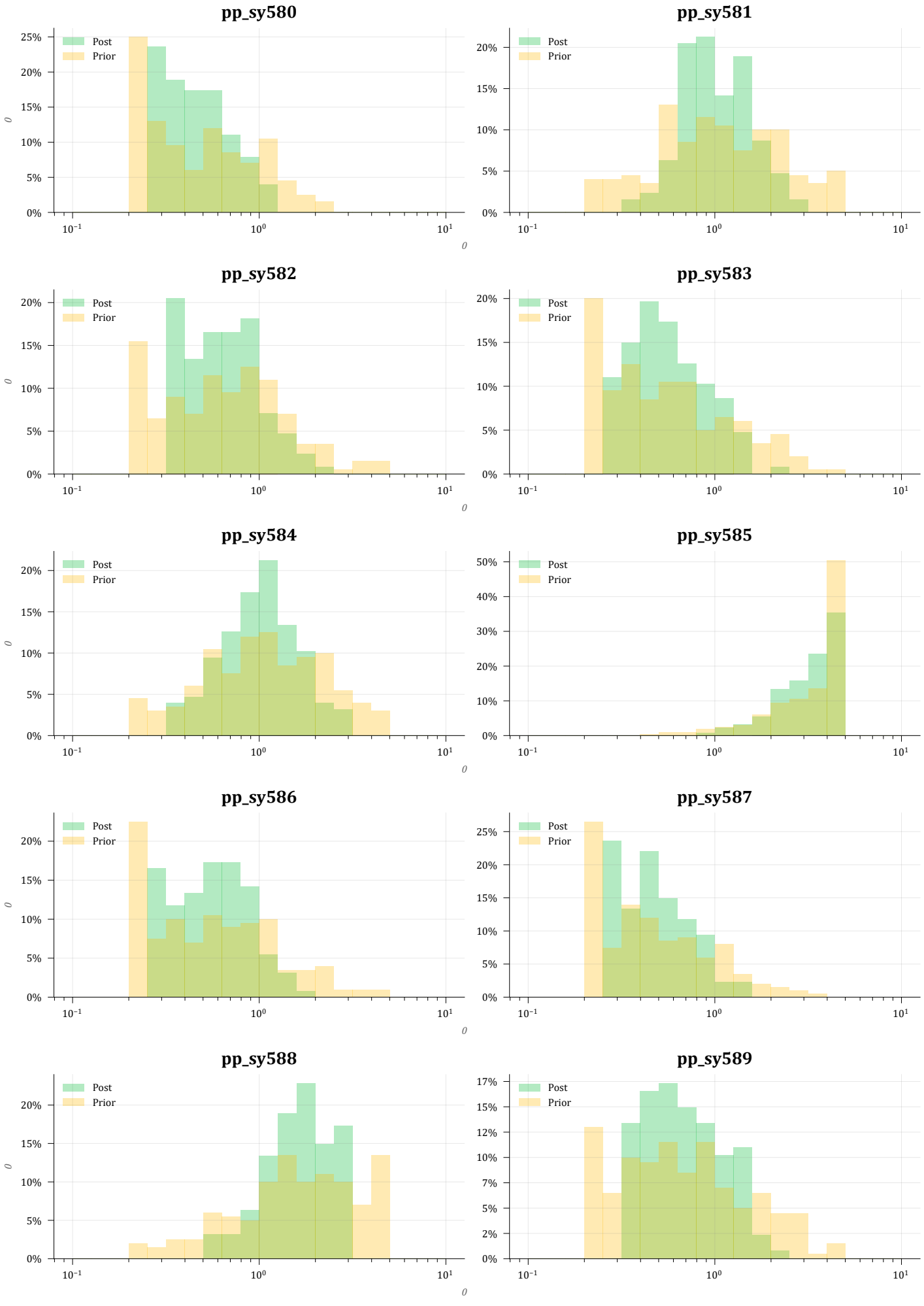

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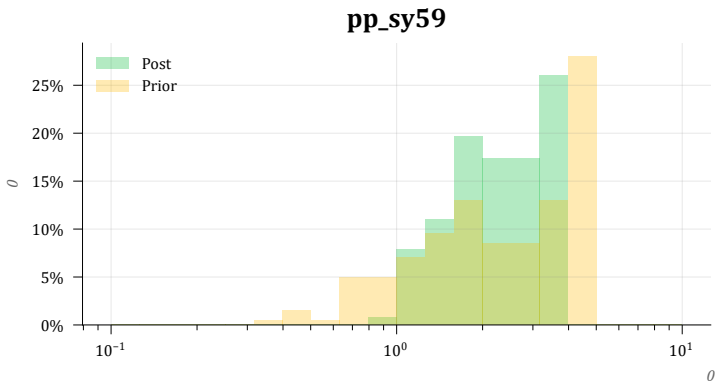

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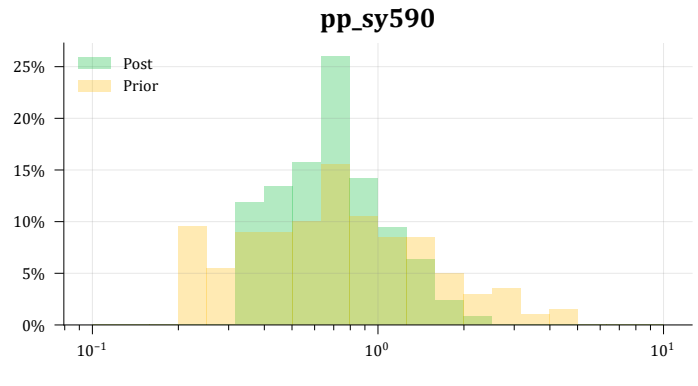

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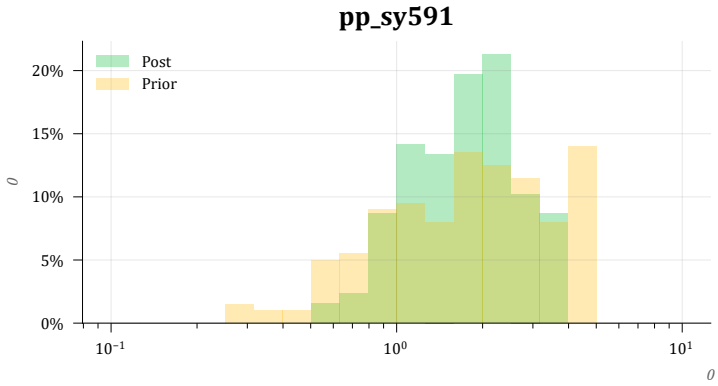

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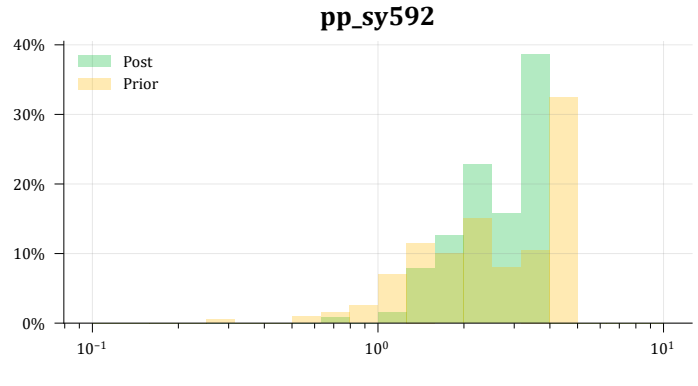

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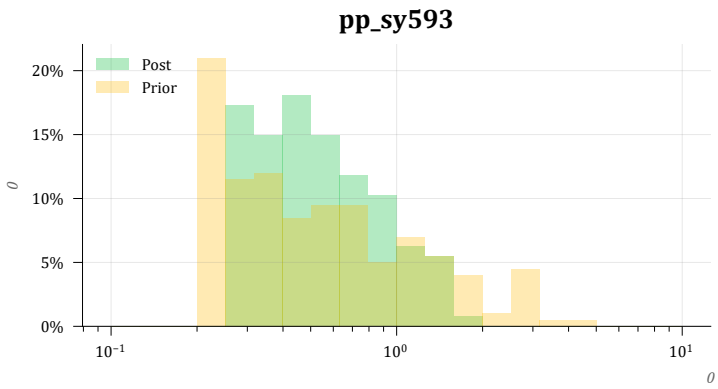

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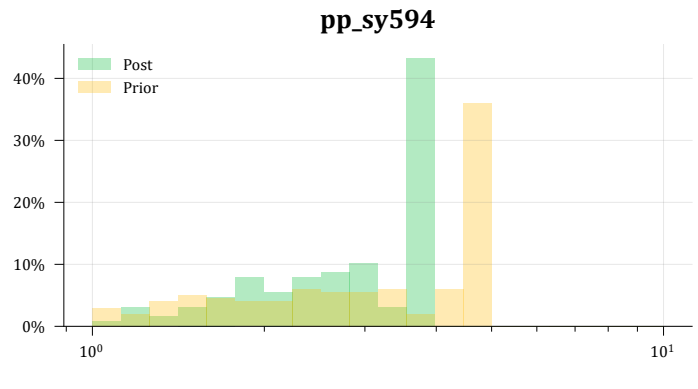

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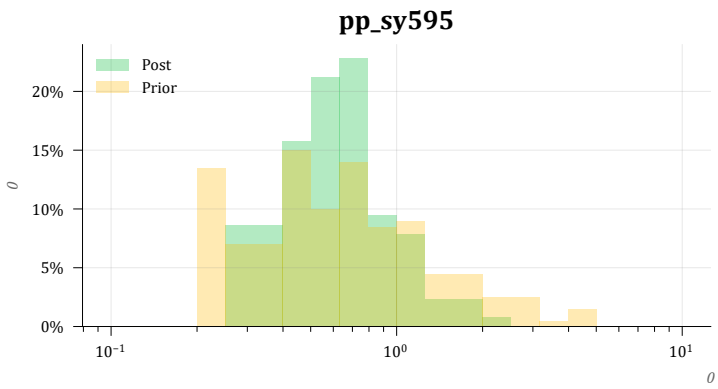

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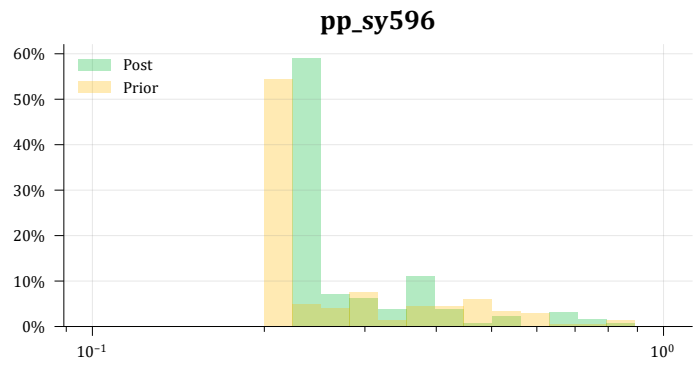

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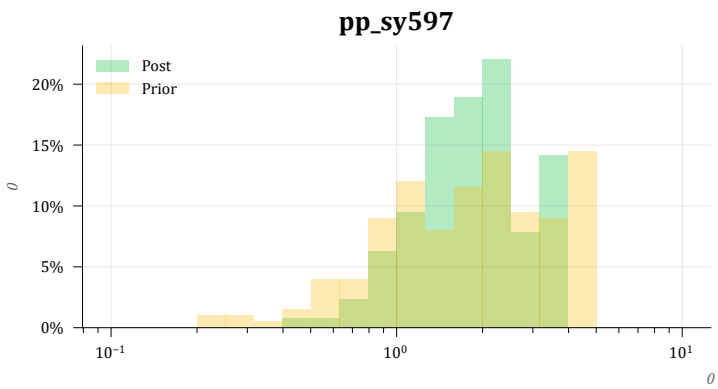

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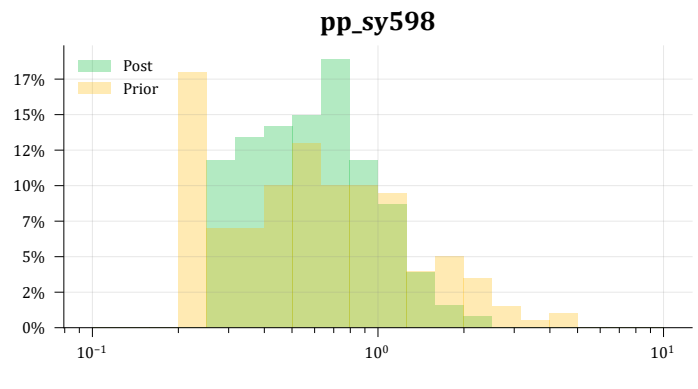

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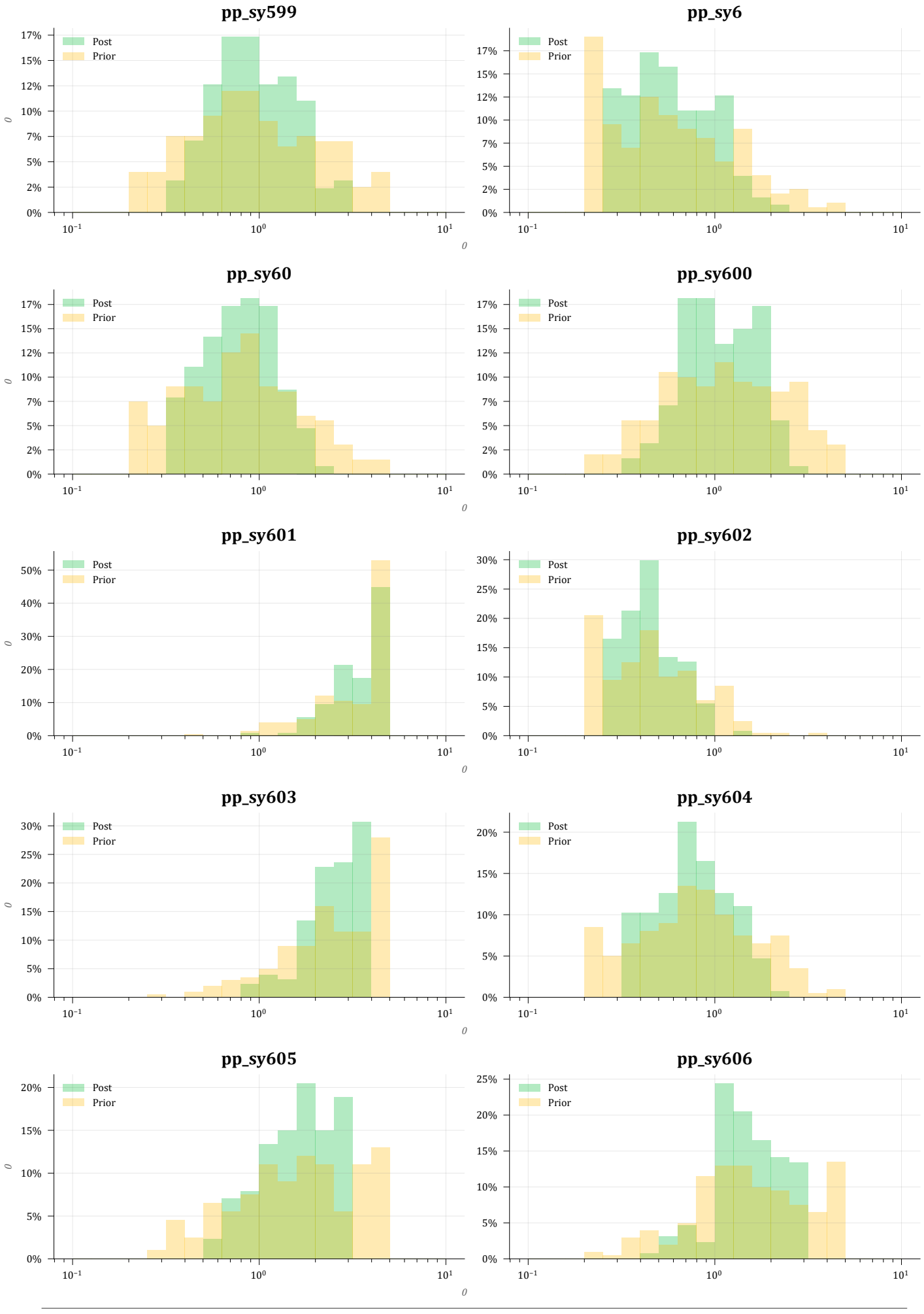

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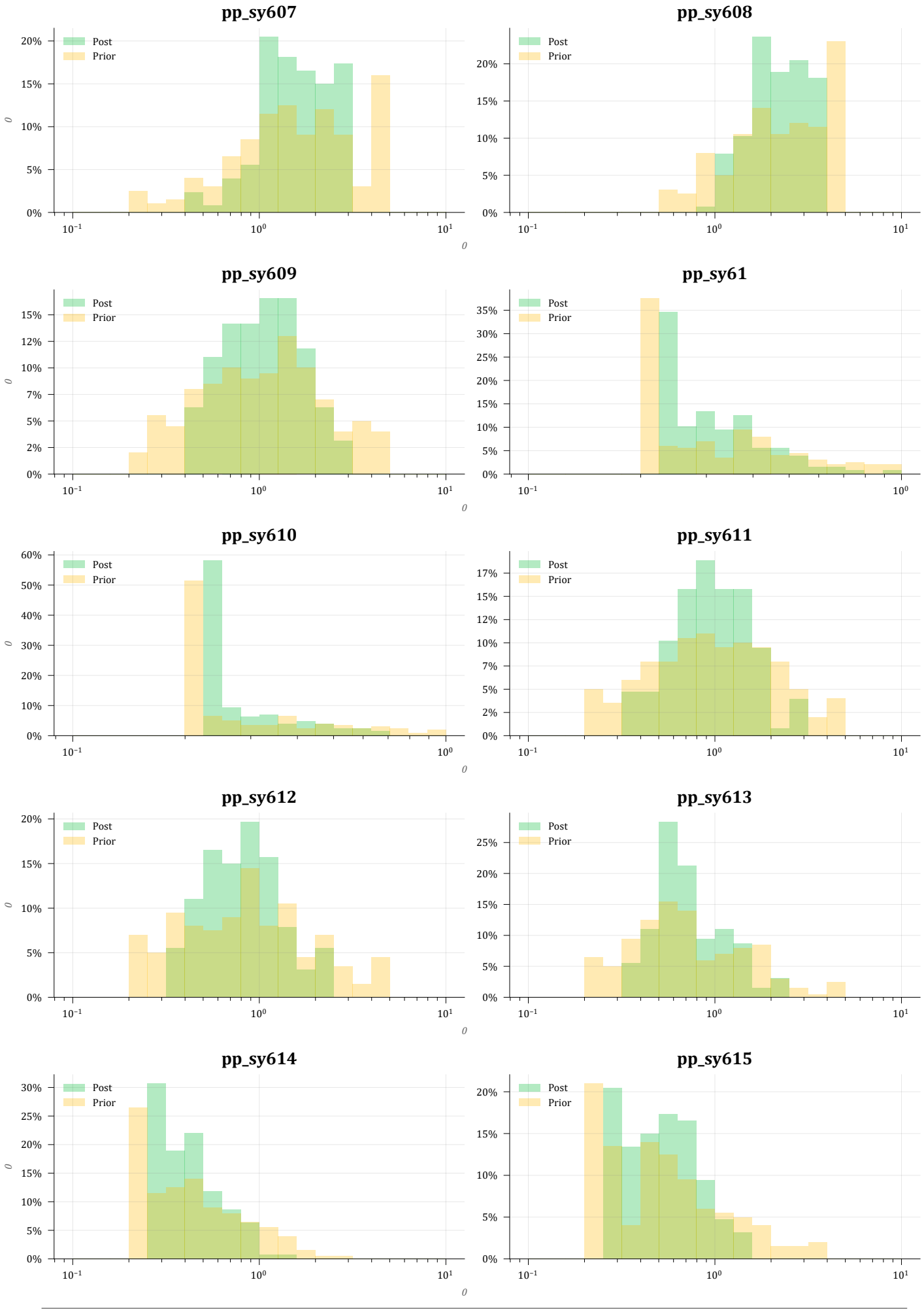

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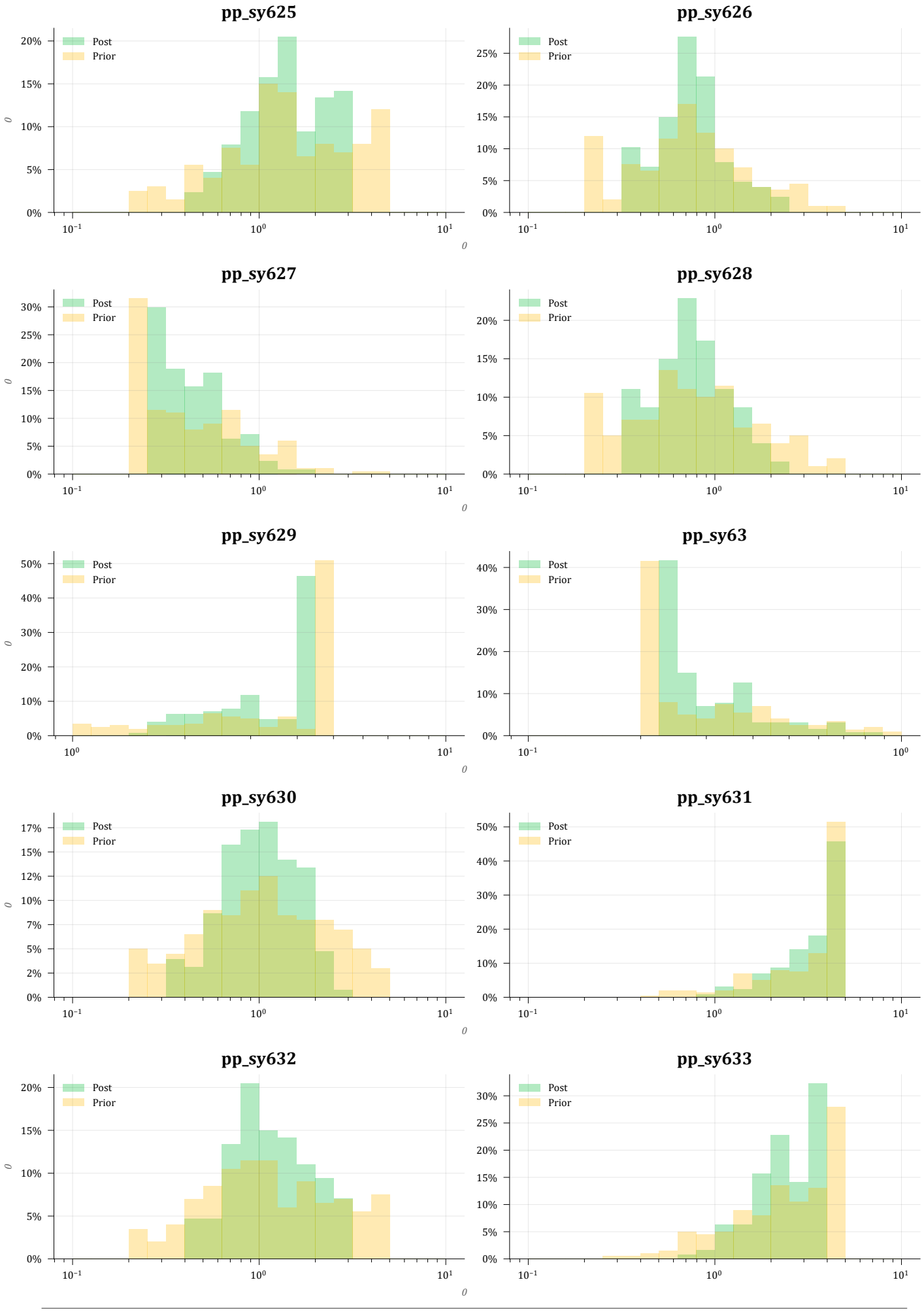

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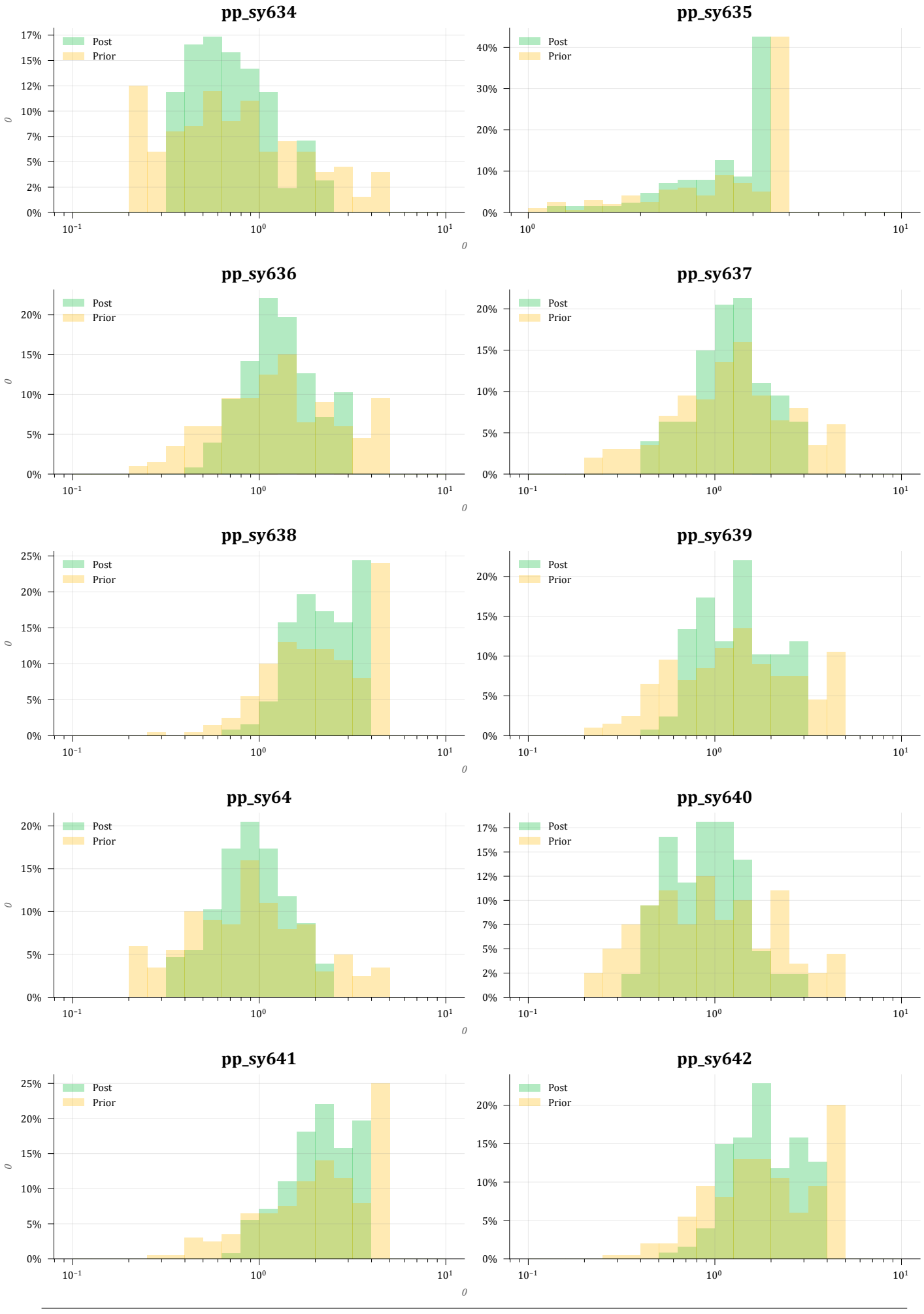

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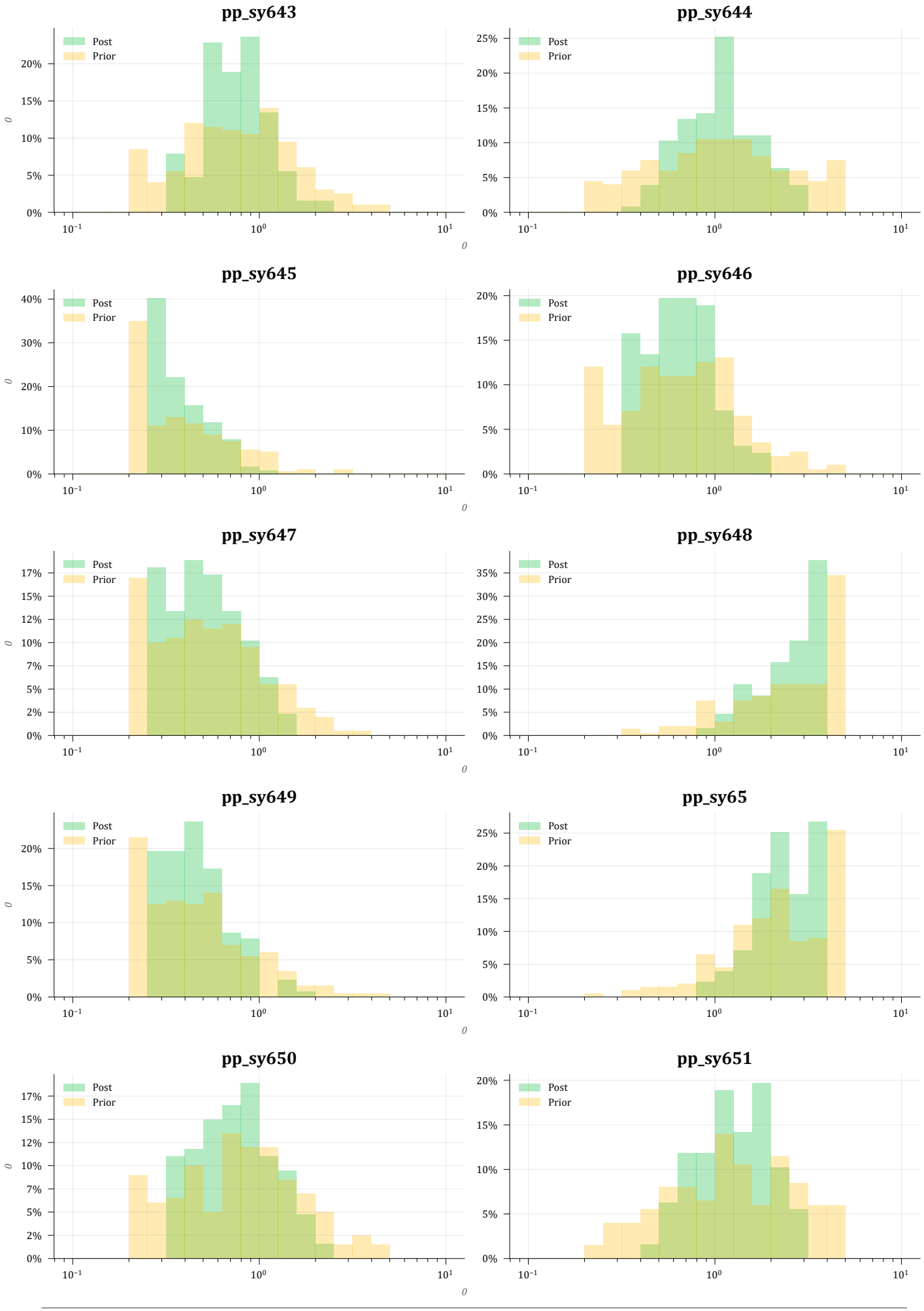

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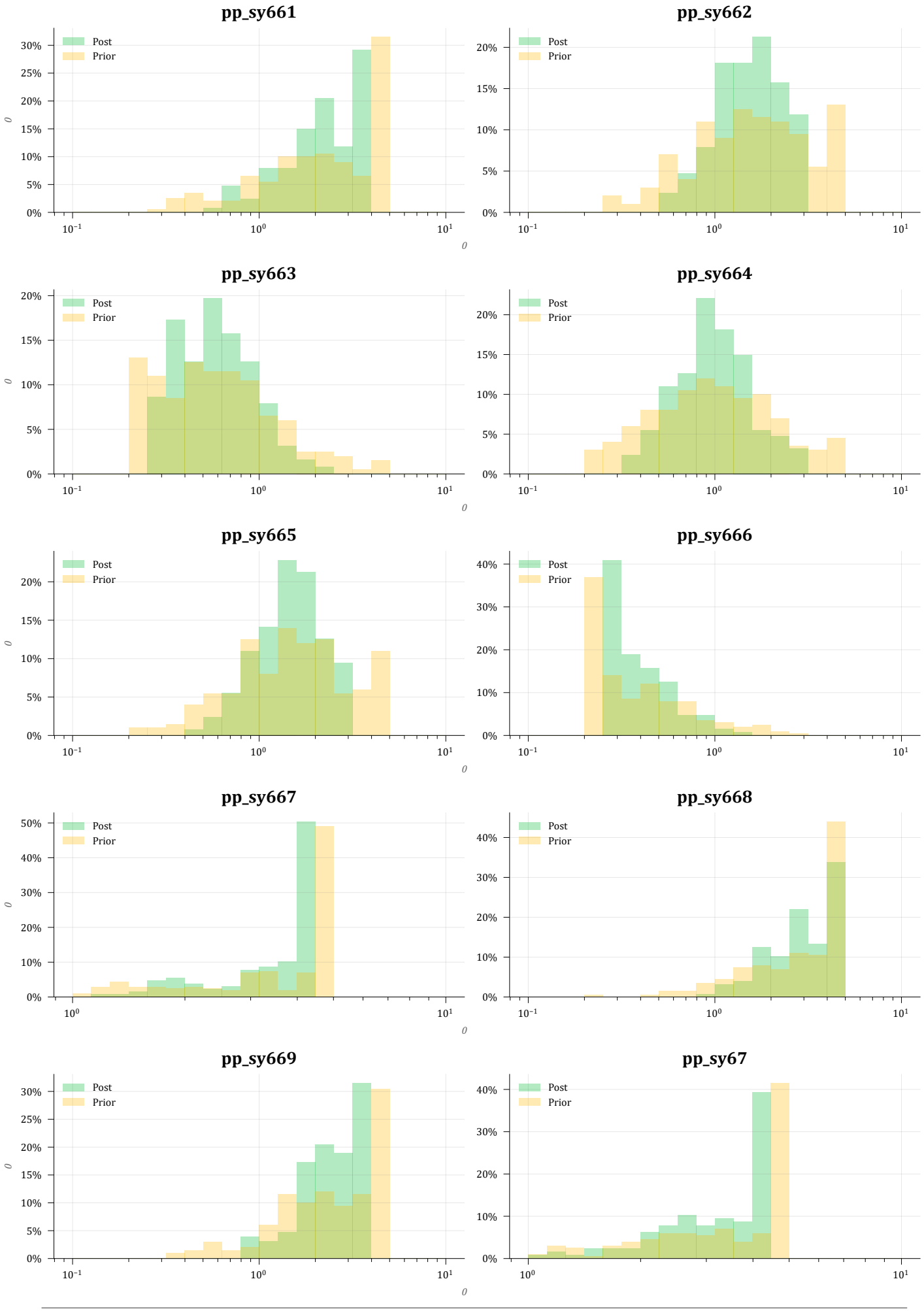

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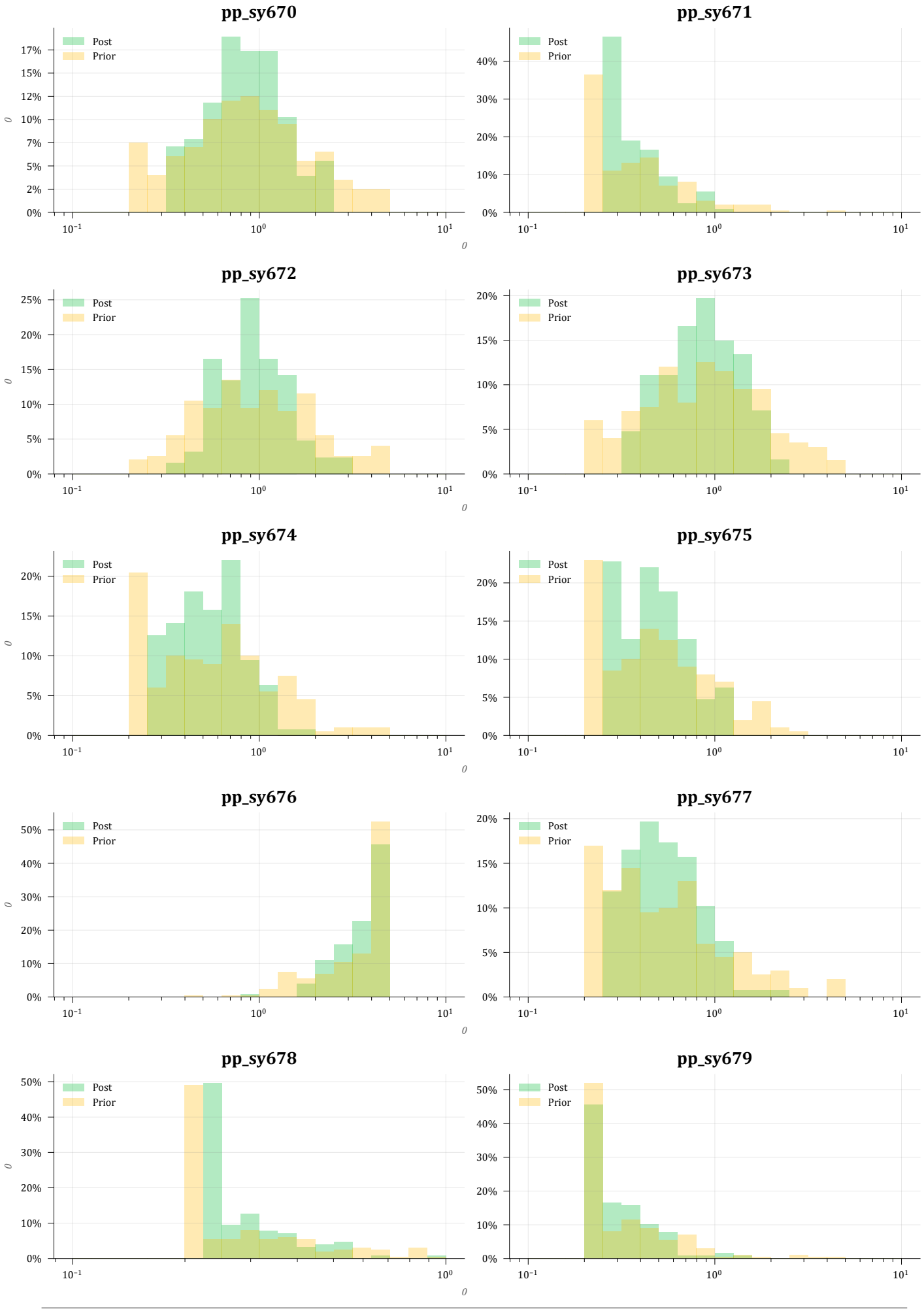

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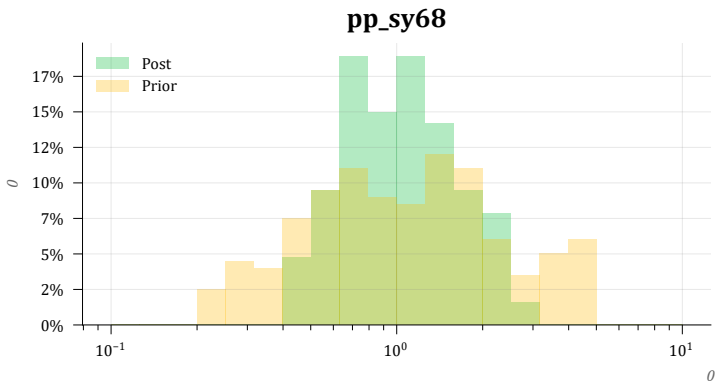

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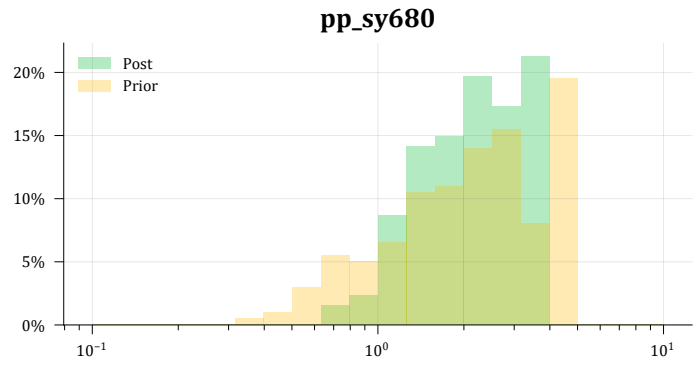

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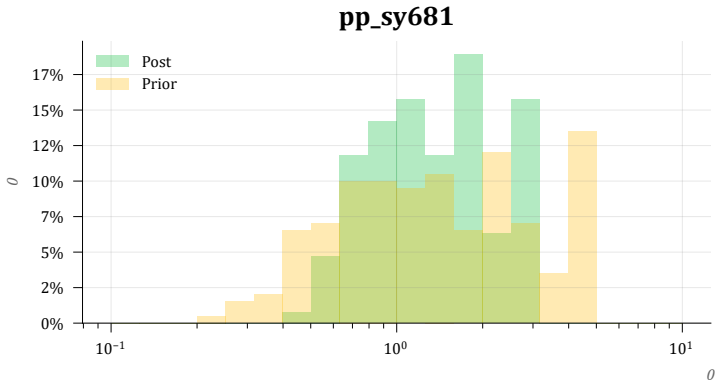

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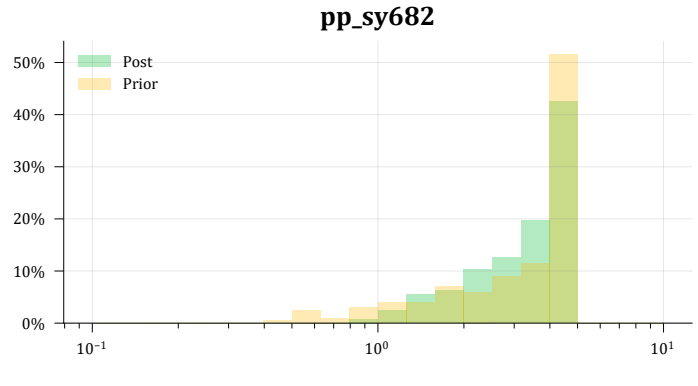

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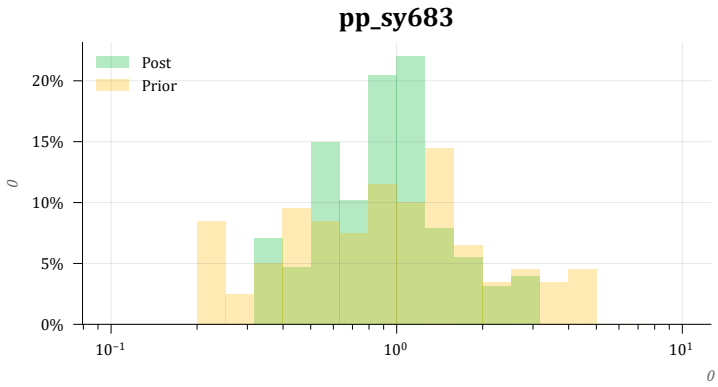

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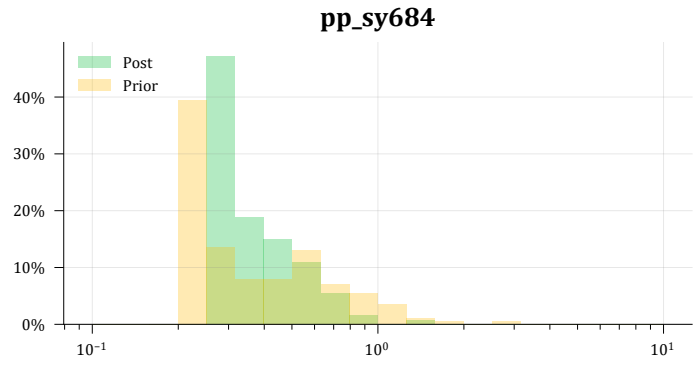

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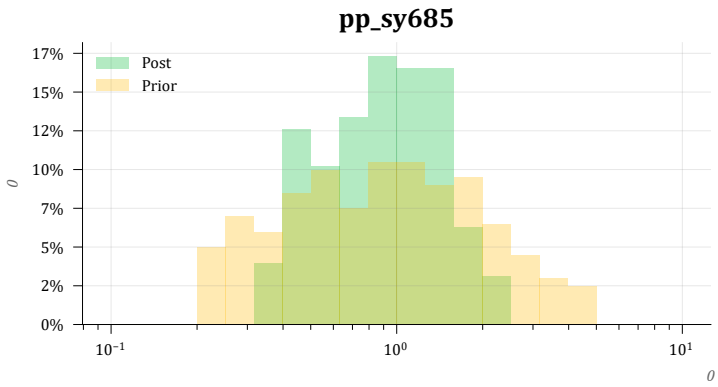

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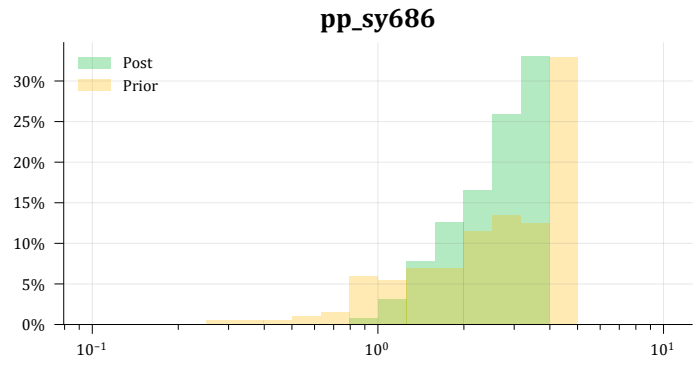

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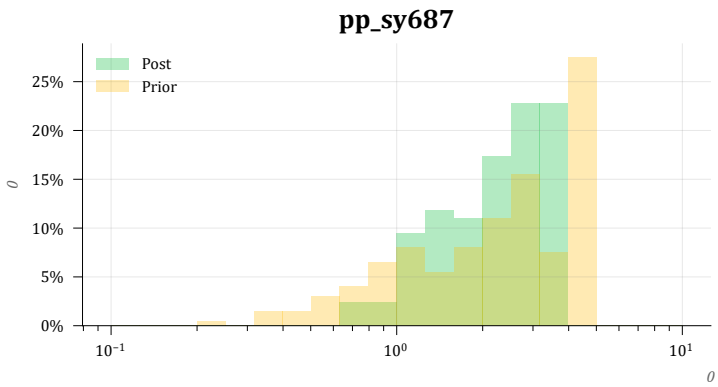

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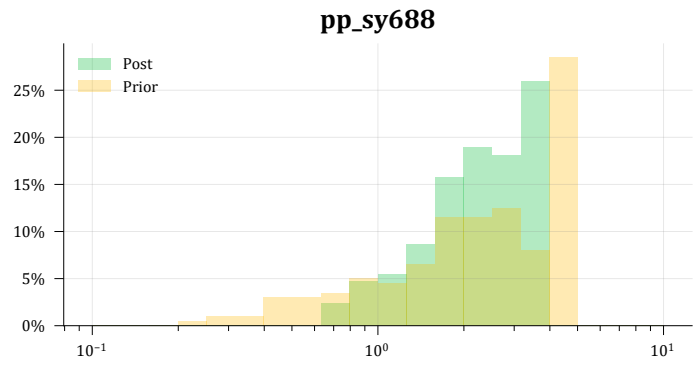

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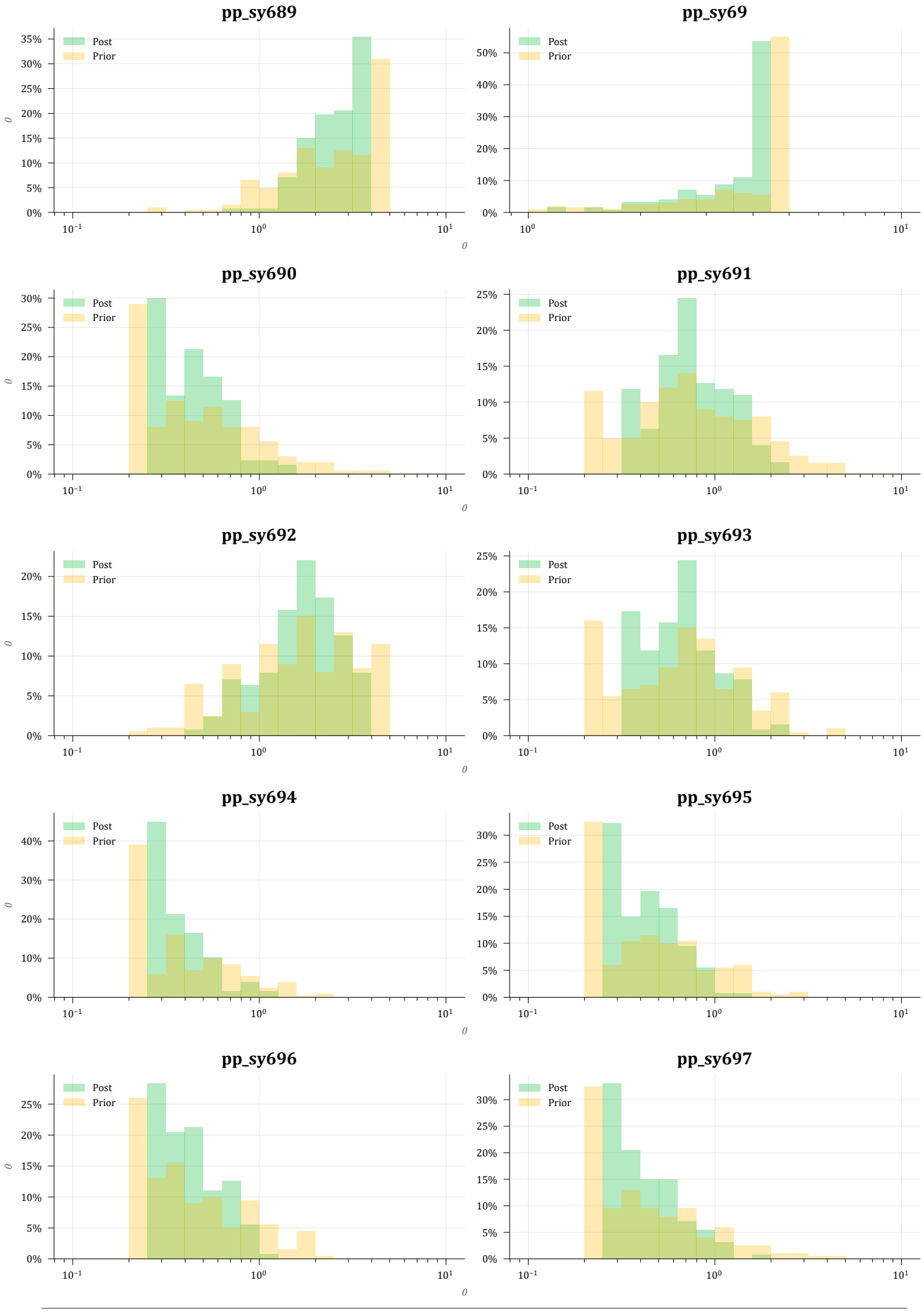

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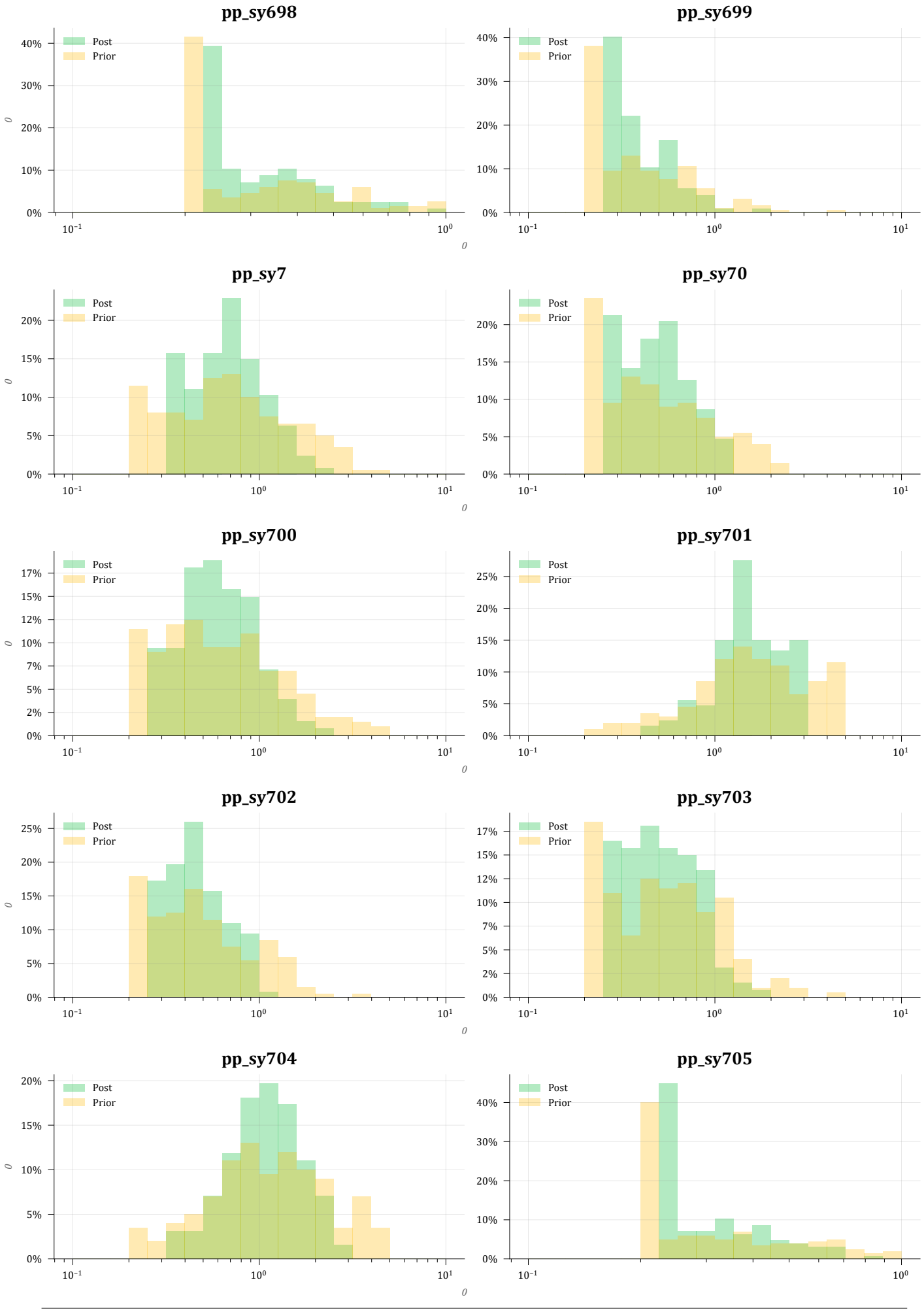

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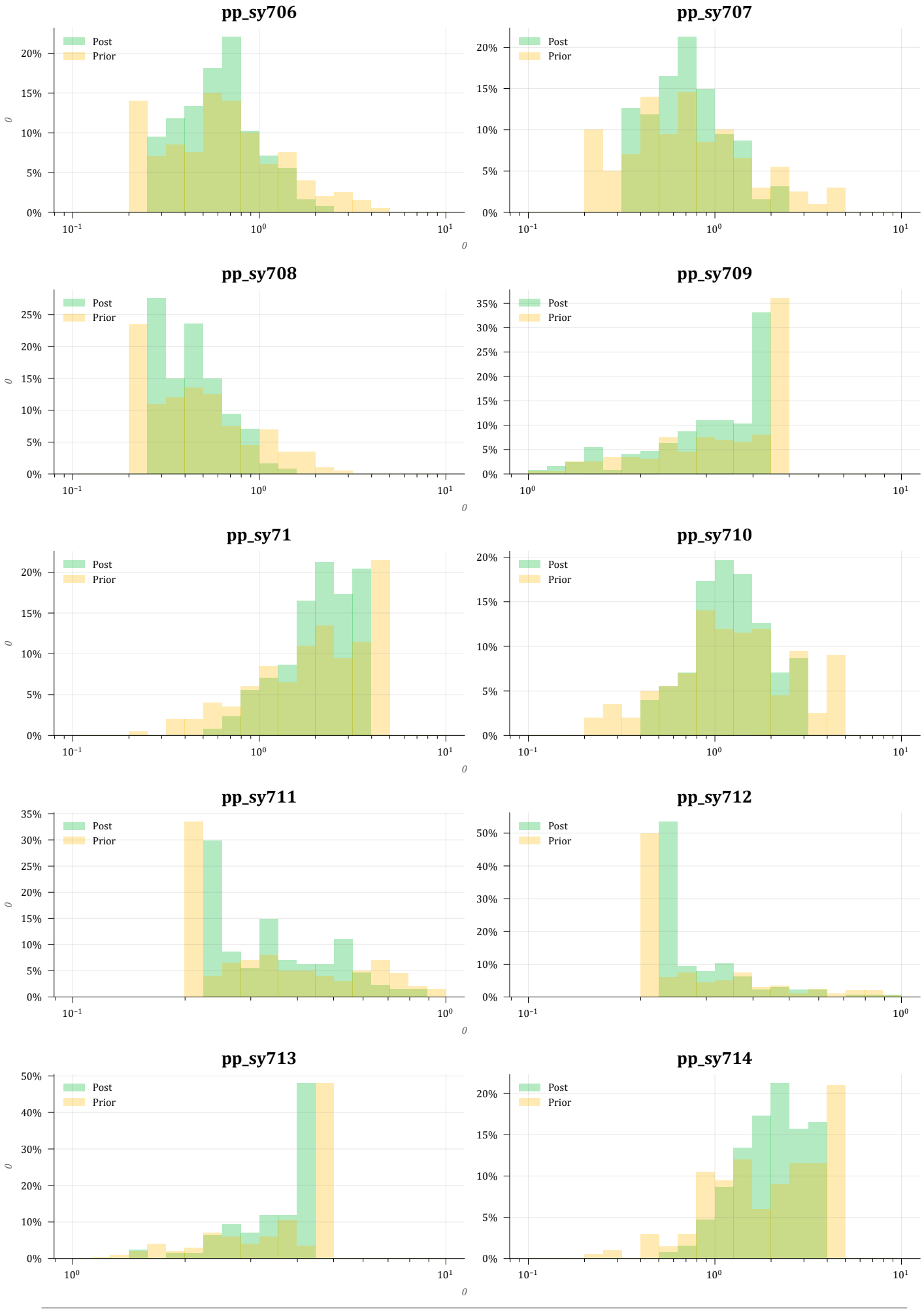

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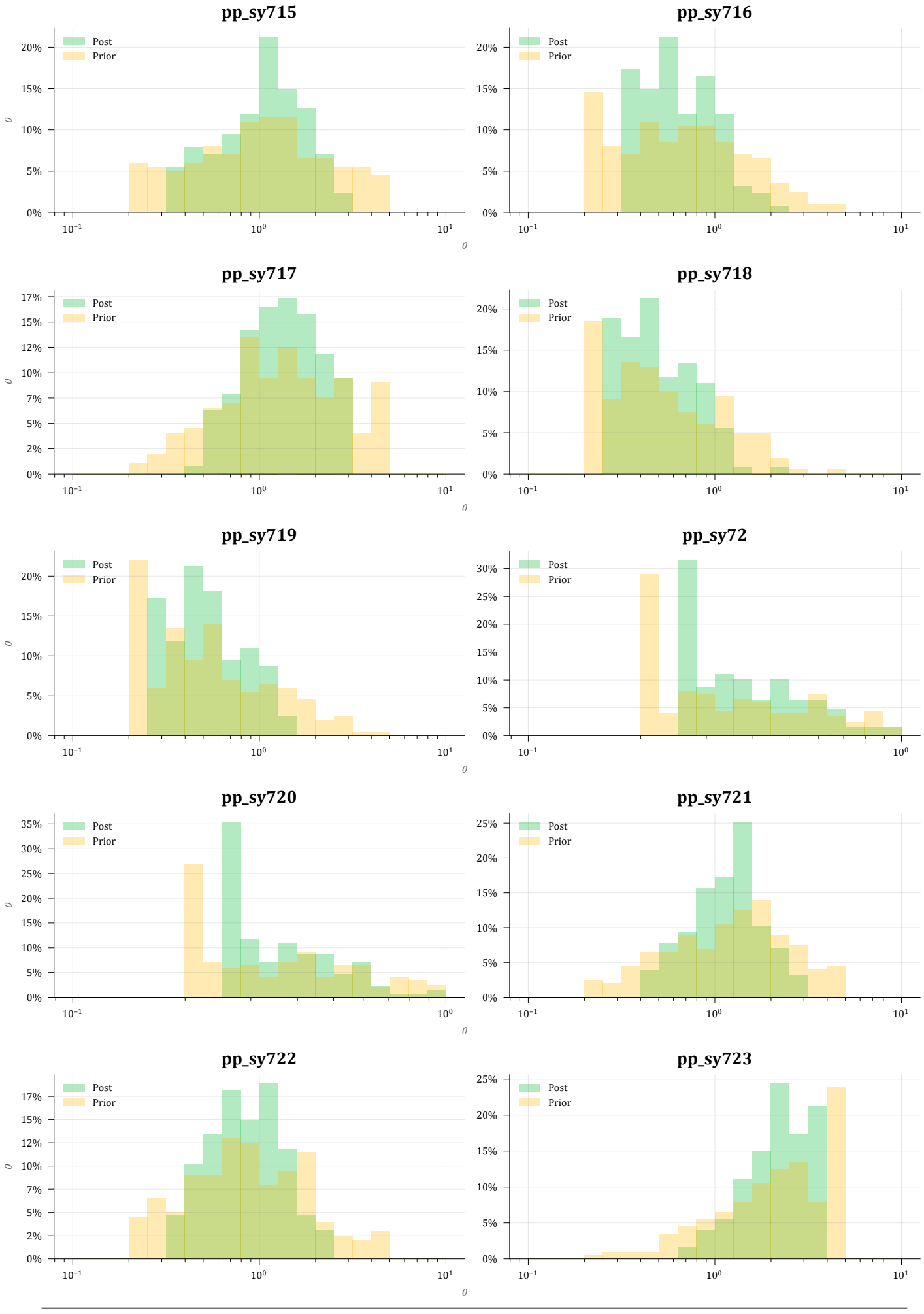

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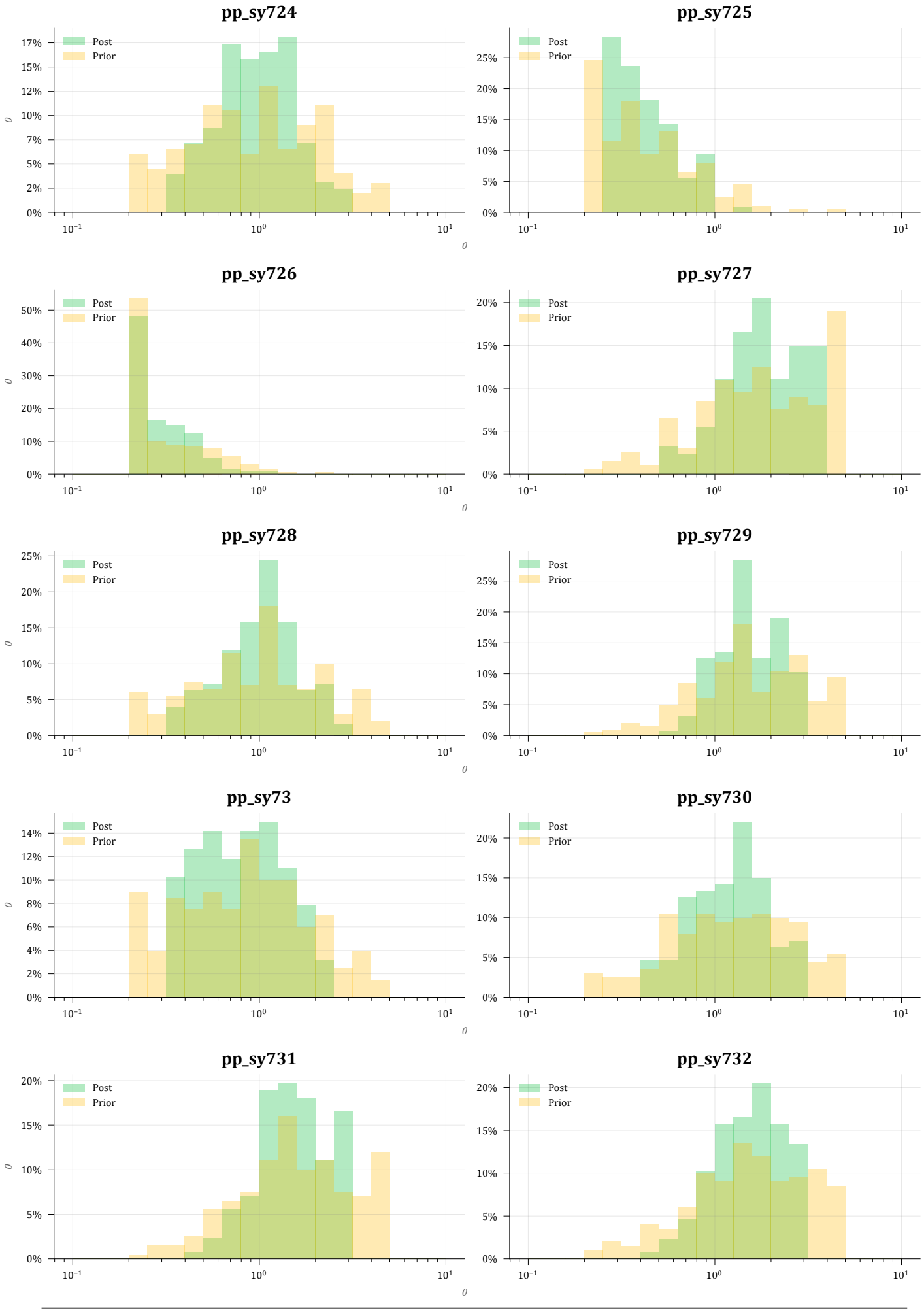

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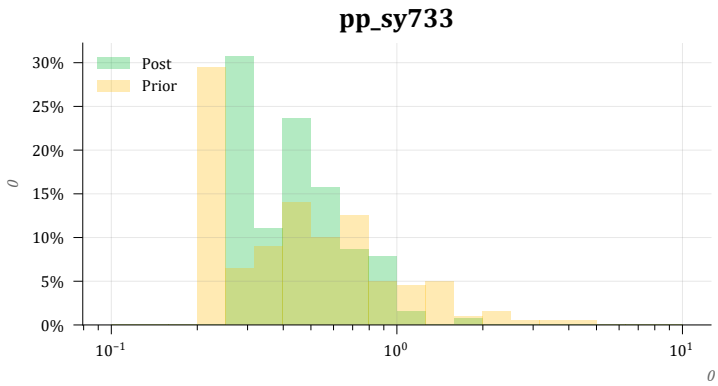

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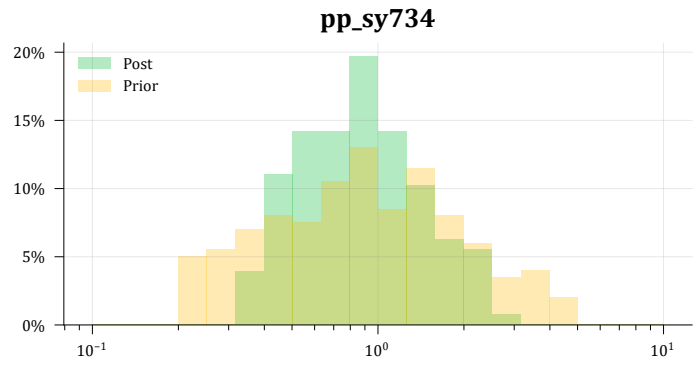

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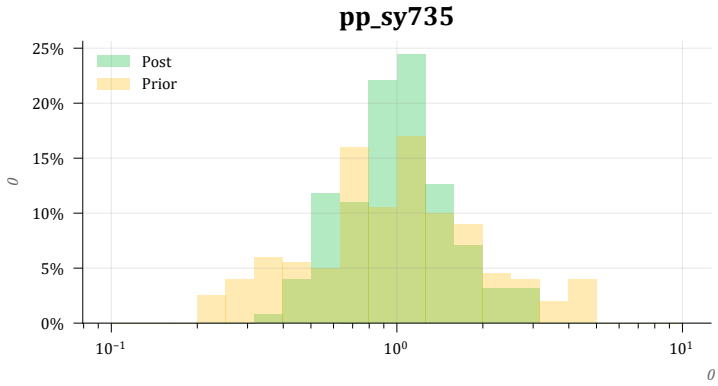

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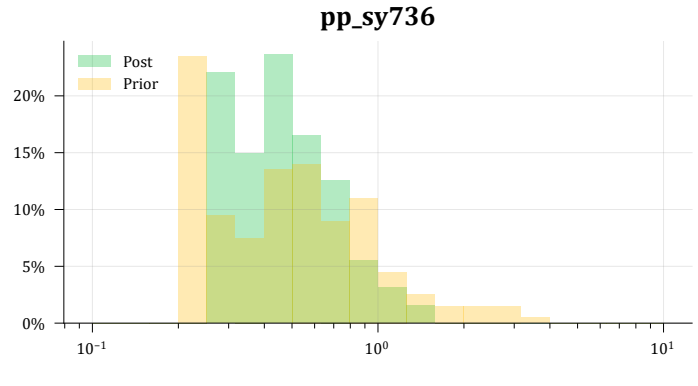

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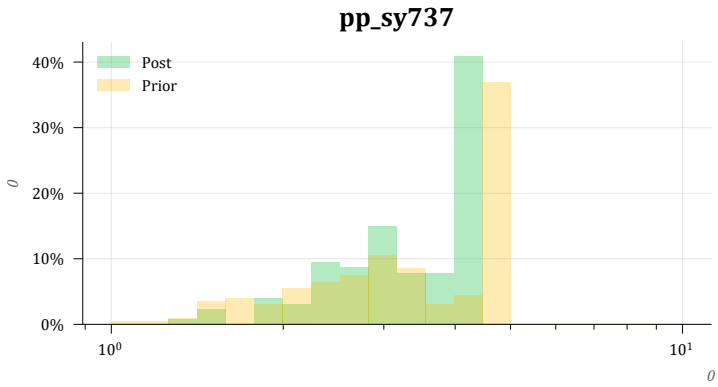

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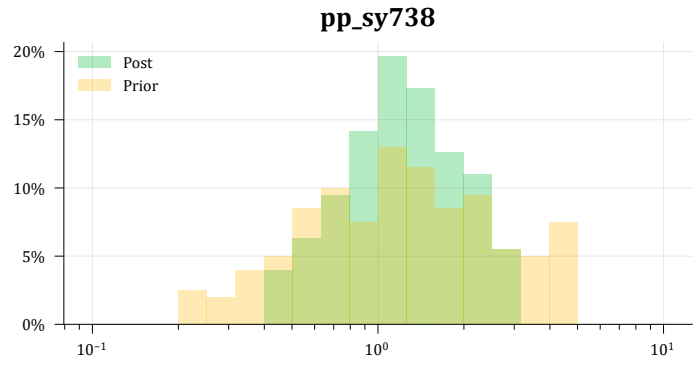

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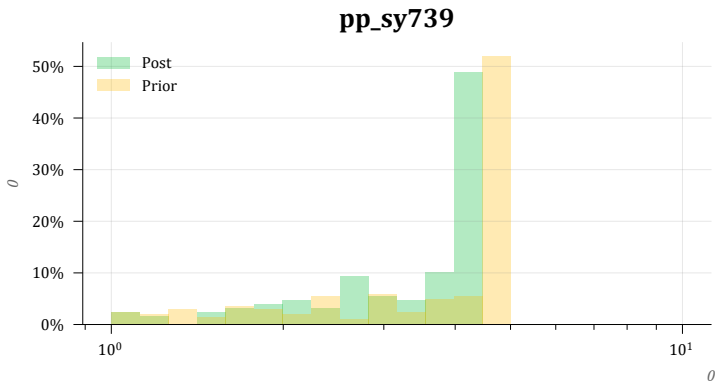

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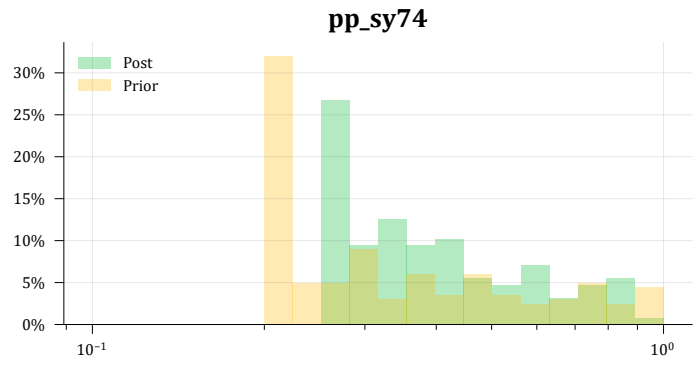

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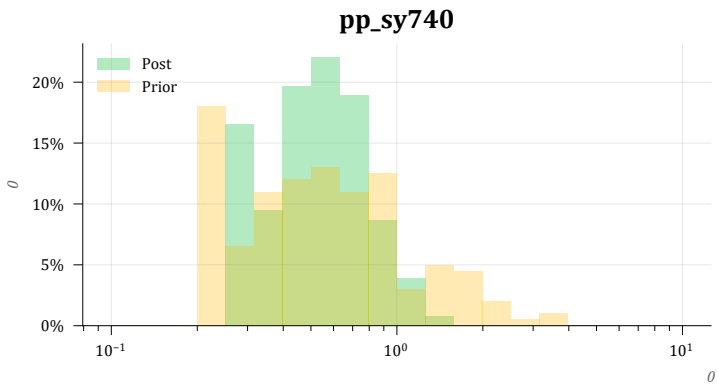

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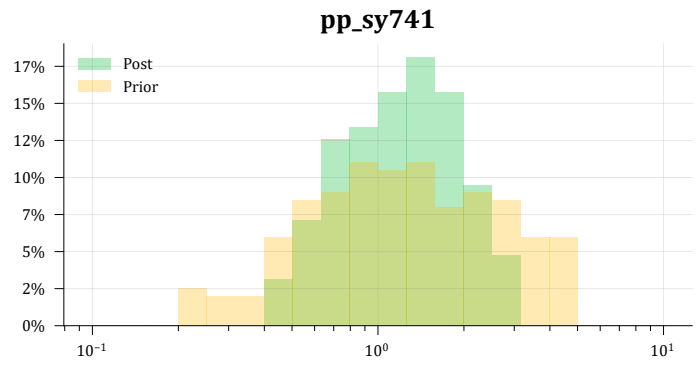

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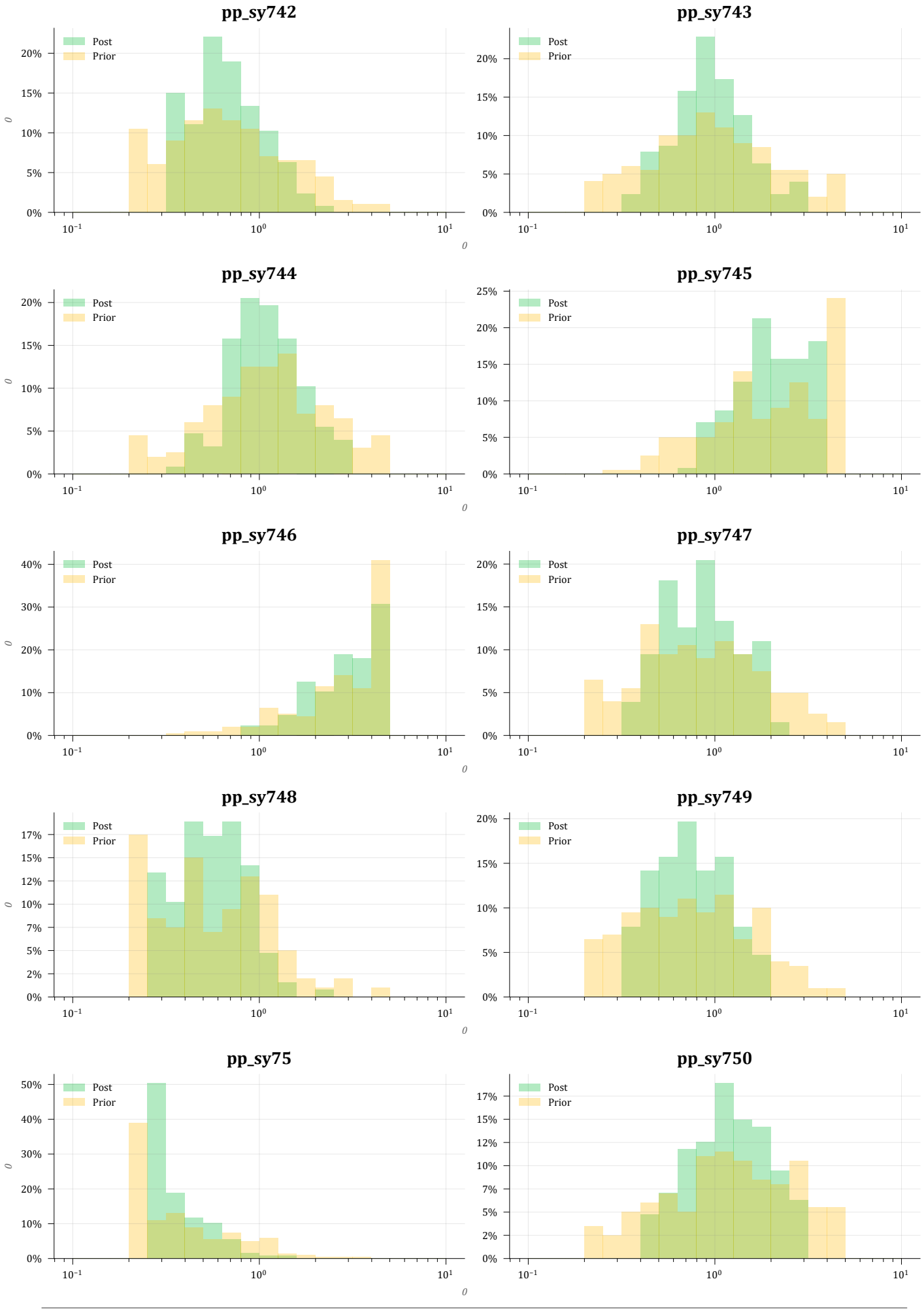

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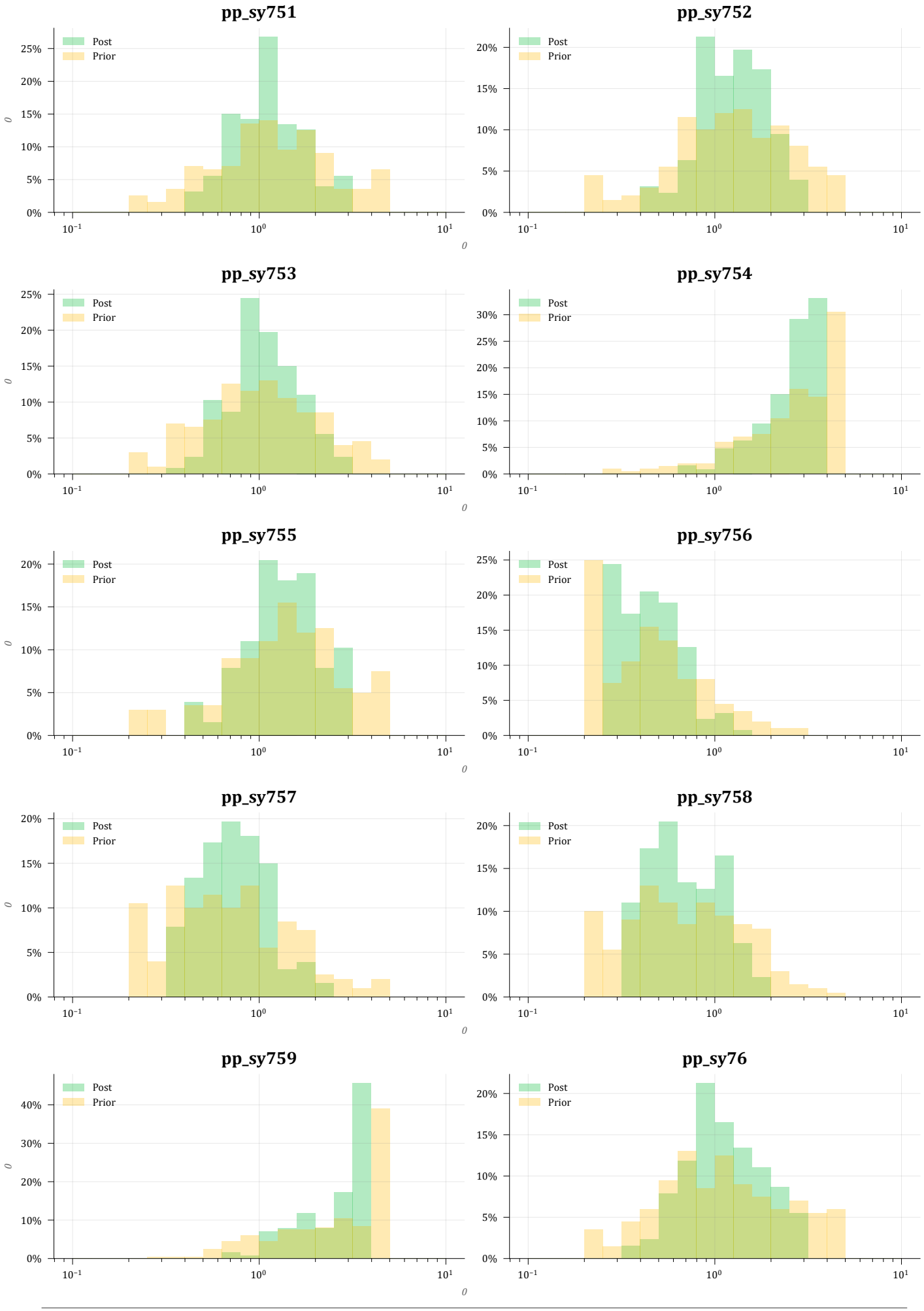

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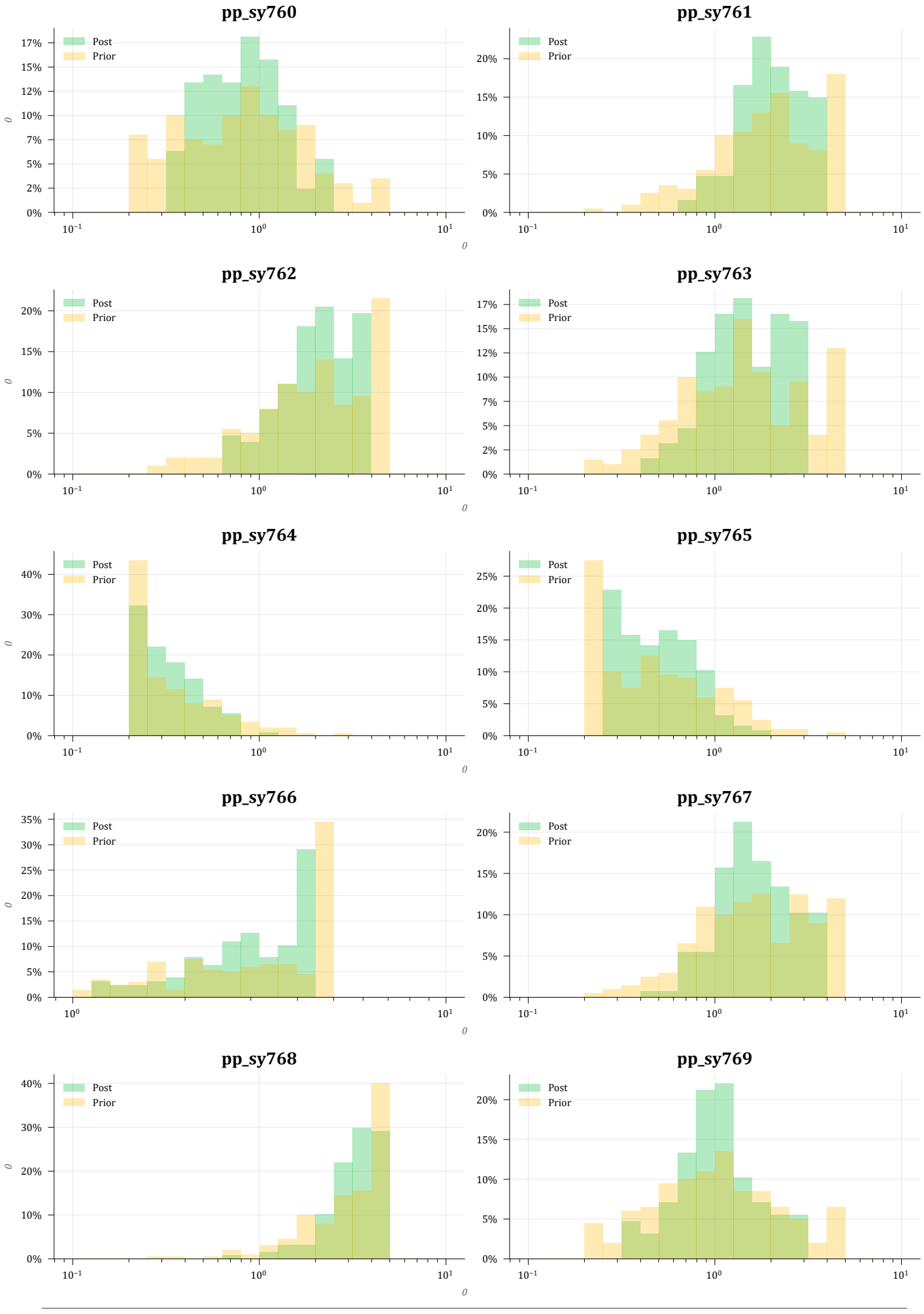

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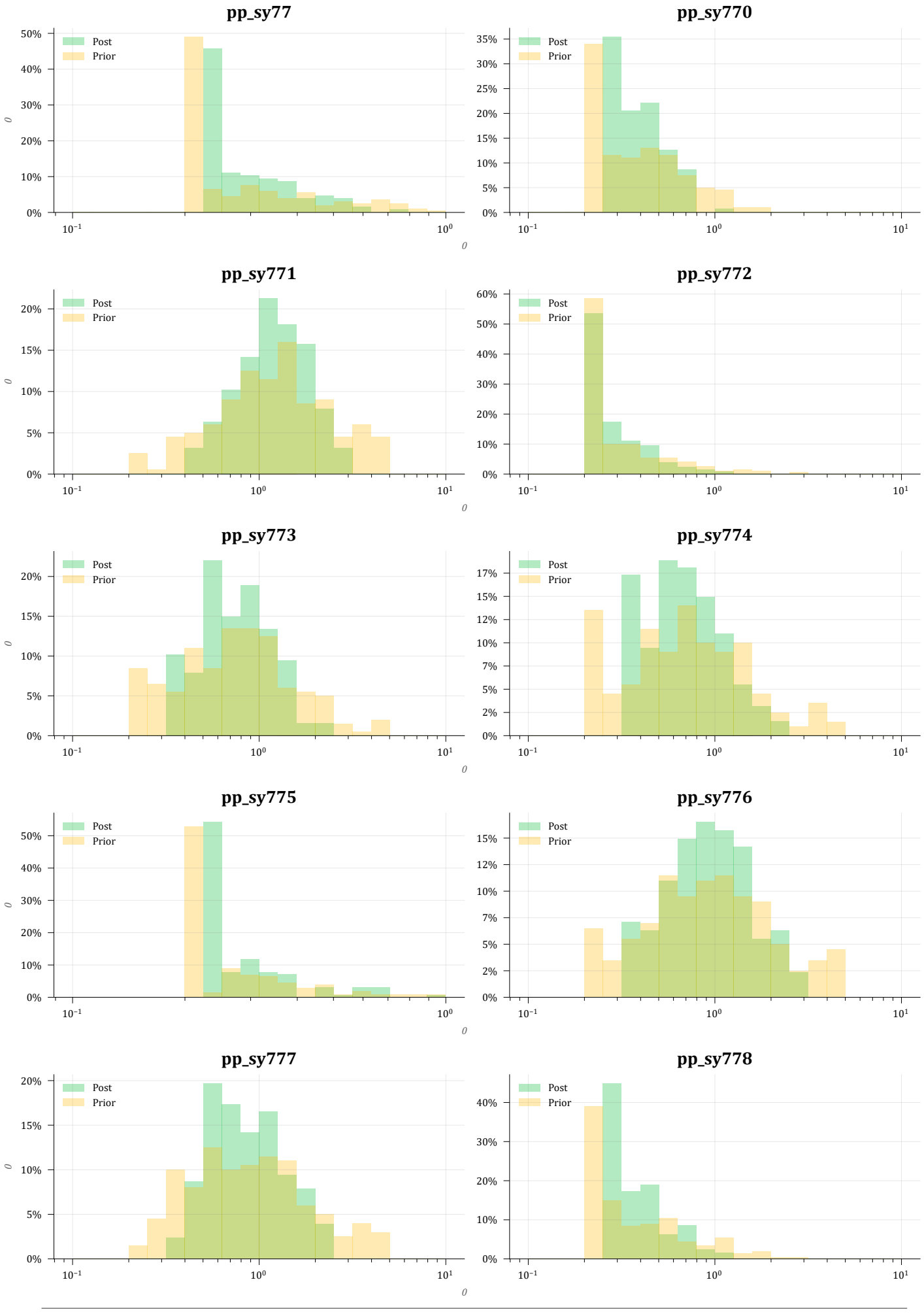

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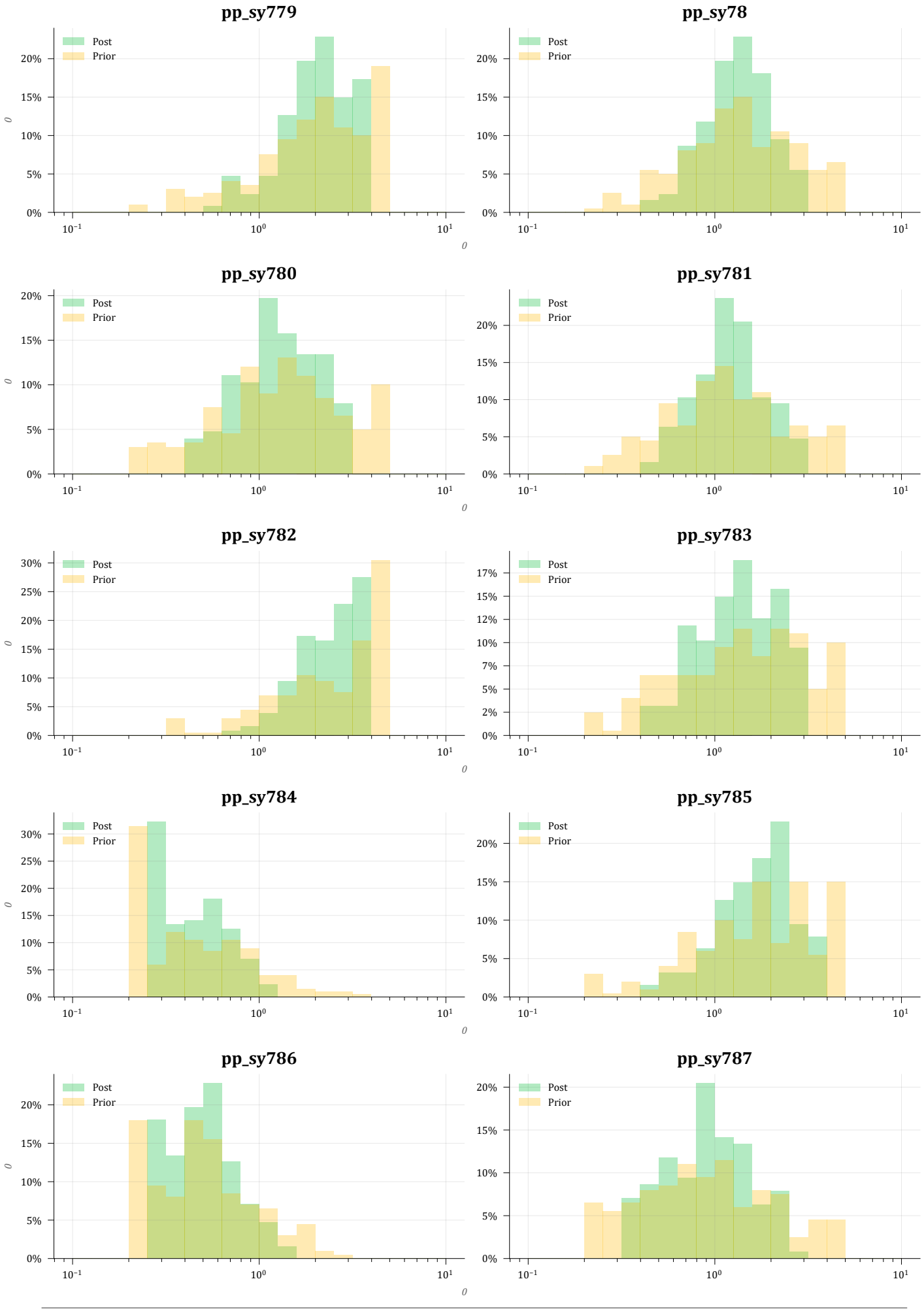

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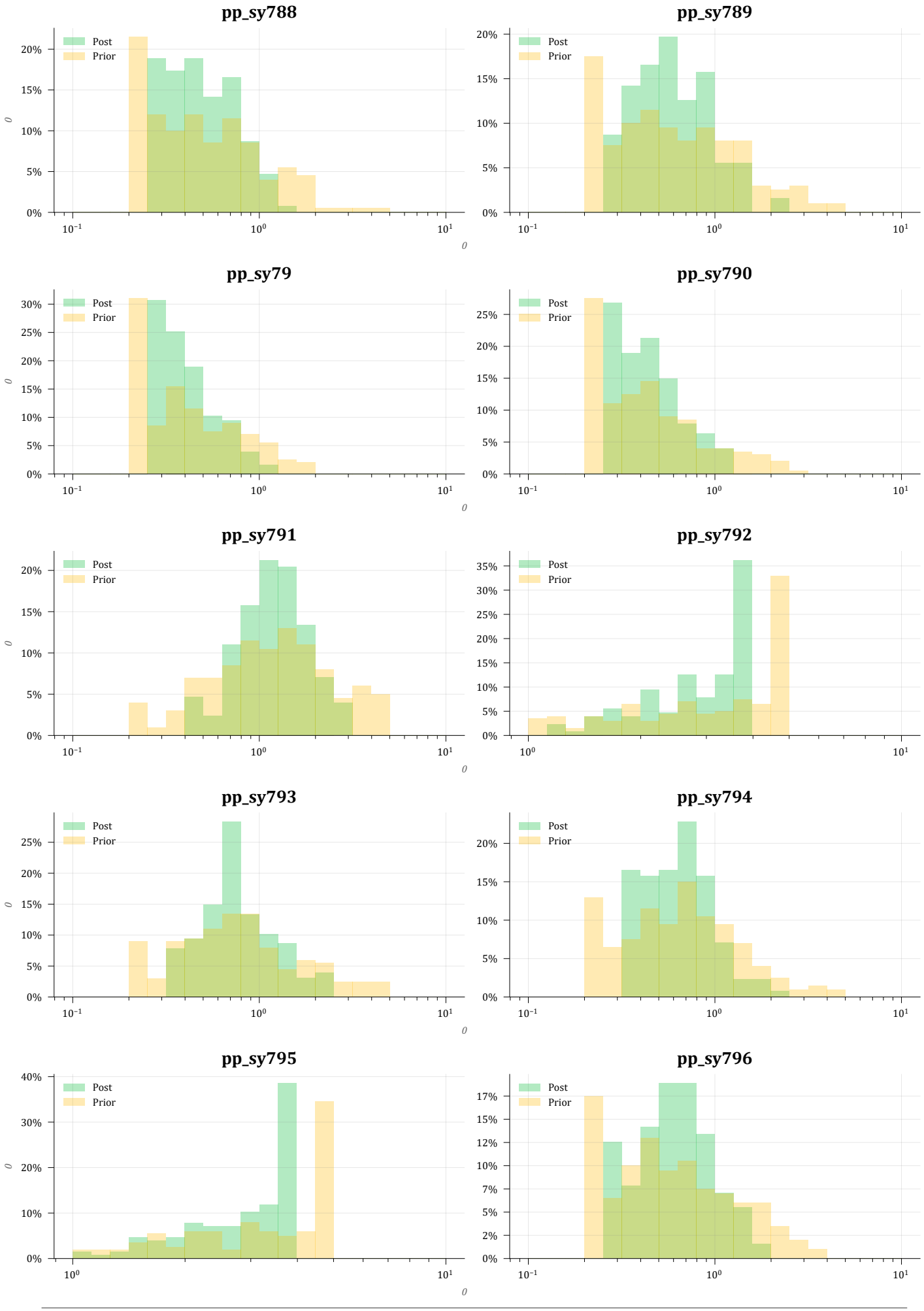

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pp_sy748
pp_sy749
pp_sy75
pp_sy750
Post
Prior
0
Parameters


pp_sy751
pp_sy752
pp_sy753
pp_sy754
pp_sy755
pp_sy756
pp_sy757
pp_sy758
pp_sy759
pp_sy76
Post
Prior
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Parameters


pp_sy760
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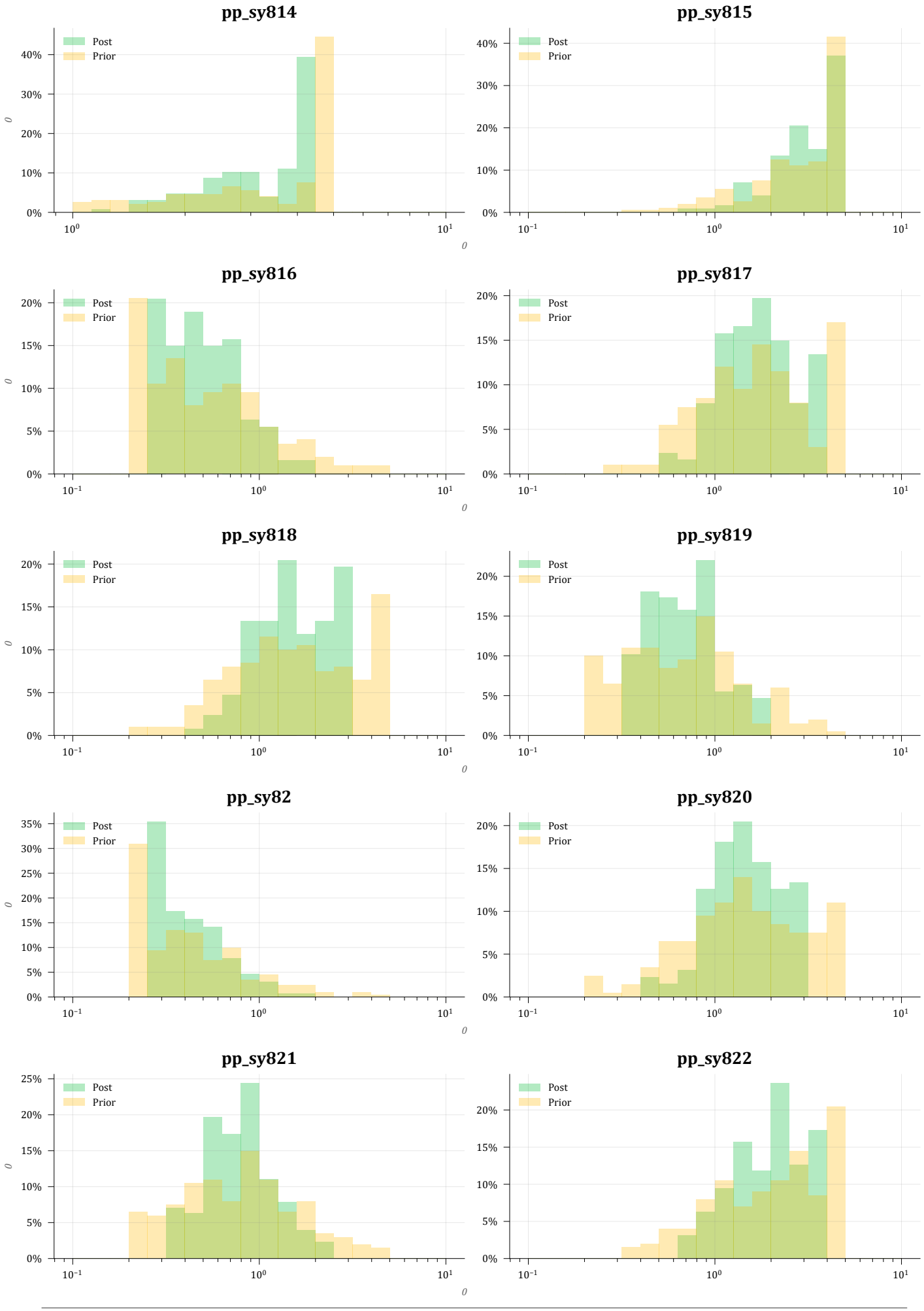

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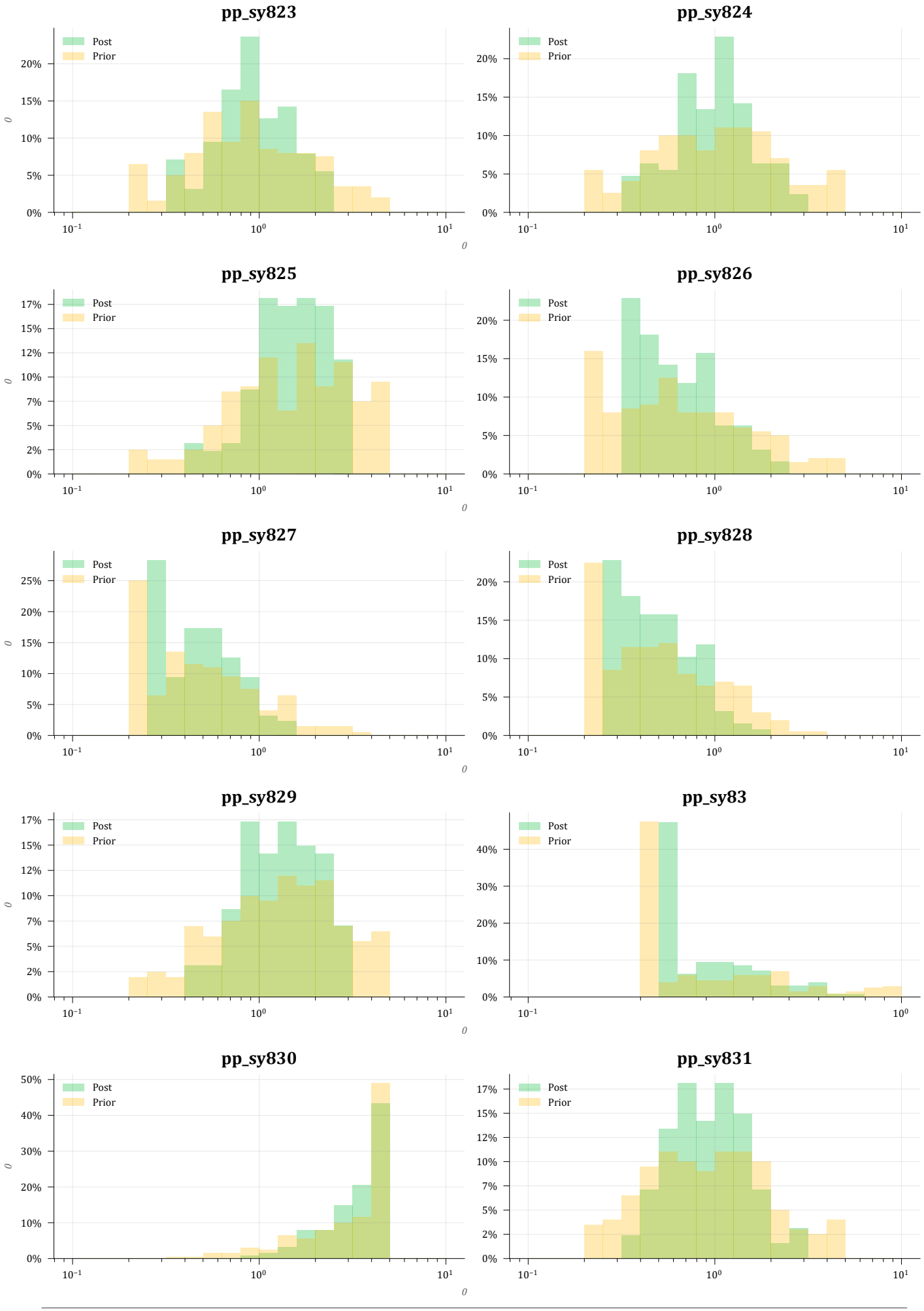

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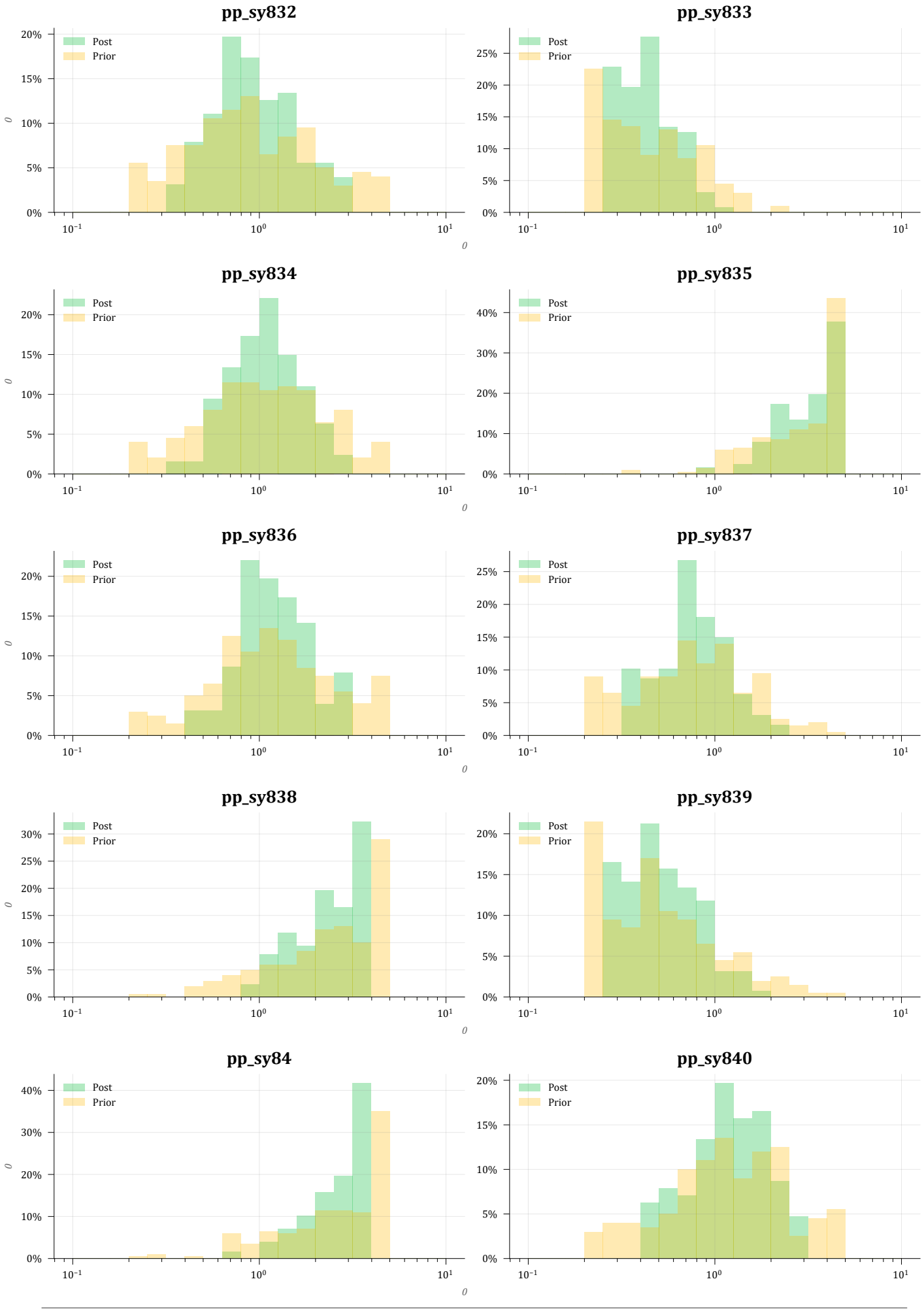

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Prior
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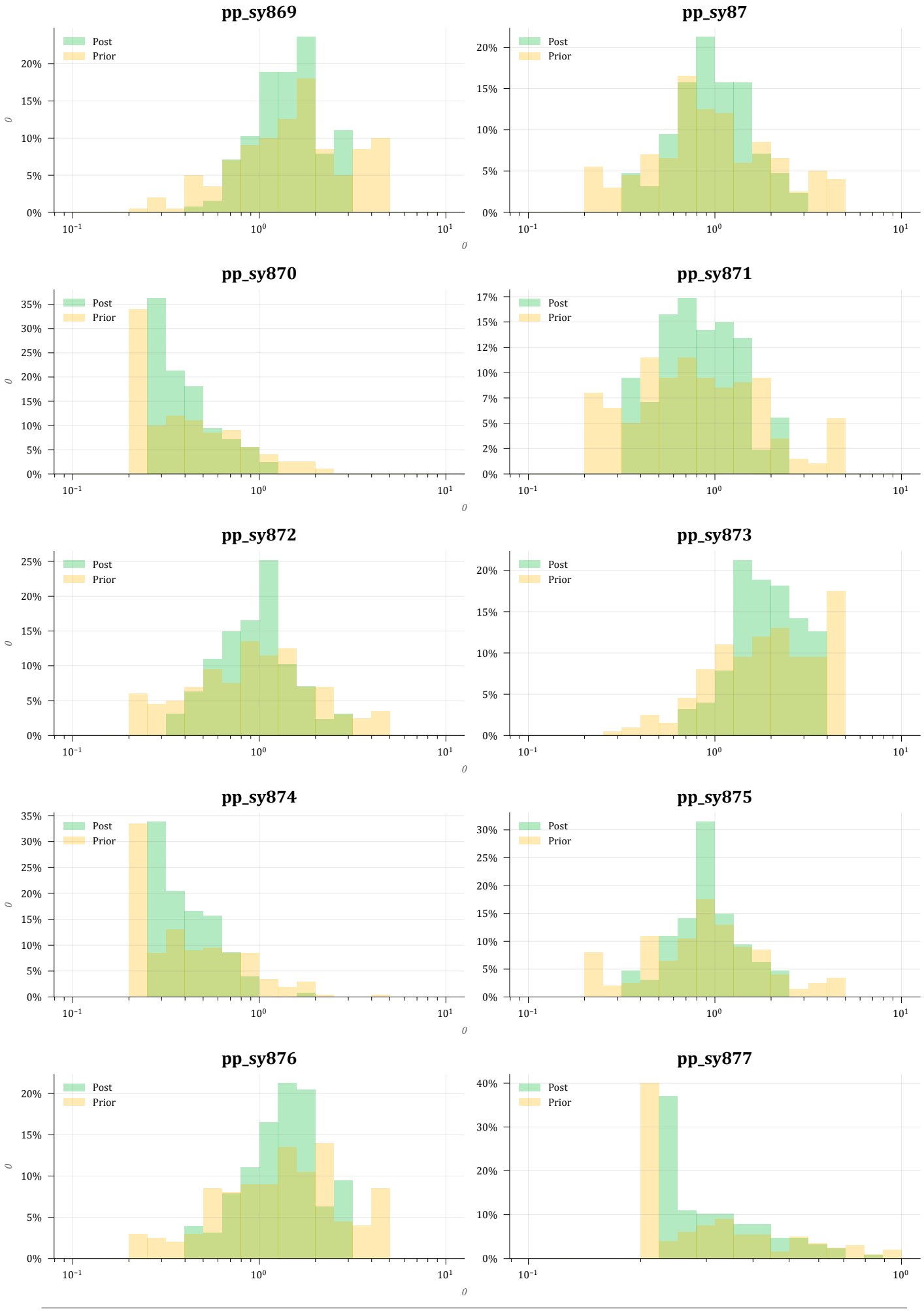

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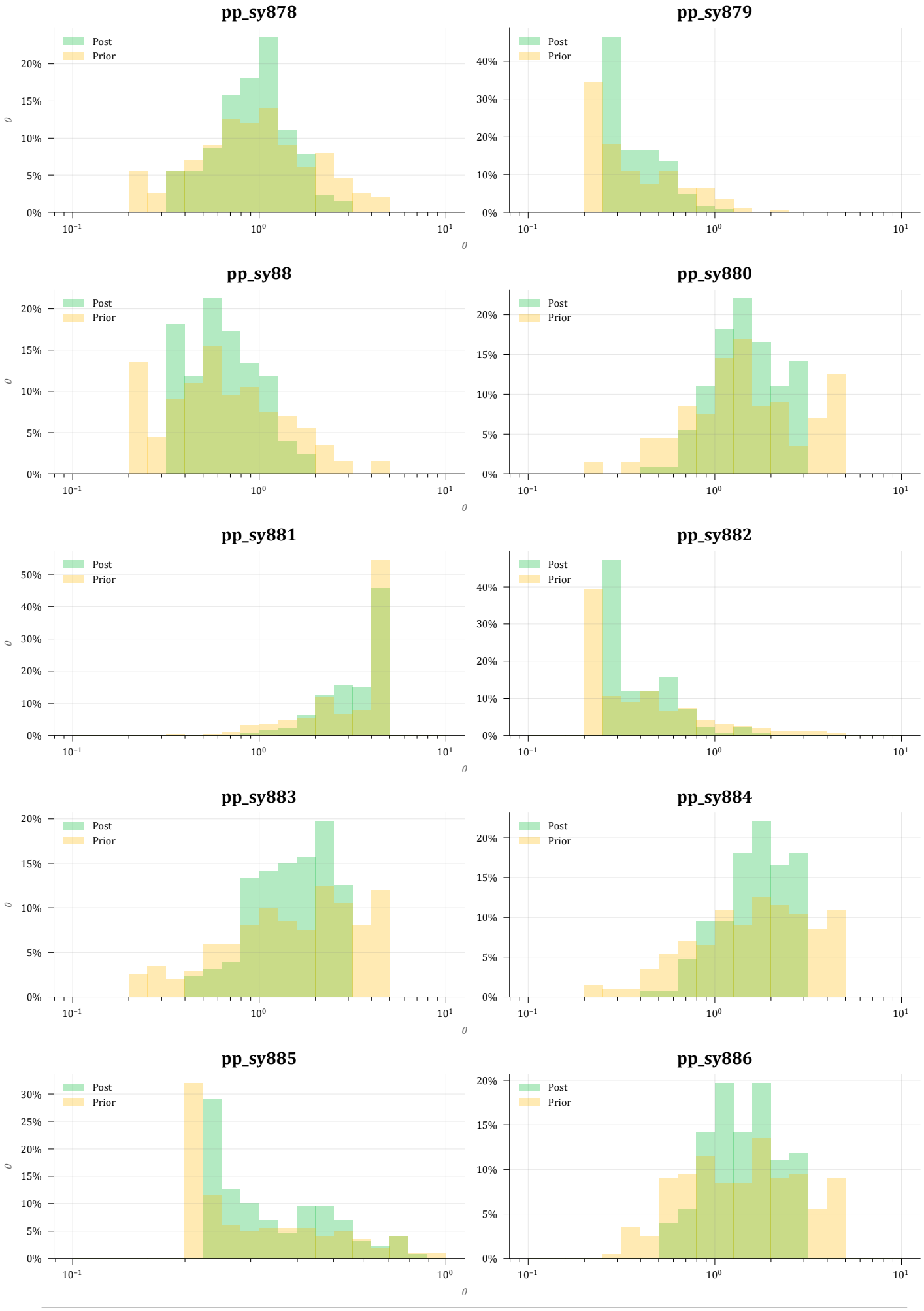

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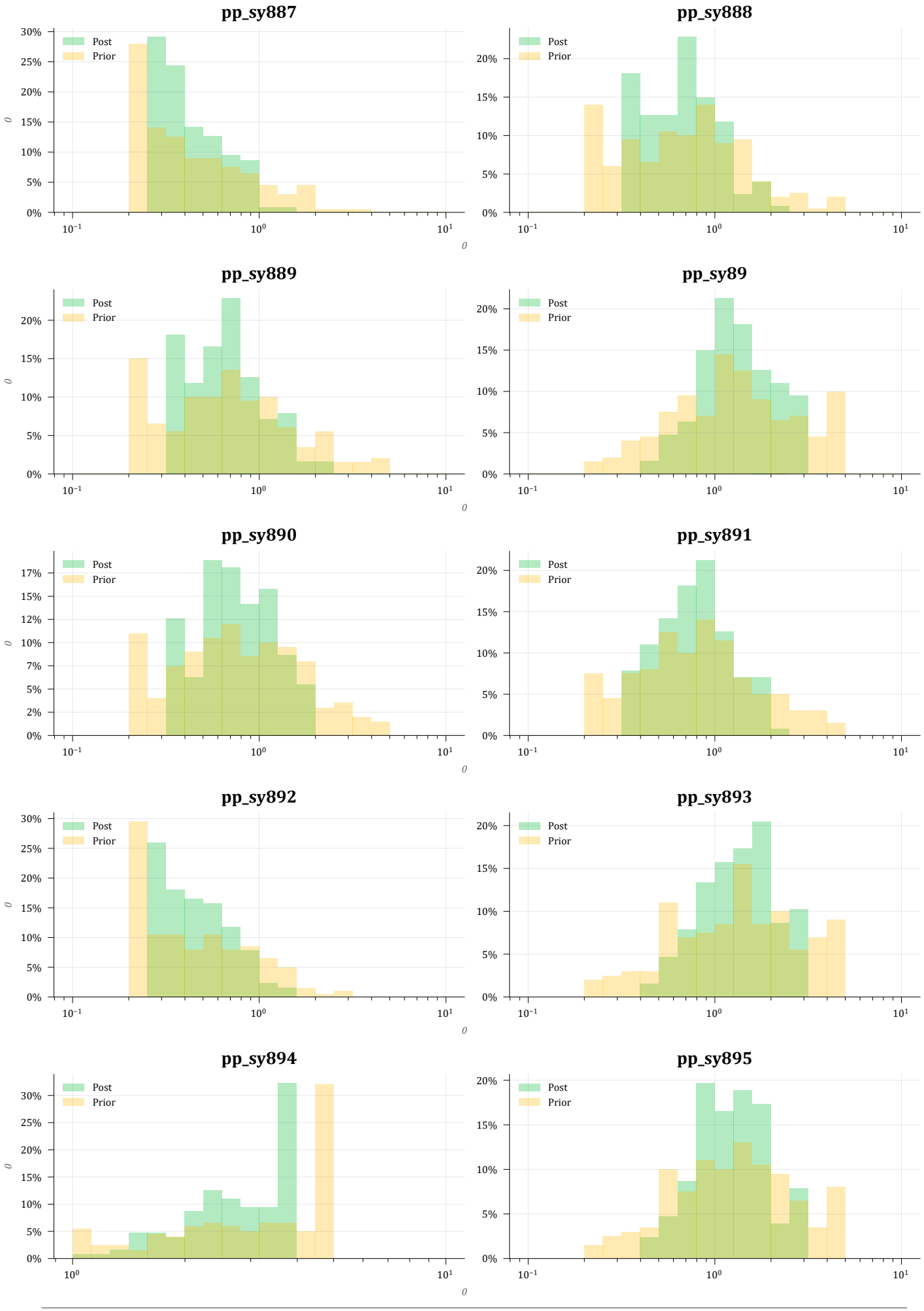

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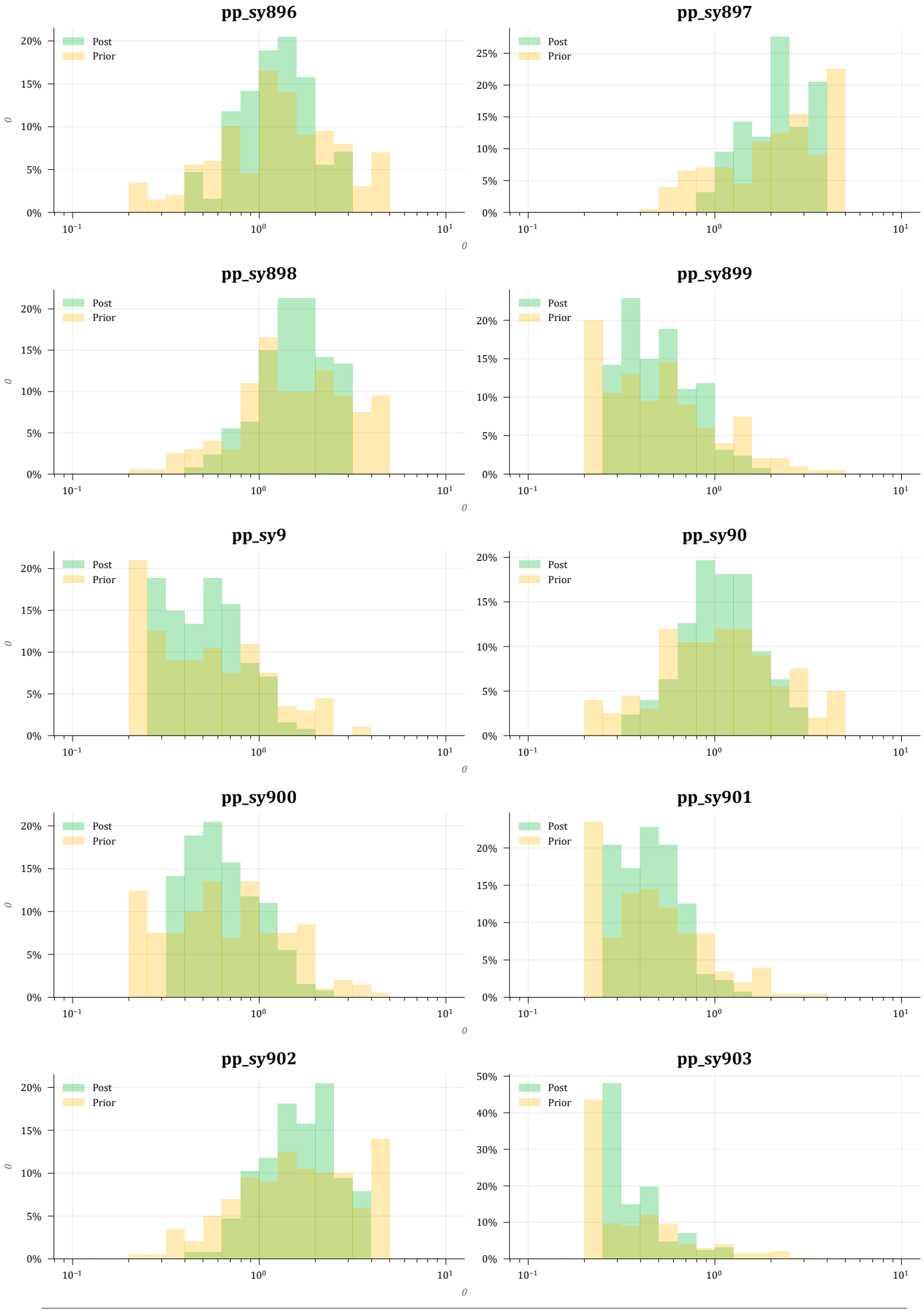

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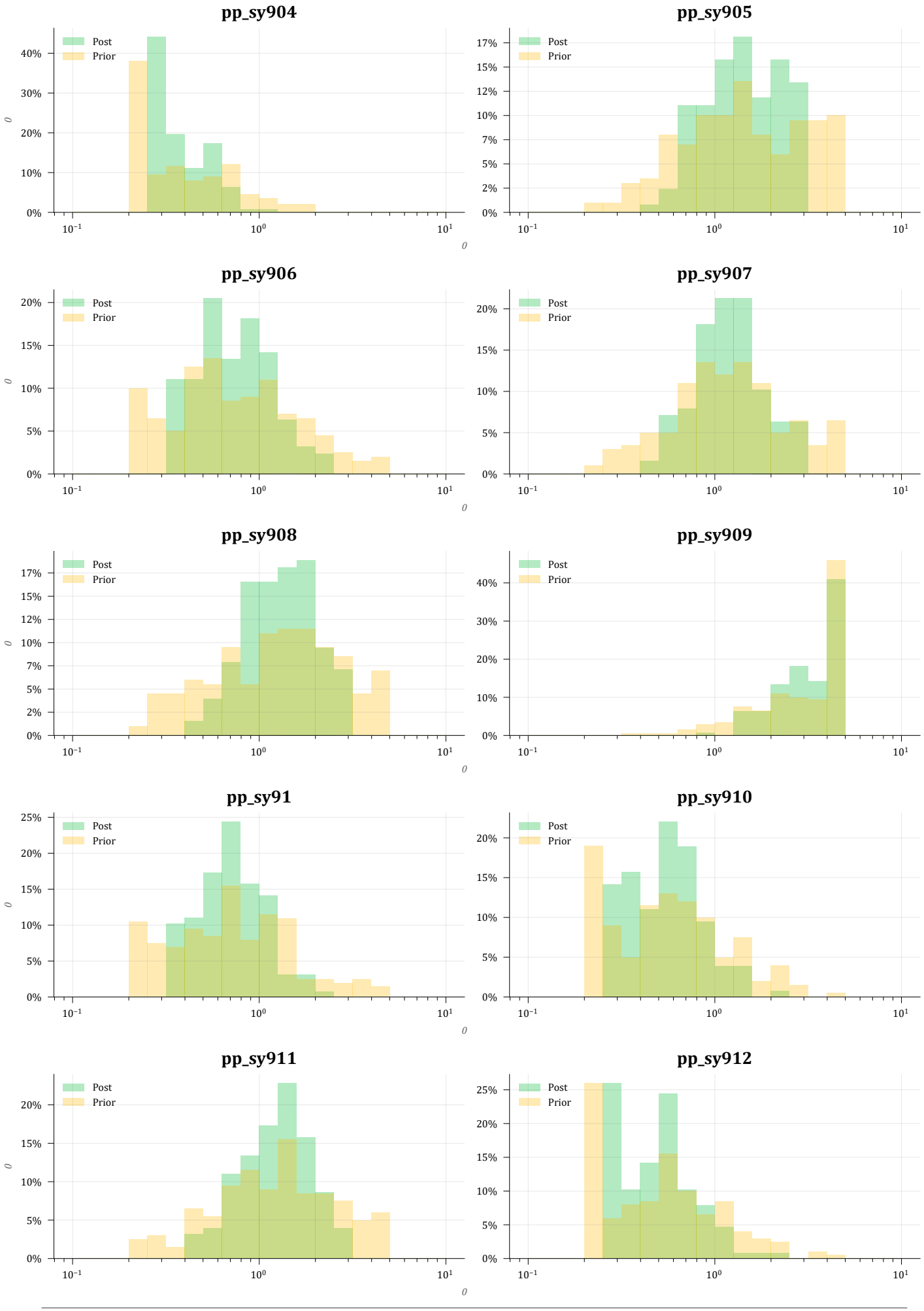

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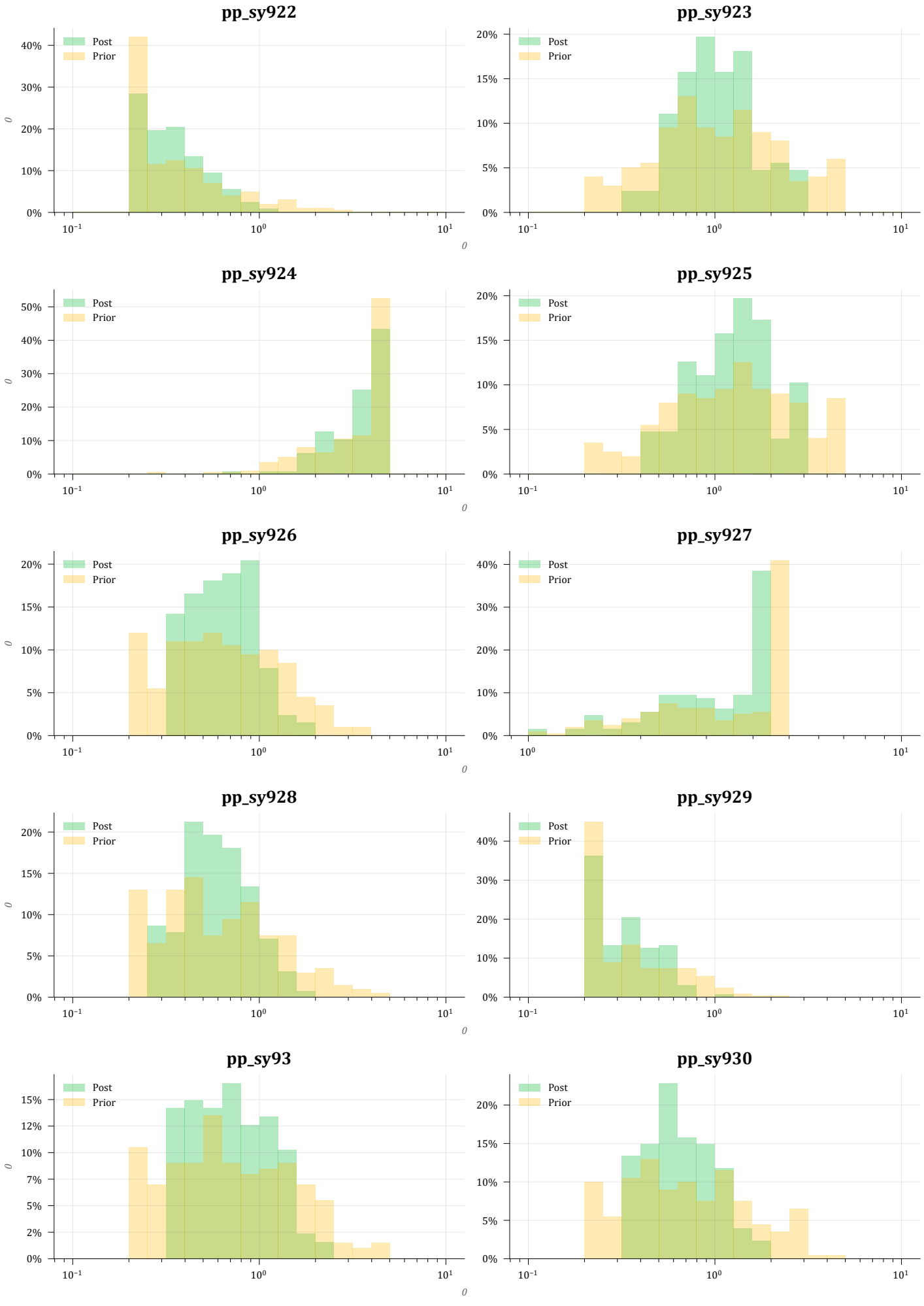

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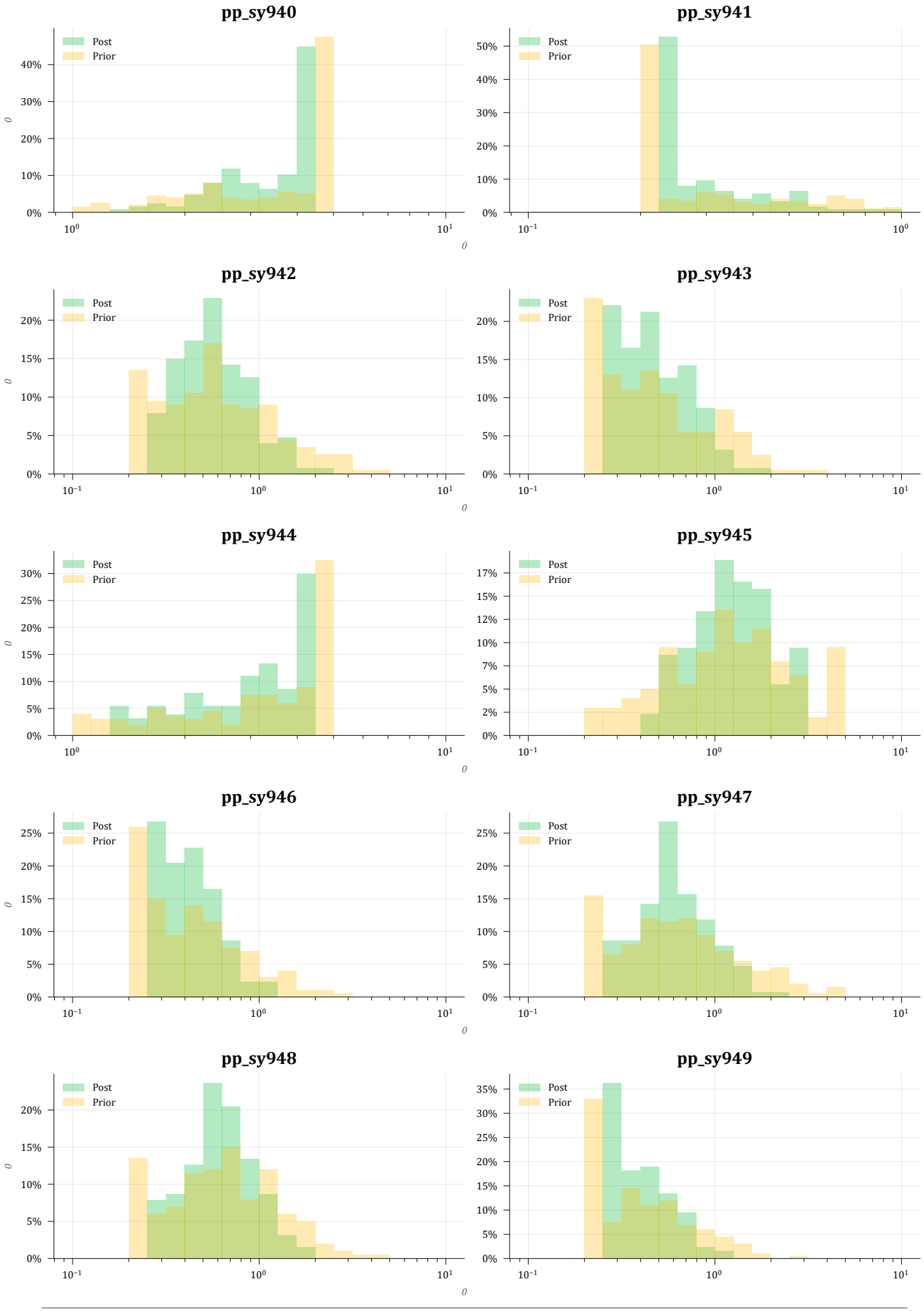

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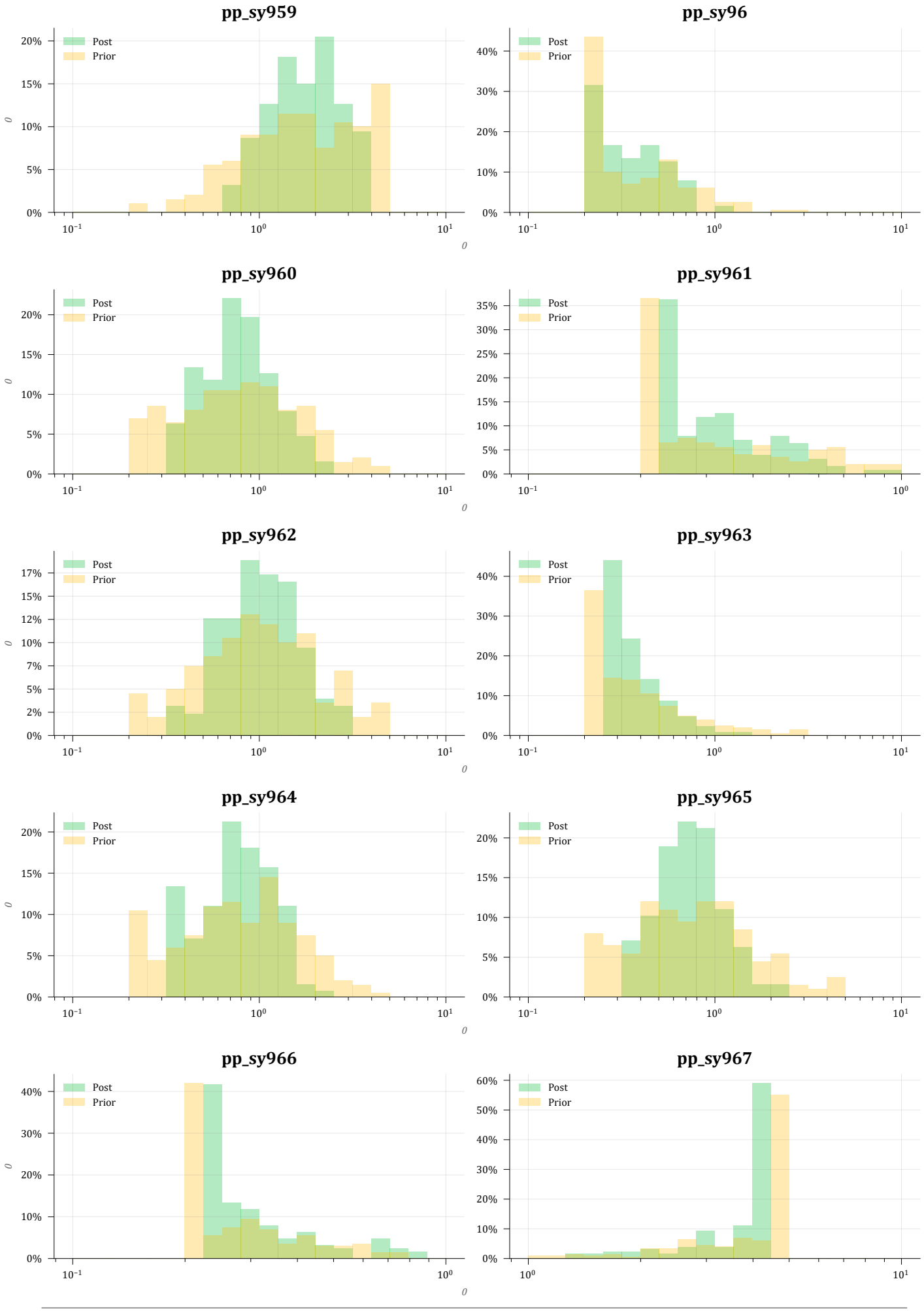

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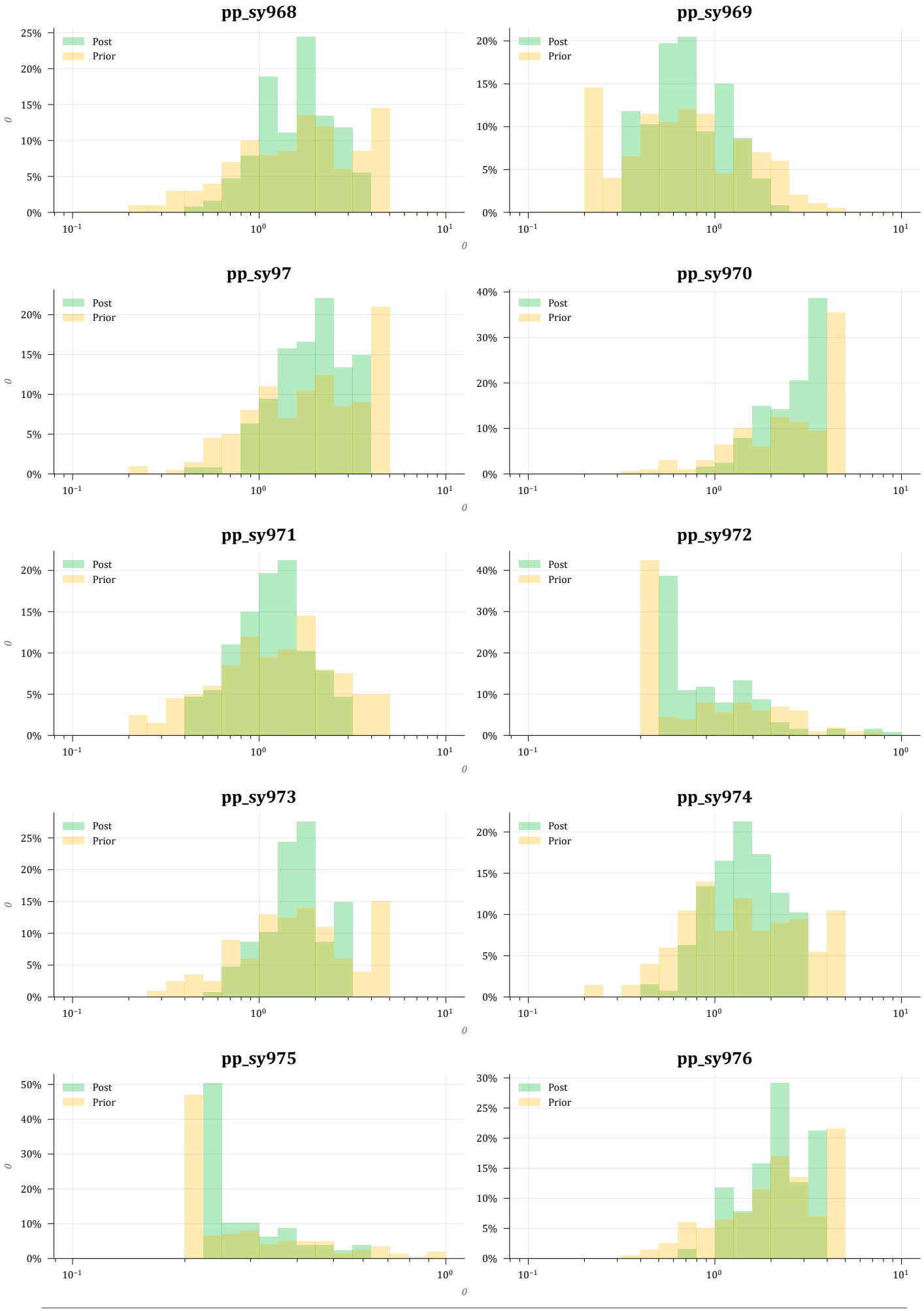

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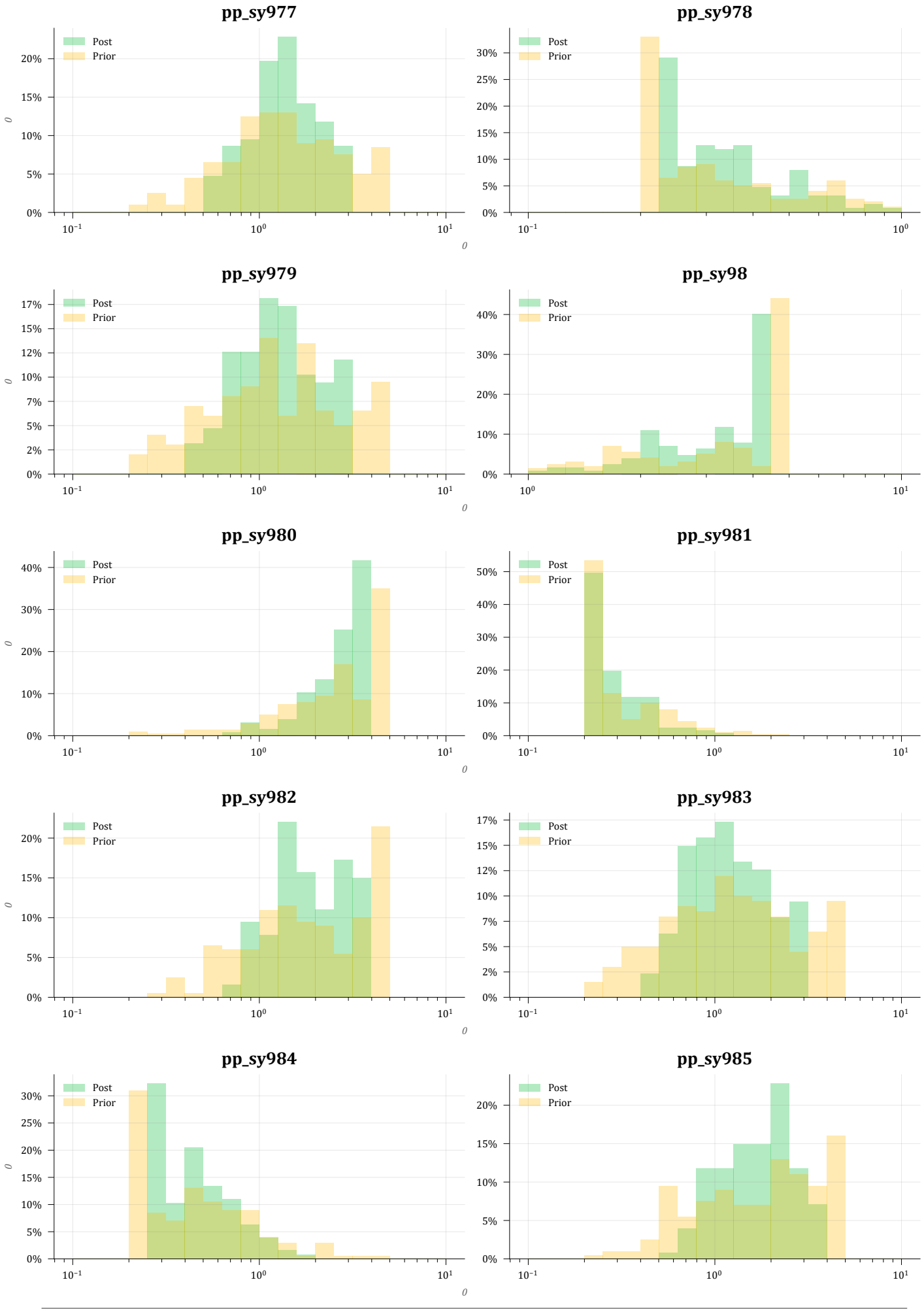

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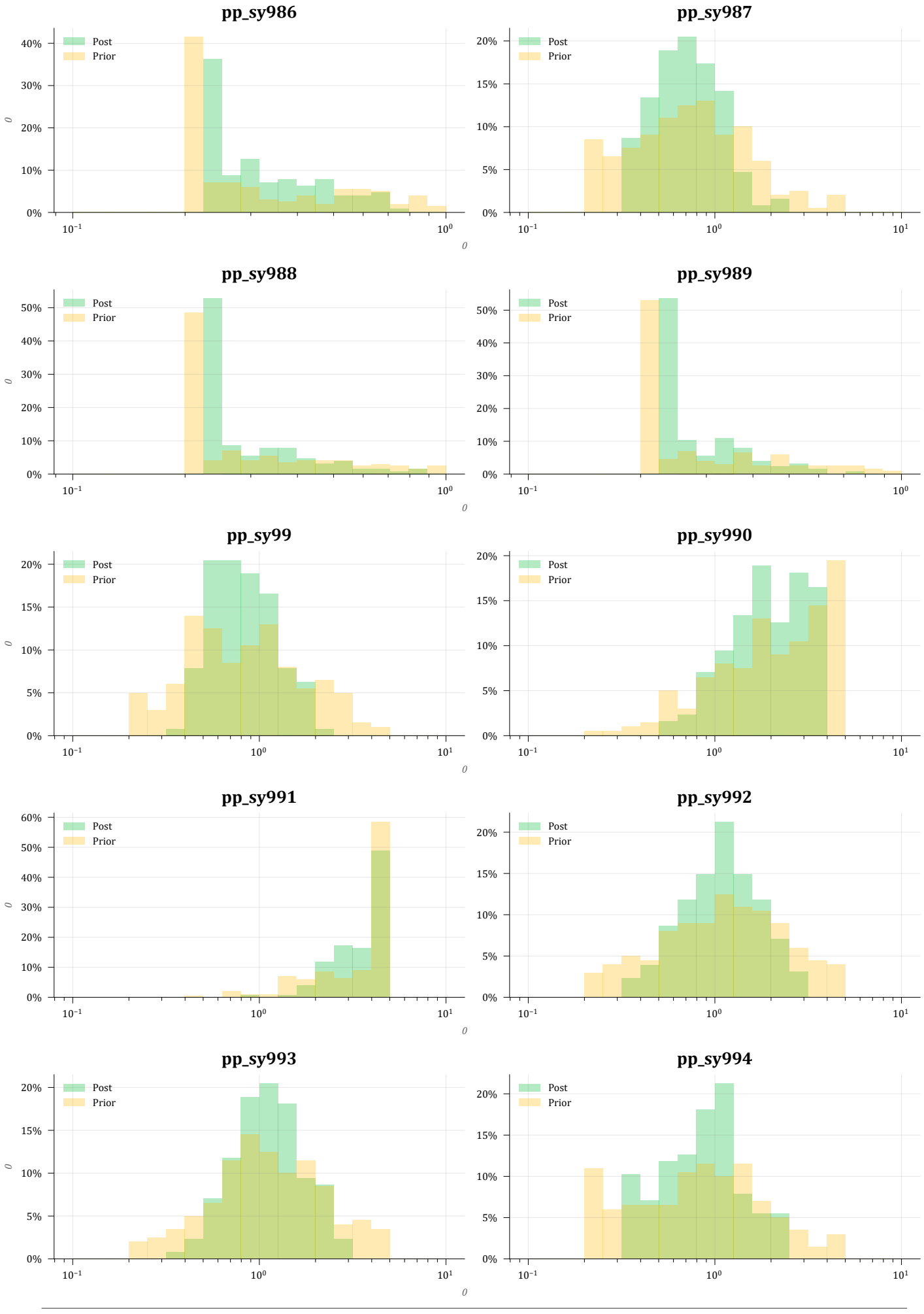

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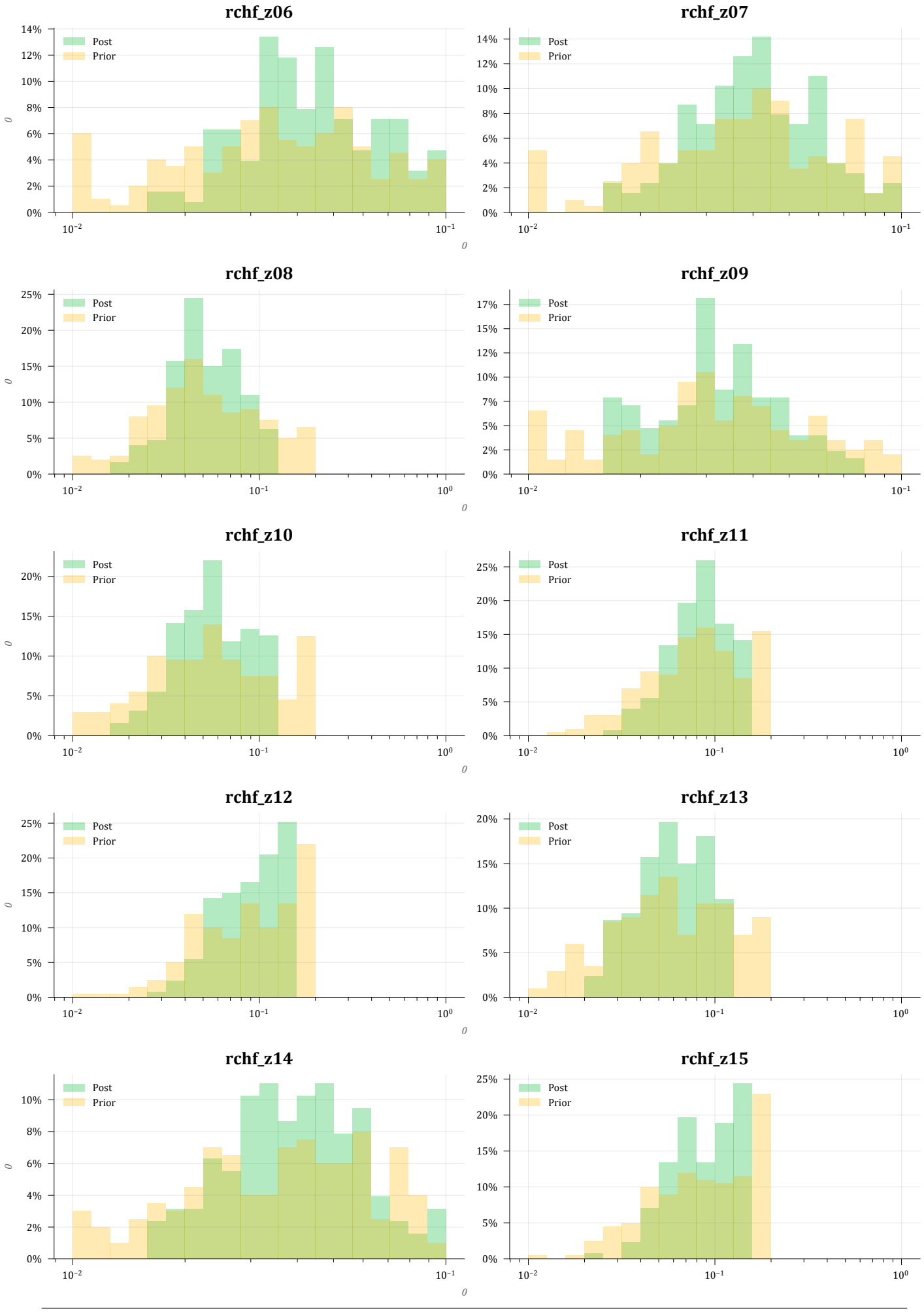

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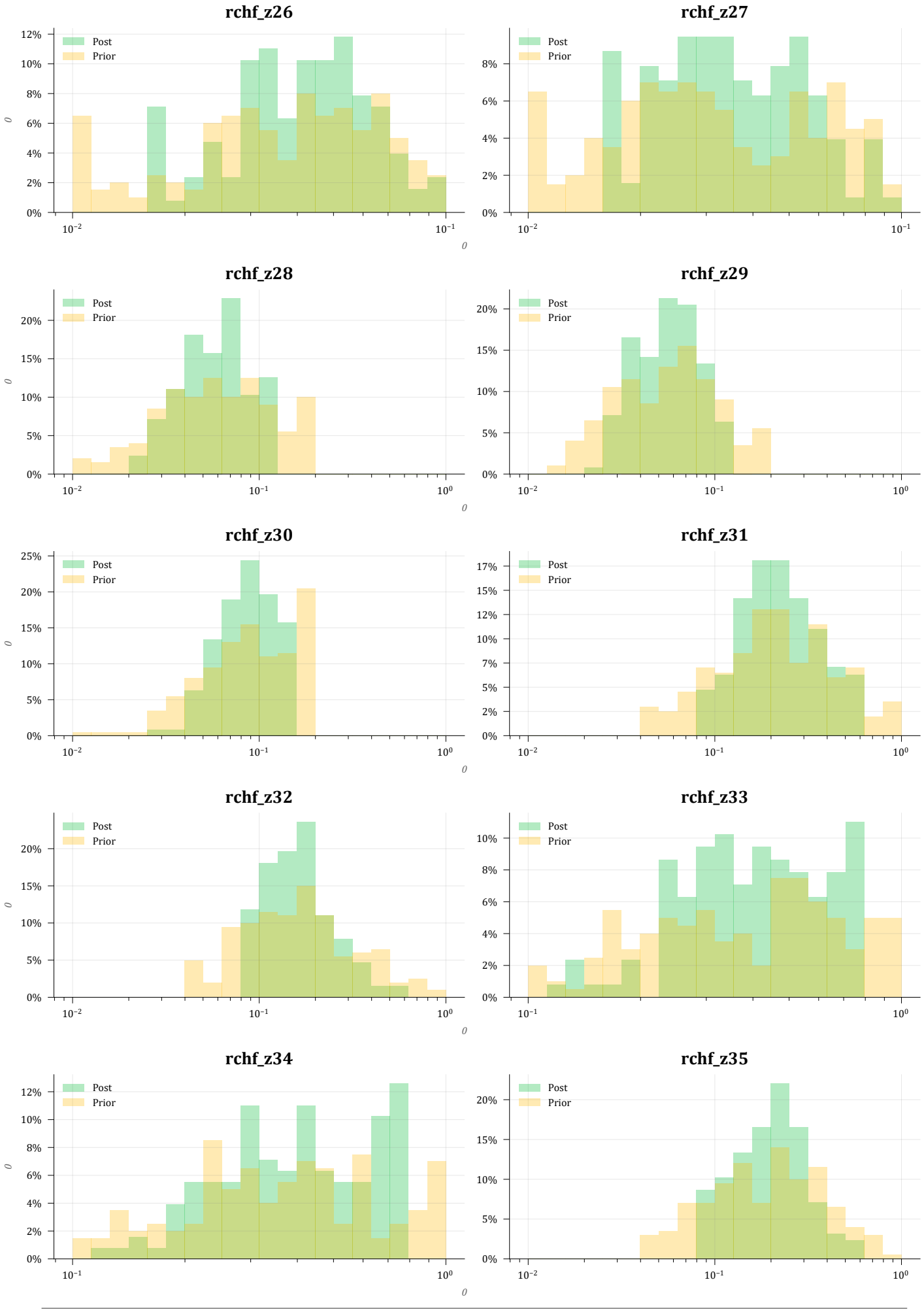

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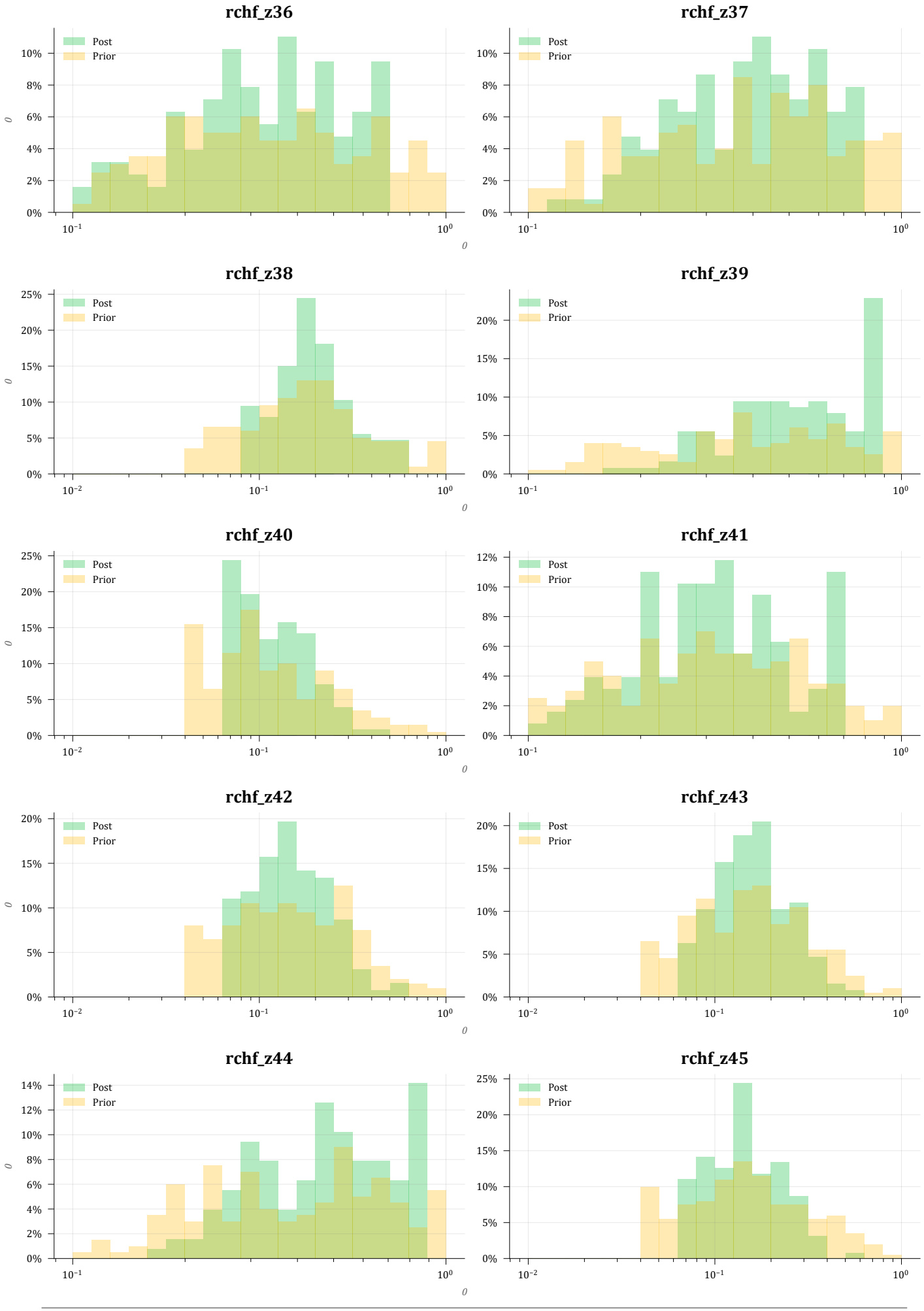

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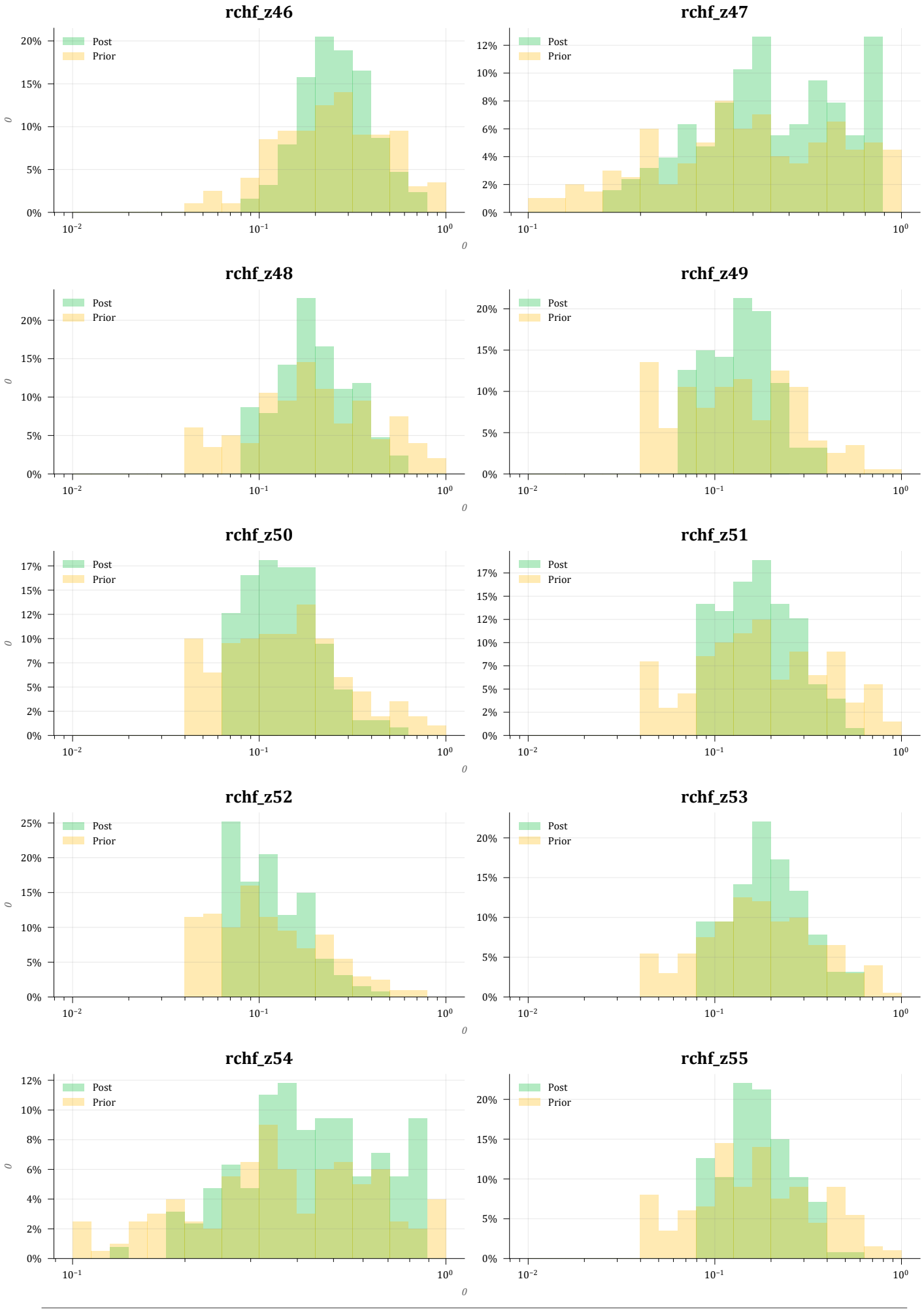

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rchf_z05
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Prior
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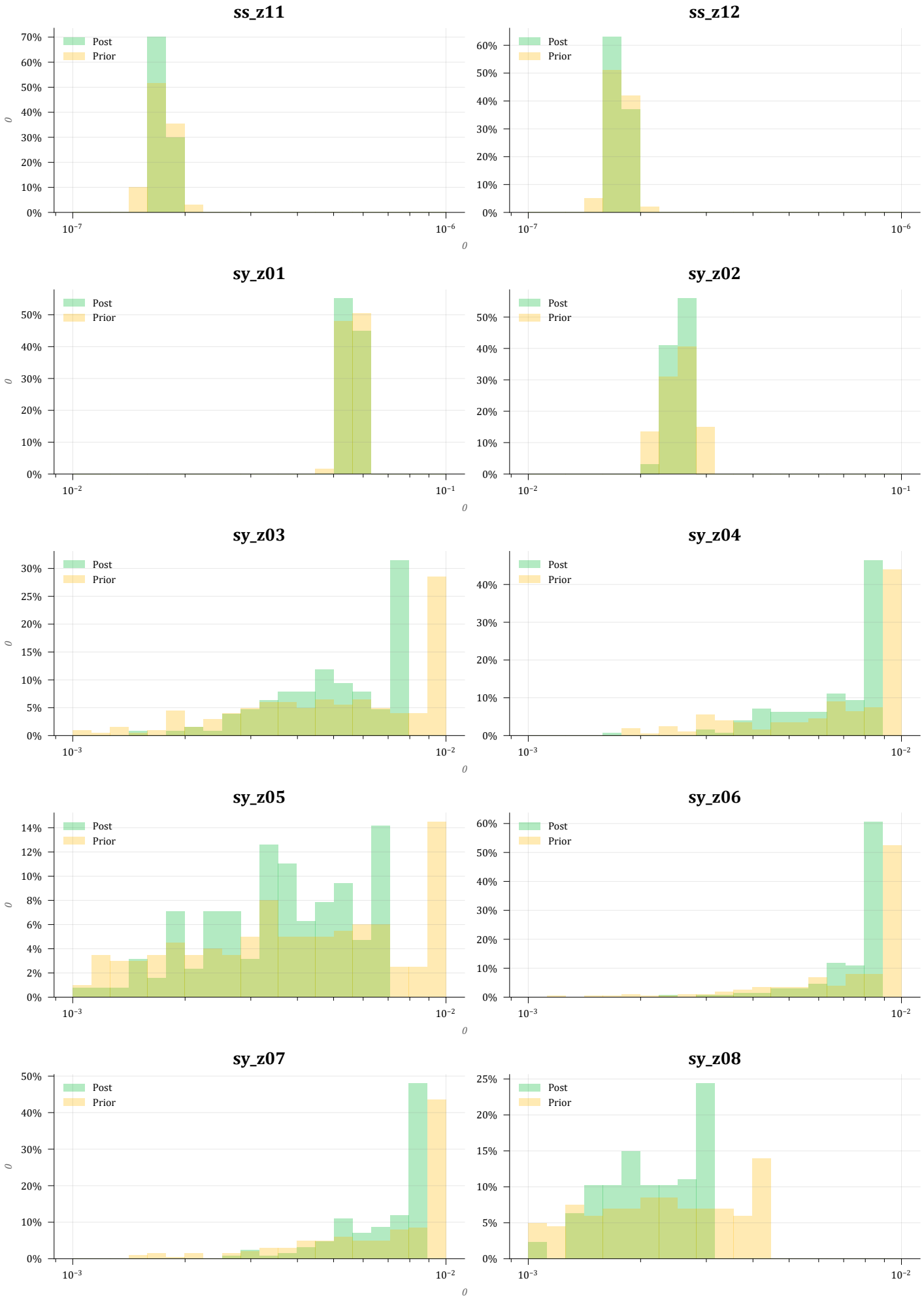

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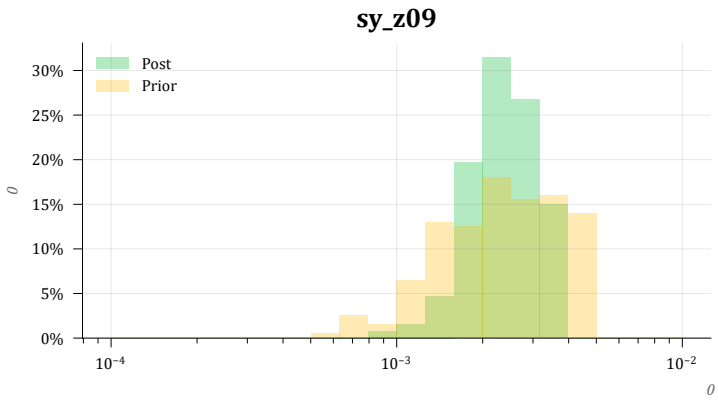

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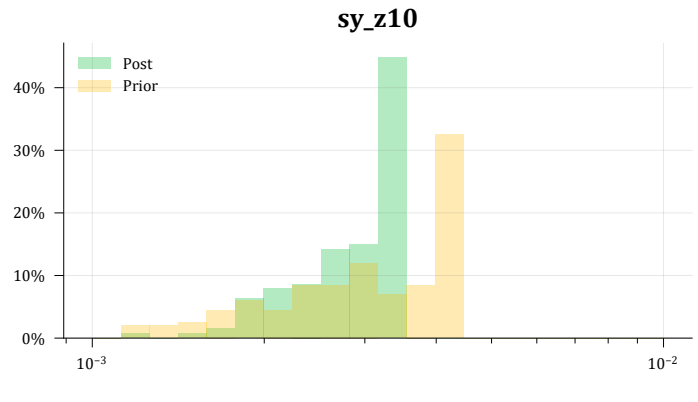

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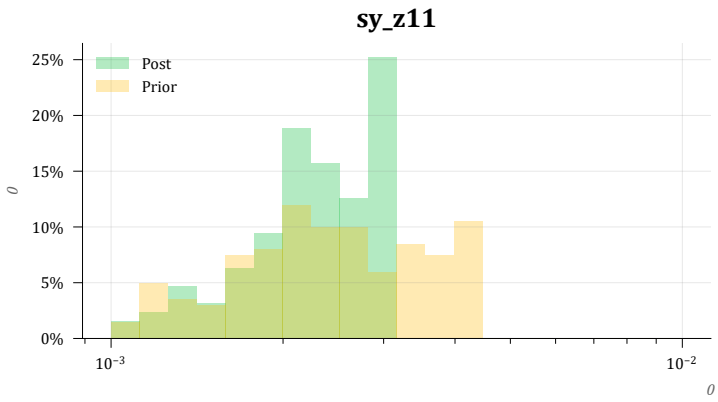

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Post
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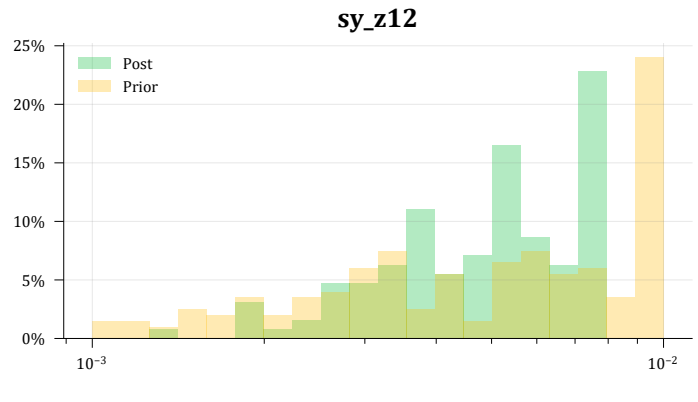

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ss_z07
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ss_z09
ss_z10
Post
Prior
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Parameters


ss_z11
ss_z12
sy_z01
sy_z02
sy_z03
sy_z04
sy_z05
sy_z06
sy_z07
sy_z08
Post
Prior
0
Parameters


sy_z09
Post
Prior
30%
25%
20%
15%
10%
5%
0%
0
10^{-4}
10^{-3}
10^{-2}
0


sy_z10
Post
Prior
40%
30%
20%
10%
0%
10^{-3}
10^{-2}


sy_z11
Post
Prior
25%
20%
15%
10%
5%
0%
0
10^{-3}
10^{-2}
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sy_z12
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Prior
25%
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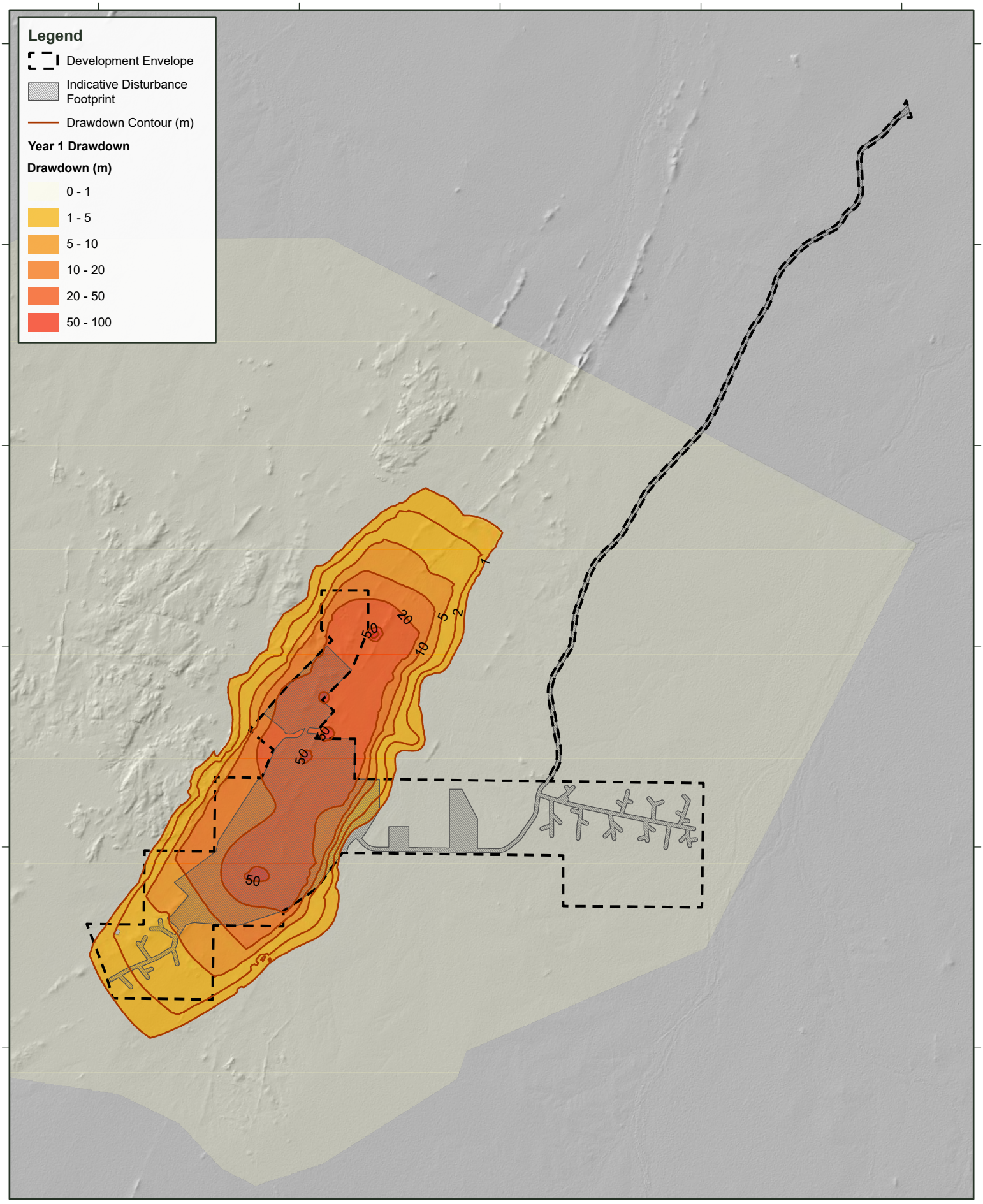
Appendix B Drawdown Maps

Tabba Tabba Lithium Mine Project

Groundwater Modelling Technical Report

Wildcat Resources

SLR Project No.: 620.042733.00001



CLIENT	620.V00796	**Project Name:** Tabba Tabba Lithium Project			
		Appendix B	**Figure:** B1	**Date:** April 2026	**Author:** JWP	**Scale:** 1:120,000
		Figure Name: Watertable Drawdown - Mining year 1			
		Data Sources: • Esri, DigitalGlobe, GeoEye, i-cubed, USDA FSA, USGS, AEX, Getmapping, Aerogrid, IGN, IGP, swisstopo, and the GIS User Community (2023) *ESRI Satellite Imagery*, Basemap			

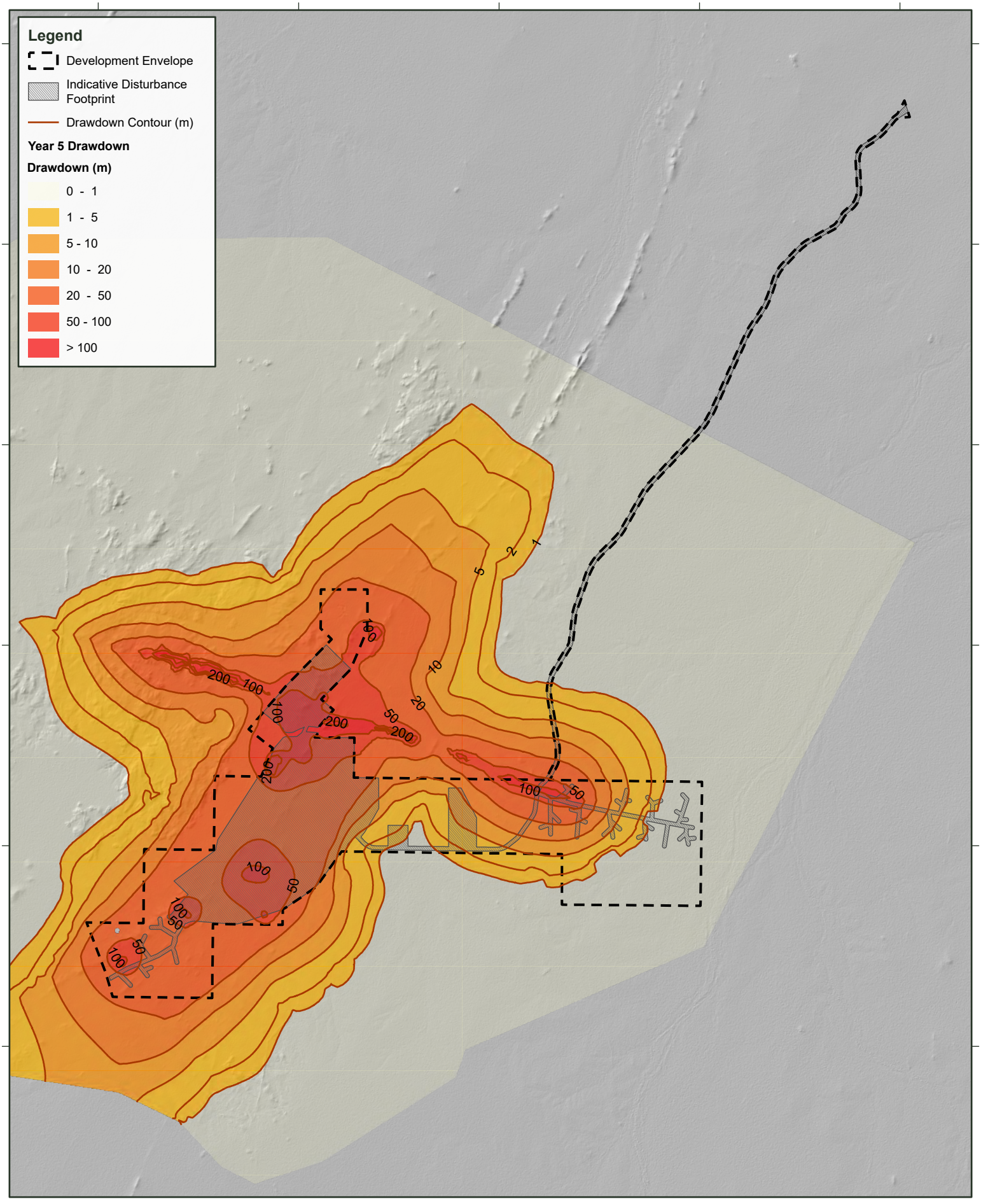
N

0 1 2 km

GDA2020 MGA Zone 50

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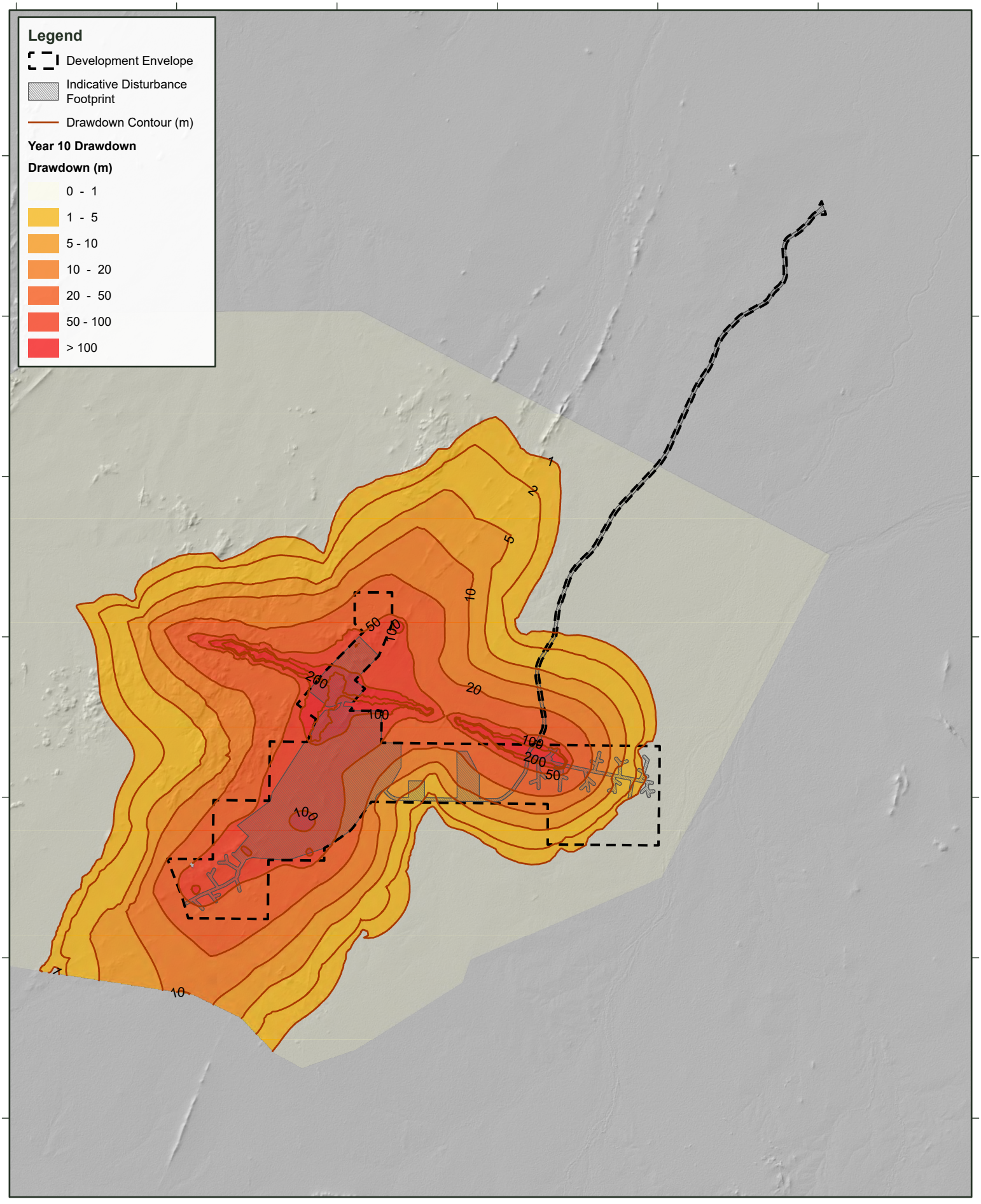
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CLIENT	620.V00796	**Project Name:** Tabba Tabba Lithium Project			
		Appendix B	**Figure:** B2	**Date:** April 2026	**Author:** JWP	**Scale:** 1:120,000
		Figure Name: Watertable Drawdown - Mining Year 5			
		Data Sources: • Esri, DigitalGlobe, GeoEye, i-cubed, USDA FSA, USGS, AEX, Getmapping, Aerogrid, IGN, IGP, swisstopo, and the GIS User Community (2023) *ESRI Satellite Imagery*, Basemap			

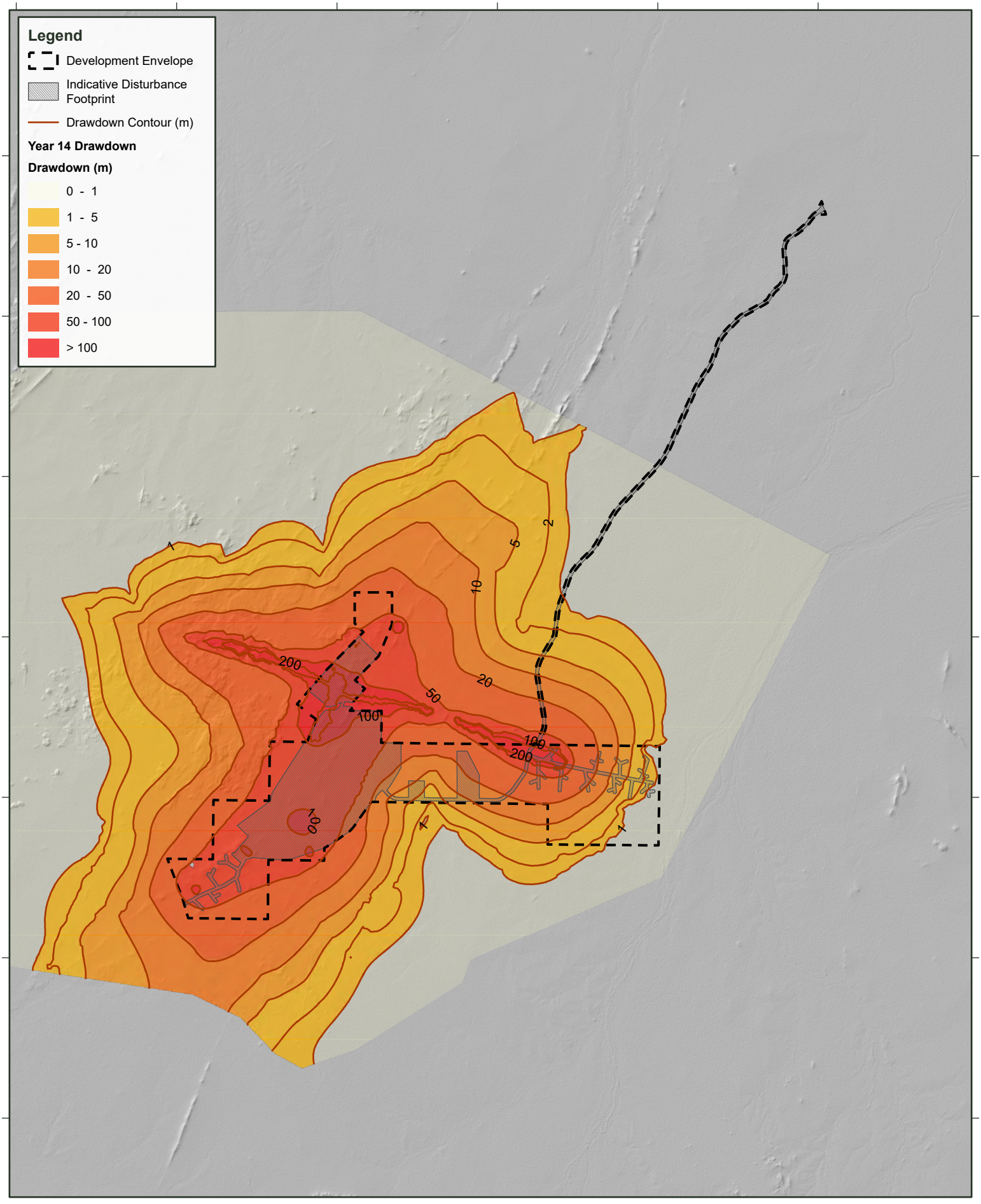
GDA2020 MGA Zone 50

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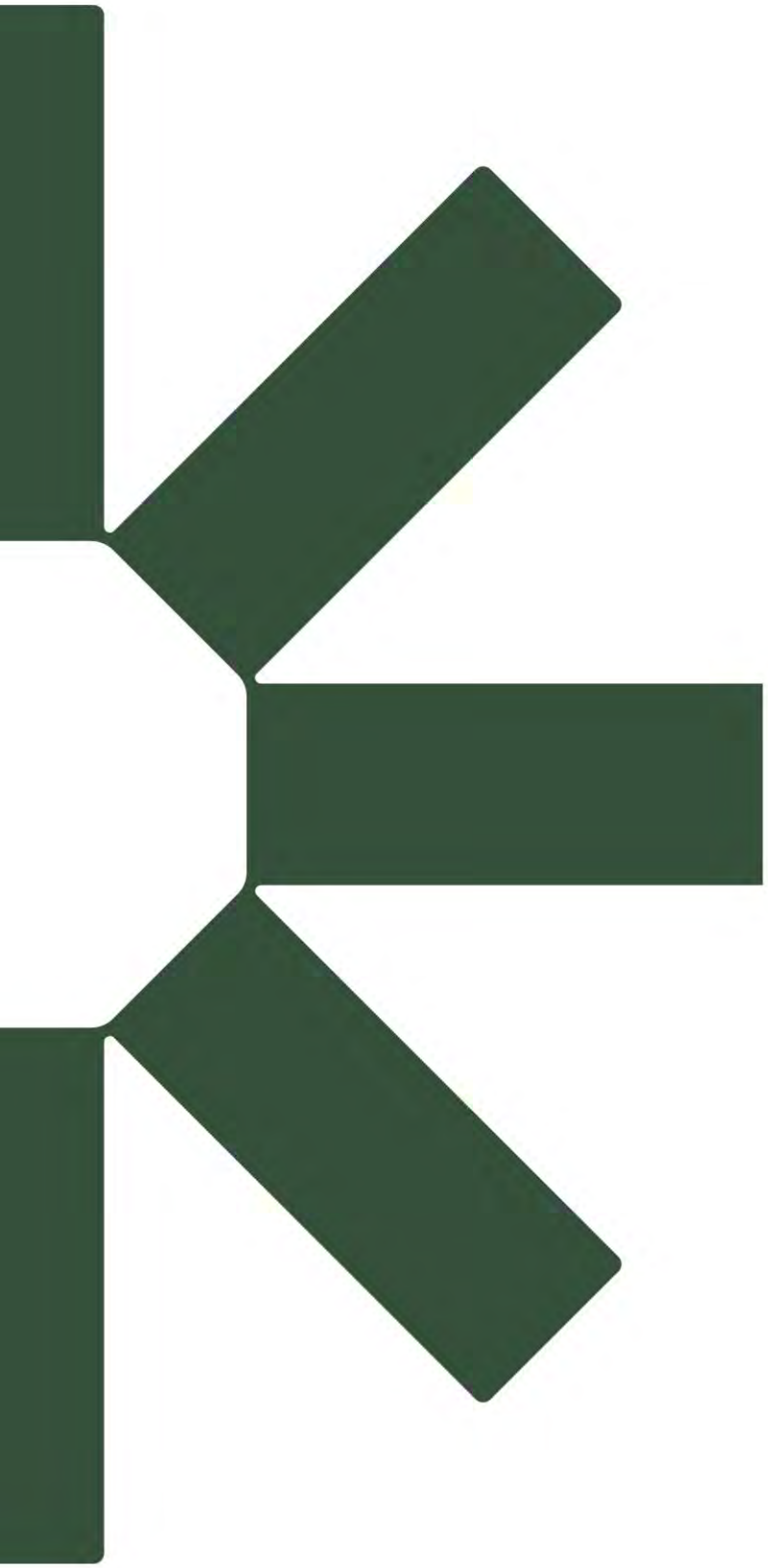
CLIENT	620.V00796	**Project Name:** Tabba Tabba Lithium Project		
WILDCAT RESOURCES	N 0 1 2 km GDA2020 MGA Zone 50	**Appendix B**	**Figure:** B3	**Date:** April 2026	**Author:** JWP	**Scale:** 1:150,000
		Figure Name: Watertable Drawdown - Mining Year 10		
		Data Sources: • Esri, DigitalGlobe, GeoEye, i-cubed, USDA FSA, USGS, AEX, Getmapping, Aerogrid, IGN, IGP, swisstopo, and the GIS User Community (2023) *ESRI Satellite Imagery*, Basemap		SLR

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CLIENT	620.V00796	Project Name: Tabba Tabba Lithium Project				
WILDCAT RESOURCES	N 0 1 2 km GDA2020 MGA Zone 50	Appendix B	Figure: B4	Date: April 2026	Author: JWP	Scale: 1:150,000
		Figure Name: Watertable Drawdown - End of Mining (Mining Year 14)				
		Data Sources: • Esri, DigitalGlobe, GeoEye, i-cubed, USDA FSA, USGS, AEX, Getmapping, Aerogrid, IGN, IGP, swisstopo, and the GIS User Community (2023) *ESRI Satellite Imagery*, Basemap				SLR

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